WIND-TUNNEL STUDY OF
15 COLUMBUS CIRCLE, NEW YORK

by

J. A. Peterka* and J. E. Cermak**

for

Lev Zetlin Associates, Inc.
95 Madison Avenue
New York, NY 10016

Fluid Mechanics and Wind Engineering Program
Fluid Dynamics and Diffusion Laboratory
Department of Civil Engineering
Colorado State University
Fort Collins, Colorado 80523

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*Associate Professor
**Professor-in-Charge, Fluid Mechanics and
Wind Engineering Program

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LIST OF SYMBOLS

Symbol	Definition
U	Local mean velocity
D	Characteristic dimension (building height, width, etc.)
ν, ρ	Kinematic viscosity and density of approach flow
$\frac{UD}{\nu}$	Reynolds number
E	Mean voltage
A, B, n	Constants
U_{rms}	Root-mean-square of fluctuating velocity
E_{rms}	Root-mean-square of fluctuating voltage
U_∞	Reference mean velocity outside the boundary layer
X, Y	Horizontal coordinates
Z	Height above surface
δ	Height of boundary layer
T_u	Turbulence intensity $\frac{U_{rms}}{U_\infty}$ or $\frac{U_{rms}}{U}$
$C_{p_{mean}}$	Mean pressure coefficient, $\frac{(p-p_\infty)_{mean}}{0.5\ \rho\ U_\infty^2}$
$C_{p_{rms}}$	Root-mean-square pressure coefficient, $\frac{\left((p-p_\infty)-(p-p_\infty)_{mean}\right)_{rms}}{0.5\ \rho\ U_\infty^2}$
$C_{p_{max}}$	Peak maximum pressure coefficient, $\frac{(p-p_\infty)_{max}}{0.5\ \rho\ U_\infty^2}$
$C_{p_{min}}$	Peak minimum pressure coefficient, $\frac{(p-p_\infty)_{min}}{0.5\ \rho\ U_\infty^2}$
$(\ )_{min}$	Minimum value during data record
$(\ )_{max}$	Maximum value during data record

Symbol	Definition
p	Fluctuating pressure at a pressure tap on the structure
p_∞	Static pressure in the wind tunnel above the model
F_x, F_y	Forces in X, Y direction
A_R	Reference Area
CF_X	Force coefficient, X direction, $\frac{F_x}{A_R \, 0.5\rho \, U_\infty^2}$
CF_Y	Force coefficient, Y direction, $\frac{F_y}{A_R \, 0.5\rho \, U_\infty^2}$

1. INTRODUCTION

1.1 General

A significant characteristic of modern building design is lighter cladding and more flexible frames. These features produce an increased vulnerability of glass and cladding to wind damage and result in larger deflections of the building frame. In addition, increased use of pedestrian plazas at the base of the buildings has brought about a need to consider the effects of wind and gustiness in the design of these areas.

The building geometry itself may increase or decrease wind loading on the structure. Wind forces may be modified by nearby structures which can produce beneficial shielding or adverse increases in loading. Overestimating loads results in uneconomical design; underestimating may result in cladding or window failures. Tall structures have historically produced unpleasant wind and turbulence conditions at their bases. The intensity and frequency of objectionable winds in pedestrian areas is influenced both by the structure shape and by the shape and position of adjacent structures.

Techniques have been developed for wind tunnel modeling of proposed structures which allow the prediction of wind pressures on cladding and windows, overall structural loading, and also wind velocities and gusts in pedestrian areas adjacent to the building. Information on sidewalk-level gustiness allows plaza areas to be protected by design changes before the structure is constructed. Accurate knowledge of the intensity and distribution of the pressures on the structure permits adequate but economical selection of cladding strength to meet selected maximum design winds and overall wind loads for the design of the frame for flexural control.

Modeling of the aerodynamic loading on a structure requires special consideration of flow conditions in order to guarantee similitude between model and prototype. A detailed discussion of the similarity requirements and their wind-tunnel implementation can be found in references (1), (2), and (3). In general, the requirements are that the model and prototype be geometrically similar, that the approach mean velocity at the building site have a vertical profile shape similar to the full-scale flow, that the turbulence characteristics of the flows be similar, and that the Reynolds number for the model and prototype be equal.

These criteria are satisfied by constructing a scale model of the structure and its surroundings and performing the wind tests in a wind tunnel specifically designed to model atmospheric boundary-layer flows. Reynolds number similarity requires that the quantity UD/ν be similar for model and prototype. Since ν, the kinematic viscosity of air, is identical for both, Reynolds numbers cannot be made precisely equal with reasonable wind velocities. To accomplish this the air velocity in the wind tunnel would have to be as large as the model scale factor times the prototype wind velocity, a velocity which would introduce unacceptable compressibility effects. However, for sufficiently high Reynolds numbers ($>2\times10^4$) the pressure coefficient at any location on the structure will be essentially constant for a large range of Reynolds numbers. Typical values encountered are 10^7-10^8 for the full-scale and 10^5-10^6 for the wind-tunnel model. In this range acceptable flow similarity is achieved without precise Reynolds number equality.

1.2 The Wind-Tunnel Test

The wind-engineering study is performed on a building or building group modeled at scales ranging from 1:150 to 1:400. The building model

is constructed of clear plastic fastened together with screws. The structure is modeled in detail to provide accurate flow patterns in the wind passing over the building surfaces. The building under test is often located in a surrounding where nearby buildings or terrain may provide beneficial shielding or adverse wind loading. To achieve similarity in wind effects the area surrounding the test building is also modeled. A flow visualization study is first made (smoke is used to make the air currents visible) to define overall flow patterns and identify regions where local flow features might cause difficulties in building curtain-wall design or produce pedestrian discomfort.

The test model, equipped with pressure taps (200 to 600 or more), is exposed to an appropriately modeled atmospheric wind in the wind tunnel and the fluctuating pressure at each tap measured electronically. The model, and the modeled area, are rotated 10 or 15 degrees and another set of data recorded for each pressure tap. Normally, 24 or 36 sets of data (360 degrees of turning) are taken; however, when flow visualization or recorded data indicate high pressure regions of small azimuthal extent, data is obtained in smaller azimuthal steps.

Data are recorded, analyzed and processed by an on-line computerized data-acquisition system. Pressure coefficients of several types are calculated by the computer for each reading on each piezometer tap and are printed in tabular form as computer readout. Using wind data applicable to the building site, representative wind velocities are selected for combination with measured pressures on the building model. Integration of test data with wind data results in prediction of peak local wind pressures for design of glass or cladding and may include overall forces and moments on the structure (by floor if desired) for design of

the structural frame. Pressure contours are drawn on the developed building surfaces showing the intensity and distribution of peak wind loads on the building. These results may be used to divide the building into zones where lighter or heavier cladding or glass may be desirable.

Based on the visualization (smoke) tests and on a knowledge of heavy pedestrian use areas, a dozen or more locations may be chosen at the base of the building where wind velocities can be measured to determine the relative comfort or discomfort of pedestrians in plaza areas, near building entrances, near building corners, or on sidewalks. Usually a reference pedestrian position is also tested to determine whether the wind environment in the building area is better or worse than the environment a block or so away in an undisturbed area.

The following pages discuss in greater detail the procedures followed and the equipment and data collecting and processing methods used. In addition, the data presentation format is explained and the implications of the data are discussed.

2. EXPERIMENTAL CONFIGURATION

2.1 Wind Tunnel

Wind-engineering studies are performed in the Fluid Dynamics and Diffusion Laboratory at Colorado State University (Figure 1). Three large wind tunnels are available for wind loading studies depending on the detailed requirements of the study. The wind tunnel used for this investigation is shown in Figure 2. All tunnels have a flexible roof adjustable in height to maintain a zero pressure gradient along the test section. The mean velocity can be adjusted continuously in each tunnel to the maximum velocity available.

2.2 Model

In order to obtain an accurate assessment of local pressures using piezometer taps, models are constructed to the largest scale that does not produce significant blockage in the wind-tunnel test section. The models are constructed of 1/2 in. thick Lucite plastic and fastened together with metal screws. Significant variations in the building surface, such as mullions, are machined into the plastic surface. Piezometer taps (1/16 in. diameter) are drilled normal to the exterior vertical surfaces in rows at several or more elevations between the bottom and top of the building. Similarly, taps are placed in the roof and on any sloping, protruding, or otherwise distinctive features of the building that might need investigation.

Pressure tap locations are chosen so that the entire surface of the building can be investigated for pressure loading and at the same time permit critical examination of areas where experience has shown that maximum wind effects may be expected to occur. Locations of the pressure taps for this study are shown in Figure 3. Dimensions are

given both for full-scale building (in ft) and for model (in in.). The pressure tap numbers are shown adjacent to the taps.

The pressure tests are sometimes made in two stages. In the first stage measurements are made on the initial distribution of pressure taps. If it becomes apparent from the data that the loading on the building is being influenced by some unsuspected geometry of the building or adjacent structures, additional pressure taps are installed in the critical areas. The locations of the taps are selected so that the maximum loading can be detected and the area over which this loading is acting can be defined. Any added taps are also shown in Figure 3.

A circular area 750 to 2000 ft in radius depending on model scale and characteristics of the surrounding buildings and terrain is modeled in detail. Structures within the modeled region are made from styrofoam and cut to the individual building geometries. They are mounted on the turntable in their proper locations. Significant terrain features are included as needed. The model is mounted on a turntable (Figure 2) near the downwind end of the test section. Any buildings or terrain features which do not fit on the turntable are placed on removable pieces which are placed upwind of the turntable for appropriate wind directions. A plan view of the building and its surroundings is shown in Figure 4. The turntable is calibrated to indicate azimuthal orientation to 0.1 degree.

The region upstream from the modeled area is covered with a randomized roughness constructed using various sized cubes placed on the floor of the wind tunnel. Different roughness sizes may be used for different wind directions. Spires are installed at the test-section entrance to provide a thicker boundary layer than would otherwise be

available. The thicker boundary layer permits a somewhat larger scale model than would otherwise be possible. The spires are approximately triangularly shaped pieces of 1/2 in. thick plywood 6 in. wide at the base and 1 in. wide at the top, extending from the floor to the top of the test section. They are placed so that the broad side intercepts the flow. A barrier approximately 8 in. high is placed on the test-section floor downstream of the spires to aid in development of the boundary-layer flow.

The distribution of the roughness cubes and the spires in the roughened area was designed to provide a boundary-layer thickness of approximately 4 ft, a velocity profile power-law exponent similar to that expected to occur in the region approaching the modeled area for each wind direction (a number of wind directions may have the same approach roughness). A photograph of the completed model in the wind tunnel is shown in Figure 5. The wind-tunnel ceiling is adjusted after placement of the model to obtain a zero pressure gradient along the test section.

3. INSTRUMENTATION AND DATA ACQUISITION

3.1 Flow Visualization

Making the air flow visible in the vicinity of the model is helpful (a) in understanding and interpreting mean and fluctuating pressures, (b) in defining zones of separated flow and reattachment and zones of vortex formation where pressure coefficients may be expected to be high and (c) in indicating areas where pedestrian discomfort may be a problem. Titanium tetrachloride smoke is released from sources on and near the model to make the flow lines visible to the eye and to make it possible to obtain motion picture records of the tests. Conclusions obtained from these smoke studies are discussed in Sections 4.1 and 5.1.

3.2 Pressures

Mean and fluctuating pressures are measured at each of the pressure taps on the model structure. Data are obtained for 24 or 36 wind directions, rotating the entire model assembly in a complete circle. Seventy-six pieces of 1/16 in. I.D. plastic tubing are used to connect 76 pressure ports at a time to an 80 tap pressure switch mounted inside the model. The switch was designed and fabricated in the Fluid Dynamics and Diffusion Laboratory to minimize the attenuation of pressure fluctuations across the switch. Each of the 76 measurement ports is directed in turn by the switch to one of four pressure transducers mounted close to the switch. The four pressure input taps not used for transmitting building surface pressures are connected to a common tube leading outside the wind tunnel. This arrangement provides both a means of performing in-place calibration of the transducers and, by connecting this tube to a pitot tube mounted inside the wind tunnel, a means of automatically monitoring the tunnel speed. The switch is operated by means of a shaft projecting through

the floor of the wind tunnel. A computer-controlled stepping motor steps the switch into each of the 20 required positions. The computer keeps track of switch position but a digital readout of position is provided at the wind tunnel.

The pressure transducers used are setra differential transducers (Model 237) with a 0.10 psid range. Reference pressures are obtained by connecting the reference sides of the four transducers, using plastic tubing, to the static side of a pitot-static tube mounted in the wind tunnel free stream above the model building. In this way the transducer measures the instantaneous difference between the local pressures on the surface of the building and the static pressure in the free stream above the model.

Output from the pressure transducers is fed to an on-line data acquisition system consisting of a Hewlett-Packard 21 MX computer, disk unit, card reader, printer, Digi-Data digital tape drive and a Preston Scientific analog-to-digital converter. The data are processed immediately into pressure coefficient form as described in Section 4.3 and stored for printout or further analysis.

All four transducers are recorded simultaneously for 16 seconds at a 250 sample per second rate. The results of an experiment to determine the length of record required to obtain stable mean and rms (root-mean-square) pressures and to determine the overall accuracy of the pressure data acquisition system is shown in Figure 6. A typical pressure port record was integrated for a number of different time periods to obtain the data shown. Examination of a large number of pressure taps showed that the overall accuracy for a 16 second period is, in pressure coefficient form, 0.03 for mean pressures, 0.1 for peak pressures, and 0.01 for rms pressures. Pressure coefficients are defined in Section 4.3.

3.3 Velocity

Mean velocity and turbulence intensity profiles are measured upstream of the model to determine that an approach boundary-layer flow appropriate to the site has been established. Tests are made at one wind velocity in the tunnel. This velocity is well above that required to produce Reynolds number similarity between the model and the prototype as discussed in Section 1.1.

In addition, mean velocity and turbulence intensity measurements are made 5 to 7 ft (prototype) above the surface at a dozen or more locations on and near the building for 16 wind directions. The measurement locations are shown on Figure 4. The surface measurements are indicative of the wind environment to which a pedestrian at the measurement location would be subjected. The locations are chosen to determine the degree of pedestrian comfort or discomfort at the building corners where relatively severe conditions frequently are found, near building entrances and on adjacent sidewalks where pedestrian traffic is heavy, and in open plaza areas. In most studies a reference pedestrian position, located about a block away, is also tested. These data are helpful in evaluating the degree of pedestrian comfort or discomfort in the proposed plaza area in terms of the undisturbed environment in the immediate vicinity.

Measurements are made with a single hot-wire anemometer mounted with its axis vertical. The instrumentation used is a Thermo Systems constant temperature anemometer (Model 1050) with a 0.001 in. diameter platinum film sensing element 0.020 in. long. Output is directed to the on-line data acquisition system for analysis.

Calibration of the hot-wire anemometer is performed by comparing output with the pitot-static tube in the wind tunnel. The calibration

data are fit to a variable exponent King's Law relationship of the form

$$E^2 = A + BU^n$$

where E is the hot-wire output voltage, U the velocity and A, B, and n are coefficients selected to fit the data. The above relationship was used to determine the mean velocity at measurement points using the measured mean voltage. The fluctuating velocity in the form U_{rms} (root-mean-square velocity) was obtained from

$$U_{rms} = \frac{2\ E\ E_{rms}}{B\ n\ U^{n-1}}$$

where E_{rms} is the root-mean-square voltage output from the anemometer. For interpretation all turbulence measurements for pedestrian winds were divided by the mean velocity outside the boundary-layer U_∞. Turbulence intensity in velocity profile measurements used the local mean velocity.

4. RESULTS

4.1 Flow Visualization

A film is included as part of this report showing the characteristics of flow about the structure using smoke to make the flow visible. A listing of the contents of the film is shown in Table 1. Several features can be noted from the visualization. As with all large structures, wind approaching the building is deflected down to the plaza level, up over the structure and around the sides. A description of the smoke test results emphasizing flow patterns of concern relative to possible high-wind load areas and pedestrian comfort is given in Section 5.1.

4.2 Velocity

Velocity and turbulence profiles are shown in Figure 7. Profiles were taken upstream from the model which are characteristic of the boundary layer approaching the model and sometimes at the building site with building removed. The boundary-layer thickness, δ, is shown in Figure 7. The corresponding prototype value of δ for this study is also shown in the figure. This value was established as a reasonable height for this study. The mean velocity profile approaching the modeled area has the form

$$\frac{U}{U_\infty} = \left(\frac{z}{\delta}\right)^n .$$

The exponent n for the approach flow established for this study is shown in Figure 7.

Profiles of longitudinal turbulence intensity in the flow approaching the modeled area are shown in Figure 7. The turbulence intensities are appropriate for the approach mean velocity profile selected. For the velocity profiles, turbulence intensity is defined

as the root-mean-square about the mean of the longitudinal velocity fluctuations divided by the local mean velocity U,

$$Tu = \frac{U_{rms}}{U} .$$

Velocity data obtained at each of the pedestrian measurement locations shown in Figure 4 are listed in Table 2 as mean velocity U/U_∞, turbulence intensity U_{rms}/U_∞, and largest effective gust

$$U_{pk} = \frac{U + 3U_{rms}}{U_\infty} .$$

These data are plotted in polar form in Figure 8. Measurements were taken 5 to 7 ft above the ground surface. A site map is superimposed on the polar plots to aid in visualization of the effects of the nearby structures on the velocity and turbulence magnitudes. An analysis of these wind data is given in Section 5.2.

To enable a quantitative assessment of the wind environment, the wind-tunnel data were combined with wind frequency and direction information obtained at the local airport. Table 3 shows wind frequency by direction and magnitude obtained from summaries published by the National Weather Service. These data, usually obtained at an elevation of about 30-40 ft, were converted to velocities at the reference velocity height for the wind-tunnel measurements and combined with the wind-tunnel data to obtain cumulative probability distributions (percent time a given velocity is exceeded) for wind velocity at each measuring location. The percentage times were summed by wind direction to obtain a percent time exceeded at each measuring position independent of wind direction (but accounting for the fact that the wind blows from different directions with varying frequency). These results are plotted in Figure 9.

Interpretation of Figure 9 is aided by a description of the effects of wind of various magnitudes on people. The earliest quantitative description of wind effects was established by Sir Francis Beaufort in 1806 for use at sea and is still in use today. Several recent investigators have added to the knowledge of wind effects on pedestrians. These investigations along with suggested criteria for acceptance have been summarized by Penwarden and Wise (4) and Melbourne (5). The Beaufort scale (from ref. 4), based on mean velocity only, is reproduced as Table 4 including qualitative descriptions of wind effects. Table 4 suggests that mean wind speeds below 12 mph are of minor concern and that mean speeds above 24 mph are definitely inconvenient. Quantitative criteria for acceptance from reference 5 are superimposed as dashed lines on Figure 9. The peak gust curves shown in Figure 9 are the percent of time during which a short gust of the stated magnitude could occur (say about one of these gusts per hour). Implications of the data plotted in Figure 9 are presented in Section 5.2.

Because some pedestrian wind measuring positions are purposely chosen at sites where the smoke tests showed large velocities of small spacial extent, the general wind environment about the structure may be less severe than one might infer from a strict analysis of Table 2 and Figure 9.

4.3 Pressures

For each of the pressure taps examined at each wind direction, the data record is analyzed to obtain four separate pressure coefficients. The first is the mean pressure coefficient

$$C_{p_{mean}} = \frac{(p-p_\infty)_{mean}}{0.5\ \rho\ U_\infty^2}$$

where the symbols are as defined in the List of Symbols. It represents the mean of the instantaneous pressure difference between the building pressure tap and the static pressure in the wind tunnel above the building model, nondimensionalized by the dynamic pressure

$$0.5\ \rho\ U_\infty^2$$

at the reference velocity position. This relationship produces a dimensionless coefficient which indicates that the mean pressure difference between building and ambient wind at a given point on the structure is some fraction less or some fraction greater than the undisturbed wind dynamic pressure near the upper edge of the boundary layer. Using the measured coefficient, prototype mean pressure values for any wind velocity may be calculated.

The magnitude of the fluctuating pressure is obtained by the rms pressure coefficient

$$C_{p_{rms}} = \frac{\left((p-p_\infty) - (p-p_\infty)_{mean}\right)_{rms}}{0.5\ \rho\ U_\infty^2}$$

in which the numerator is the root-mean-square of the instantaneous pressure difference about the mean .

If the pressure fluctuations followed a Gaussian probability distribution, no additional data would be required to predict the

frequency with which any given pressure level would be observed. However, the pressure fluctuations do not, in general, follow a Gaussian probability distribution so that additional information is required to show the extreme values of pressure expected. The peak maximum and peak minimum pressure coefficients are used to determine these values:

$$C_{p_{max}} = \frac{(p-p_\infty)_{max}}{0.5\ \rho\ U_\infty^2}$$

$$C_{p_{min}} = \frac{(p-p_\infty)_{min}}{0.5\ \rho\ U_\infty^2}$$

The values of $p-p_\infty$ which were digitized at 250 samples per second for 16 seconds, representing about one hour of time in the full-scale, are examined individually by the computer to obtain the most positive and most negative values during the 16-second period. These are converted to $C_{p_{max}}$ and $C_{p_{min}}$ by nondimensionalizing with the free stream dynamic pressure.

The four pressure coefficients are calculated by the on-line data acquisition system computer and tabulated along with the approach wind azimuth in degrees from true north. The list of coefficients is included as Appendix A. The pressure tap code numbers used in the appendix are explained in Figure 3.

To determine the largest peak loads acting at any point on the structure for cladding design purposes, the pressure coefficients for all wind directions were searched to obtain, at each pressure tap, the largest peak positive and peak negative pressure coefficients. Table 6 lists the larger values and associated wind directions. Included in Section 5.3 is an analysis of the coefficients of Table 6 including the maximum values obtained and where they occurred on the building.

The pressure coefficients of Table 6 can be converted to full-scale loads by multiplication by a suitable reference pressure selected for the field site. This reference pressure is represented in the equations for pressure coefficients by the $0.5\ \rho\ U_{\infty}^{2}$ denominator. This value is the dynamic pressure associated with an hourly mean wind at the reference velocity measurement position at the edge of the boundary layer. In general, the method of arriving at a design reference pressure for a particular site involves selection of a design wind velocity, translation of the velocity to an hourly mean wind at the reference velocity location and conversion to a reference pressure. Selection of the design velocity can be made from statistical analysis of extreme wind data or selected from wind maps contained in the proposed wind loading code ANSI A58.1 of the American National Standards Institute (6). The calculation of reference pressure for this study is shown in Table 5. The factor used in Table 5 to reduce gust winds to hourly mean winds is given in reference (7).

The reference pressure associated with the design hourly mean velocity at the reference velocity location can be used directly with the peak-pressure coefficients to obtain peak local design wind loads for cladding design. Local, instantaneous peak loads on the full-scale building suitable for cladding design were computed by multiplying the reference pressure of Table 5 by the peak coefficients of Table 6 and are listed as peak pressures in that table. The maximum psf loads given at each tap location are the largest peak positive and peak negative values found in the tests. For ease in visualizing the loads on the structure, contours of equal peak pressures for cladding load shown in Table 6 have been plotted on developed elevation views of the structure,

Figure 10. For control of water infiltration from outside to inside, the largest positive (inward-acting) pressure at each tap location is tabulated in Table 6.

For glass design pressures, a glass load factor is used to account for the different duration between measured peak pressures and the one minute loading commonly used in glass design charts. The design pressure used for glass is normally less than the peak pressures used for cladding design because of the static fatigue property of glass which can withstand higher pressures for short duration loads than for long duration loads. Recent research (8) indicates that the period of application of the peak pressures reported herein is about 5-10 seconds or less. If a glass design is based on these peak-pressure values, then a glass strength associated with this duration load should be used. Because glass design charts are normally based on some alternate load duration--usually one minute--then some reduction in peak loads should be made. An estimate of a load reduction factor can be obtained from an empirical relation of glass strength as a function of load duration. Current glass selection charts showing glass strength as a function of load duration (9) and older references (10) indicate the following load reduction factors:

	ref 9	ref 10
annealed float	0.80	0.81
heat strengthened	0.94	
tempered	0.97	0.98

Loadings appropriate for glass design can be computed by multiplying the peak-pressure loads of Table 6 by these load factors.

4.4 Forces and Moments

Force coefficients in the horizontal X and Y directions and moment coefficients about the X, Y, and Z axes with the origin at ground level at the base of the building with Z axis vertical may be computed for all wind directions tested by integration of mean pressures on the building. Overall forces and moments acting on the full-scale building due to wind loading which are useful in designing the structural framing of the proposed building may be obtained from use of these coefficients.

Force coefficients were computed for each floor for each wind direction using the equations shown below.

$$CF_X = \frac{F_X}{A_R \; 0.5 \; \rho \; U_\infty^2} \qquad CF_Y = \frac{F_Y}{A_R \; 0.5 \; \rho \; U_\infty^2}$$

Terms and symbols used in the equations are defined in the List of Symbols and the axes are defined for the building in Figure 3. Force coefficients CF_X and CF_Y were computed for the horizontal forces acting along the X and Y axes using the mean pressure coefficient at each pressure tap. A_R represents a constant reference area for nondimensionalization of the forces and moments.

The total forces acting on the full-scale building for each floor and wind direction were computed by multiplying the above coefficients by the appropriate full-scale reference area, by the reference pressure of Table 5, and by a gust load factor selected for an appropriate wind gust duration. The gust load factor, shown in Table 5, was selected to increase the loads from an hourly mean load to that of a gust whose duration would be sufficient for its effect to be fully felt by the structure. A table of gust load factors for various gust durations is

incorporated in Table 5 so that force and moment data of Table 7 may be adjusted to a different load duration if desired.

The forces obtained at each floor were used to obtain load, shear, and moment diagrams for the building for each wind direction. The shear diagram, in kips, was obtained by algebraic sum of all forces in each coordinate direction acting above the floor of interest. The load diagram, in psf, was obtained by dividing the shear values by their contributing areas (listed in Table 7). The moment diagram, in 1000 ft-kips, was obtained by integration of the shear values so that the moment due to forces acting above the floor level of interest was calculated. The sign of the moment was established by the right-hand rule about an X', Y' axis through the floor of interest. Moments about the Z axis were calculated by considering the displacement of forces in the X and Y directions from the Z axis shown in Figure 3. Eccentricities were computed such that the product of the Y force and X eccentricity minus the product of the X force and Y eccentricity equaled the Z moment. Load, shear, and moment diagrams are shown in Figure 11 for several wind directions.

5. DISCUSSION

5.1 Flow Visualization

Flow patterns identified with smoke showed that the highest cladding pressures would probably be found near building corners. This is consistent with data previously measured on other rectangular buildings. Local vortex flows, which can substantially increase local pressures, were not evident. Winds in pedestrian areas at the base of the building appeared to be strongest near the building corners at the base of the building. This is a common phenomena about tall buildings. High velocity flow was observed to pass under the undercut at the entrance on the south side of the building. It appeared that the highest velocity flow was closer to the soffit than to the ground. This situation is good for the pedestrian wind environment but could result in higher pressure loads on the soffit. The pedestrian winds at ground level outside the overhang appeared stronger than those directly under the overhang. The proximity of the 15 Columbus Circle building to Central Park provides an exposed approach relatively unprotected by nearby buildings. The general level of building heights to the southwest through the northwest (see Figure 5) is substantially less than the 15 Columbus Circle building exposing the upper half of the building to winds from those directions.

5.2 Pedestrian Winds

Figure 4 shows the 18 locations selected for investigation of pedestrian wind comfort. Location 1 was selected as a reference location which would be away from the high velocity regions identified at the immediate base of the building. Table 2 and Figure 8 show that the largest values of mean velocity were found at locations 5, 11, 16 and 17 with values ranging from 60 to 72 percent of U_∞, the mean velocity at

the boundary-layer height. These areas are the same ones identified with smoke flow. For comparison, the largest value of mean velocity at location 1 was 29 percent of U_∞ while about 40 to 45 percent might be expected in an open-country environment.

The largest values of fluctuating velocity, U_{rms}, were measured at location 17 with values ranging from 23 to 29 percent of U_∞. For comparison, reference location 1 had a maximum U_{rms} of 13 percent while an open-country environment might expect a value of 10 to 12 percent. The largest value of peak gust, represented by the mean plus 3 rms as discussed in Section 4.2, were measured at locations 16 and 17 with values ranging from 116 to 136 percent of U_∞. For comparison, the largest value of peak gust measured at location 1 was 60 percent while about 80 to 85 percent would be expected in an open-country environment.

Velocity data of Table 2 integrated with local wind data listed in Table 3 are shown in Figure 9. Based on the data of this figure, the windiest location measured was location 3 which is predicted to be unacceptably windy about 10 to 20 percent of the time for mean winds on the basis of the acceptance criteria used. Several other locations are predicted to be unacceptably windy 10 percent or less of the time: locations 2, 5, 9, 11, 16 and 17. Wind gusts appeared to be of less concern than mean wind speeds. The building's main entrance, location 10, was predicted to be comfortable for long-duration activities nearly 90 percent of the time and uncomfortable for walking less than 2 percent of the time.

The results of the pedestrian wind analysis showed that, on the basis of the acceptance criteria used, several locations about the base

of the building may be considered to be quite windy up to 10 percent of the time (20 percent for one location, 3). The main entrance should not be considered to be windy. Since the structure has been in place for a number of years, frequent users of the sidewalk areas about the building could confirm the predicted acceptability of the pedestrian environment. The winds which create the higher velocity areas originate high on the structure and hit the ground near the high wind areas. Thus, little can be done to improve local wind environments except trees or foliage in the immediate vicinity of the area to be improved.

5.3 Pressures

Table 6 shows the largest peak pressure coefficients and corresponding loads measured on the building for each pressure tap location. Data identified as Configuration A in Table 6 and Appendix A represent data obtained at all tap locations for 36 wind directions. Configuration B represents data obtained at selected taps at 2-degree azimuthal increments near azimuths where large pressure peaks were observed in Configuration A to ensure that the largest peaks were obtained. Pressure coefficients were combined with the all-direction, 50-year recurrence wind reference pressure shown in Table 5 to obtain peak cladding pressures which are listed in Table 6 and plotted in contour plots in Figure 10. The second page of Table 5 shows load ratios for individual wind directions based on predictions of hurricane wind speeds. Application of this directionality resulted in peak cladding pressures which are listed in the second half of Table 6 and plotted in Figure 10. Consideration of wind directionality results in a significant reduction in cladding loads.

The largest peak pressure coefficients obtained were -2.6 and -2.2 measured at taps 342 and 239 for wind azimuths of 130 and 250 degrees respectively. These measurements were repeated during the 2-degree resolution data acquisition, Configuration B, resulting in a peak coefficient of -1.4 at an azimuth of 134 degrees for tap 342. The large difference in these two measurements resulted from the first measurement being well out on the probability density function describing the range of peak pressure fluctuations. The smaller value is more representative of the peak pressures to be found on the structure during the design storm. For the all-direction 50-year recurrence wind of Table 5, the -1.4 pressure coefficient represents a peak pressure of -46 psf at tap location 342. For tap 239, the resulting peak pressure is 74 psf.

Table 7 lists load, shear and moment distributions for three locations of the coordinate axis shown in Figure 3. These cases were calculated for the all-direction 50-year recurrence wind of Table 5. Application of load ratios to individual wind directions can be made, if desired, by multiplying all loads for a given wind direction by the appropriate load ratio in Table 5. Figure 11 shows load, shear and moment distributions plotted from Table 7 for two wind directions where maximum frame loads occur for the X and Y coordinate directions.

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FIGURES

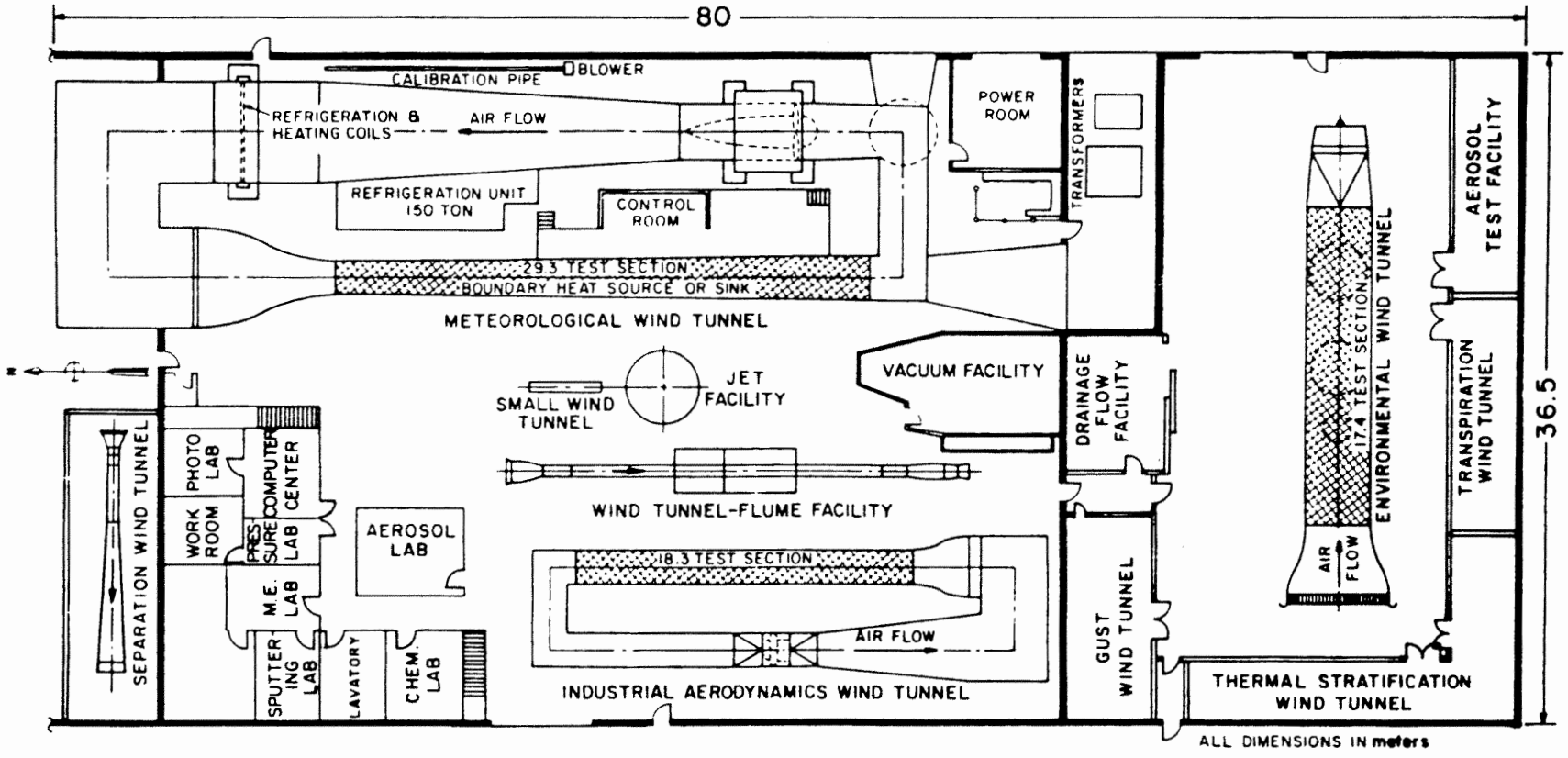
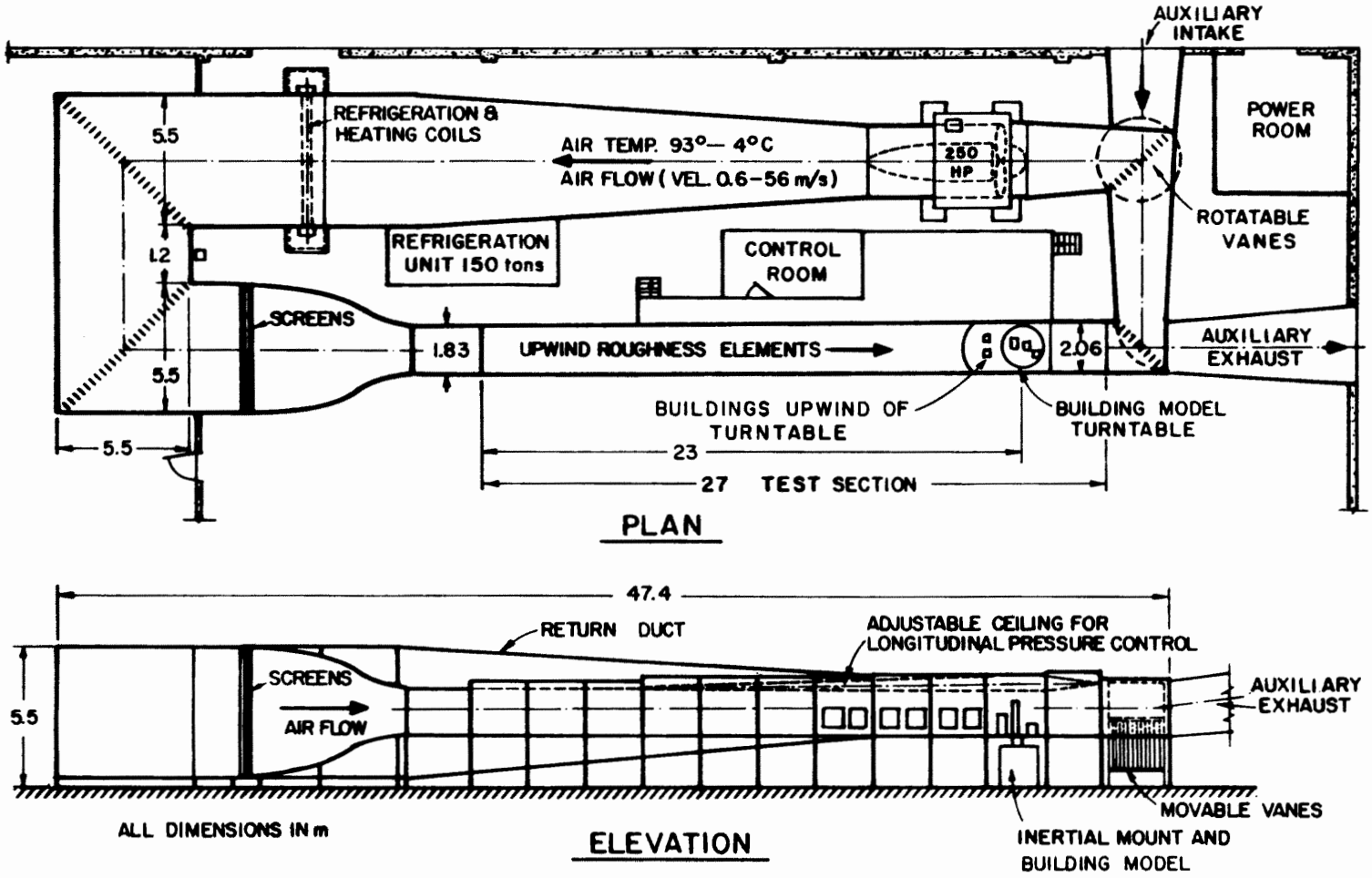


Figure 1. **FLUID DYNAMICS AND DIFFUSION LABORATORY COLORADO STATE UNIVERSITY**



METEOROLOGICAL WIND TUNNEL

Figure 2. Wind–Tunnel Configuration

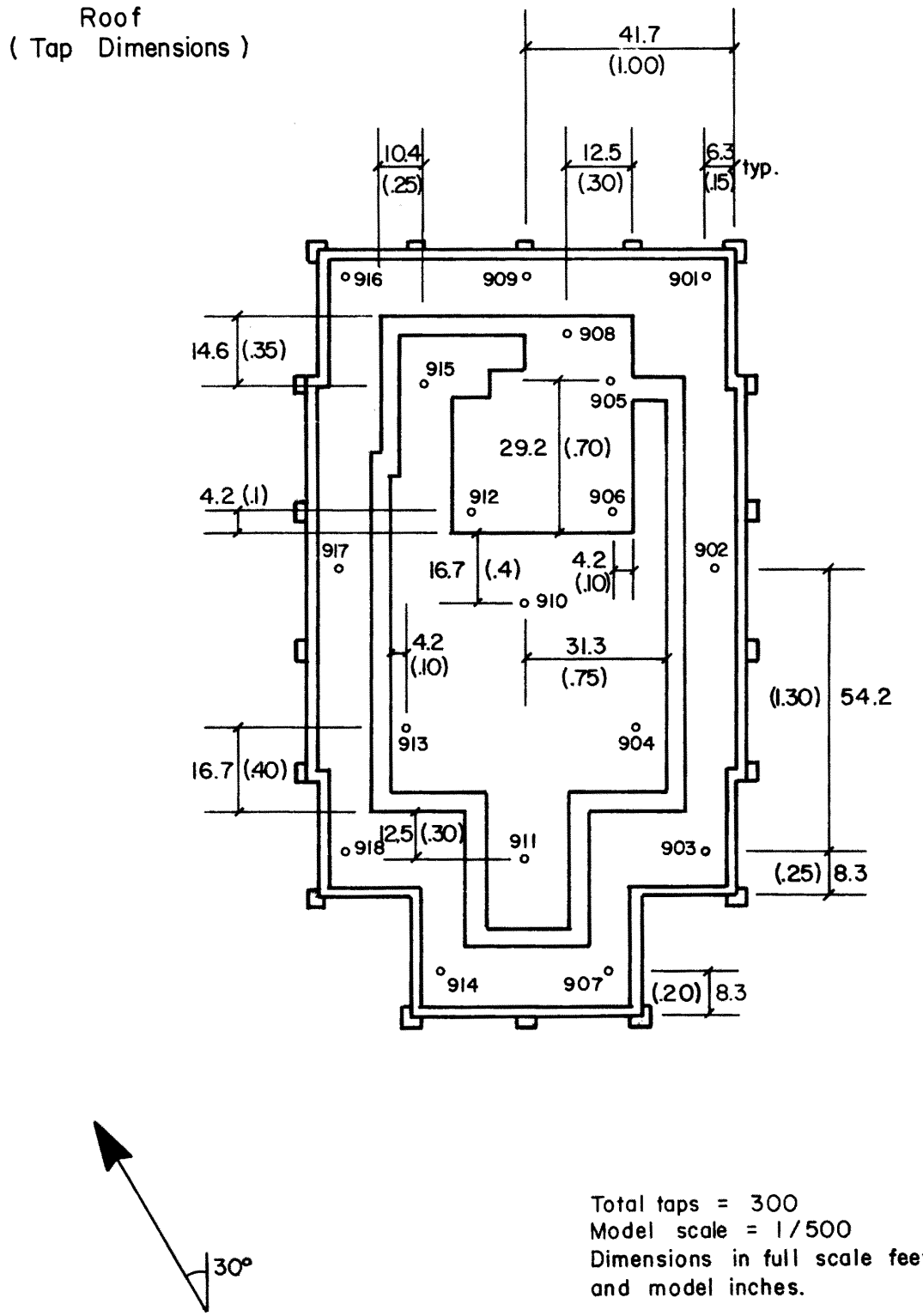


Figure 3a. Pressure Tap Locations

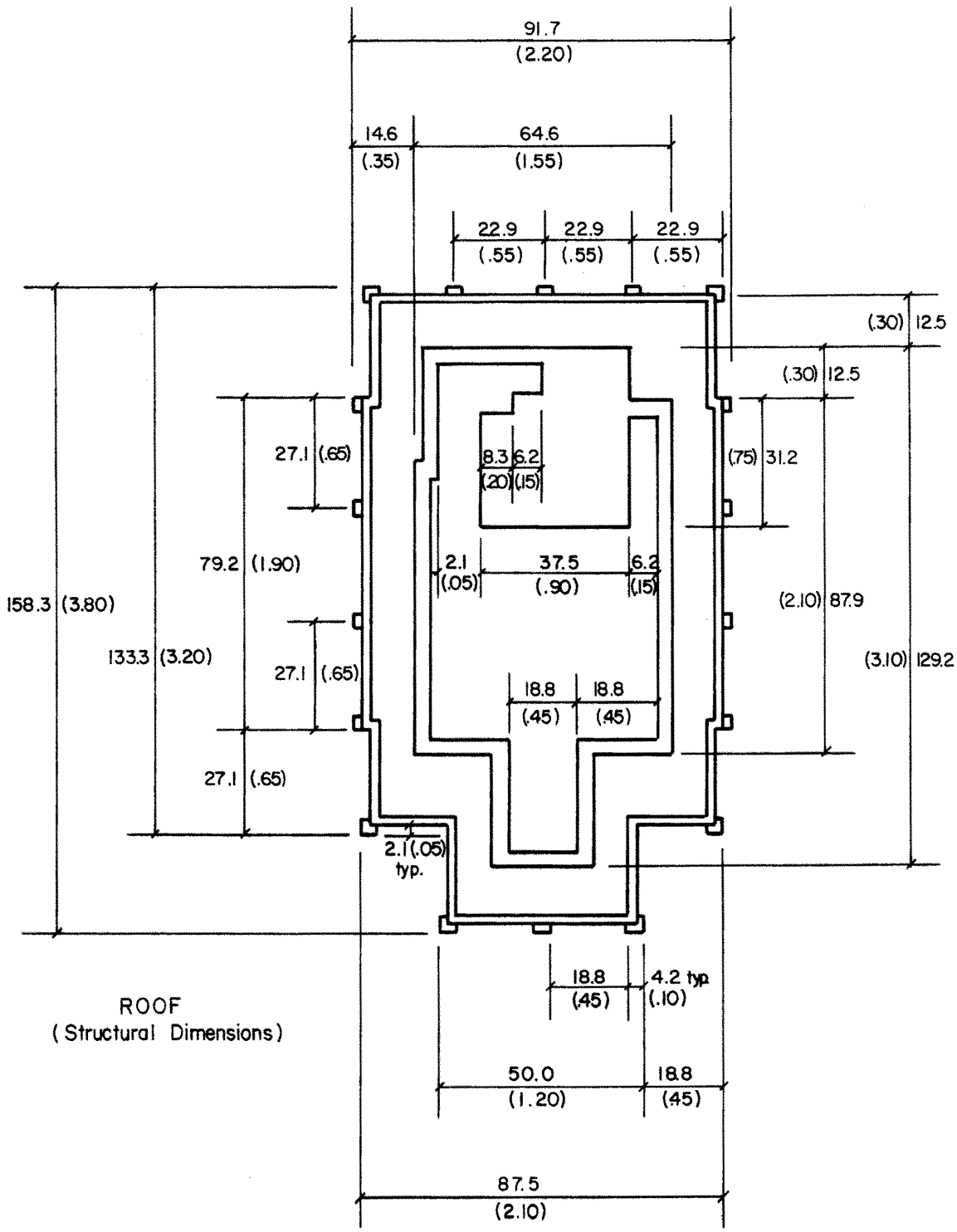
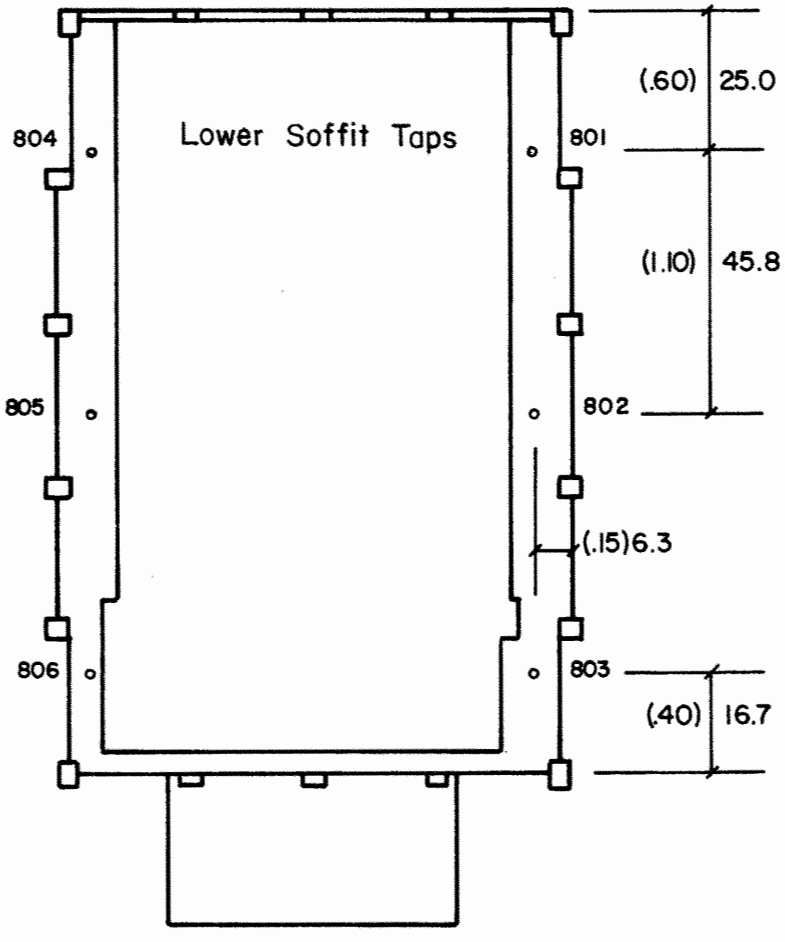


Figure 3b. Pressure Tap Locations



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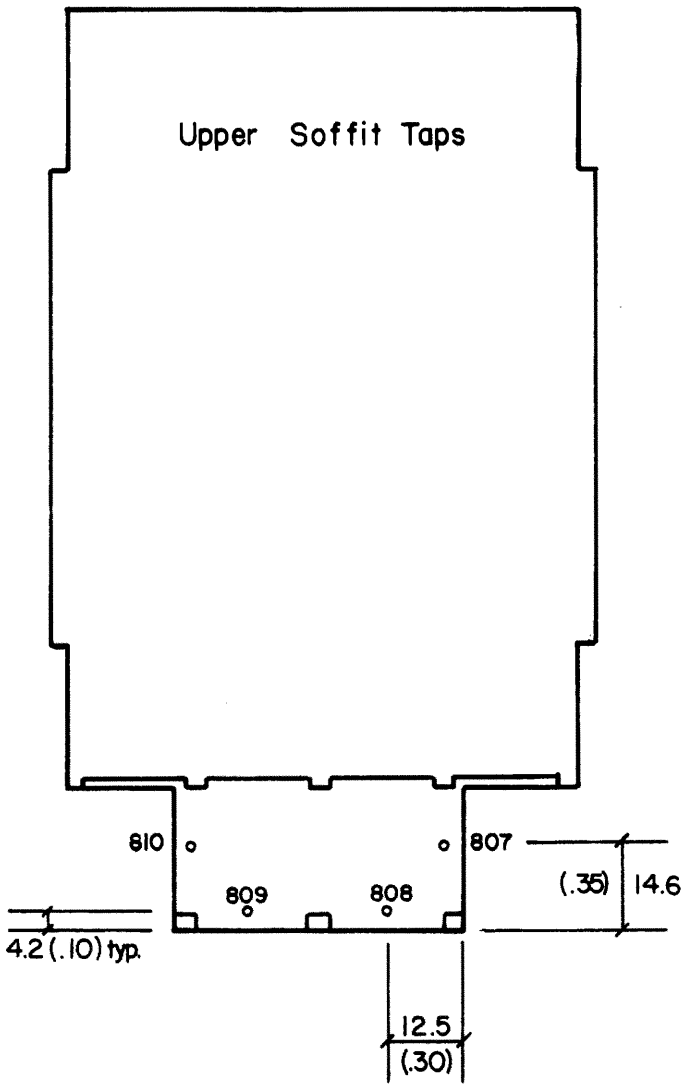


Figure 3d. Pressure Tap Locations

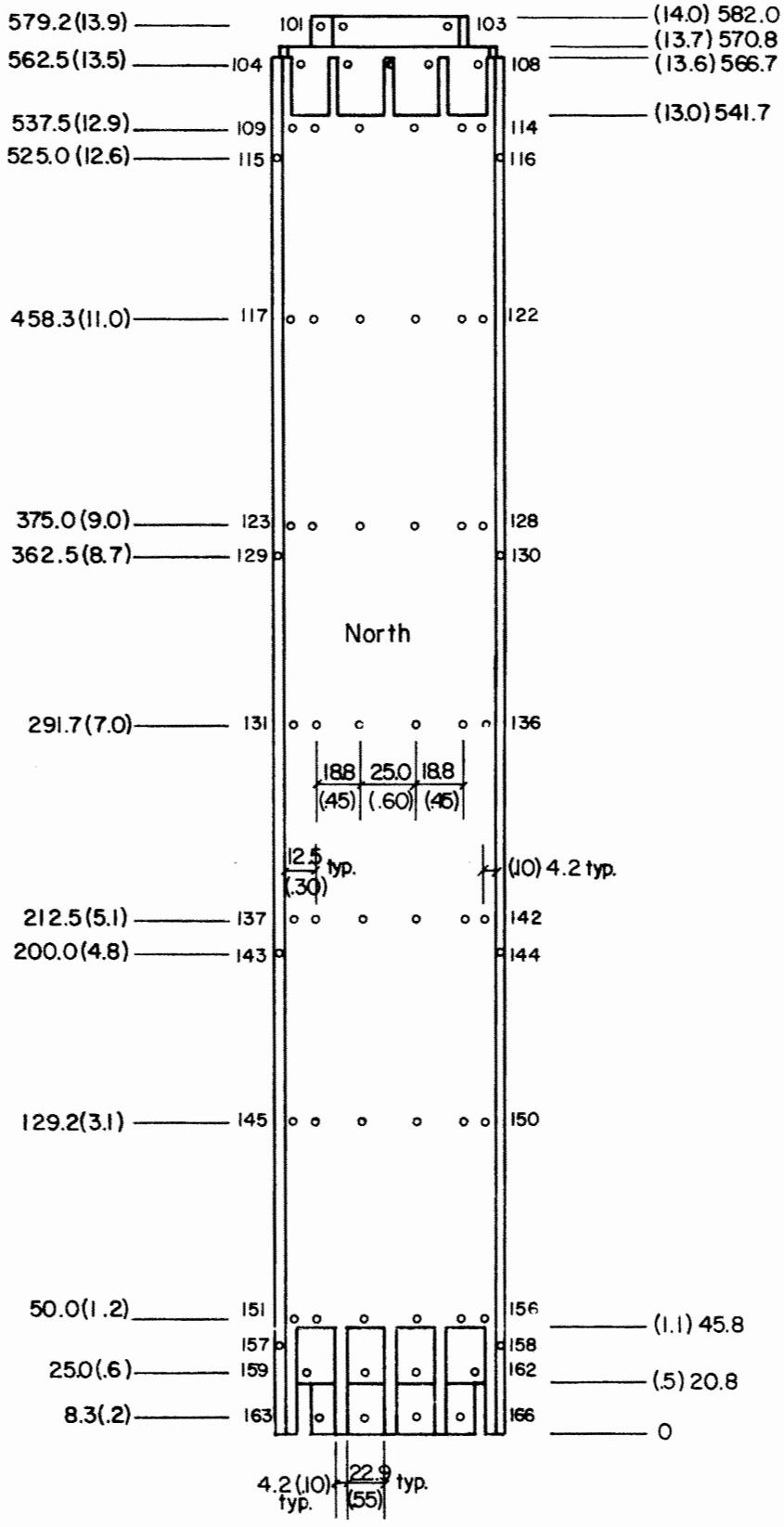


Figure 3e. Pressure Tap Locations

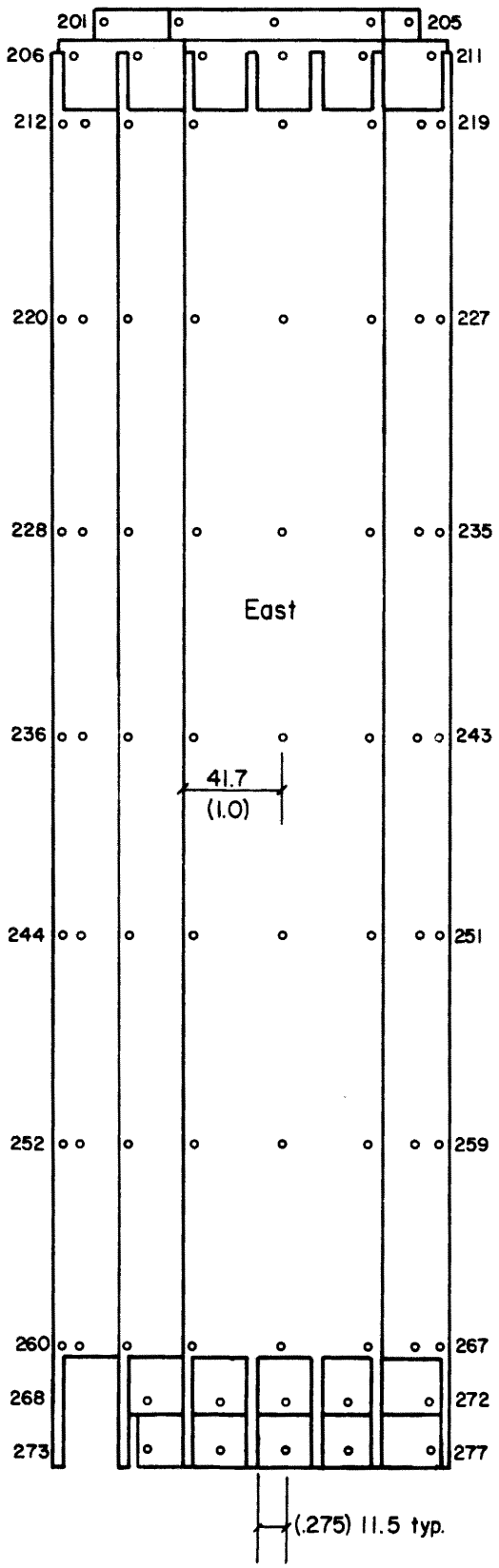


Figure 3f. Pressure Tap Locations

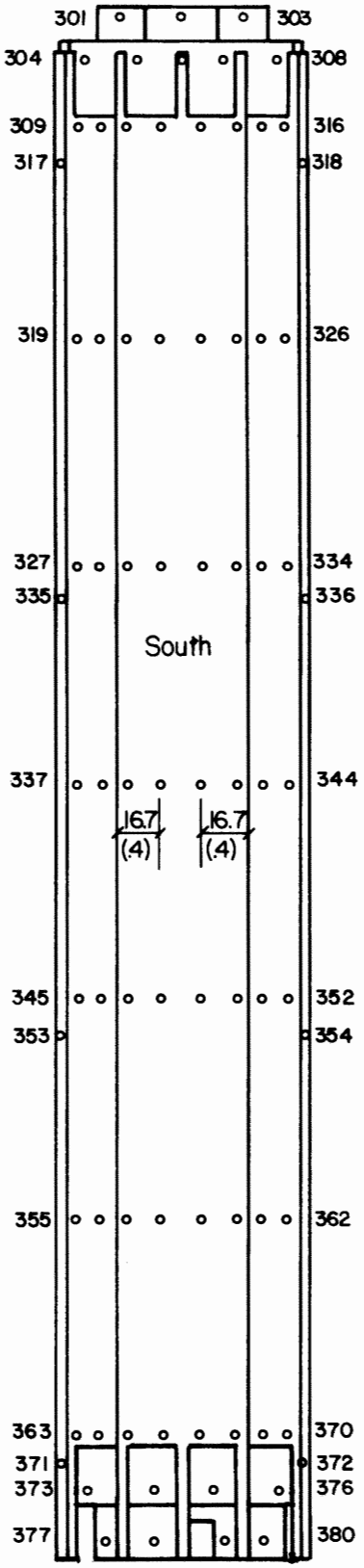


Figure 3g. Pressure Tap Locations

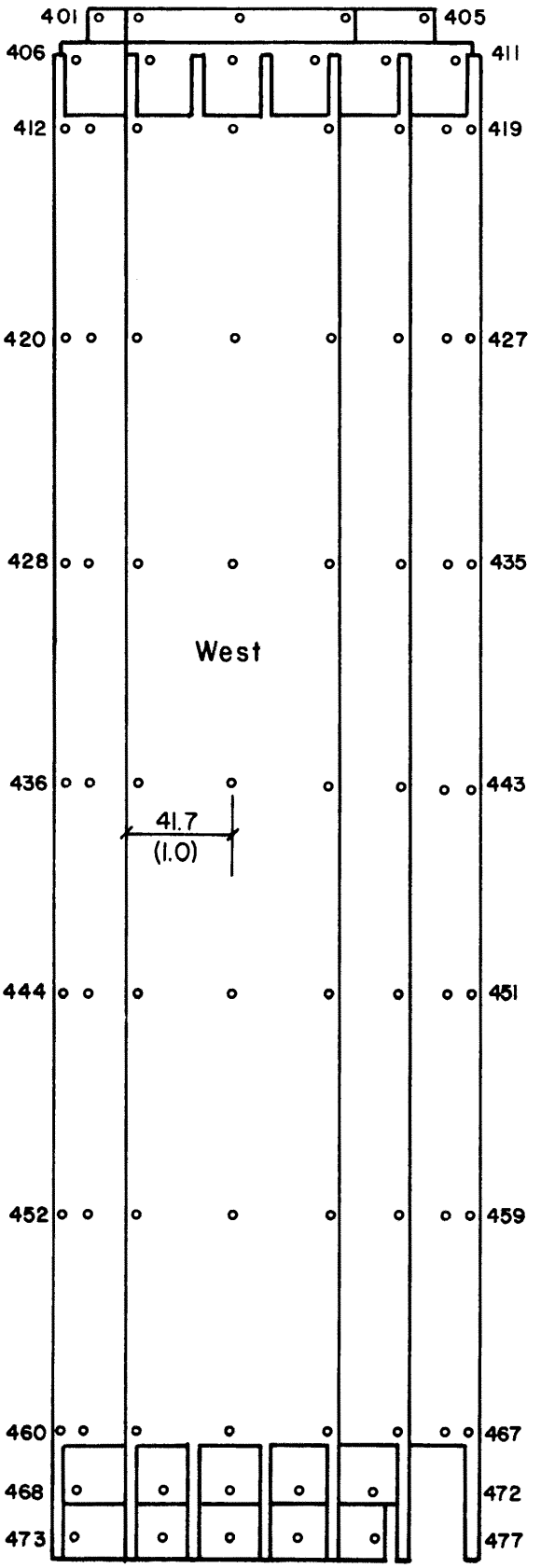


Figure 3h. Pressure Tap Locations

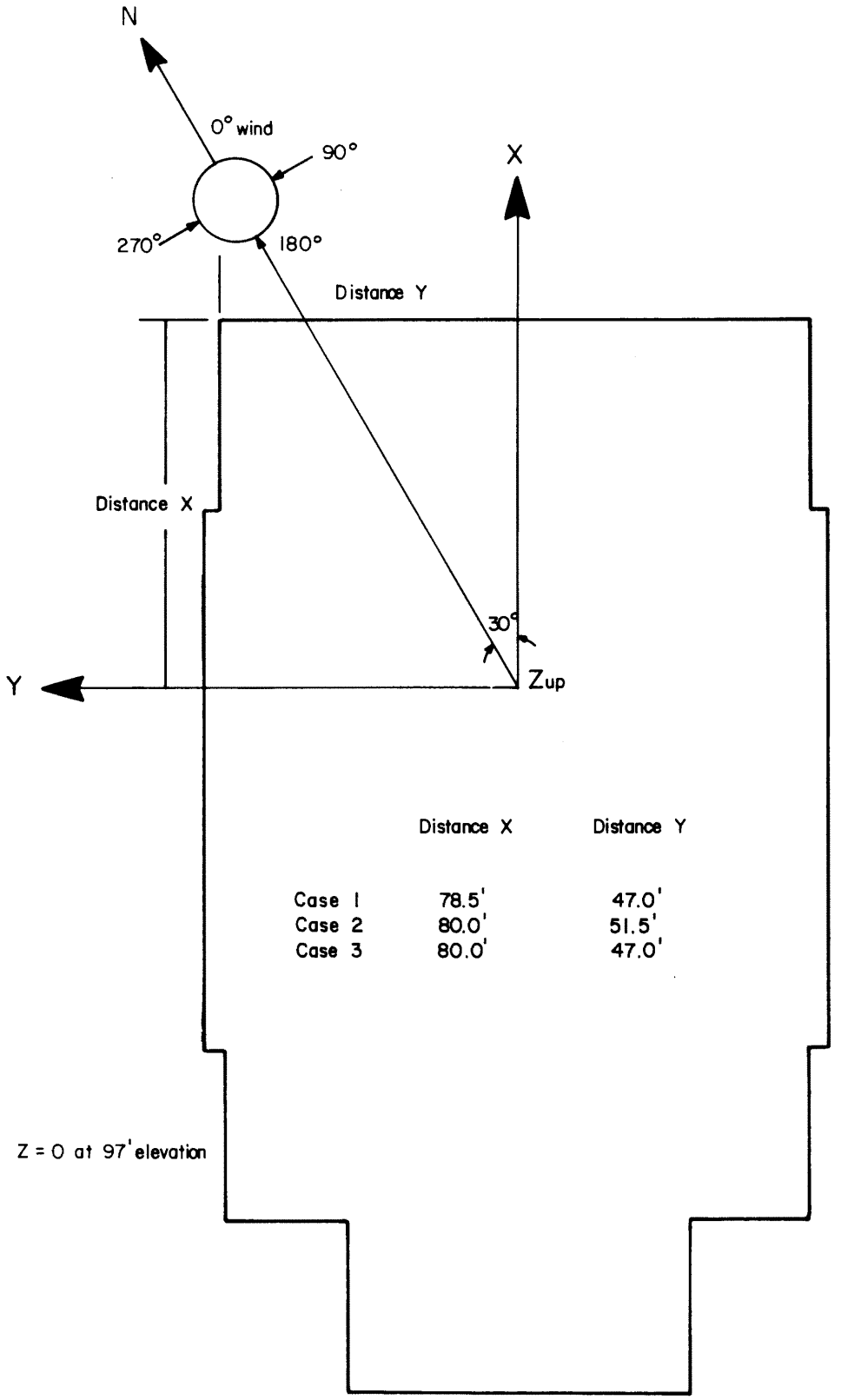


Figure 3i. Pressure Tap Locations

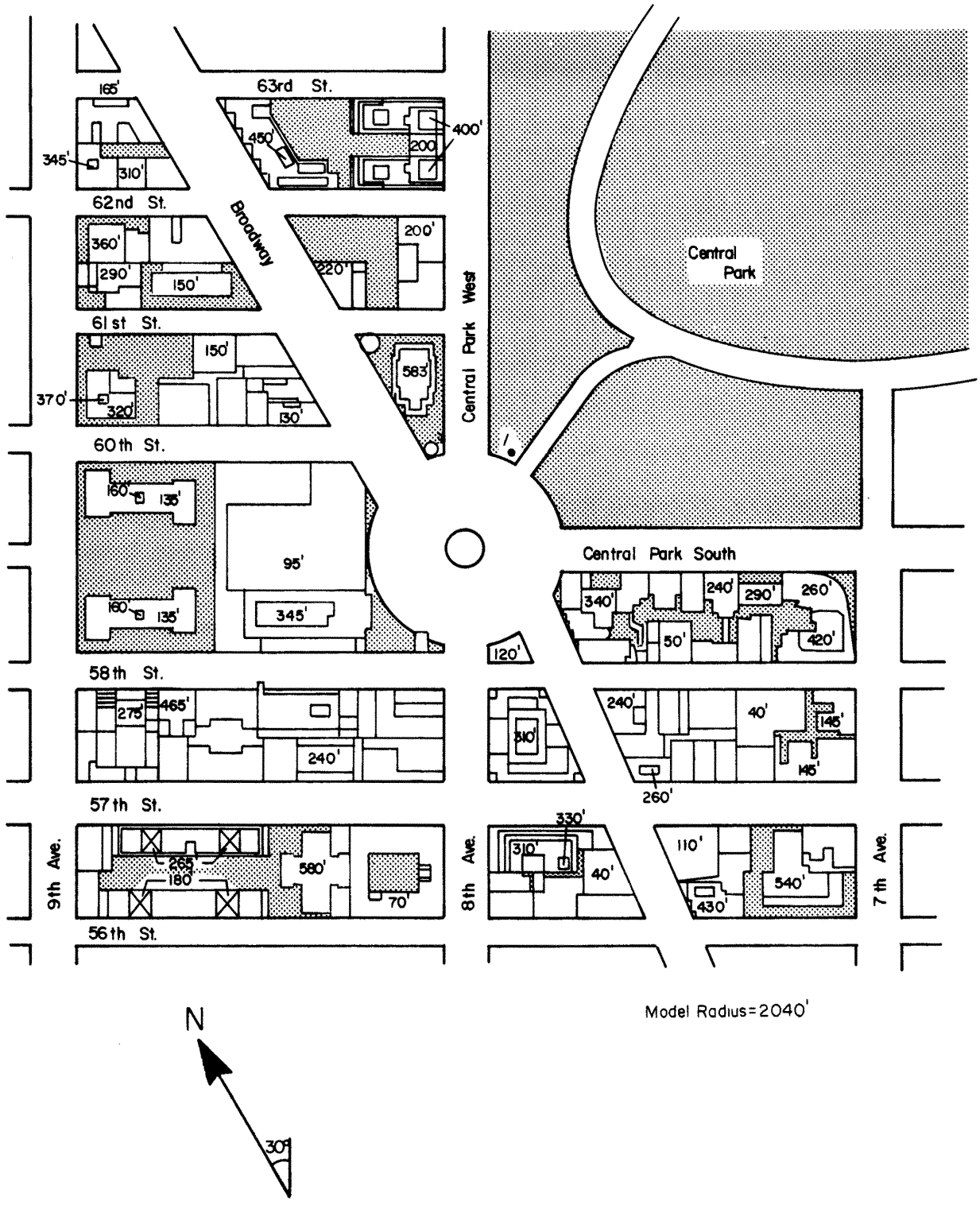


Figure 4a. Building Location and Pedestrian Wind Velocity Measuring Positions

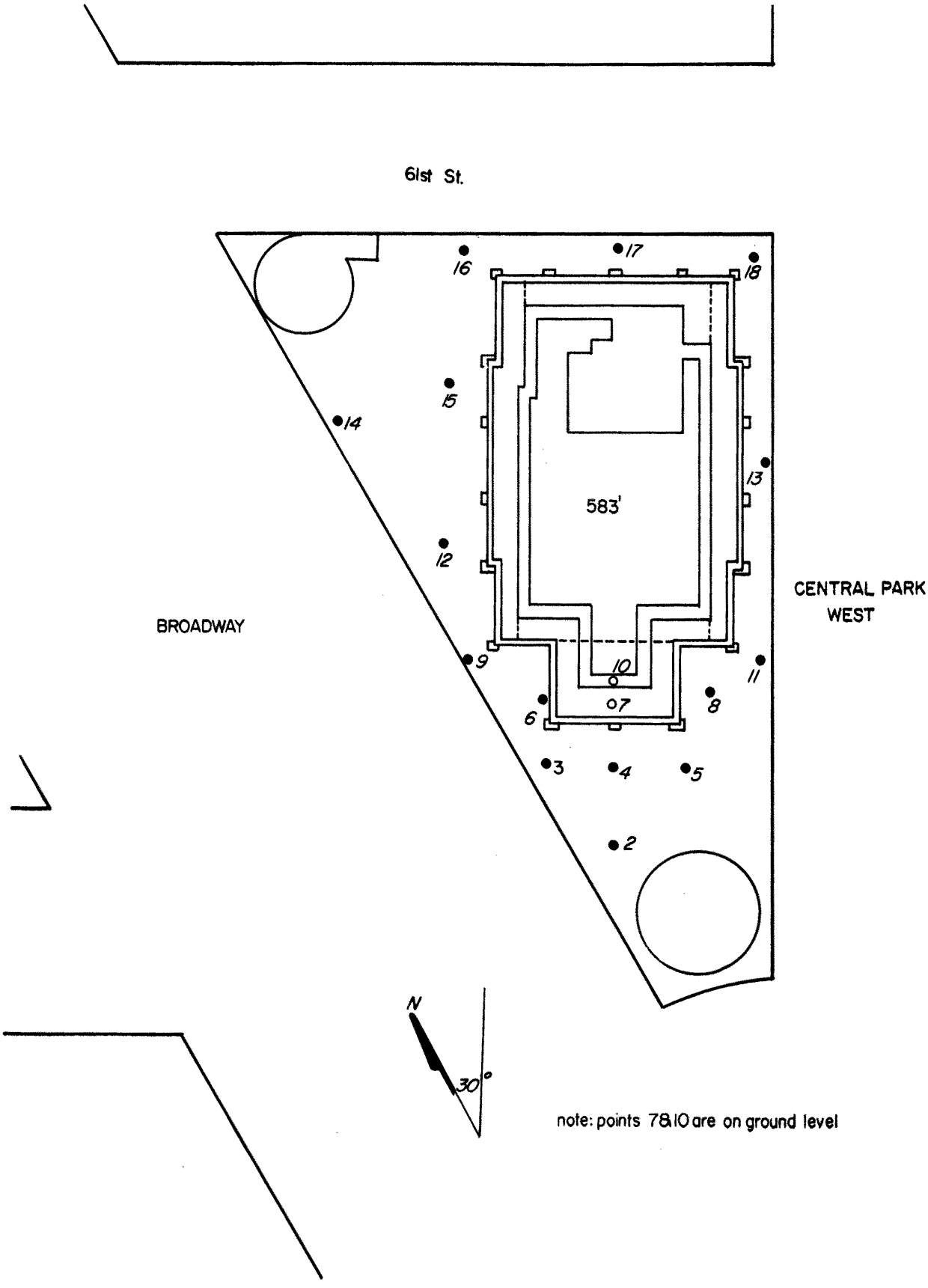


Figure 4b. Building Location and Pedestrian Wind Velocity Measuring Positions

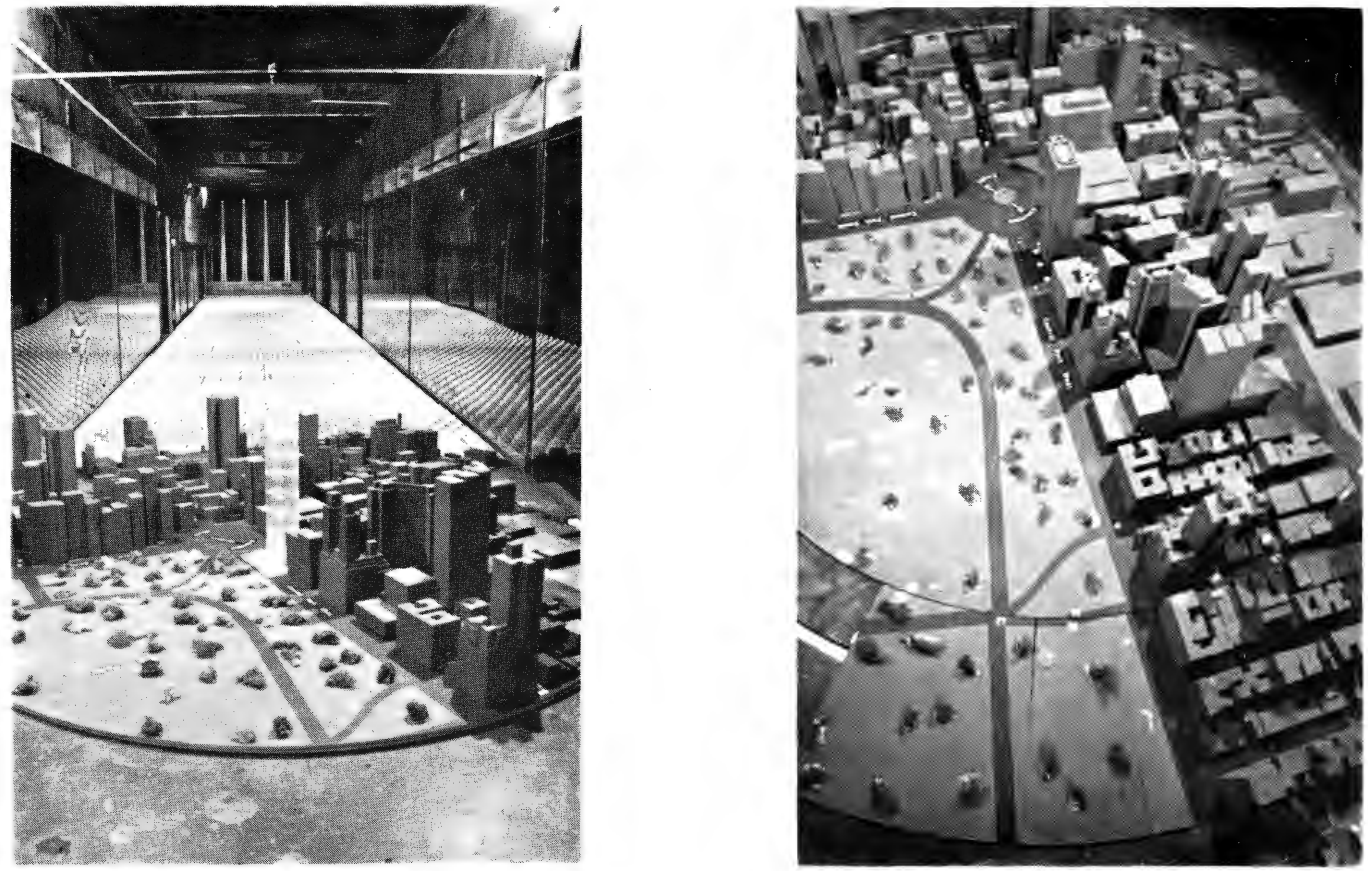


Figure 5. Completed Model in Wind Tunnel

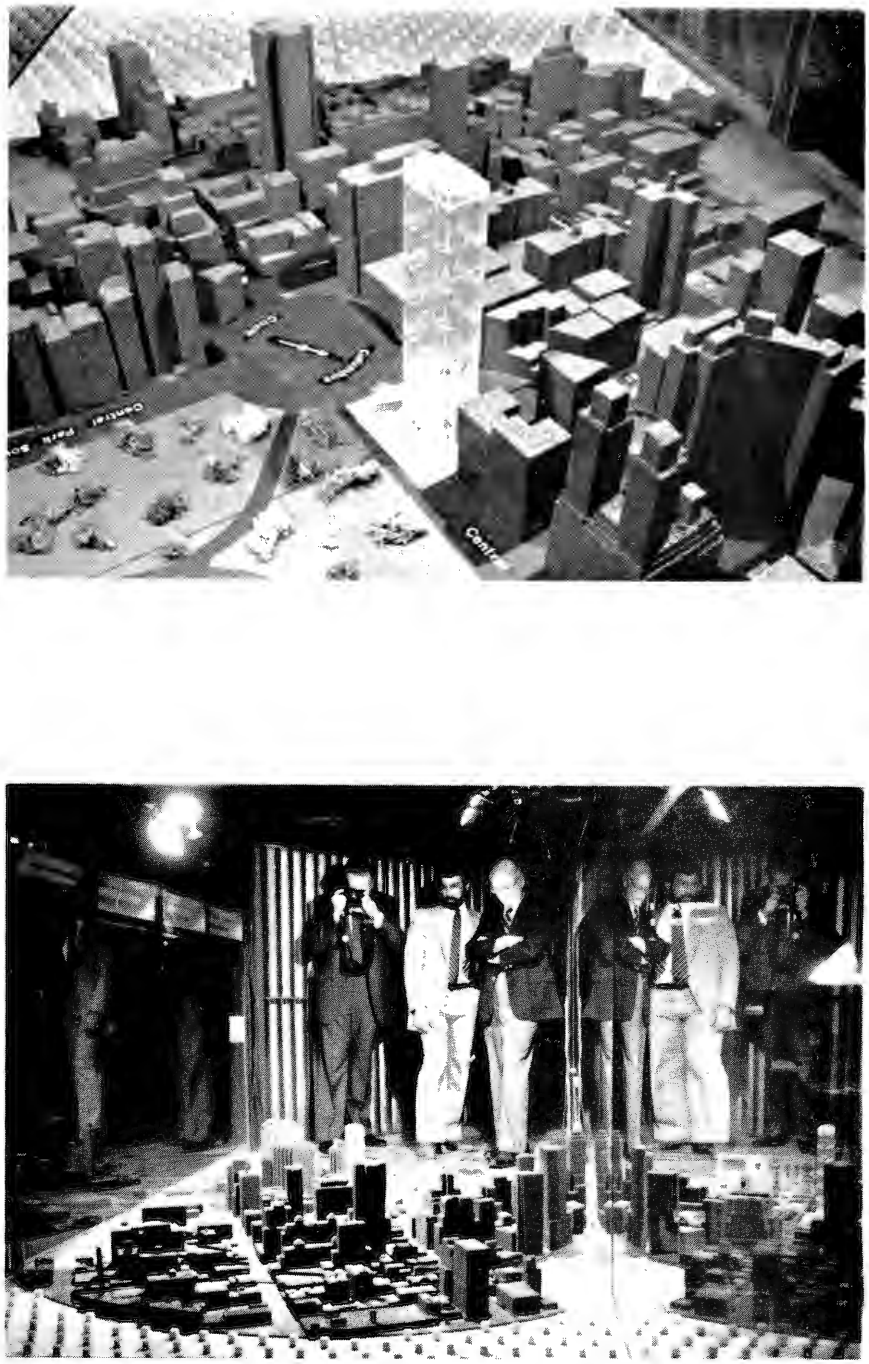


Figure 5. Completed Model

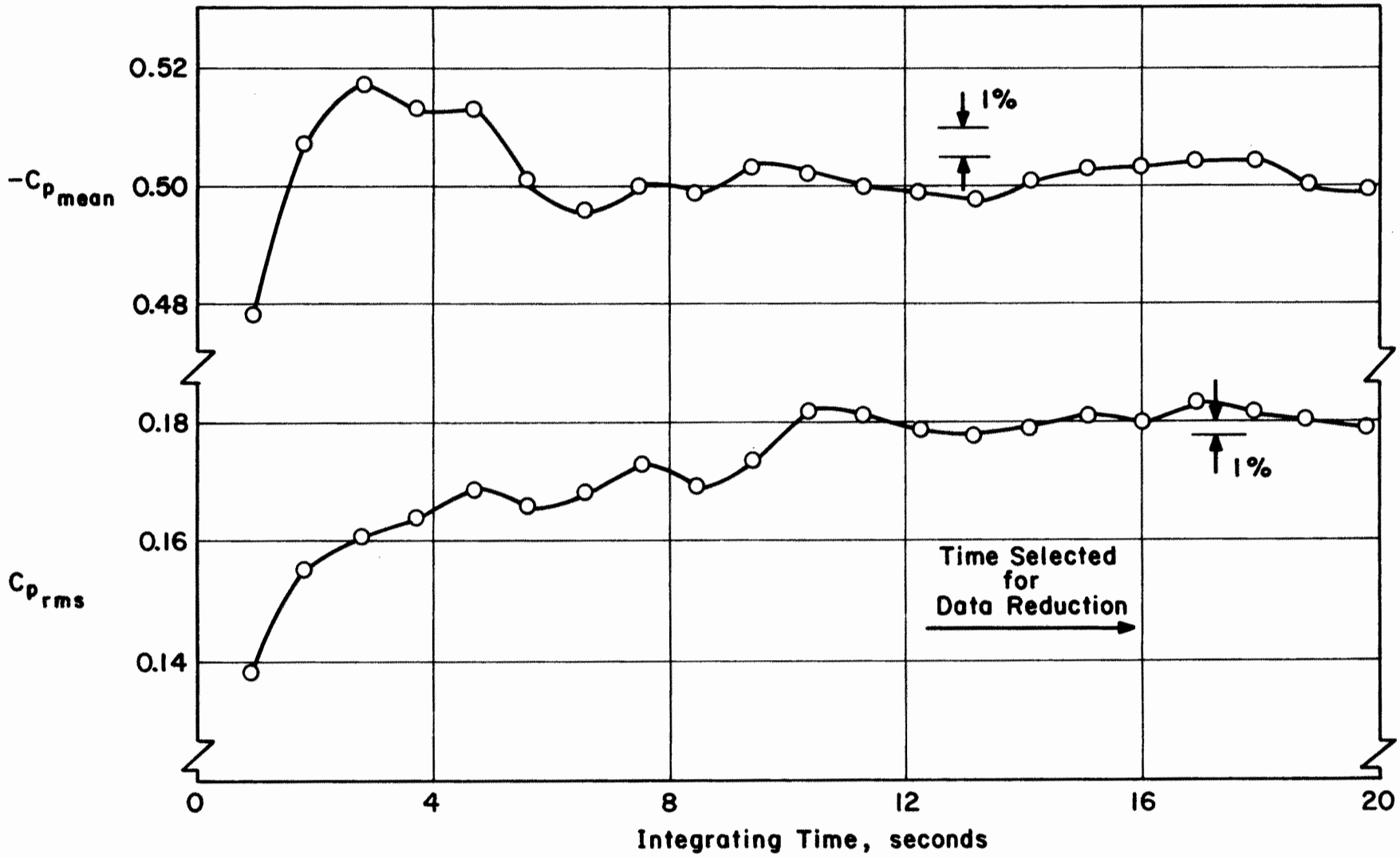


Figure 6. Data Sampling Time Verification

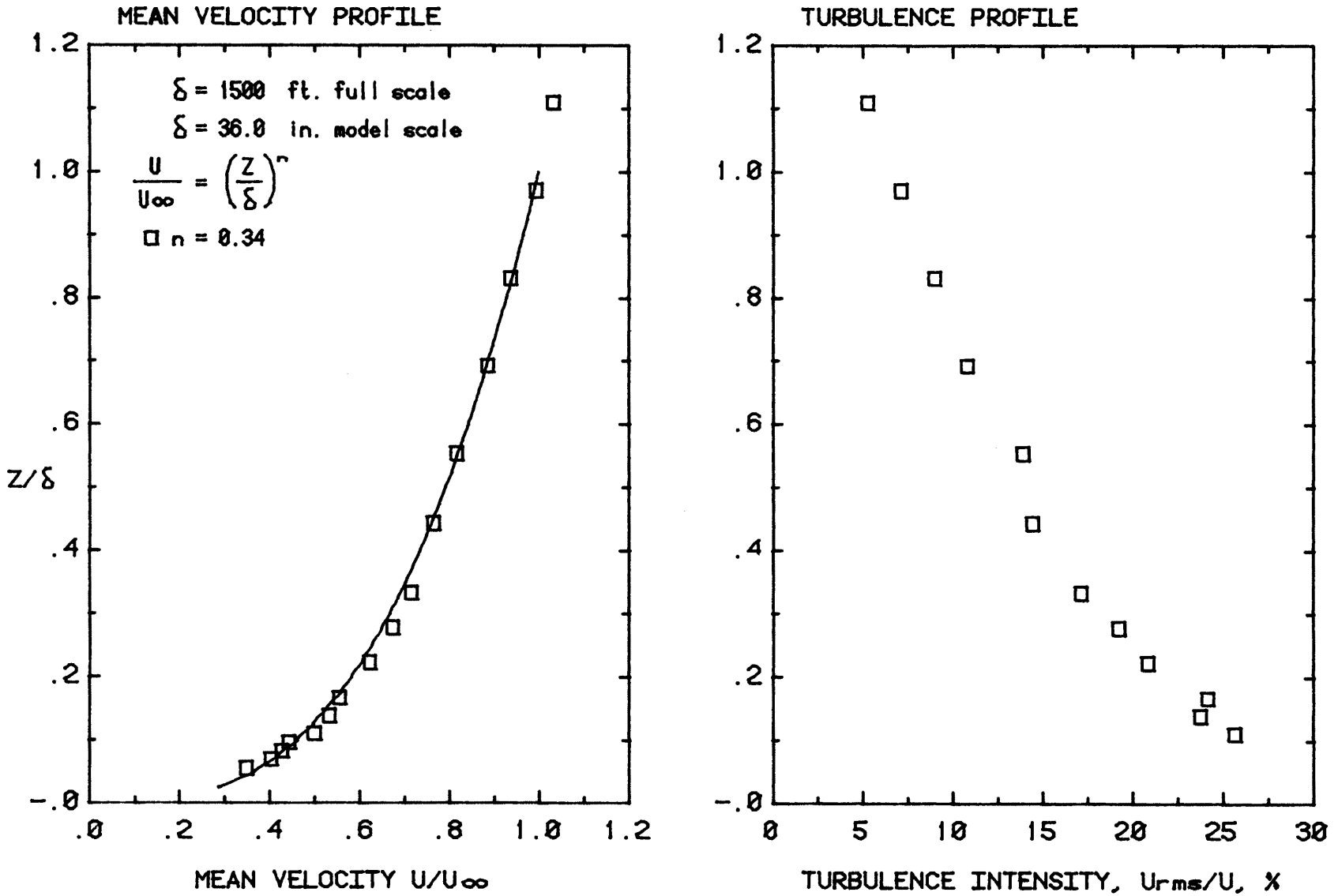


Figure 7. Mean Velocity and Turbulence Profiles Approaching the Model

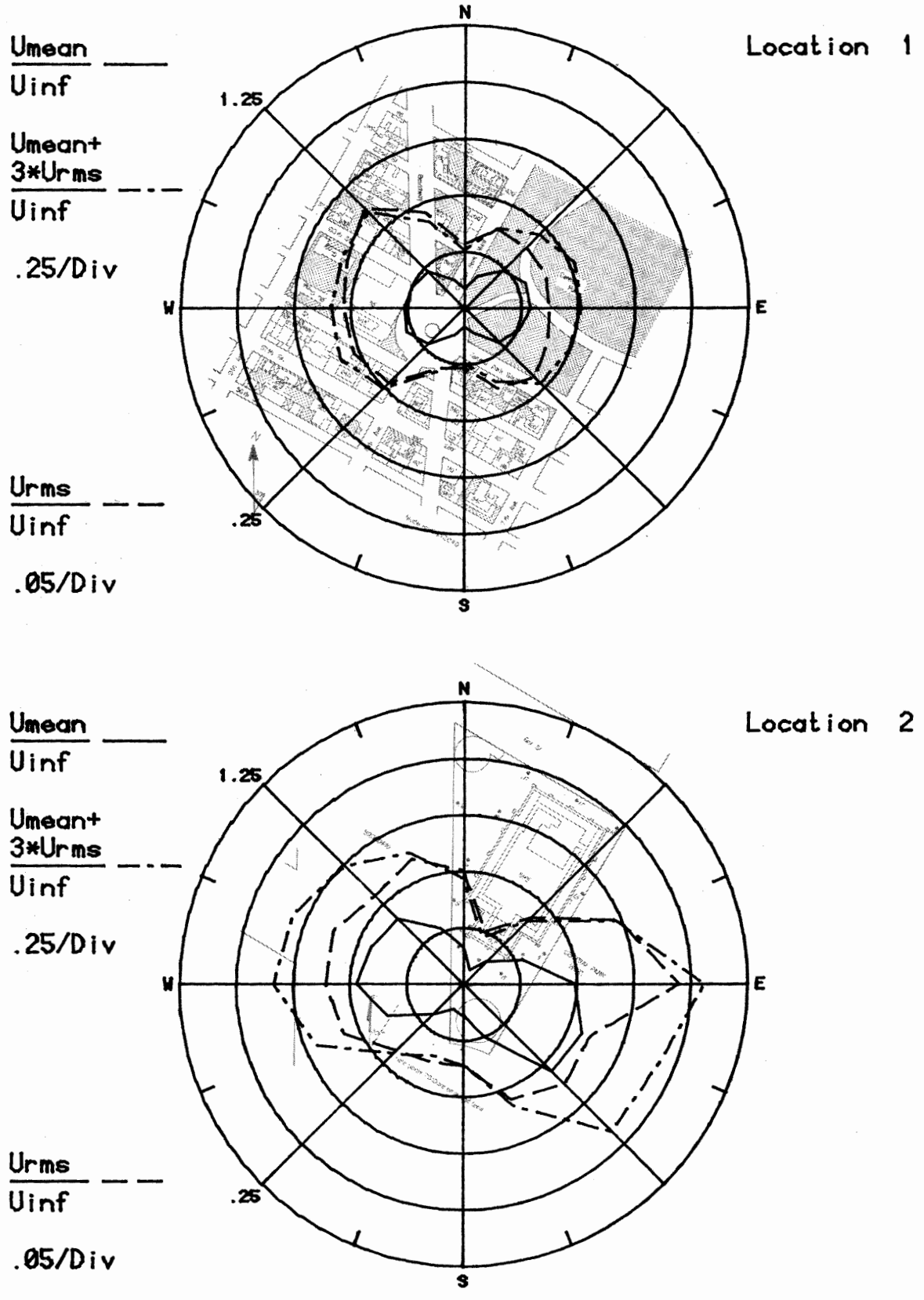


Figure 8a. Mean Velocities and Turbulence Intensities at Pedestrian Locations 1 and 2

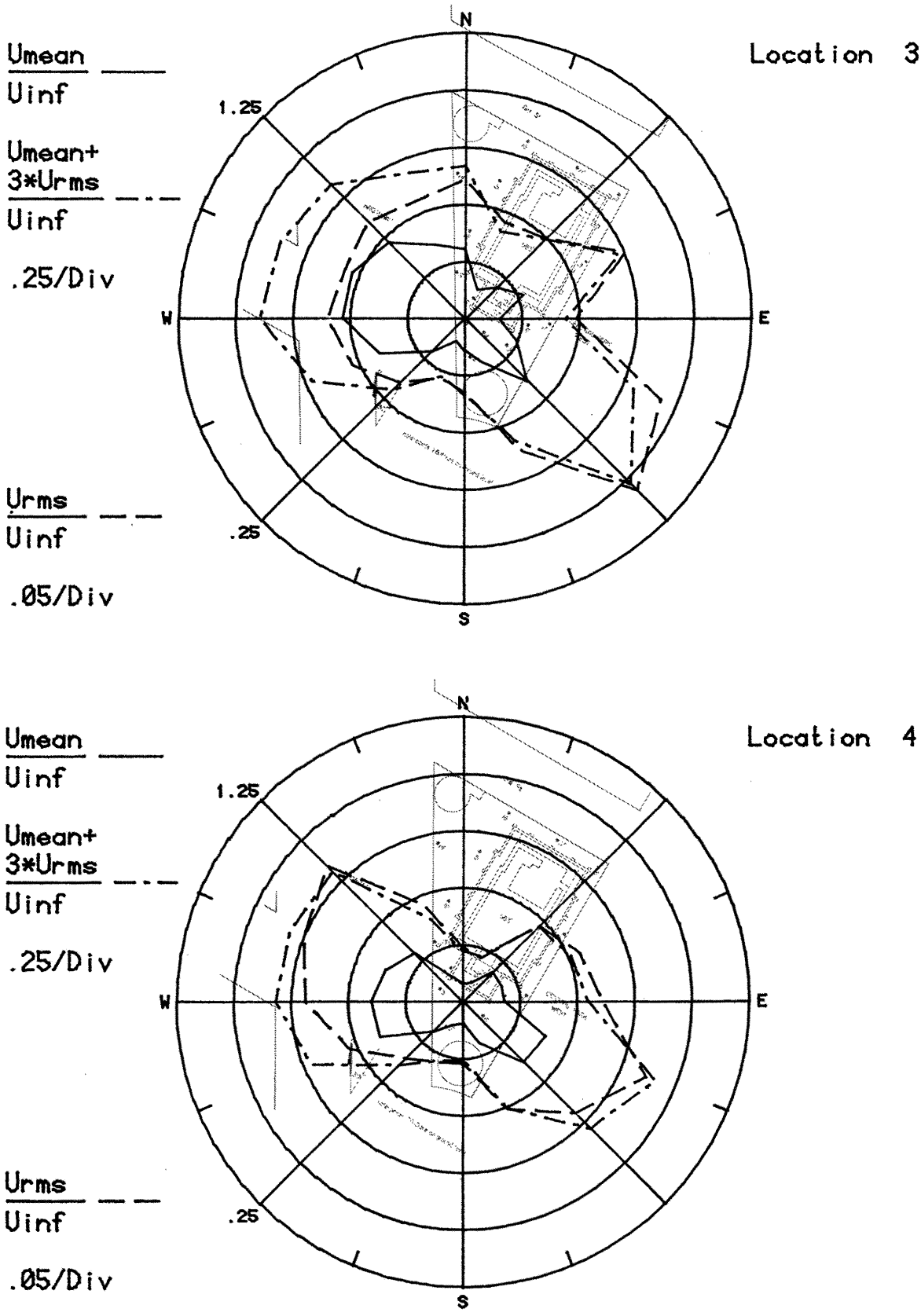


Figure 8b. Mean Velocities and Turbulence Intensities at Pedestrian Locations 3 and 4

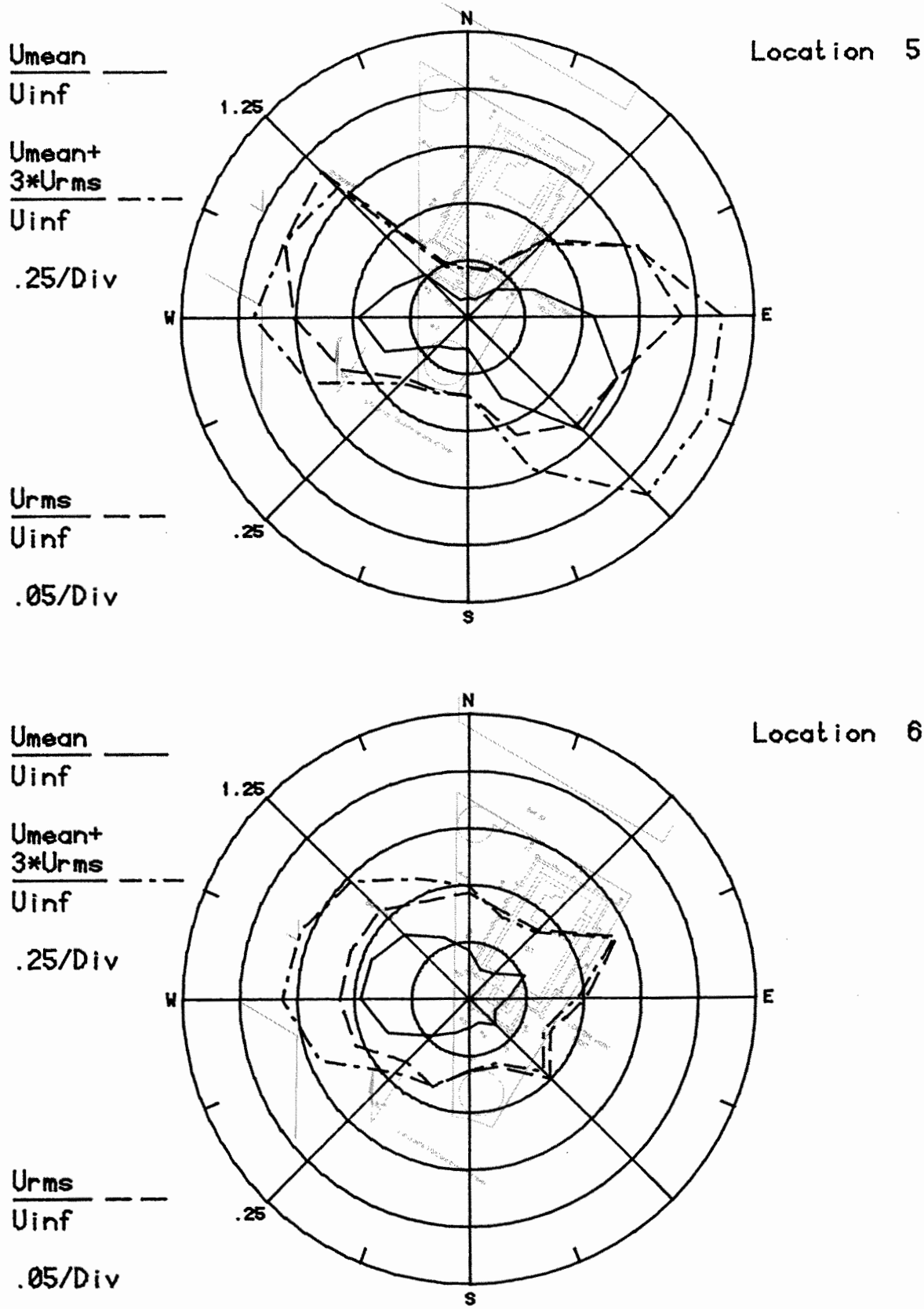


Figure 8c. Mean Velocities and Turbulence Intensities at Pedestrian Locations 5 and 6

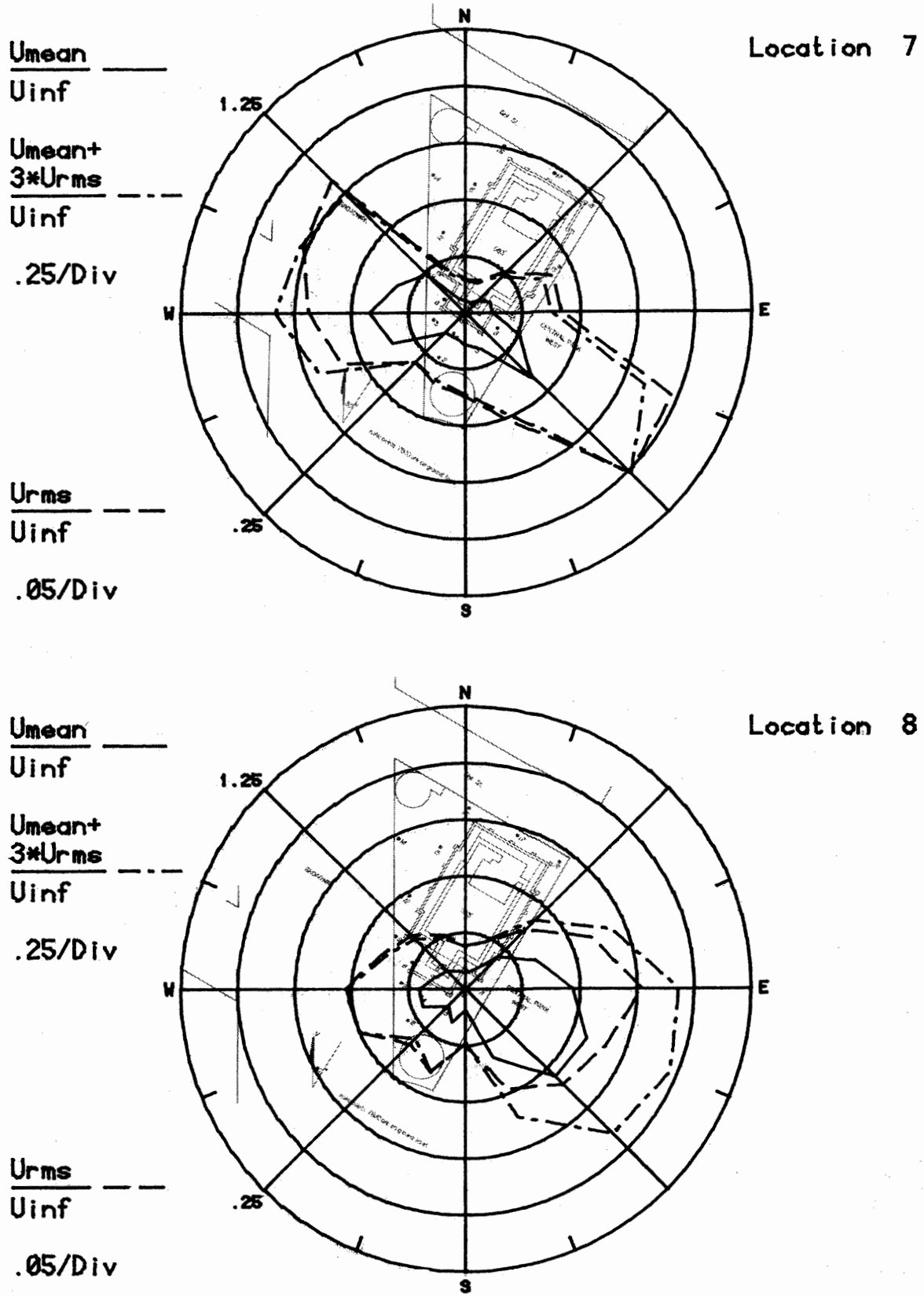


Figure 8d. Mean Velocities and Turbulence Intensities at Pedestrian Locations 7 and 8

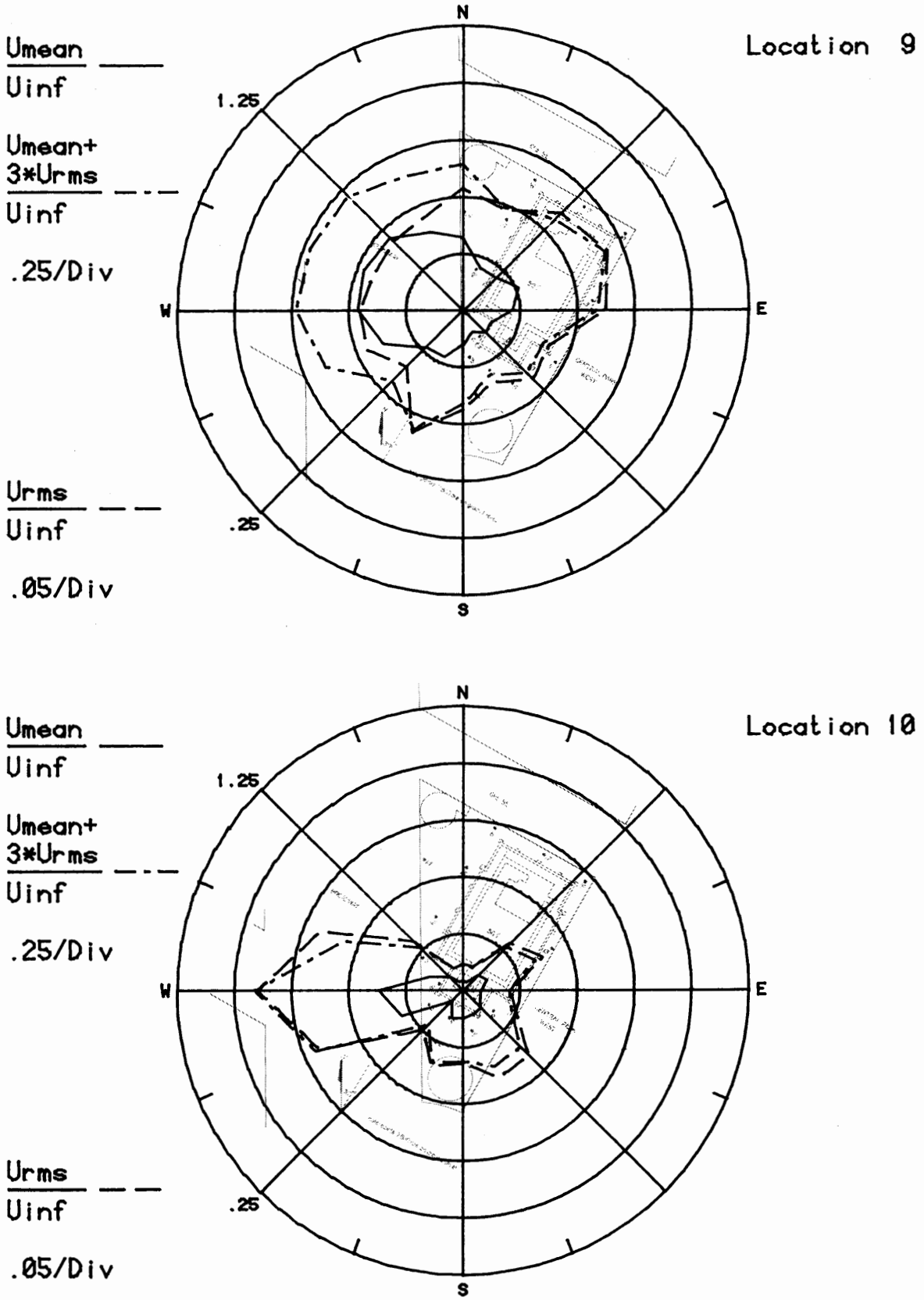


Figure 8e. Mean Velocities and Turbulence Intensities at Pedestrian Locations 9 and 10

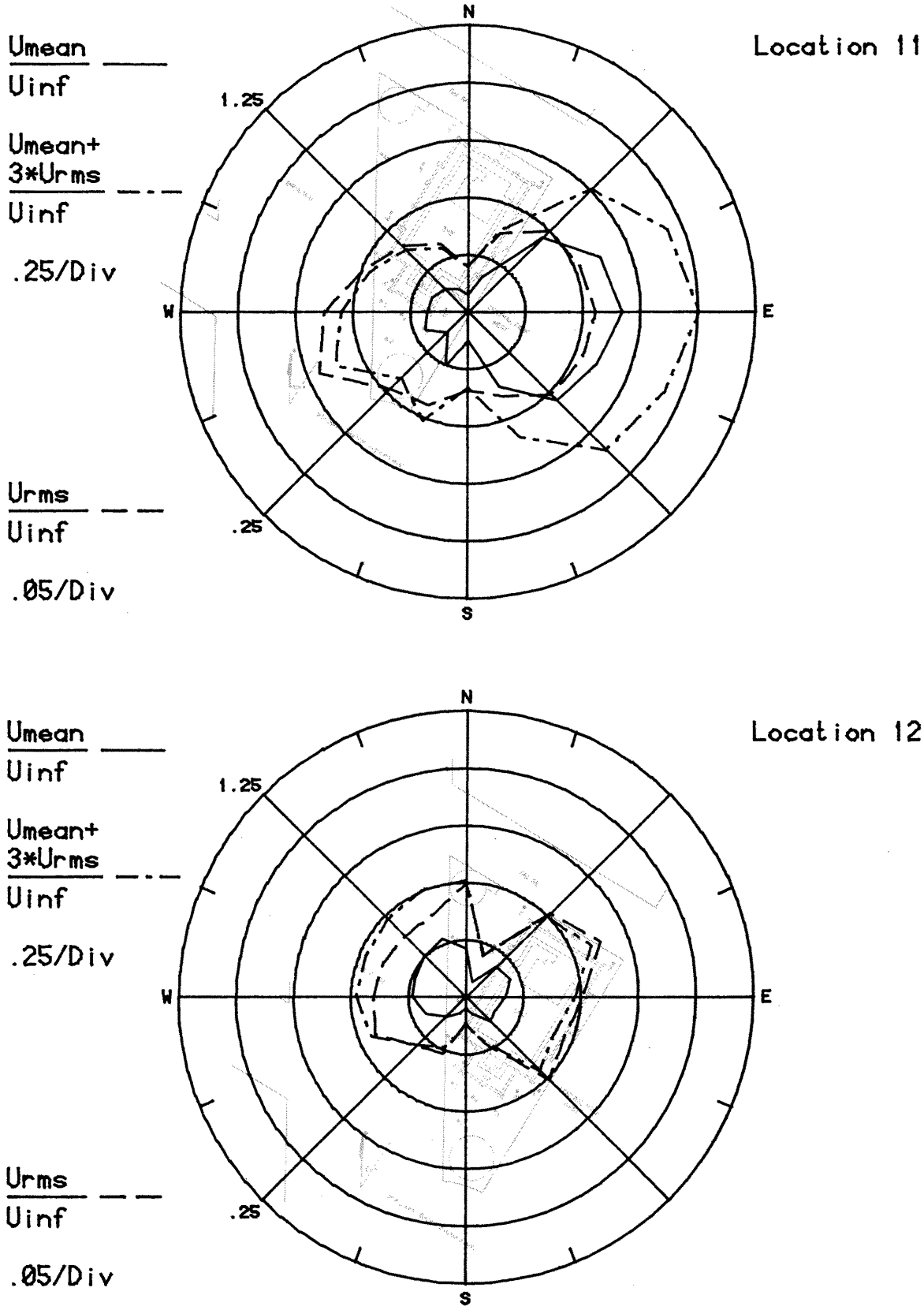


Figure 8f. Mean Velocities and Turbulence Intensities at Pedestrian Locations 11 and 12

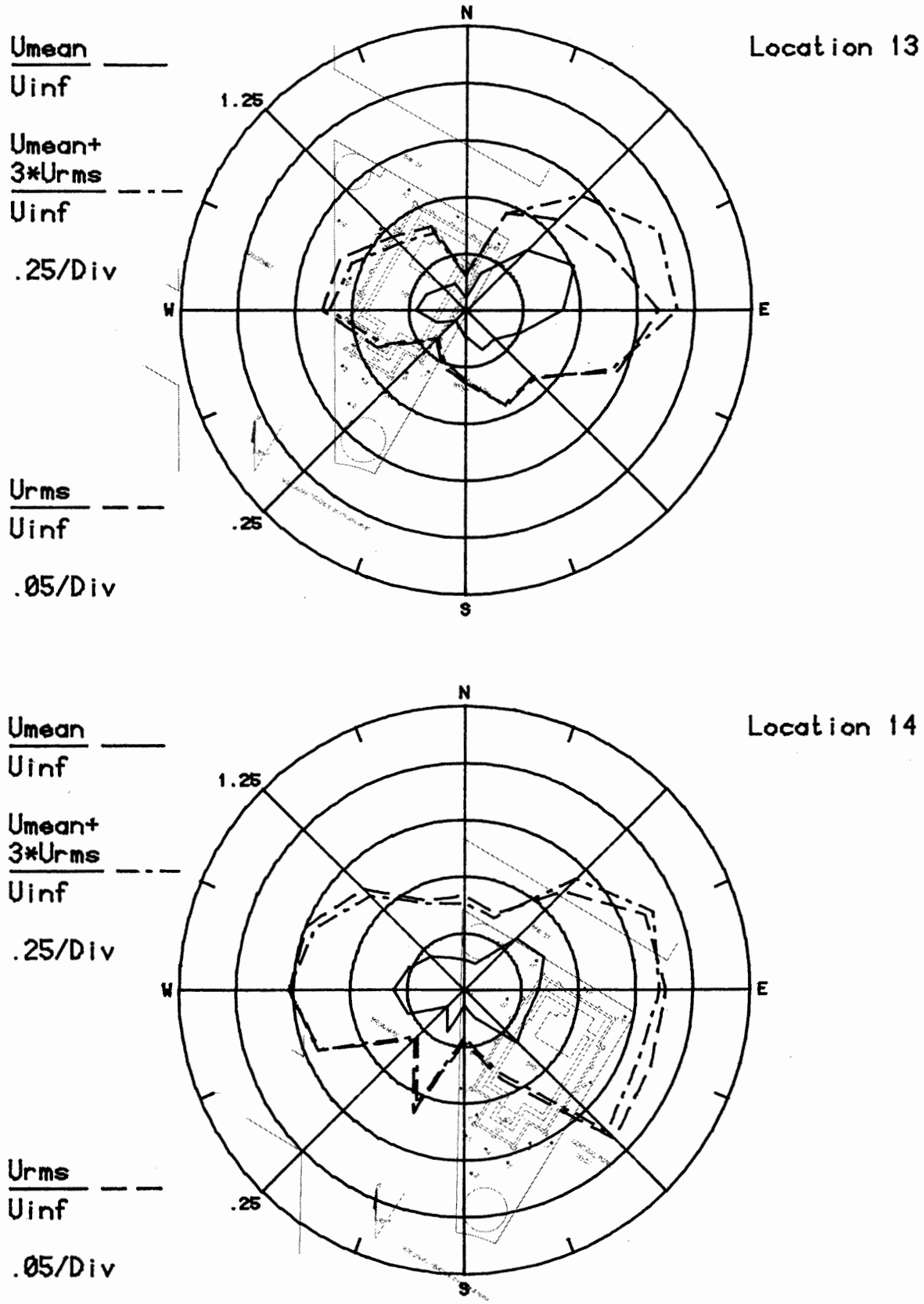


Figure 8g. Mean Velocities and Turbulence Intensities at Pedestrian Locations 13 and 14

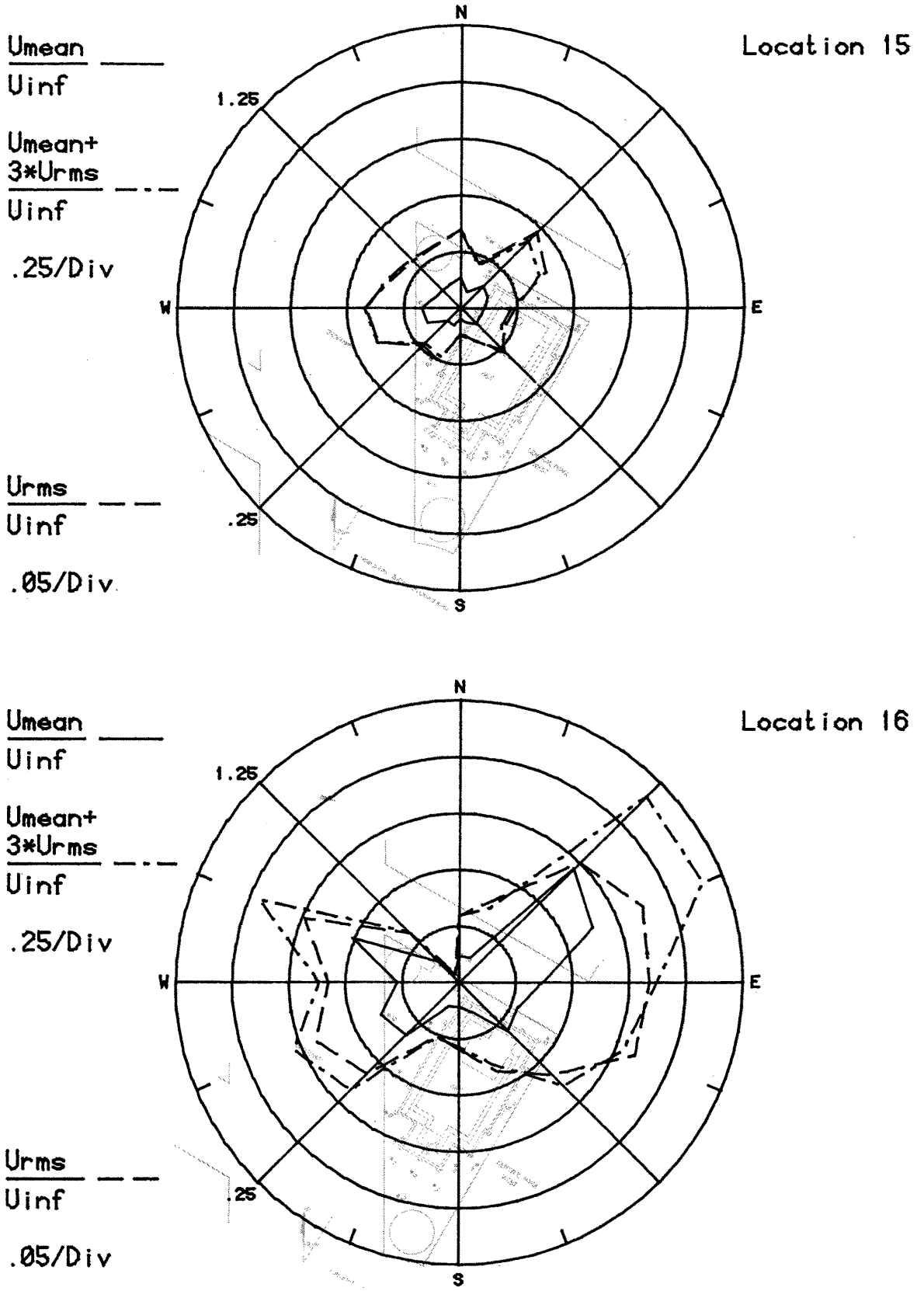


Figure 8h. Mean Velocities and Turbulence Intensities at Pedestrian Locations 15 and 16

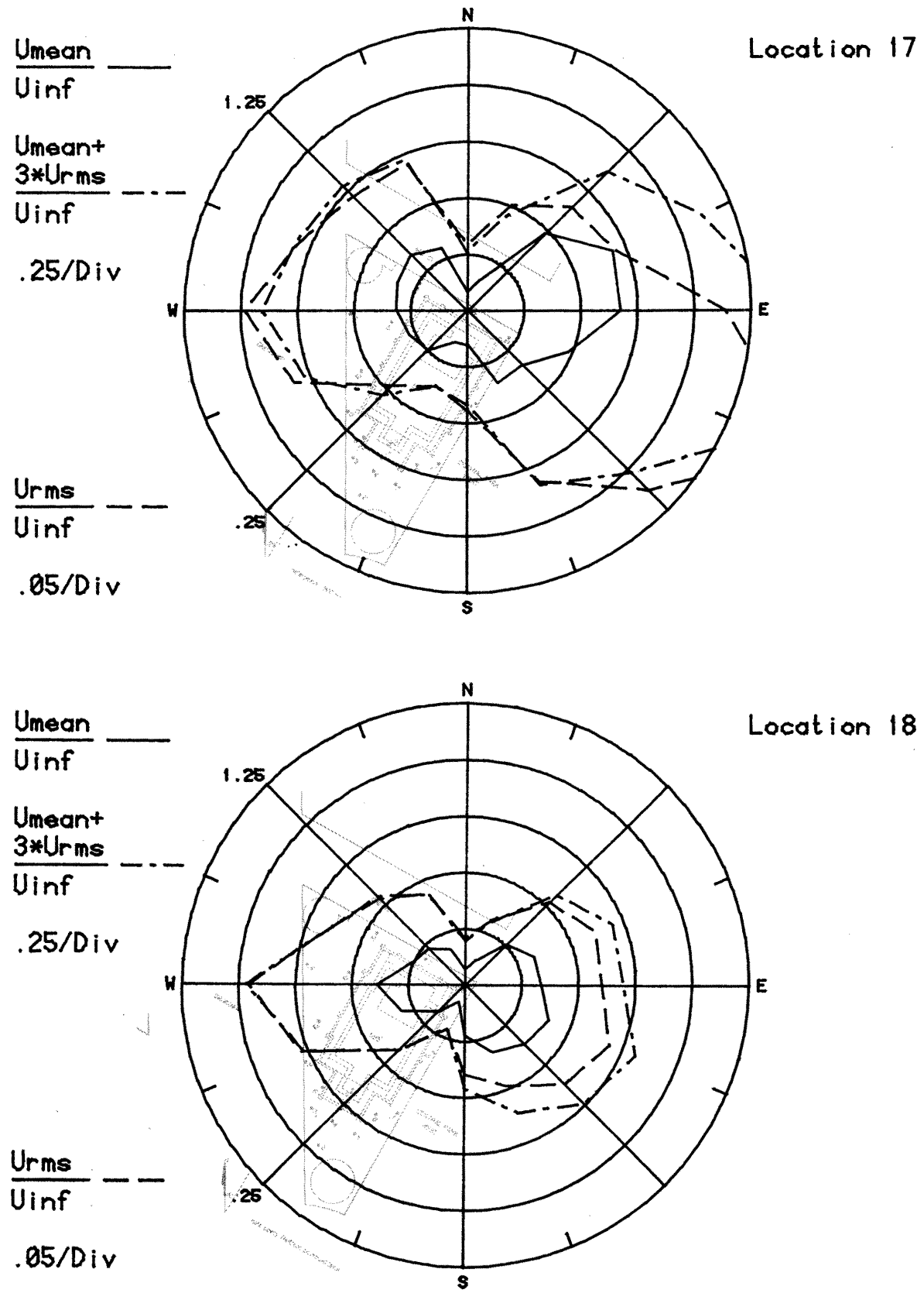


Figure 8i. Mean Velocities and Turbulence Intensities at Pedestrian Locations 17 and 18

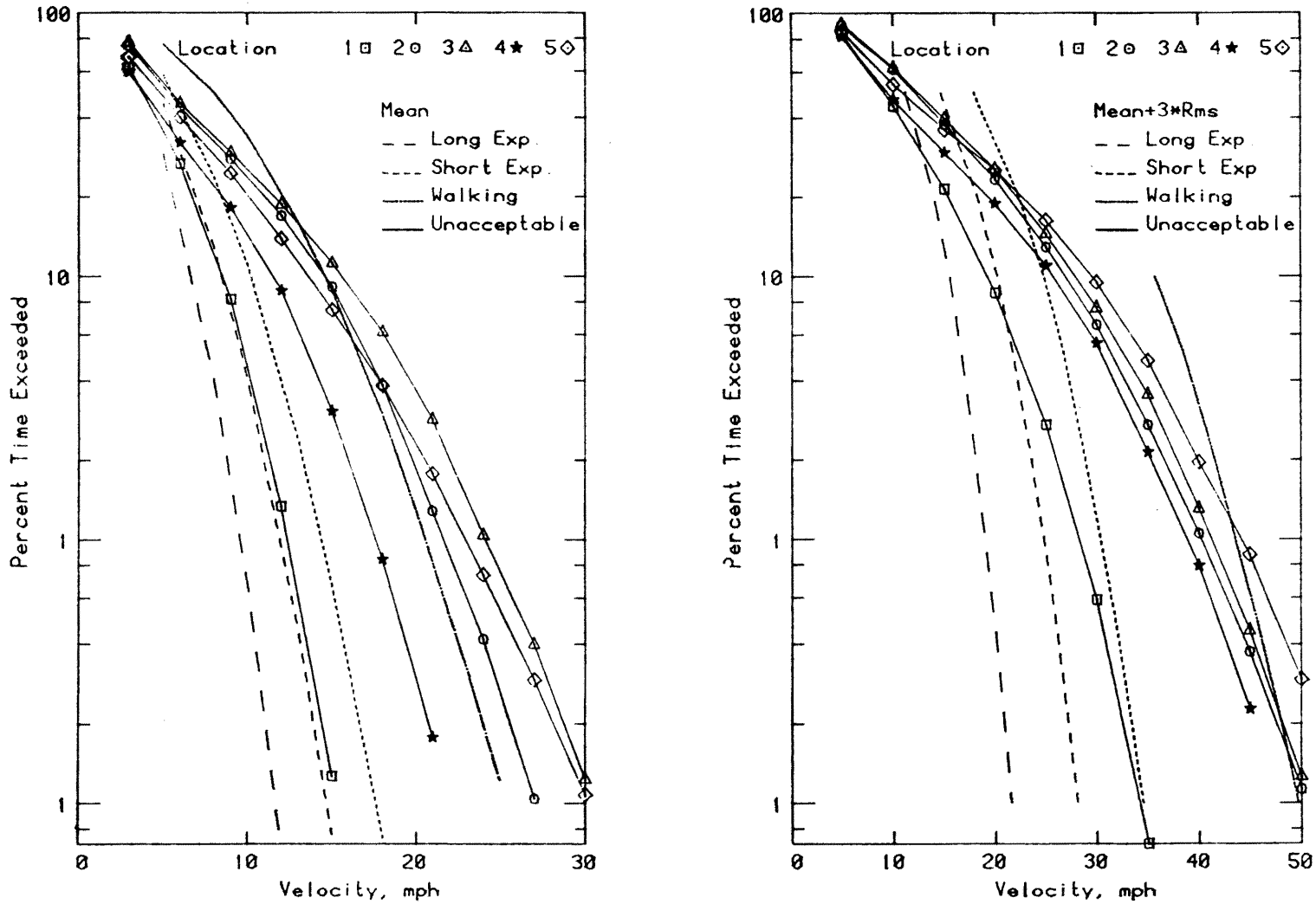


Figure 9a. Wind Velocity Probabilities for Pedestrian Locations

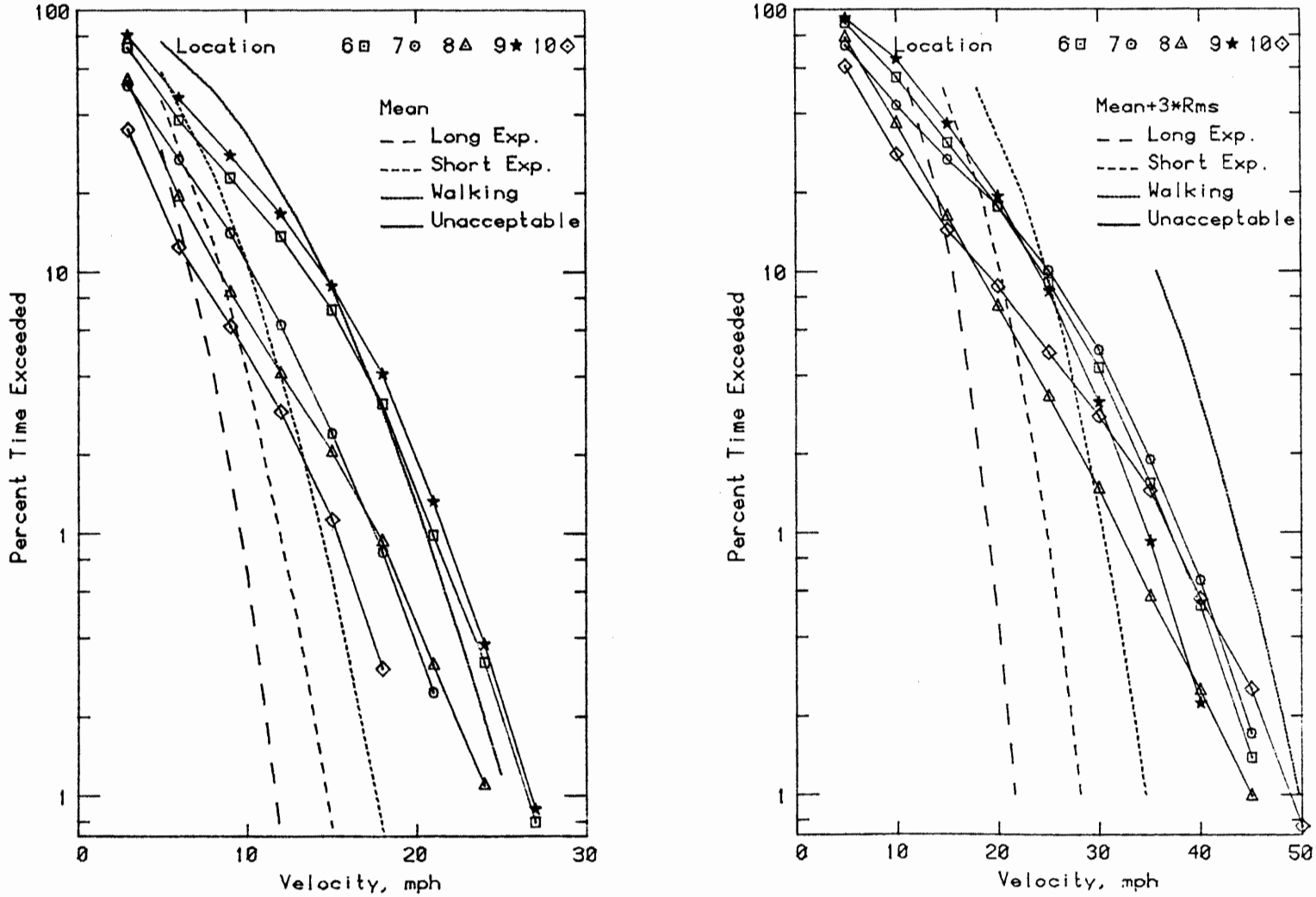


Figure 9b. Wind Velocity Probabilities for Pedestrian Locations

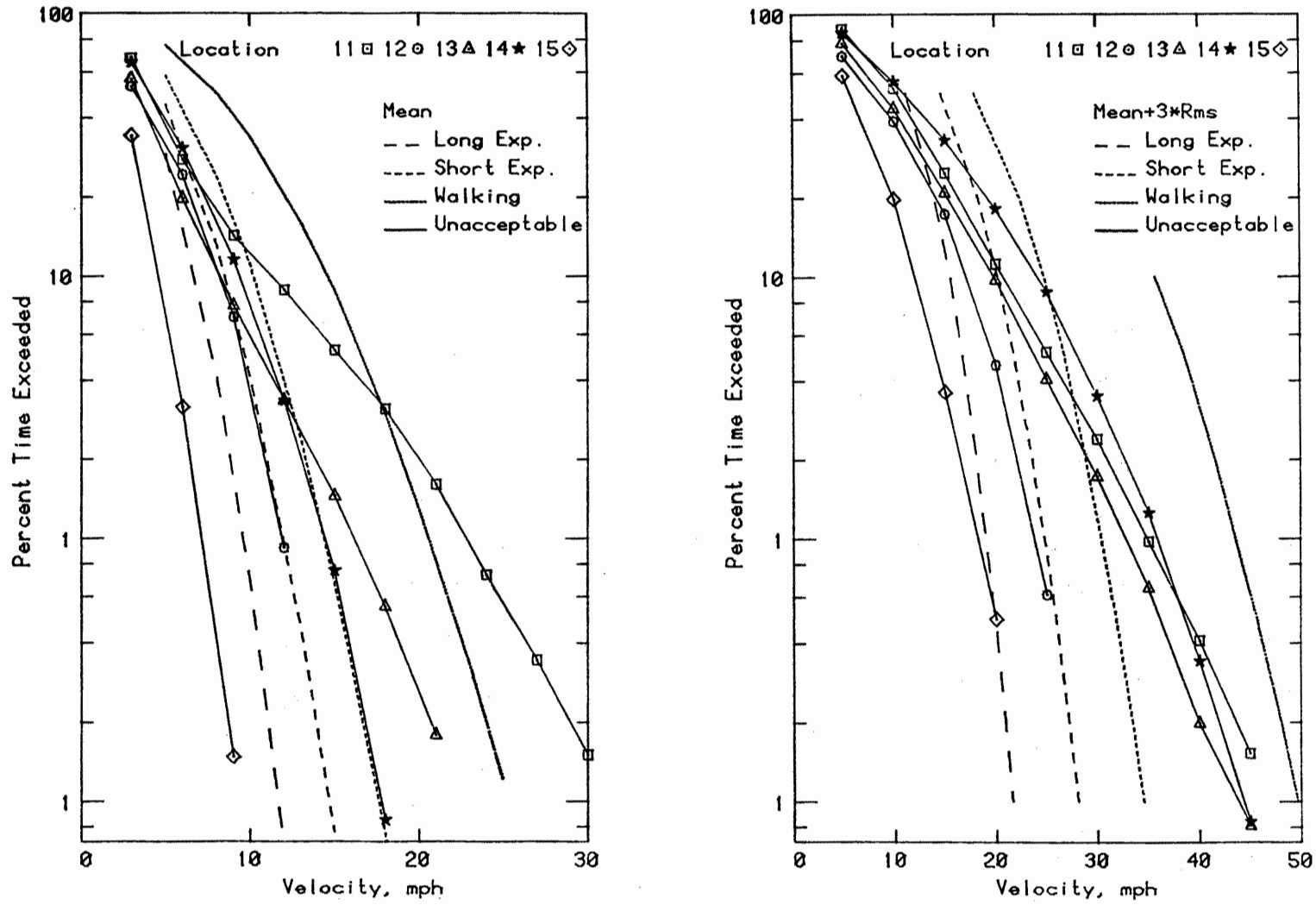


Figure 9c. Wind Velocity Probabilities for Pedestrian Locations

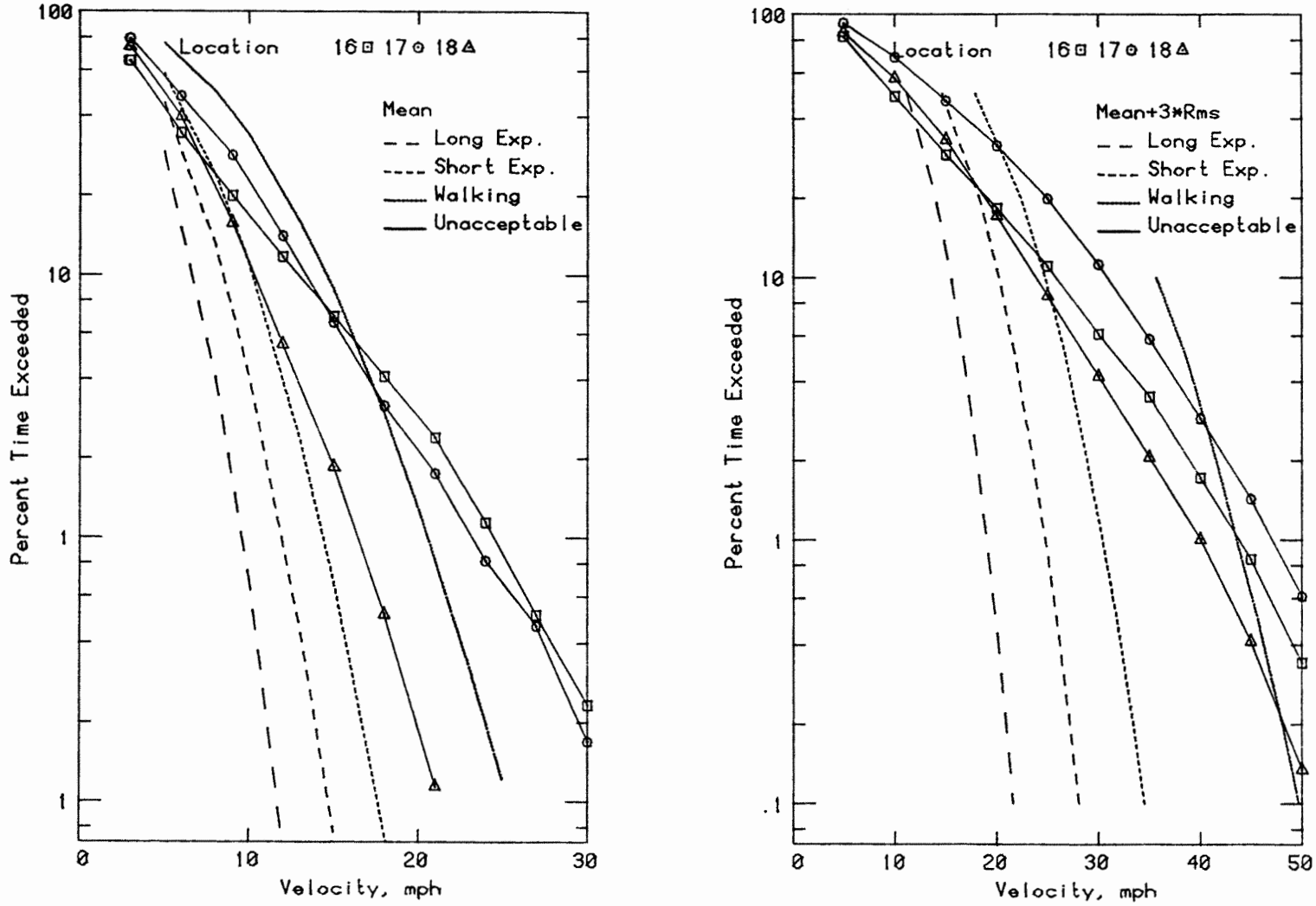


Figure 9d. Wind Velocity Probabilities for Pedestrian Locations

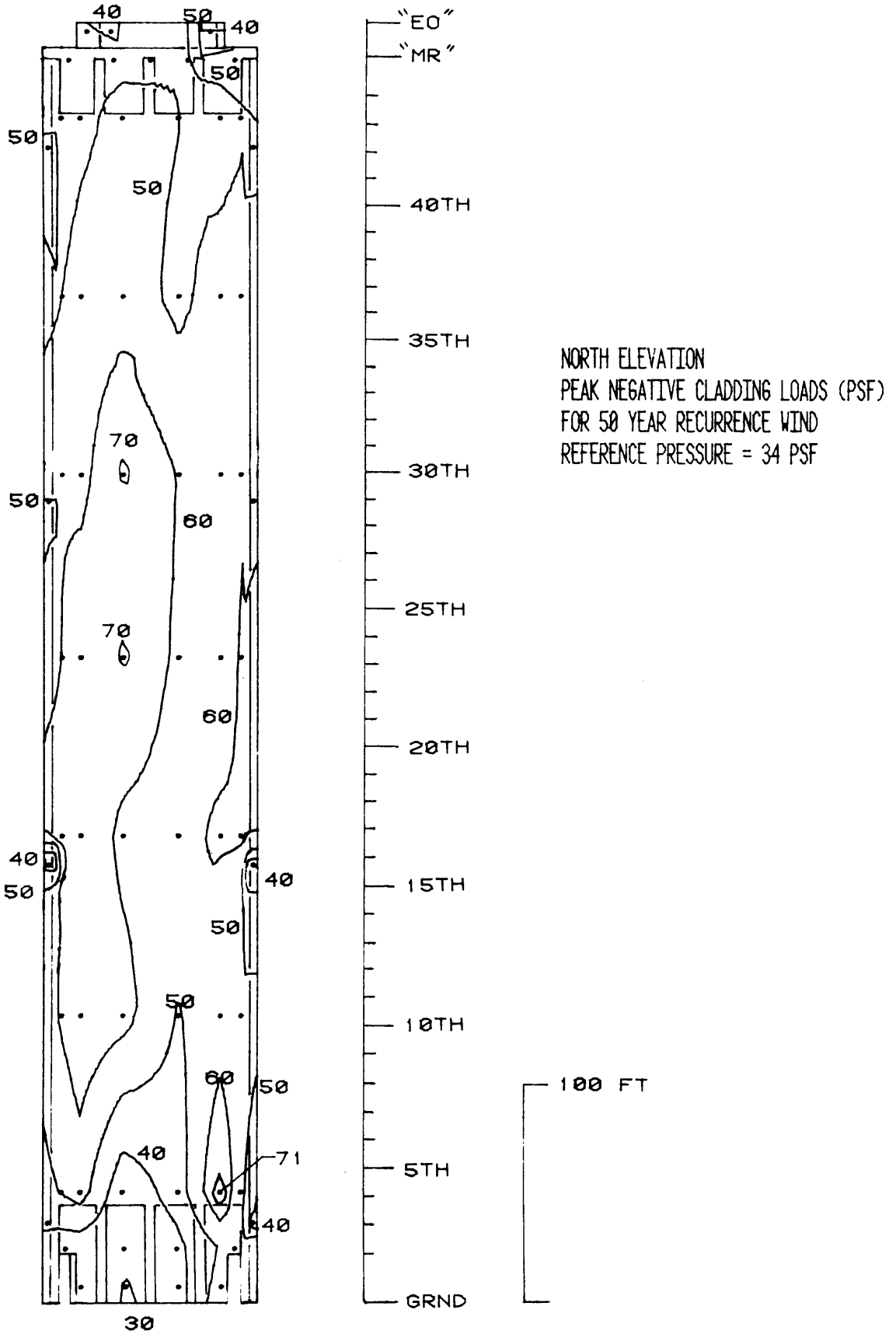
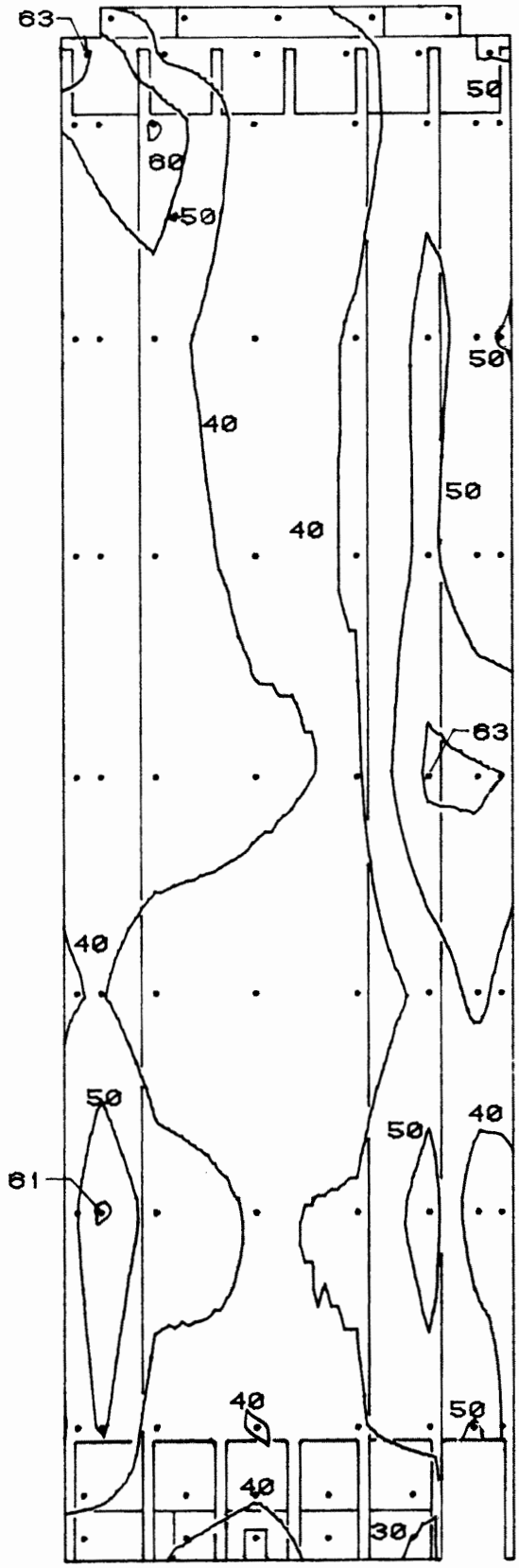
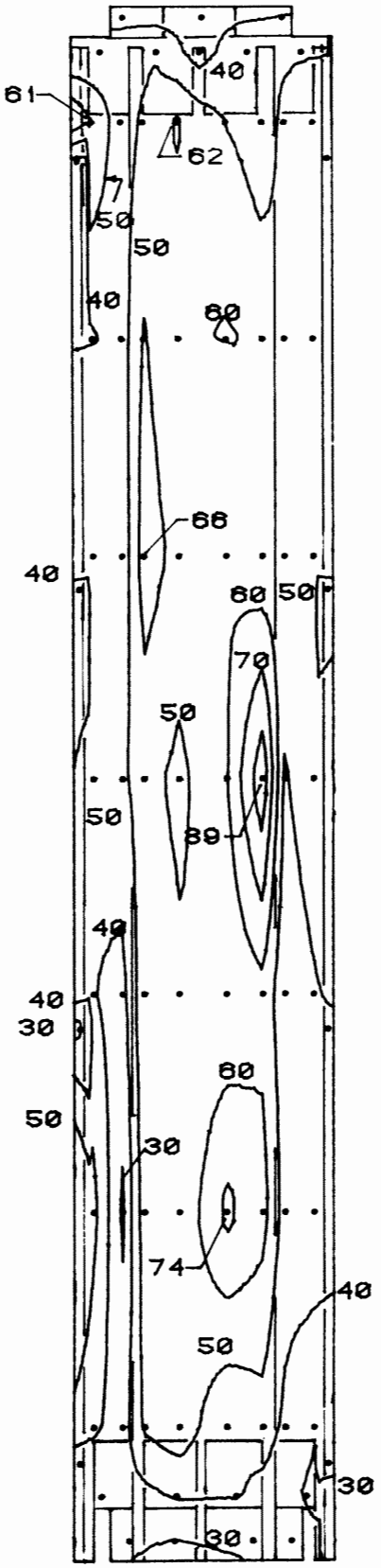


Figure 10a. Peak Pressure Contours on the Building for Cladding Loads



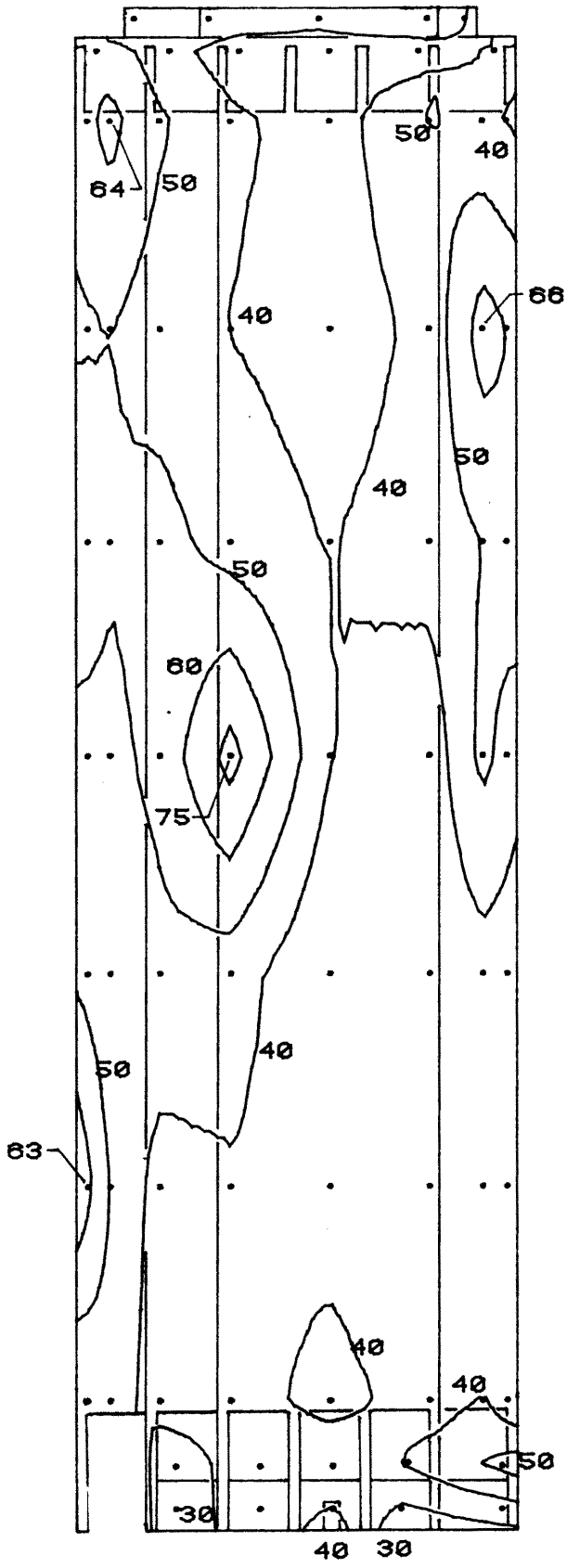
WEST ELEVATION
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 50 YEAR RECURRENCE WIND
REFERENCE PRESSURE = 34 PSF

Figure 10b. Peak Pressure Contours on the Building for Cladding Loads



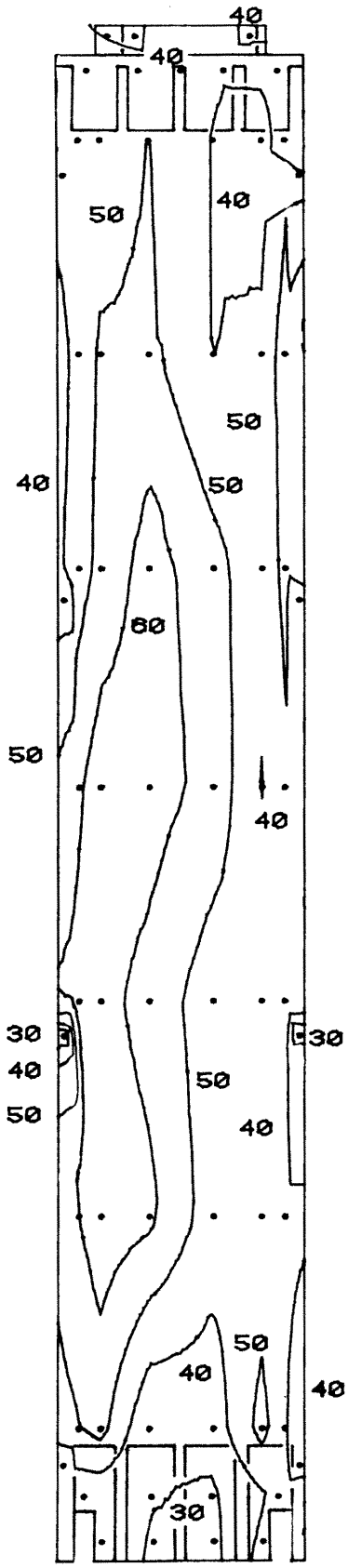
SOUTH ELEVATION
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 50 YEAR RECURRENCE WIND
REFERENCE PRESSURE = 34 PSF

Figure 10c. Peak Pressure Contours on the Building for Cladding Loads



EAST ELEVATION
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 50 YEAR RECURRENCE WIND
REFERENCE PRESSURE = 34 PSF

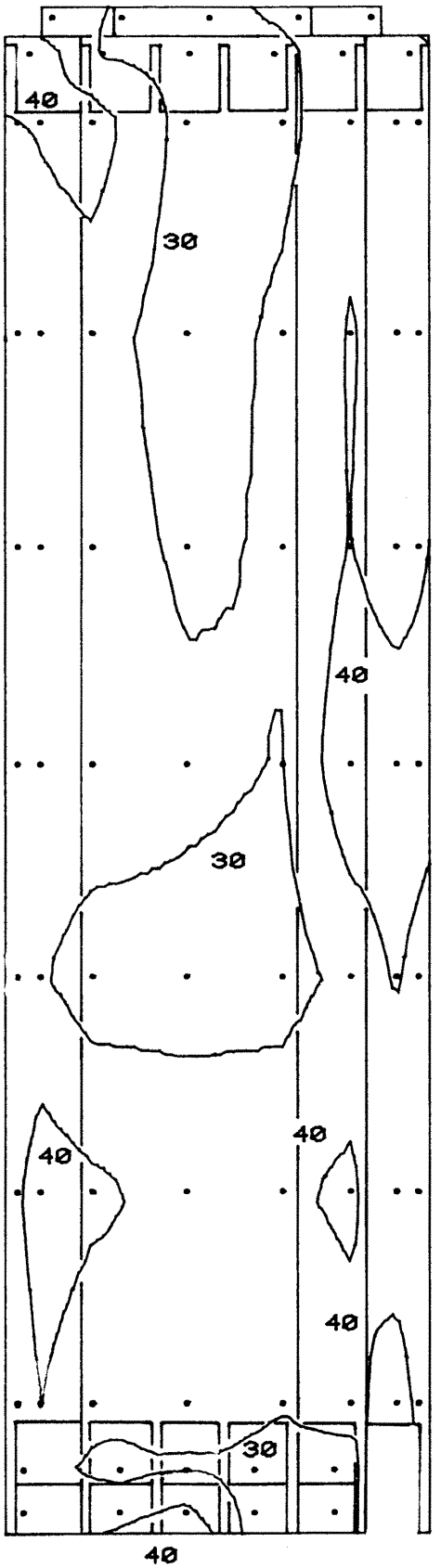
Figure 10d. Peak Pressure Contours on the Building for Cladding Loads



NORTH ELEVATION
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 50-YEAR RECURRENCE WIND
REFERENCE PRESSURE = 34 PSF

DIRECTIONAL CASE

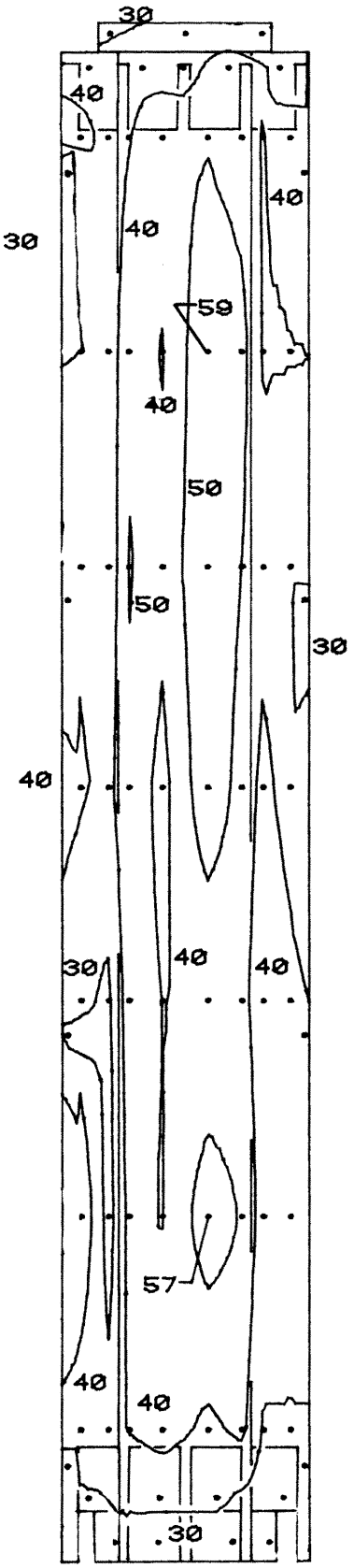
Figure 10e. Peak Pressure Contours on the Building for Cladding Loads



WEST ELEVATION
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 50-YEAR RECURRENCE WIND
REFERENCE PRESSURE = 34 PSF

DIRECTIONAL CASE

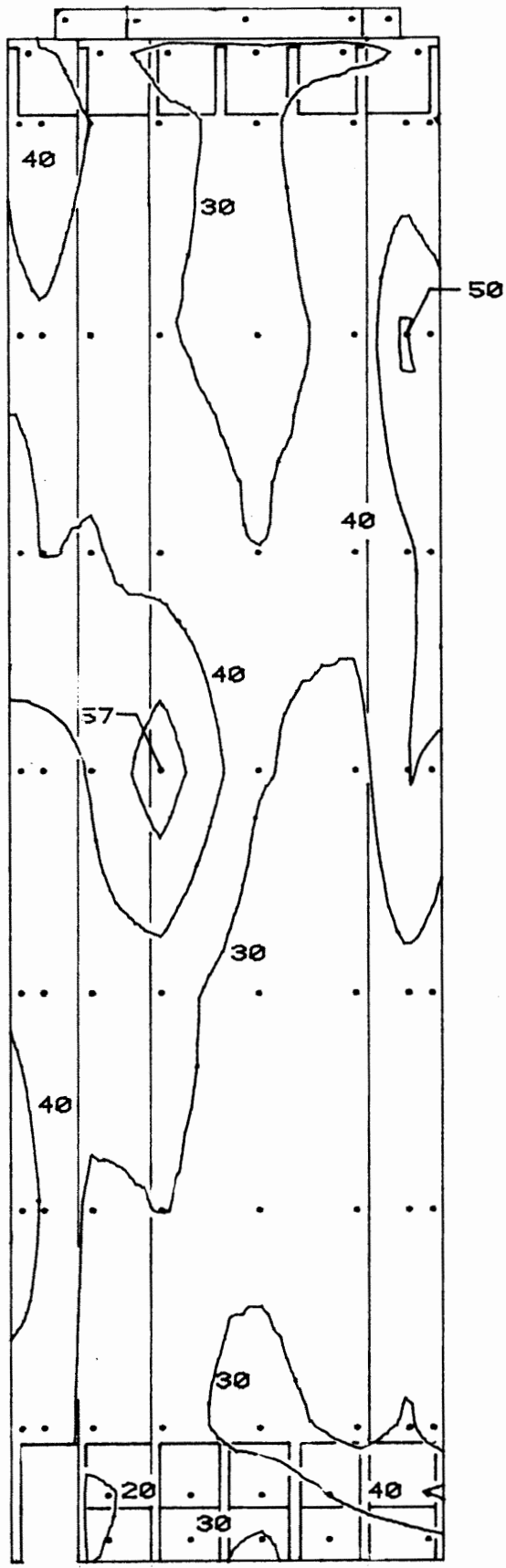
Figure 10f. Peak Pressure Contours on the Building for Cladding Loads



SOUTH ELEVATION
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 50-YEAR RECURRENCE WIND
REFERENCE PRESSURE = 34 PSF

DIRECTIONAL CASE

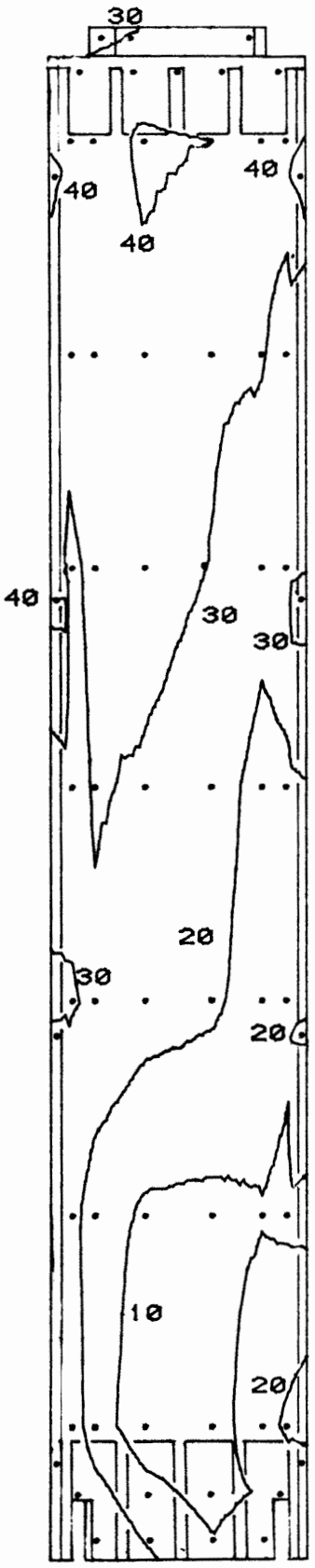
Figure 10g. Peak Pressure Contours on the Building for Cladding Loads



EAST ELEVATION
PEAK NEGATIVE CLADDING LOADS (PSF)
FOR 50-YEAR RECURRENCE WIND
REFERENCE PRESSURE = 34 PSF

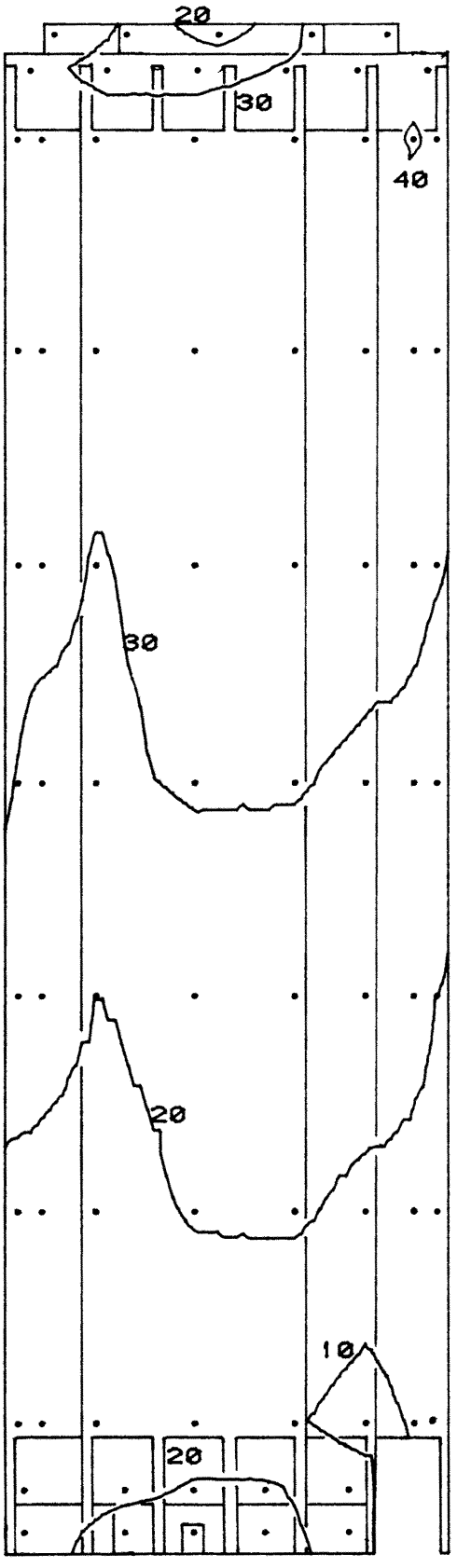
DIRECTIONAL CASE

Figure 10h. Peak Pressure Contours on the Building for Cladding Loads



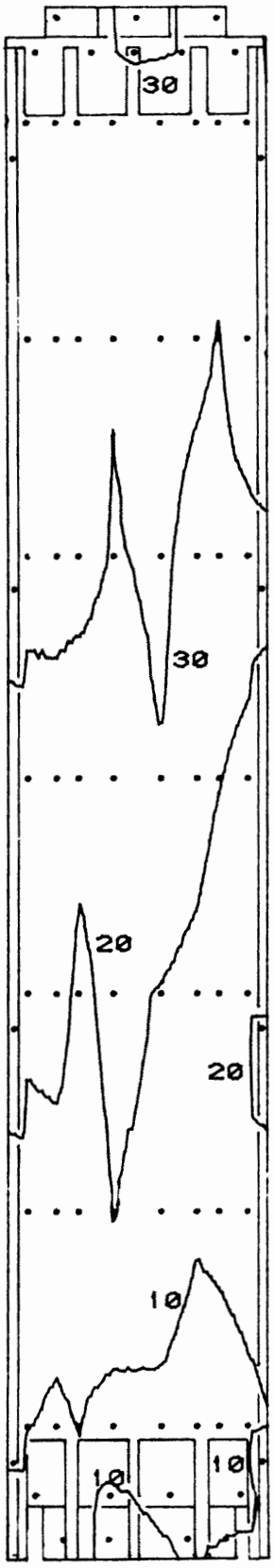
NORTH ELEVATION
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 50 YEAR RECURRENCE WIND
REFERENCE PRESSURE = 34 PSF

Figure 10i. Peak Pressure Contours on the Building for Cladding Loads



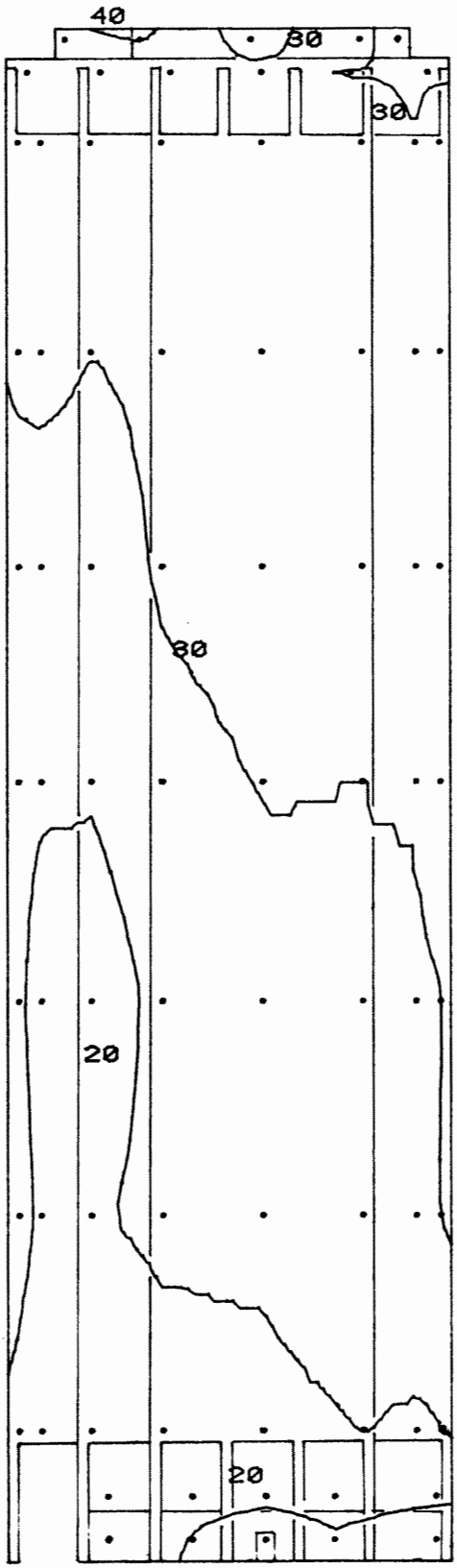
WEST ELEVATION
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 50 YEAR RECURRENCE WIND
REFERENCE PRESSURE = 34 PSF

Figure 10j. Peak Pressure Contours on the Building for Cladding Loads



SOUTH ELEVATION
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 50 YEAR RECURRENCE WIND
REFERENCE PRESSURE = 34 PSF

Figure 10k. Peak Pressure Contours on the Building for Cladding Loads



EAST ELEVATION
PEAK POSITIVE CLADDING LOADS (PSF)
FOR 50 YEAR RECURRENCE WIND
REFERENCE PRESSURE = 34 PSF

Figure 101. Peak Pressure Contours on the Building for Cladding Loads

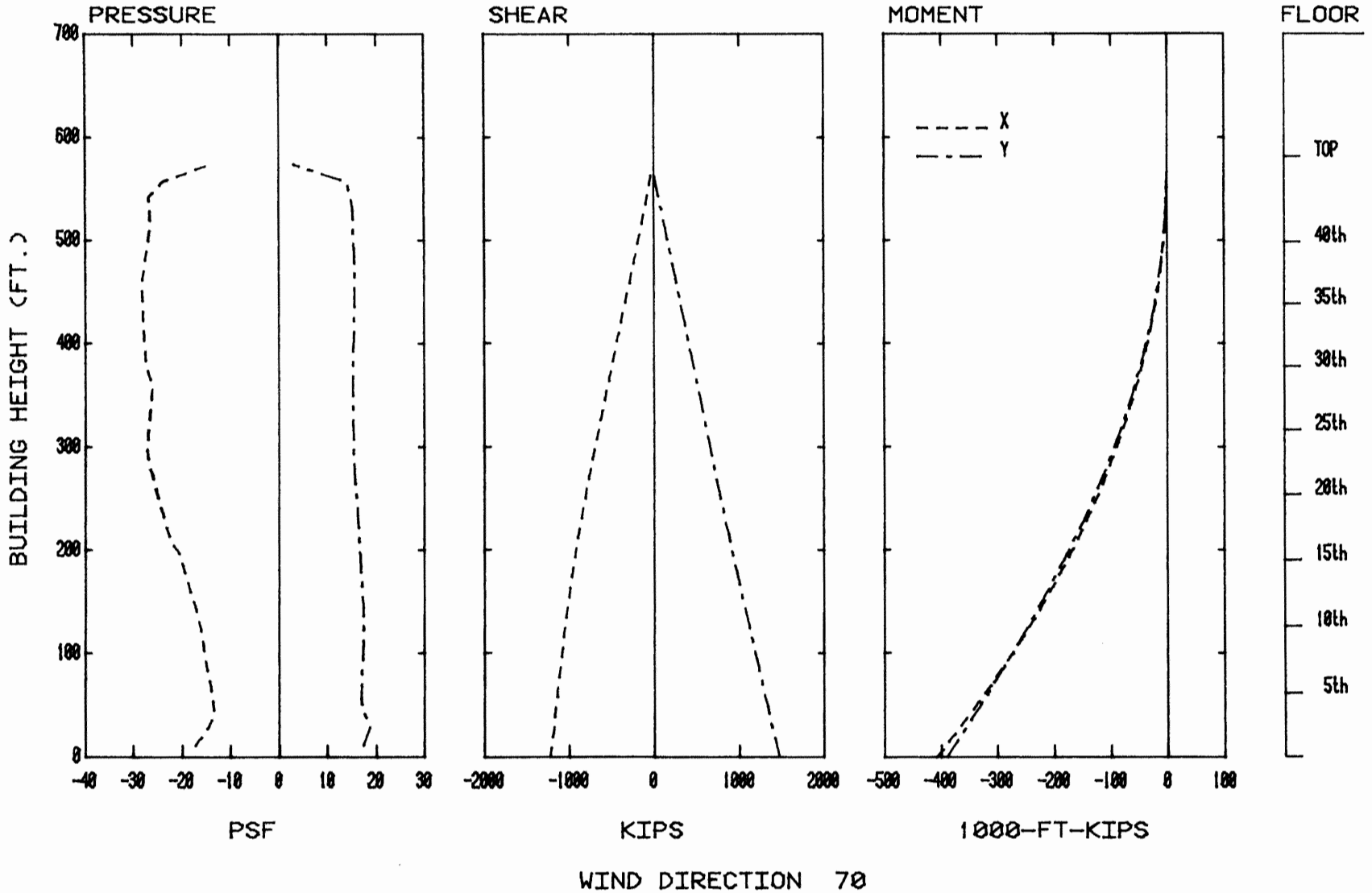


Figure 11. Load, Shear, and Moment Diagrams for Selected Wind Directions

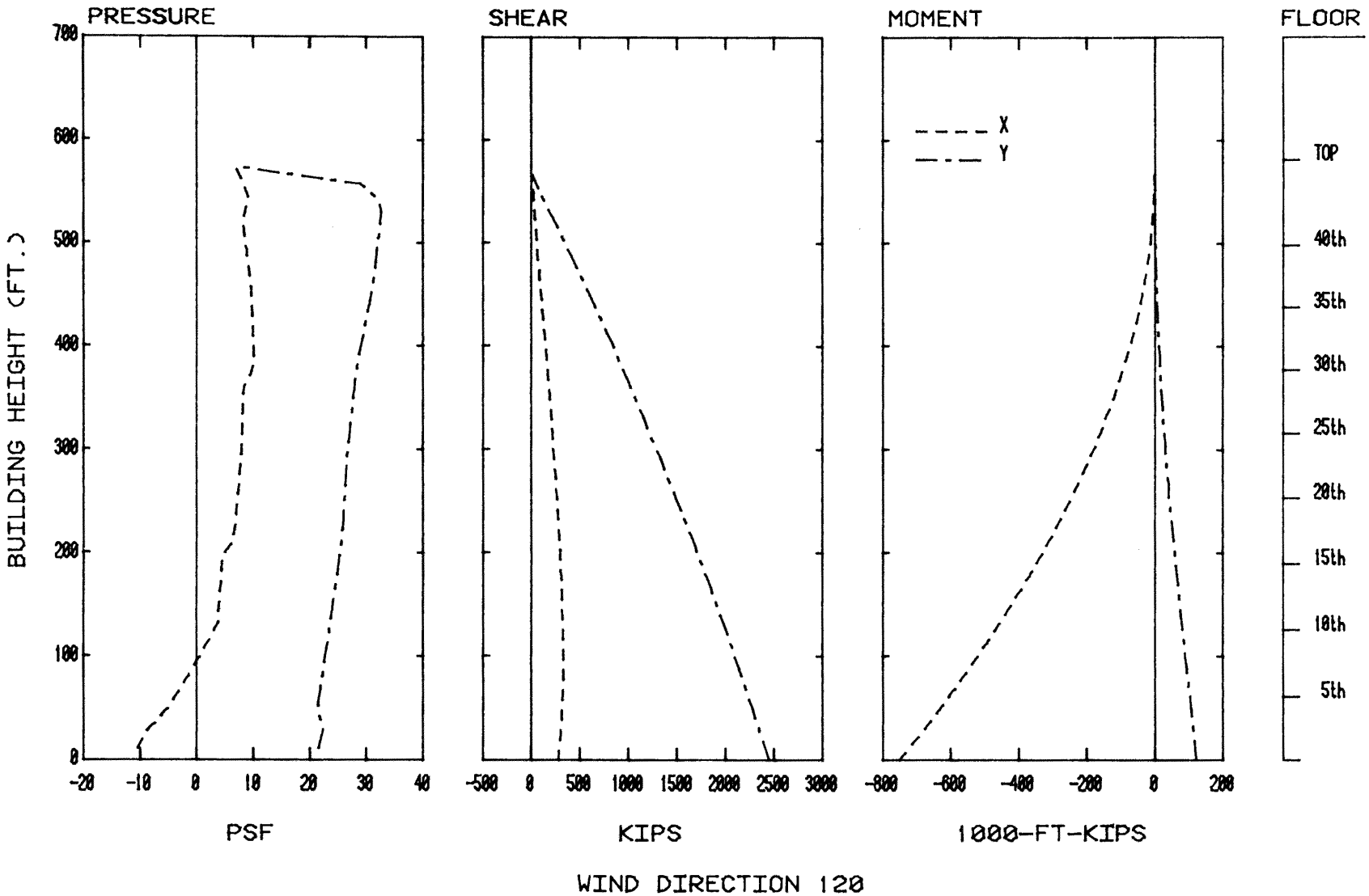


Figure 11. Load, Shear, and Moment Diagrams for Selected Wind Directions

TABLES

TABLE 1

MOTION PICTURE SCENE GUIDE

1. Introduction
2. Purposes for model testing
3. Procedures for conducting tests
4. Specific flow visualization scenes for

NO. 15 COLUMBUS CIRCLE

High Pressure Areas

Run	Pressure Tap	Azimuth, °
1	125,133	120
2	155,239	250

High Pedestrian Wind Velocities

Run	Pedestrian Location	Azimuth, °
3	16	67.5
4	5	112.5

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

NO. 15 COLUMBUS CIRCLE, NEW YORK

LOCATION 1

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	8.8	5.6	25.7
22.50	15.3	7.6	38.1
45.00	23.4	7.6	46.2
67.50	29.0	7.8	52.4
90.00	29.1	7.5	51.5
112.50	25.6	7.9	49.4
135.00	21.2	8.7	47.3
157.50	12.0	7.7	35.1
180.00	8.5	5.3	24.4
202.50	12.8	5.8	30.2
225.00	22.3	9.4	50.3
247.50	27.5	10.5	59.2
270.00	26.6	10.6	58.5
292.50	24.8	11.2	58.3
315.00	22.6	12.5	60.0
337.50	13.8	9.1	41.2

LOCATION 2

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	16.6	10.0	46.7
22.50	7.0	5.0	22.1
45.00	14.1	8.3	39.0
67.50	28.1	14.8	72.4
90.00	49.1	18.9	106.0
112.50	56.7	12.0	92.8
135.00	54.6	12.6	92.3
157.50	25.6	11.0	58.6
180.00	14.1	7.2	35.8
202.50	11.9	7.5	34.3
225.00	18.6	8.3	43.5
247.50	36.1	11.4	70.2
270.00	47.3	12.1	83.6
292.50	44.0	12.4	81.1
315.00	40.7	11.1	73.9
337.50	26.9	12.0	62.8

LOCATION 3

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	30.5	12.1	66.9
22.50	13.8	9.1	41.1
45.00	19.3	9.9	49.0
67.50	27.3	15.1	72.7
90.00	14.9	9.7	43.9
112.50	24.2	18.5	79.7
135.00	38.7	21.3	102.6
157.50	20.7	12.5	58.1
180.00	14.2	6.5	33.6
202.50	10.6	5.6	27.4
225.00	20.3	7.9	44.1
247.50	40.1	10.6	72.0
270.00	53.5	12.0	89.4
292.50	53.1	11.3	87.1
315.00	47.1	12.0	83.0
337.50	35.1	11.1	68.6

LOCATION 4

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	7.9	4.8	22.3
22.50	9.0	4.2	21.5
45.00	18.6	9.4	46.6
67.50	18.2	11.1	51.3
90.00	18.0	12.2	54.7
112.50	39.1	17.3	91.0
135.00	37.0	13.9	78.6
157.50	19.8	10.2	50.4
180.00	9.4	5.4	25.6
202.50	10.8	5.7	28.0
225.00	18.3	7.0	39.5
247.50	39.4	10.7	71.5
270.00	40.2	13.8	81.5
292.50	36.4	15.0	81.3
315.00	30.1	16.8	80.3
337.50	12.0	9.3	39.7

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

NO. 15 COLUMBUS CIRCLE, NEW YORK

LOCATION 5

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	8.3	4.4	21.4
22.50	8.5	4.5	21.9
45.00	17.0	9.5	45.4
67.50	31.1	16.1	79.3
90.00	55.1	18.7	111.2
112.50	70.4	14.1	112.7
135.00	70.4	13.4	110.7
157.50	38.6	11.2	72.3
180.00	13.8	6.9	34.4
202.50	15.0	7.0	36.0
225.00	18.1	7.6	40.9
247.50	39.1	11.9	74.8
270.00	47.8	15.2	93.3
292.50	34.4	17.3	86.2
315.00	26.3	18.0	80.4
337.50	8.3	5.2	24.0

LOCATION 6

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	21.4	9.3	49.4
22.50	13.6	8.2	38.2
45.00	15.4	8.5	40.8
67.50	26.3	14.0	68.3
90.00	16.5	10.2	47.1
112.50	12.3	7.6	35.2
135.00	15.8	9.9	45.6
157.50	11.9	6.5	30.5
180.00	12.5	6.4	31.6
202.50	16.0	8.3	41.0
225.00	22.5	7.8	45.8
247.50	38.4	10.7	70.5
270.00	47.6	11.3	81.6
292.50	45.8	11.1	79.2
315.00	39.6	11.0	72.6
337.50	29.1	9.3	56.9

LOCATION 7

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	5.4	2.9	14.1
22.50	5.1	3.0	14.2
45.00	7.3	5.1	22.6
67.50	12.0	8.2	36.5
90.00	12.1	8.3	37.0
112.50	26.1	19.4	84.4
135.00	41.0	20.2	101.6
157.50	17.2	10.4	48.5
180.00	14.0	7.4	36.2
202.50	12.0	6.8	32.4
225.00	12.3	6.2	30.9
247.50	34.5	11.7	69.6
270.00	42.3	13.7	83.5
292.50	31.9	15.4	78.0
315.00	24.2	16.5	73.7
337.50	6.5	4.1	18.9

LOCATION 8

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	7.2	3.8	18.7
22.50	9.2	4.4	22.5
45.00	20.3	7.3	42.4
67.50	33.0	11.8	68.5
90.00	46.8	15.4	93.1
112.50	57.3	13.2	96.9
135.00	54.9	12.0	90.8
157.50	32.6	9.6	61.4
180.00	9.6	4.9	24.3
202.50	15.6	7.9	39.4
225.00	10.5	6.8	30.9
247.50	20.3	10.0	50.4
270.00	20.5	10.6	52.2
292.50	14.0	8.0	37.9
315.00	11.2	6.7	31.3
337.50	8.5	5.1	23.9

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

NO. 15 COLUMBUS CIRCLE, NEW YORK

LOCATION 9

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	32.1	10.7	64.2
22.50	20.0	9.6	48.6
45.00	26.3	12.0	56.4
67.50	26.2	13.6	67.1
90.00	21.4	12.5	58.8
112.50	13.4	8.1	37.7
135.00	13.6	8.6	39.3
157.50	10.2	6.9	30.8
180.00	15.0	8.7	41.2
202.50	21.8	11.5	56.6
225.00	22.8	7.0	43.8
247.50	37.9	9.0	65.1
270.00	46.2	9.0	73.3
292.50	46.9	8.4	72.2
315.00	45.1	8.6	70.9
337.50	37.4	8.9	64.1

LOCATION 10

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	4.2	2.3	11.0
22.50	3.9	2.3	10.7
45.00	9.3	5.8	26.8
67.50	11.8	7.6	34.3
90.00	7.8	4.2	20.5
112.50	8.2	5.1	23.4
135.00	11.1	8.2	35.6
157.50	11.3	8.3	36.1
180.00	12.1	6.4	31.3
202.50	13.0	7.2	34.5
225.00	6.6	4.9	21.3
247.50	29.0	13.6	69.7
270.00	37.2	18.0	91.1
292.50	15.9	13.5	56.4
315.00	8.1	6.1	26.5
337.50	4.2	2.1	10.6

LOCATION 11

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	7.6	4.0	19.7
22.50	16.6	7.4	38.8
45.00	45.8	9.9	75.6
67.50	62.3	10.5	93.8
90.00	67.3	11.1	100.6
112.50	60.2	10.7	92.3
135.00	54.5	10.2	85.2
157.50	35.3	8.0	59.2
180.00	12.8	6.9	33.4
202.50	24.8	8.8	51.3
225.00	12.3	9.5	40.9
247.50	20.1	13.9	61.9
270.00	17.6	12.5	55.0
292.50	16.9	9.7	46.1
315.00	13.8	8.2	38.3
337.50	10.8	6.4	30.1

LOCATION 12

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	21.5	9.9	51.1
22.50	7.4	4.0	19.4
45.00	18.4	10.3	49.4
67.50	20.9	12.7	58.9
90.00	16.9	10.2	47.4
112.50	13.9	9.2	41.6
135.00	14.7	10.2	45.3
157.50	8.0	4.4	21.2
180.00	5.0	2.3	11.9
202.50	7.5	5.3	23.5
225.00	11.6	6.0	29.6
247.50	18.9	8.5	44.5
270.00	23.6	8.0	47.7
292.50	23.7	7.8	47.0
315.00	25.6	7.5	48.1
337.30	27.2	7.7	50.4

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

NO. 15 COLUMBUS CIRCLE, NEW YORK

LOCATION 13

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	5.6	3.2	15.2
22.50	18.0	9.3	45.8
45.00	37.6	11.2	71.2
67.50	50.9	13.4	91.1
90.00	42.0	16.9	92.6
112.50	25.8	14.2	68.5
135.00	17.8	8.3	42.7
157.50	18.4	9.0	45.4
180.00	11.6	6.4	30.8
202.50	8.2	5.4	24.3
225.00	6.4	3.6	17.3
247.50	13.7	8.5	39.0
270.00	22.1	12.6	60.0
292.50	18.4	11.9	54.2
315.00	14.2	9.2	41.7
337.50	12.9	8.0	36.8

LOCATION 14

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	13.2	8.3	38.1
22.50	12.6	7.2	34.3
45.00	32.0	12.2	68.7
67.50	37.9	17.1	89.2
90.00	32.5	17.6	85.5
112.50	29.3	17.6	82.1
135.00	32.5	18.5	87.8
157.50	17.5	8.5	39.1
180.00	7.1	4.6	20.9
202.50	19.4	11.7	54.4
225.00	10.7	6.1	28.7
247.50	26.2	13.3	66.3
270.00	31.2	15.3	77.1
292.50	26.7	14.9	70.7
315.00	20.7	12.5	58.2
337.50	15.5	8.5	41.0

LOCATION 15

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	13.4	6.9	34.2
22.50	7.6	4.3	20.4
45.00	13.7	9.5	42.3
67.50	13.1	8.1	37.5
90.00	10.6	4.5	24.2
112.50	9.3	3.9	21.0
135.00	9.8	5.6	26.5
157.50	6.7	3.0	15.7
180.00	5.2	2.3	12.1
202.50	8.1	5.0	23.1
225.00	7.9	4.7	22.0
247.50	16.0	7.8	39.5
270.00	17.4	8.4	42.6
292.50	12.4	6.9	33.0
315.00	11.1	6.2	29.6
337.50	11.7	6.0	29.7

LOCATION 16

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	11.8	5.9	29.4
22.50	12.0	7.8	35.5
67.50	71.6	15.0	116.4
90.00	63.6	17.5	116.2
112.50	36.6	16.8	87.1
135.00	28.0	16.8	78.3
157.50	29.9	11.6	64.7
180.00	14.0	8.5	39.4
202.50	10.7	5.9	28.4
225.00	10.9	5.5	26.4
247.50	32.9	11.4	67.3
270.00	37.9	13.5	78.4
292.50	27.2	11.5	61.6
315.00	51.2	14.8	95.5
337.50	13.1	6.1	31.5

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

NO. 15 COLUMBUS CIRCLE, NEW YORK

LOCATION 17

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	8.7	5.9	26.3
22.50	15.0	10.1	45.4
45.00	48.2	12.9	87.0
67.50	69.1	14.1	111.3
90.00	67.5	22.7	135.7
112.50	47.7	29.2	135.4
135.00	34.2	22.5	101.7
157.50	34.6	16.4	83.7
180.00	15.4	8.8	41.9
202.50	14.9	7.2	36.6
225.00	24.6	9.4	52.8
247.50	27.7	16.6	77.5
270.00	31.6	19.7	90.6
292.50	32.3	16.0	81.3
315.00	35.1	14.3	78.1
337.50	30.2	14.1	72.4

LOCATION 18

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	7.1	4.2	19.6
22.50	11.8	6.2	30.4
45.00	25.4	10.4	56.6
67.50	32.9	12.4	70.2
90.00	33.7	12.0	69.8
112.50	40.0	13.8	81.4
135.00	36.7	12.4	74.0
157.50	32.1	9.7	61.1
180.00	22.5	7.9	46.2
202.50	8.0	4.2	20.6
225.00	16.3	8.1	40.7
247.50	30.3	15.6	77.0
270.00	39.3	19.1	96.6
292.50	25.8	13.0	64.7
315.00	22.8	10.7	55.0
337.50	17.1	8.7	43.2

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES
NO. 15 COLUMBUS CIRCLE, NEW YORK

* * GREATEST VALUES * *

UMEAN/UINF (PERCENT)

LOC	AZ	MEAN	RMS	M+3RMS
16	67.5	71.5	15.0	116.4
5	112.5	70.4	14.1	112.7
5	135.0	70.4	13.4	110.7
17	67.5	69.1	14.1	111.3
17	90.0	67.5	22.7	135.7
11	90.0	67.3	11.1	100.6
16	90.0	63.6	17.5	116.2
11	67.5	62.3	10.5	93.8
11	112.5	60.2	10.7	92.3
8	112.5	57.3	13.2	96.9

URMS/UINF (PERCENT)

LOC	AZ	MEAN	RMS	M+3RMS
17	112.5	47.7	29.2	135.4
17	90.0	67.5	22.7	135.7
17	135.0	34.2	22.5	101.7
3	135.0	38.7	21.3	102.6
7	135.0	41.0	20.2	101.6
17	270.0	31.6	19.7	90.6
7	112.5	26.1	19.4	84.4
18	270.0	39.3	19.1	96.6
2	90.0	49.1	18.9	106.0
5	90.0	55.1	18.7	111.2

UMEAN+3*RMS/UINF (PERCENT)

LOC	AZ	MEAN	RMS	M+3RMS
17	90.0	67.5	22.7	135.7
17	112.5	47.7	29.2	135.4
16	67.5	71.5	15.0	116.4
16	90.0	63.6	17.5	116.2
5	112.5	70.4	14.1	112.7
17	67.5	69.1	14.1	111.3
5	90.0	55.1	18.7	111.2
5	135.0	70.4	13.4	110.7
2	90.0	49.1	18.9	106.0
3	135.0	38.7	21.3	102.6

TABLE 3

PERCENTAGE FREQUENCY OF WIND DIRECTION AND SPEED

NEW YORK,NEW YORK JOHN F. KENNEDY INTERNATIONAL AP (65-74)

SEASON : ANNUAL NO. OF OBS.= 29216 HT. OF MEAS.= 20. FT.

VELOCITY LEVELS IN MPH

DIRECTION	0- 3	4- 7	8-12	13-18	19-24	25-31	32-38	39-46	47 +	TOTAL
N	.10	1.00	2.90	3.00	.60	.20	.01	0.00	0.00	7.81
NNE	.10	.90	2.10	1.40	.30	.10	.01	.01	0.00	4.92
NE	.20	1.30	1.90	1.30	.30	.10	.01	0.00	0.00	5.11
ENE	.30	1.50	1.60	.90	.30	.02	.01	0.00	0.00	4.72
E	.40	1.50	1.60	1.20	.30	.10	.01	.01	0.00	5.12
ESE	.20	.80	1.00	.50	.10	.02	.01	0.00	0.00	2.73
SE	.10	.70	1.10	.70	.10	.02	0.00	0.00	0.00	2.72
SSE	.20	.70	1.30	.80	.10	.02	.01	.01	0.00	3.14
S	.30	1.80	5.70	5.40	1.20	.20	.01	0.00	0.00	14.61
SSW	.20	1.20	2.80	1.80	.30	.10	.01	0.00	0.00	6.41
SW	.10	1.40	2.90	1.20	.20	.02	0.00	0.00	0.00	5.82
WSW	.20	1.50	3.60	2.00	.30	.10	.01	.01	0.00	7.72
W	.10	1.10	2.60	3.10	1.40	.40	.10	.01	.01	8.82
WNW	.10	.40	1.20	2.20	1.10	.30	.10	.01	0.00	5.41
NW	.10	.50	2.00	3.90	1.90	.50	.10	.01	0.00	9.01
NNW	.10	.50	1.80	2.50	.70	.10	.01	.01	0.00	5.72
CALM	.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	.40
TOT	3.10	16.80	36.10	32.00	9.20	2.30	.41	.08	.01	100.00

TABLE 4

SUMMARY OF WIND EFFECTS ON PEOPLE

	Beaufort number	Speed (mph)	Effects
Calm, light air	0, 1	0- 3	Calm, no noticeable wind
Light breeze	2	4- 7	Wind felt on face
Gentle breeze	3	8-12	Wind extends light flag Hair is disturbed Clothing flaps
Moderate breeze	4	13-18	Raises dust, dry soil and loose paper Hair disarranged
Fresh breeze	5	19-24	Force of wind felt on body Drifting snow becomes airborne Limit of agreeable wind on land
Strong breeze	6	25-31	Umbrellas used with difficulty Hair blown straight Difficult to walk steadily Wind noise on ears unpleasant Windborne snow above head height (blizzard)
Near gale	7	32-38	Inconvenience felt when walking
Gale	8	39-46	Generally impedes progress Great difficulty with balance in gusts
Strong gale	9	47-54	People blown over by gusts

Note: Table from Reference 4, p. 40.

TABLE 5

CALCULATION OF REFERENCE PRESSURE

1. Basic wind speed from ANSI A58.1 (Ref. 6):

   50-yr fastest mile at 30 ft = 80 mph

   Mean hourly wind speed, 30 ft = $\frac{80}{1.27}$ = 63.0 mph

   Mean hourly gradient wind speed = $63(\frac{1000}{30})^{.17}$ = 114.3 mph

   Reference wind speed U_∞ = gradient wind speed

   Reference pressure = $0.5\ \rho U_\infty^2 = 0.00256\ (114.3)^2$ = 33.5 psf

   Use 34 psf

2. Loads for 100-yr recurrence wind:

   100-yr fastest mile at 30 ft = 90 mph (Ref. 6)

   Multiply 50-yr loads by $(\frac{90}{80})^2$ = 1.27

3. Gust load factors to convert hourly mean integrated load to mean load for various gust durations (see Section 4.4):

Gust Duration, sec	Gust Load Factor
10-15	$(1.4)^2$ = 1.96
30	$(1.32)^2$ = 1.74*
45	$(1.26)^2$ = 1.59

*Used for calculations of TABLE 7.

TABLE 5 (Continued)

WIND DIRECTIONALITY - NEW YORK CITY

Largest Wind at Mile Post 2550 or 2600*, 70 mph minimum

WIND DIRECTION	WIND SPEED (WS)	SPEED RATIO WS/80	LOAD RATIO $(WS/80)^2$
N (0°)	70	0.88	0.77
NNE	70	0.88	0.77
NE	70	0.88	0.77
ENE	70	0.88	0.77
E (90°)	71	0.89	0.79
ESE	77	0.96	0.93
SE	79	0.99	0.98
SSE	71	0.89	0.79
S (180°)	70	0.88	0.77
SSW	70	0.88	0.77
SW	70	0.88	0.77
WSW	70	0.88	0.77
W (270°)	70	0.88	0.77
WNW	70	0.88	0.77
NW	70	0.88	0.77
NNW	70	0.88	0.77

* Data on directionality based on

Batts, M. E., M. R. Cordes, L. R. Russel, J. R. Shaver, E. Simiu, "Hurricane Wind Speeds in the United States," NBS Building Science Series 124, National Bureau of Standards, 1980.

TABLE 6H. PEAK LOADS FOR CONFIGURATION A : NO. 15 COLUMBUS CIRCLE, NEW YORK
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 34.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF ----	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF ----	POSITIVE PEAK	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF ----	POSITIVE PEAK
101	110	-1.25	-42.4	28.2	149	280	-1.62	-54.9	9.6	231	240	-1.36	-46.2	31.7
102	120	-1.12	-38.2	30.1	150	280	-1.63	-55.2	8.3	232	240	-1.17	-39.9	34.4
103	140	-1.20	-40.6	38.0	151	130	-1.49	-50.7	25.7	233	30	-1.32	-44.7	36.3
104	110	-1.45	-49.4	31.9	152	130	-1.62	-55.0	14.8	234	20	-1.48	-50.3	37.2
105	130	-1.38	-47.1	37.4	153	110	-.97	-33.0	3.8	235	20	-1.64	-55.8	35.5
106	110	-1.43	-48.6	33.8	154	270	-1.31	-44.5	5.6	236	240	-1.37	-46.6	23.1
107	320	-1.46	-49.8	34.3	155	250	-2.07	-70.2	16.4	237	250	-1.39	-47.3	22.2
108	300	-1.64	-55.6	32.2	156	250	-1.59	-54.2	21.9	238	250	-1.57	-53.2	21.4
109	110	-1.30	-44.0	32.1	157	270	-1.23	-42.0	26.4	239	250	-2.19	-74.3	26.5
110	110	-1.38	-46.9	36.7	158	110	-1.14	-38.7	14.4	240	250	-1.19	-40.6	30.8
111	110	-1.60	-54.4	41.7	159	130	-1.01	-34.2	27.2	241	250	-.98	-33.3	30.3
112	310	-1.49	-50.6	40.4	160	130	-.92	-31.4	13.4	242	40	-1.56	-53.0	30.8
113	320	-1.33	-45.2	34.6	161	260	-1.09	-37.2	7.0	243	30	-1.38	-46.9	32.5
114	320	-1.42	-48.2	36.1	162	250	-1.61	-54.8	12.4	244	290	-1.37	-46.4	22.5
115	30	-1.69	-57.5	40.1	163	130	-1.09	-37.1	27.9	245	240	-1.25	-42.4	14.9
116	30	-1.38	-46.9	40.3	164	130	-.87	-29.7	19.0	246	250	-1.39	-47.3	13.9
117	300	-1.48	-50.2	33.3	165	270	-1.07	-36.3	10.7	247	270	-1.32	-44.9	23.2
118	110	-1.64	-55.7	36.8	166	280	-1.63	-55.4	17.1	248	260	-.90	-30.8	26.7
119	120	-1.64	-55.9	38.2	201	240	-1.24	-42.2	36.4	249	280	-.98	-33.2	29.0
120	310	-1.40	-47.6	31.2	202	240	-1.39	-47.4	40.8	250	40	-1.06	-36.0	29.3
121	310	-1.61	-54.8	31.2	203	240	-1.24	-42.1	26.8	251	290	-1.02	-34.6	30.1
122	130	-1.66	-56.3	25.2	204	240	-1.41	-47.8	35.9	252	50	-1.85	-62.9	25.9
123	270	-1.75	-59.4	29.2	205	40	-1.19	-40.6	21.3	253	50	-1.45	-49.4	17.9
124	110	-1.69	-57.4	31.9	206	240	-1.70	-57.7	32.4	254	260	-1.07	-36.5	19.3
125	120	-2.05	-69.7	33.5	207	240	-1.27	-43.3	30.7	255	300	-1.15	-39.1	22.4
126	320	-1.76	-59.9	30.0	208	240	-1.01	-34.4	33.2	256	300	-1.05	-35.7	22.7
127	320	-1.58	-53.8	24.3	209	240	-1.08	-36.7	32.0	257	270	-.92	-31.4	26.9
128	320	-1.70	-57.7	26.9	210	30	-1.04	-35.2	29.8	258	0	-.92	-31.3	26.6
129	30	-1.41	-48.0	42.9	211	40	-1.21	-41.2	29.2	259	310	-.94	-31.9	30.3
130	30	-1.59	-53.9	33.6	212	240	-1.69	-57.6	35.6	260	100	-1.21	-41.1	14.7
131	140	-1.78	-60.4	27.6	213	240	-1.87	-63.6	38.9	261	260	-1.36	-46.3	10.5
132	140	-1.97	-67.1	30.8	214	210	-1.53	-52.0	35.2	262	270	-1.03	-35.0	12.6
133	120	-2.05	-69.7	29.1	215	240	-1.25	-42.5	37.1	263	270	-1.03	-34.9	15.6
134	130	-1.72	-58.3	25.1	216	240	-1.04	-35.5	33.2	264	300	-1.30	-44.2	17.2
135	300	-1.51	-51.5	16.4	217	30	-1.47	-50.0	36.1	265	270	-1.03	-35.0	20.4
136	300	-1.81	-61.5	18.1	218	30	-1.25	-42.5	30.2	266	260	-1.20	-40.8	18.9
137	120	-1.98	-67.2	30.7	219	30	-1.17	-39.8	34.9	267	270	-.98	-33.3	20.0
138	120	-1.98	-67.2	29.3	220	240	-1.44	-49.1	32.2	268	280	-.73	-24.9	19.0
139	130	-1.70	-57.7	24.7	221	240	-1.48	-50.2	34.8	269	270	-1.10	-37.3	16.8
140	280	-1.64	-55.7	22.2	222	200	-1.33	-45.1	30.4	270	300	-.93	-31.8	17.1
141	300	-1.85	-63.0	15.2	223	240	-1.18	-40.0	32.7	271	270	-1.19	-40.3	16.4
142	290	-1.82	-61.8	12.5	224	120	1.03	-34.9	35.1	272	280	-1.57	-53.2	17.8
143	280	-1.08	-36.8	29.0	225	30	-1.25	-42.6	33.3	273	280	-.78	-26.6	10.6
144	40	-1.08	-36.8	21.4	226	20	-1.92	-65.2	36.0	274	270	-1.02	-34.6	20.8
145	130	-1.81	-61.5	22.8	227	20	-1.78	-60.4	35.5	275	300	-1.20	-40.7	27.7
146	130	-1.98	-67.2	14.9	228	240	-1.66	-56.4	25.1	276	270	-.85	-28.7	21.3
147	130	-1.88	-63.9	8.3	229	240	-1.53	-51.6	21.9	277	280	-1.07	-36.4	27.4
148	280	-1.46	-49.6	7.6	230	210	-1.58	-53.7	23.5	301	220	1.15	-38.0	39.2

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : NO. 15 COLUMBUS CIRCLE, NEW YORK
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 34.9 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF ----	POSITIVE PEAK
302	290	-1.10	-37.3	26.8
303	240	-1.19	-40.5	33.3
304	190	-1.26	-42.7	32.8
305	280	-1.45	-49.1	32.0
306	140	-1.04	-35.5	29.2
307	130	-1.43	-48.6	30.3
308	240	-1.45	-49.4	35.2
309	190	-1.79	-61.0	37.8
310	190	-1.31	-44.7	33.5
311	280	-1.52	-51.5	38.2
312	280	-1.82	-61.8	35.5
313	140	-1.48	-50.3	35.3
314	140	-1.35	-45.7	34.8
315	240	-1.52	-51.8	37.7
316	240	-1.67	-56.8	36.6
317	270	1.10	-35.8	37.4
318	240	-1.74	-59.3	32.0
319	190	-1.14	-38.9	30.6
320	190	-1.32	-44.8	38.0
321	290	-1.81	-61.4	38.9
322	290	-1.49	-50.5	30.9
323	140	-1.77	-60.2	34.6
324	140	-1.63	-55.5	33.0
325	240	-1.51	-51.3	29.7
326	240	-1.52	-51.7	36.6
327	200	-1.41	-48.0	33.0
328	190	-1.25	-42.4	32.3
329	270	-1.93	-65.6	34.2
330	270	-1.68	-57.3	29.4
331	130	-1.75	-59.4	32.3
332	130	-1.51	-51.3	26.0
333	240	-1.66	-56.5	26.8
334	240	-1.75	-59.5	27.2
335	290	1.02	-34.2	34.7
336	240	-1.28	-43.5	23.0
337	200	-1.29	-44.0	26.3
338	200	-1.44	-49.0	28.0
339	290	-1.57	-53.5	23.0
340	260	-1.40	-47.6	24.7
341	130	-1.74	-59.2	29.8
342	130	-2.60	-88.4	25.5
343	240	-1.44	-49.1	20.8
344	280	-1.67	-56.7	16.6
345	190	-1.20	-40.7	23.4
346	330	-1.07	-36.3	24.5
347	80	-1.70	-57.9	18.0
348	280	-1.53	-52.1	22.9
349	50	-1.50	-50.8	19.7
350	50	-1.67	-56.8	16.8
351	240	-1.27	-43.2	12.0
352	300	-1.44	-48.9	12.0
353	120	-.88	-30.0	27.3
354	250	-1.36	-46.1	24.5
355	120	-1.57	-53.4	15.4
356	190	-.83	-28.4	16.3
357	280	-1.65	-56.1	15.6
358	60	-1.52	-51.7	20.1
359	70	-2.16	-73.4	17.7
360	50	-1.89	-64.3	11.7
361	50	-1.36	-46.1	13.1
362	280	-1.39	-47.3	15.3
363	90	-1.24	-42.0	10.6
364	110	-1.05	-35.6	8.5
365	80	-1.53	-52.0	10.3
366	80	-1.67	-56.9	6.7
367	120	-1.20	-40.8	7.4
368	120	-1.35	-45.9	4.7
369	270	-1.12	-37.9	4.7
370	120	-.93	-31.5	7.6
371	100	-1.02	-34.7	11.5
372	310	-1.00	-34.1	18.6
373	110	-.94	-31.9	9.5
374	270	-1.21	-41.0	11.0
375	270	-1.21	-41.2	8.4
376	90	-.85	-29.0	8.0
377	110	-.94	-32.0	5.3
378	300	-.88	-29.9	12.7
379	300	-.99	-33.7	9.4
380	300	-.98	-33.3	10.2
401	290	-1.28	-43.6	37.4
402	310	-1.05	-35.7	28.2
403	320	-.97	-32.9	16.2
404	40	-1.28	-43.5	31.7
405	200	-1.21	-41.2	32.3
406	20	-1.85	-62.8	32.8
407	30	-1.11	-37.6	26.7
408	30	-1.05	-35.9	27.9
409	180	-.98	-33.3	31.1
410	200	-1.43	-48.6	30.6
411	190	-1.49	-50.5	31.2
412	30	-1.51	-51.3	34.8
413	30	-1.58	-53.6	37.9
414	30	-1.76	-59.8	37.2
415	310	1.02	-34.2	34.5
416	200	-1.05	-35.8	35.7
417	210	-1.39	-47.3	38.3
418	200	-1.45	-49.4	40.7
419	210	-1.34	-45.5	37.6
420	30	-1.18	-40.0	34.4
421	30	-1.24	-42.3	34.7
422	30	-1.29	-43.9	35.7
423	310	1.02	-33.4	34.7
424	200	-1.22	-41.4	37.0
425	210	-1.57	-53.4	36.0
426	190	-1.37	-46.7	34.2
427	190	-1.47	-50.0	33.3
428	30	-1.44	-49.0	33.8
429	30	-1.41	-47.9	34.8
430	40	-1.35	-45.8	29.5
431	40	-1.08	-36.6	35.8
432	200	-1.21	-41.1	36.8
433	190	-1.55	-52.6	34.8
434	190	-1.20	-40.9	33.1
435	210	-1.18	-40.2	31.1
436	40	-1.34	-45.7	29.6
437	40	-1.46	-49.6	25.7
438	40	-1.46	-49.5	27.6
439	40	-1.26	-42.8	31.5
440	190	-1.13	-38.6	30.2
441	200	-1.85	-62.8	28.2
442	170	-1.82	-61.8	27.2
443	170	-1.77	-60.2	25.2
444	40	-1.16	-39.5	24.2
445	40	-1.19	-40.4	23.8
446	60	-.94	-32.0	20.2
447	60	-1.00	-34.0	22.1
448	60	-1.00	-34.1	23.8
449	60	-1.25	-42.6	22.6
450	190	-1.58	-53.7	22.2
451	190	-1.39	-47.4	20.2
452	40	-1.48	-50.2	17.8
453	40	-1.78	-60.4	17.8
454	120	-1.35	-45.8	17.8
455	120	-1.16	-39.5	20.8
456	110	-1.22	-41.4	21.6
457	70	-1.62	-55.1	17.8
458	290	-.95	-32.3	18.4
459	70	-1.07	-36.5	18.4
460	50	-1.29	-43.7	17.4
461	50	-1.53	-52.0	19.4
462	110	-1.04	-35.0	15.0
463	120	-1.18	-40.0	13.7
464	80	-1.15	-39.3	11.1
465	70	-1.37	-46.7	5.6

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : NO. 15 COLUMBUS CIRCLE, NEW YORK
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 34.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
466	120	-1.50	-51.1	11.5
467	120	-1.17	-39.8	10.0
468	60	-1.26	-42.7	14.6
469	100	-1.00	-33.9	16.7
470	70	-1.14	-38.8	21.5
471	70	-1.00	-33.9	21.8
472	90	-.94	-31.9	16.0
473	120	-1.04	-35.3	12.0
474	120	-1.16	-39.6	26.3
475	120	-1.35	-46.0	24.7
476	70	-1.02	-34.6	23.9
477	70	-.89	-30.2	16.2
801	280	-1.08	-36.9	17.8
802	270	-.88	-29.9	24.2
803	270	-.99	-33.5	22.7
804	120	-1.37	-46.6	21.0
805	70	-.79	-27.0	24.1
806	60	-.96	-32.7	23.8
807	120	-1.02	-34.8	4.3
808	80	-1.08	-36.6	4.9
809	280	-.91	-31.1	3.0
810	280	-1.00	-33.9	5.3
901	130	-1.17	-39.9	11.0
902	240	-1.13	-38.4	12.2
903	110	-1.10	-37.4	13.9
904	140	-.91	-30.9	16.7
905	130	-1.11	-37.8	5.8
906	140	-1.12	-38.0	7.9
907	130	-1.21	-41.0	19.4
908	80	-1.40	-47.8	2.5
909	130	-1.16	-39.3	21.6
910	300	-1.12	-38.0	7.4
911	300	-1.31	-44.5	22.6
912	280	-.96	-32.8	4.7
913	120	-1.05	-35.9	20.7
914	240	-1.28	-43.6	17.4
915	290	-.97	-33.0	12.0
916	330	-1.15	-39.1	21.2
917	50	-1.00	-33.9	14.5
918	240	-1.26	-42.8	9.1

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : NO. 15 COLUMBUS CIRCLE, NEW YORK
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 34.0 PSF

* * 15 GREATEST PRESSURE COEFFICIENT MAGNITUDES * *

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
342	130	-2.60	-88.4	25.5
239	250	-2.19	-74.3	26.5
359	70	-2.16	-73.4	17.7
155	250	-2.07	-70.2	16.4
125	120	-2.05	-69.7	33.5
133	120	-2.05	-69.7	29.1
138	120	-1.98	-67.2	29.3
137	120	-1.98	-67.2	30.7
146	130	-1.98	-67.2	14.9
132	140	-1.97	-67.1	30.8
329	270	-1.93	-65.6	34.2
226	20	-1.92	-65.2	36.0
360	50	-1.89	-64.3	11.7
147	130	-1.88	-63.9	8.3
213	240	-1.87	-63.6	38.9

TABLE 6A. PEAK LOADS FOR CONFIGURATION B : NO. 15 COLUMBUS CIRCLE, NEW YORK
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 34.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
125	112	-1.69	-57.3	29.4	155	258	-2.01	-68.5	2.8	342	134	-1.36	-46.3	5.8
133	112	-2.00	-68.1	32.1	239	250	-1.84	-62.7	34.3	359	66	-2.14	-72.8	1.6

TABLE 6A. PEAK LOADS FOR CONFIGURATION B : NO. 15 COLUMBUS CIRCLE, NEW YORK
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 34.0 PSF

* * 6 GREATEST PRESSURE COEFFICIENT MAGNITUDES * *

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK PSF	POSITIVE PEAK PSF
359	66	-2.14	-72.8	1.6
155	258	-2.01	-68.5	2.8
133	112	-2.00	-68.1	32.1
239	250	-1.84	-62.7	34.3
125	112	-1.69	-57.3	29.4
342	134	-1.36	-46.3	5.8

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : NO. 15 COLUMBUS CIRCLE, NEW YORK--WIND DIRECTIONALITY INCLUDED
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 34.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
101	130	-1.19	-39.8	21.7
102	130	-1.11	-36.9	23.2
103	140	-1.20	-39.8	29.3
104	110	-1.45	-45.9	24.6
105	130	-1.38	-46.1	28.8
106	110	-1.43	-45.2	26.0
107	130	-1.22	-40.7	26.4
108	300	-1.64	-42.8	25.6
109	110	-1.30	-41.0	24.7
110	110	-1.38	-43.6	28.3
111	110	-1.60	-50.6	32.1
112	120	-1.26	-39.8	31.1
113	130	-1.05	-35.0	26.7
114	130	-1.37	-45.7	27.8
115	30	-1.69	-44.3	34.3
116	30	-1.38	-36.1	31.0
117	130	-1.31	-43.6	25.6
118	110	-1.64	-51.8	28.4
119	120	-1.64	-51.9	29.4
120	110	-1.27	-40.0	24.0
121	130	-1.28	-42.5	24.1
122	130	-1.66	-55.2	19.4
123	270	-1.75	-45.8	23.1
124	110	-1.69	-53.4	24.5
125	120	-2.05	-64.8	25.8
126	130	-1.61	-53.6	23.1
127	120	-1.38	-43.7	18.7
128	120	-1.66	-52.3	20.7
129	30	-1.41	-37.0	33.9
130	30	-1.59	-41.5	25.9
131	140	-1.78	-59.2	21.6
132	140	-1.97	-65.8	23.7
133	120	-2.05	-64.8	22.4
134	130	-1.72	-57.2	19.3
135	300	-1.51	-39.7	12.6
136	130	-1.44	-48.0	14.0
137	120	-1.98	-62.5	23.6
138	140	-1.90	-63.4	22.5
139	130	-1.70	-56.6	19.0
140	140	-1.33	-44.2	17.1
141	130	-1.47	-48.9	11.7
142	290	-1.82	-47.6	9.6
143	280	-1.08	-28.4	25.8
144	40	-1.08	-28.4	16.5
145	130	-1.81	-60.2	18.6
146	130	-1.98	-65.8	11.5
147	130	-1.88	-62.6	7.3
148	130	-1.35	-44.9	5.8
149	280	-1.62	-42.3	7.4
150	280	-1.62	-42.5	6.4
151	130	-1.49	-49.7	20.3
152	130	-1.62	-53.9	12.8
153	110	-.97	-30.7	2.9
154	270	-1.31	-34.2	4.3
155	250	-2.07	-54.1	12.6
156	250	-1.59	-41.7	16.9
157	270	-1.23	-32.3	20.3
158	110	-1.14	-36.0	11.1
159	130	-1.01	-33.5	25.3
160	130	-.92	-30.8	12.5
161	260	-1.09	-28.6	5.5
162	250	-1.61	-42.2	9.6
163	130	-1.09	-36.3	27.3
164	130	-.87	-29.1	17.7
165	270	-1.07	-27.9	10.4
166	280	-1.63	-42.7	13.2
201	240	-1.24	-32.5	30.6
202	140	1.20	-39.5	40.0
203	120	-1.16	-36.7	26.3
204	110	-1.18	-37.2	28.3
205	130	-1.03	-34.4	16.8
206	240	-1.70	-44.4	31.6
207	240	-1.27	-33.3	30.1
208	140	.98	-26.5	32.5
209	240	-1.08	-28.3	27.1
210	130	.88	-27.1	29.2
211	40	-1.21	-31.8	27.2
212	240	-1.69	-44.3	34.9
213	240	-1.87	-49.0	38.1
214	210	-1.53	-40.0	30.5
215	140	1.09	-32.7	36.4
216	140	.97	-27.3	32.2
217	30	-1.47	-38.5	33.6
218	30	-1.25	-32.7	27.9
219	30	-1.17	-30.7	27.6
220	240	-1.44	-37.8	31.6
221	240	-1.48	-38.7	34.1
222	200	-1.33	-34.7	23.8
223	240	-1.18	-30.8	30.4
224	130	1.03	-26.9	34.3
225	30	-1.25	-32.8	31.0
226	20	-1.92	-50.2	28.5
227	20	-1.78	-46.5	28.0
228	240	-1.66	-43.4	23.3
229	240	-1.52	-39.7	20.7
230	210	-1.58	-41.3	22.1
231	240	-1.36	-35.6	31.1
232	130	1.01	-30.7	33.7
233	30	-1.32	-34.4	28.7
234	20	-1.48	-38.7	29.4
235	20	-1.64	-43.0	28.1
236	240	-1.37	-35.9	22.7
237	250	-1.39	-36.5	21.8
238	250	-1.57	-41.0	21.0
239	250	-2.19	-57.2	24.7
240	250	-1.19	-31.3	29.7
241	130	.80	-25.7	26.5
242	40	-1.56	-40.8	25.7
243	30	-1.38	-36.1	25.5
244	290	-1.37	-35.7	21.0
245	240	-1.25	-32.7	13.0
246	250	-1.39	-36.4	13.3
247	270	-1.32	-34.5	22.7
248	130	.77	-23.7	25.7
249	110	.85	-25.6	26.9
250	40	-1.06	-27.7	27.3
251	290	-1.02	-26.6	23.8
252	50	-1.85	-48.4	25.4
253	50	-1.45	-38.1	15.8
254	260	-1.07	-28.1	17.9
255	300	-1.15	-30.1	20.9
256	300	-1.05	-27.5	22.3
257	270	-.92	-24.2	21.6
258	0	-.92	-24.1	21.5
259	310	-.94	-24.5	23.9
260	100	-1.21	-32.4	14.4
261	260	-1.36	-35.6	10.3
262	270	-1.03	-27.0	12.3
263	270	-1.03	-26.9	14.5
264	300	-1.30	-34.0	16.5
265	270	-1.03	-26.9	20.0
266	260	-1.20	-31.4	18.5
267	270	-.98	-25.6	19.1
268	280	-.73	-19.2	18.6
269	270	-1.10	-28.7	15.6
270	300	-.93	-24.5	15.9
271	270	-1.19	-31.0	15.9
272	280	-1.57	-41.0	14.8
273	280	-.78	-20.5	9.9
274	270	-1.02	-26.6	20.0
275	300	-1.20	-31.3	27.2
276	270	-.85	-22.1	20.9
277	280	-1.07	-28.0	21.1
301	220	1.15	-29.3	30.2

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : NO. 15 COLUMBUS CIRCLE, NEW YORK--WIND DIRECTIONALITY INCLUDED
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 34.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
302	130	-1.07	-35.6	20.6
303	140	-.96	-32.0	25.6
304	190	-1.26	-32.9	25.2
305	280	-1.45	-37.8	24.6
306	140	-1.04	-34.8	22.5
307	130	-1.43	-47.6	23.3
308	240	-1.45	-38.0	27.1
309	190	-1.79	-47.0	29.1
310	190	-1.31	-34.4	25.8
311	280	-1.52	-39.7	29.4
312	280	-1.82	-47.6	27.4
313	140	-1.48	-49.3	27.2
314	140	-1.35	-44.8	26.8
315	240	-1.52	-39.9	31.9
316	240	-1.67	-43.7	30.0
317	270	1.10	-27.6	28.8
318	240	-1.74	-45.7	30.2
319	190	-1.14	-29.9	23.7
320	190	-1.32	-34.5	29.2
321	290	-1.81	-47.3	30.0
322	130	-1.18	-39.3	23.8
323	140	-1.77	-59.0	26.7
324	140	-1.63	-54.4	25.4
325	240	-1.51	-39.5	26.1
326	240	-1.52	-39.8	28.2
327	140	-1.14	-38.0	25.4
328	190	-1.25	-32.7	24.8
329	80	-1.91	-51.2	26.3
330	270	-1.68	-44.1	22.6
331	130	-1.75	-58.2	24.9
332	130	-1.51	-50.3	20.0
333	240	-1.66	-43.5	20.7
334	240	-1.75	-45.9	20.9
335	130	-.95	-31.5	26.7
336	240	-1.28	-33.5	22.1
337	140	-1.25	-41.5	20.3
338	200	-1.44	-37.7	21.6
339	130	-1.43	-47.5	17.7
340	260	-1.40	-36.6	19.0
341	130	-1.74	-58.0	23.0
342	130	-1.40	-46.6	19.6
343	240	-1.44	-37.8	16.0
344	280	-1.67	-43.7	12.8
345	130	-.97	-32.2	18.0
346	330	-1.07	-28.0	18.9
347	80	-1.70	-45.8	13.9
348	280	-1.53	-40.1	17.6
349	120	-1.28	-40.4	15.2
350	50	-1.67	-43.8	13.0
351	240	-1.27	-33.3	11.1
352	300	-1.44	-37.6	9.3
353	120	-.88	-27.9	21.1
354	250	-1.36	-35.5	22.8
355	120	-1.57	-49.7	11.9
356	110	-.82	-25.8	12.6
357	280	-1.65	-43.2	12.0
358	60	-1.52	-39.8	15.4
359	70	-2.16	-56.5	13.6
360	50	-1.89	-49.5	9.0
361	50	-1.36	-35.5	12.2
362	280	-1.39	-36.4	11.8
363	90	-1.24	-33.2	8.2
364	110	-1.05	-33.1	6.5
365	80	-1.53	-41.1	8.0
366	80	-1.67	-45.0	5.2
367	120	-1.20	-38.0	5.7
368	120	-1.35	-42.7	3.7
369	110	-.93	-29.5	3.6
370	120	-.93	-29.3	5.9
371	100	-1.02	-27.5	8.9
372	310	-1.00	-26.3	17.3
373	110	-.94	-29.7	5.0
374	270	-1.21	-31.6	8.5
375	270	-1.21	-31.7	6.5
376	120	-.73	-23.2	6.1
377	110	-.94	-29.8	4.1
378	120	-.86	-27.2	9.8
379	110	-.84	-26.7	7.2
380	110	-.90	-28.4	7.8
401	290	-1.28	-33.6	28.8
402	130	-.87	-29.0	21.7
403	320	-.97	-25.3	12.4
404	40	-1.28	-33.5	24.4
405	140	-1.07	-35.7	24.9
406	20	-1.85	-48.4	25.3
407	30	-1.11	-29.0	20.5
408	30	-1.05	-27.6	21.5
409	180	-.98	-25.6	24.0
410	200	-1.43	-37.4	23.5
411	190	-1.49	-38.9	24.0
412	30	-1.51	-39.5	26.8
413	30	-1.58	-41.3	29.2
414	30	-1.76	-46.1	28.6
415	310	1.02	-26.3	26.6
416	200	-1.05	-27.5	27.5
417	210	-1.39	-36.5	29.5
418	200	-1.45	-38.0	31.4
419	210	-1.34	-35.0	28.9
420	30	-1.18	-30.8	26.5
421	30	-1.24	-32.6	26.7
422	30	-1.29	-33.8	27.2
423	310	1.02	-25.6	26.6
424	200	-1.22	-31.9	29.0
425	210	-1.57	-41.0	27.8
426	190	-1.37	-36.0	26.4
427	190	-1.47	-38.5	25.3
428	30	-1.44	-37.8	26.1
429	30	-1.41	-36.9	26.8
430	40	-1.35	-35.3	22.5
431	40	-1.08	-28.2	26.9
432	200	-1.21	-31.7	28.4
433	190	-1.55	-40.5	26.8
434	140	-1.00	-33.4	25.4
435	140	-1.14	-38.0	23.9
436	40	-1.34	-35.2	22.8
437	40	-1.46	-38.3	19.9
438	40	-1.46	-38.1	21.5
439	40	-1.26	-32.9	24.2
440	190	-1.13	-29.7	23.8
441	200	-1.85	-48.4	21.7
442	170	-1.82	-47.5	21.2
443	170	-1.77	-46.4	19.4
444	40	-1.16	-30.4	19.1
445	40	-1.19	-31.3	18.1
446	60	-.94	-24.7	15.6
447	60	-1.00	-26.2	17.0
448	60	-1.00	-26.3	18.3
449	60	-1.25	-32.8	20.2
450	190	-1.58	-41.3	17.1
451	190	-1.39	-36.5	15.6
452	40	-1.48	-38.6	13.7
453	40	-1.78	-46.5	13.7
454	120	-1.35	-42.6	13.8
455	120	-1.16	-36.7	16.0
456	110	-1.22	-38.5	16.7
457	70	-1.62	-42.4	13.8
458	130	-.91	-30.4	14.1
459	130	-.94	-31.3	14.0
460	50	-1.29	-33.7	13.4
461	50	-1.53	-40.1	15.0
462	110	-1.04	-32.9	11.6
463	120	-1.18	-37.2	10.5
464	80	-1.15	-31.0	8.5
465	70	-1.37	-35.9	4.3

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : NO. 15 COLUMBUS CIRCLE, NEW YORK--WIND DIRECTIONALITY INCLUDED
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 34.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)
466	120	-1.50	-47.5	8.8	803	270	-.99	-25.8	22.2	906	140	-1.12	-37.2	6.1
467	120	-1.17	-37.0	7.7	804	120	-1.37	-43.3	16.1	907	130	-1.21	-40.2	14.9
468	130	-1.00	-33.5	11.2	805	110	-.69	-21.7	18.6	908	80	-1.40	-37.7	1.9
469	100	-1.00	-26.8	12.9	806	80	-.96	-25.7	18.4	909	130	-1.16	-38.5	16.6
470	70	-1.14	-29.9	16.5	807	120	-1.02	-32.3	3.3	910	130	-1.09	-36.2	5.7
471	120	-.86	-27.0	16.8	808	120	-1.00	-31.6	3.8	911	130	-1.22	-40.8	17.4
472	90	-.94	-25.2	12.3	809	280	-.91	-23.9	2.3	912	120	-.95	-30.2	3.6
473	120	-1.04	-32.9	9.2	810	280	-1.00	-26.1	4.1	913	140	-1.02	-33.8	15.9
474	120	-1.16	-36.8	20.2	901	130	-1.17	-39.1	8.5	914	240	-1.28	-33.5	13.4
475	120	-1.35	-42.8	19.0	902	120	-1.12	-35.3	11.9	915	120	-.93	-29.3	9.2
476	70	-1.02	-26.6	18.4	903	130	-1.06	-35.4	10.7	916	330	-1.15	-30.1	16.4
477	120	-.85	-26.8	12.4	904	140	-.91	-30.3	12.9	917	140	-.84	-28.0	11.1
801	280	-1.08	-28.4	15.8	905	130	-1.11	-37.0	4.4	918	240	-1.26	-33.0	7.0
802	130	.71	-23.0	23.7										

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : NO. 15 COLUMBUS CIRCLE, NEW YORK--WIND DIRECTIONALITY INCLUDED
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 34.0 PSF

* * 15 GREATEST PRESSURE MAGNITUDES * *

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
146	130	-1.98	-65.8	11.5
132	140	-1.97	-65.8	23.7
133	120	-2.05	-64.8	22.4
125	120	-2.05	-64.8	25.8
138	140	-1.90	-63.4	22.5
147	130	-1.88	-62.6	7.3
137	120	-1.98	-62.5	23.6
145	130	-1.81	-60.2	18.6
131	140	-1.78	-59.2	21.6
323	140	-1.77	-59.0	26.7
331	130	-1.75	-58.2	24.9
341	130	-1.74	-58.0	23.0
239	250	-2.19	-57.2	24.7
134	130	-1.72	-57.2	19.3
139	130	-1.70	-56.6	19.0

TABLE 6A. PEAK LOADS FOR CONFIGURATION B : NO. 15 COLUMBUS CIRCLE, NEW YORK--WIND DIRECTIONALITY INCLUDED
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 34.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
125	112	-1.69	-53.3	22.7	155	258	-2.01	-52.7	2.1	342	134	-1.36	-45.4	5.7
133	112	-2.00	-63.3	24.7	239	250	-1.84	-48.3	33.6	359	66	-2.14	-56.0	1.2

TABLE 6A. PEAK LOADS FOR CONFIGURATION B : NO. 15 COLUMBUS CIRCLE, NEW YORK--WIND DIRECTIONALITY INCLUDED
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 34.0 PSF

* * 6 GREATEST PRESSURE MAGNITUDES * *

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
133	112	-2.00	-63.3	24.7
359	66	-2.14	-56.0	1.2
125	112	-1.69	-53.3	22.7
155	258	-2.01	-52.7	2.1
239	250	-1.84	-48.3	33.6
342	134	-1.36	-45.4	5.7

TABLE 7. BASE SHEAR AND MOMENT SUMMARY : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
CONFIGURATION A REFERENCE PRESSURE 34.0 GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

AZIMUTH	SHEAR (KIPS)		MOMENT (1000-FT-KIPS)			ECCEN (%)	
	X	Y	X	Y	Z	X	Y
0	-290.1	-620.8	192.2	-124.8	-14.2	37	29
10	-199.6	-389.8	128.0	-89.5	-8.1	35	31
20	-237.9	-126.0	49.0	-108.1	-2.2	-8	-27
30	-497.3	260.5	-67.0	-202.2	1.5	-3	9
40	-983.6	559.8	-120.2	-346.9	.5	-1	2
50	-1207.7	822.6	-188.1	-402.3	8.1	-11	27
60	-1118.8	1161.1	-297.8	-370.3	17.5	264	-433
70	-1221.6	1476.6	-406.8	-388.9	28.2	76	-107
80	-1099.3	1689.9	-489.7	-338.9	39.5	51	-56
90	-829.2	1912.2	-561.0	-244.0	40.9	33	-24
100	-415.8	2066.9	-611.8	-106.0	40.3	25	-9
110	13.5	2293.8	-693.9	42.8	31.7	17	0
120	281.5	2453.9	-748.5	122.1	21.6	11	2
130	334.6	2144.7	-668.8	118.9	15.4	9	2
140	163.5	1700.2	-563.9	76.7	10.0	7	1
150	133.3	1169.2	-408.2	69.1	2.4	3	1
160	168.4	724.7	-273.6	69.5	-2.2	-4	-2
170	243.3	827.9	-311.7	84.5	-6.9	-11	-6
180	189.8	579.7	-229.2	69.3	-6.1	-15	-8
190	283.4	486.0	-206.0	108.3	-7.7	-30	-30
200	345.6	300.3	-134.1	132.7	-5.8	75	147
210	346.9	-174.2	55.7	128.5	1.9	5	-16
220	206.9	-445.5	153.3	85.0	6.2	-22	18
230	194.2	-836.2	295.9	88.2	8.6	-14	5
240	131.2	-1509.5	516.7	83.1	8.0	-7	1
250	486.5	-1779.0	576.8	197.7	4.1	-3	1
260	308.2	-2101.2	665.7	118.1	6.1	-4	1
270	247.8	-2449.2	765.0	88.5	6.5	-3	1
280	134.7	-2376.7	763.6	62.7	3.9	-2	0
290	136.6	-2112.1	693.0	58.6	-1.6	1	-0
300	201.5	-2016.0	665.4	84.1	-10.3	6	-1
310	186.6	-1871.2	624.0	84.1	-15.8	11	-2
320	39.3	-1564.9	529.3	33.5	-21.0	17	-1
330	-215.8	-1250.9	421.5	-75.6	-25.3	26	8
340	-344.3	-1054.1	351.1	-137.2	-24.3	32	18
350	-352.6	-859.0	285.8	-144.0	-21.1	37	26

TABLE 7. BASE SHEAR AND MOMENT SUMMARY : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
CONFIGURATION A REFERENCE PRESSURE 34.0 GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

AZIMUTH	SHEAR (KIPS)		MOMENT (1000-FT-KIPS)			ECCEN (%)	
	X	Y	X	Y	Z	X	Y
0	-290.1	-620.8	192.2	-124.8	-14.1	36	29
10	-199.6	-389.8	128.9	-89.5	-8.0	35	30
20	-237.9	-126.0	49.0	-108.1	-1.5	-6	-19
30	-497.3	260.5	-67.0	-202.2	3.9	-7	23
40	-983.6	559.8	-120.2	-346.9	5.5	-6	18
50	-1207.7	822.6	-188.1	-402.3	14.5	-19	48
60	-1118.8	1161.1	-297.8	-370.3	24.1	364	-596
70	-1221.6	1476.6	-406.8	-388.9	35.8	96	-135
80	-1099.3	1689.9	-489.7	-338.9	46.9	60	-67
90	-829.2	1912.2	-561.0	-244.0	47.5	38	-28
100	-415.8	2066.9	-611.8	-106.0	45.4	29	-10
110	13.5	2293.8	-693.9	42.8	35.3	19	0
120	281.5	2453.0	-748.5	122.1	24.3	13	2
130	334.6	2144.7	-668.8	118.9	17.4	10	3
140	163.5	1700.2	-563.9	76.7	12.1	9	1
150	133.3	1169.2	-408.2	69.1	3.6	4	1
160	168.4	724.7	-273.6	69.5	-1.9	-3	-1
170	243.3	827.9	-311.7	84.5	-6.8	-11	-6
180	189.8	579.7	-229.2	69.3	-6.3	-15	-8
190	283.4	486.0	-206.0	108.3	-8.5	-33	-33
200	345.6	300.3	-134.1	132.7	-7.3	93	183
210	346.9	-174.2	55.7	128.5	-.3	-1	3
220	206.9	-445.5	153.3	95.0	4.2	-15	12
230	194.2	-836.2	295.9	88.2	6.0	-9	4
240	131.2	-1509.5	516.7	83.1	4.5	-4	1
250	486.5	-1779.0	576.8	197.7	-1.4	1	-0
260	308.2	-2101.2	665.7	118.1	.9	-1	0
270	247.8	-2449.2	765.0	88.5	1.0	-1	0
280	134.7	-2376.7	763.6	62.7	-1.0	1	-0
290	136.6	-2112.1	693.0	58.6	-6.0	4	-0
300	201.5	-2016.0	665.4	84.1	-14.8	9	-2
310	186.6	-1871.2	624.9	84.1	-20.1	14	-2
320	39.3	-1564.9	529.3	33.5	-24.0	19	-1
330	-215.8	-1250.9	421.5	-75.6	-26.6	27	8
340	-344.3	-1054.1	351.1	-137.2	-24.7	33	18
350	-352.6	-859.0	285.8	-144.0	-21.1	37	26

TABLE 7. BASE SHEAR AND MOMENT SUMMARY : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
CONFIGURATION A REFERENCE PRESSURE 34.0 GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

AZIMUTH	SHEAR (KIPS)		MOMENT (1000-FT-KIPS)			ECCEN (%)	
	X	Y	X	Y	Z	X	Y
0	-290.1	-620.8	192.2	-124.8	-15.4	40	32
10	-199.6	-389.8	128.0	-89.5	-8.9	38	34
20	-237.9	-126.9	49.0	-108.1	-2.6	-10	-32
30	-497.3	260.5	-67.0	-202.2	1.7	-3	10
40	-983.6	559.8	-120.2	-346.9	1.1	-1	4
50	-1207.7	822.6	-188.1	-402.3	9.1	-12	30
60	-1118.8	1161.1	-297.8	-370.3	19.1	288	-472
70	-1221.6	1476.6	-406.8	-388.9	30.3	81	-115
80	-1099.3	1689.9	-489.7	-338.9	42.0	54	-60
90	-829.2	1912.2	-561.0	-244.0	43.8	35	-26
100	-415.8	2066.9	-611.8	-106.0	43.5	27	-9
110	13.5	2293.8	-693.9	42.8	35.4	19	0
120	281.5	2453.0	-748.5	122.1	25.6	13	3
130	334.6	2144.7	-668.8	118.9	18.9	11	3
140	163.5	1706.2	-563.9	76.7	12.8	10	2
150	133.3	1169.2	-408.2	69.1	4.2	5	1
160	168.4	724.7	-273.6	69.5	-1.1	-2	-1
170	243.3	827.9	-311.7	84.5	-5.7	-9	-5
180	189.8	579.7	-229.2	69.3	-5.4	-13	-7
190	293.4	486.0	-206.0	108.3	-7.2	-28	-28
200	345.6	300.3	-134.1	132.7	-5.7	73	144
210	346.9	-174.2	55.7	128.5	1.2	3	-10
220	206.9	-445.5	153.3	85.0	5.1	-18	14
230	194.2	-836.2	295.9	88.2	6.9	-11	4
240	131.2	-1509.5	516.7	83.1	5.1	-4	1
250	486.5	-1779.0	576.8	197.7	.8	-1	0
260	308.2	-2101.2	665.7	118.1	2.3	-1	0
270	247.8	-2449.2	765.0	88.5	2.1	-1	0
280	134.7	-2376.7	763.6	62.7	-.4	0	-0
290	136.6	-2112.1	693.0	58.6	-5.4	3	-0
300	201.5	-2016.0	665.4	84.1	-13.9	9	-1
310	186.6	-1871.2	624.0	84.1	-19.2	13	-2
320	39.3	-1564.9	529.3	33.5	-23.9	19	-1
330	-215.8	-1250.9	421.5	-75.6	-27.6	28	8
340	-344.3	-1054.1	351.1	-137.2	-26.3	35	19
350	-352.6	-859.0	285.8	-144.0	-22.7	40	28

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 0 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-290.1	-620.8	192.2	-124.8	-14.2
2ND	23.00	1.3	-15.7	2147	3699	.6	-4.3	25	-4	-291.4	-605.0	178.1	-118.1	-13.9
3RD	35.92	.6	-9.8	1206	2078	.5	-4.7	20	-2	-292.1	-595.2	170.3	-114.4	-13.8
4TH	48.84	.6	-10.0	1206	2078	.5	-4.8	21	-2	-292.7	-585.2	162.7	-110.6	-13.6
5TH	61.76	.6	-10.3	1206	2078	.5	-4.9	23	-2	-293.3	-575.0	155.2	-106.8	-13.4
6TH	74.68	.6	-10.8	1206	2078	.5	-5.2	25	-3	-293.9	-564.2	147.9	-103.0	-13.2
7TH	87.60	.7	-11.2	1206	2078	.5	-5.4	26	-3	-294.6	-553.0	140.6	-99.2	-13.0
8TH	100.52	.7	-11.7	1206	2078	.6	-5.6	27	-3	-295.3	-541.3	133.6	-95.4	-12.7
9TH	113.44	.7	-12.2	1206	2078	.6	-5.9	28	-3	-296.0	-529 1	126.7	-91.6	-12.4
10TH	126.27	.7	-12.6	1197	2063	.6	-6.1	30	-3	-296.7	-516 5	120.0	-87.8	-12.1
11TH	139.10	.6	-13.0	1197	2063	.5	-6.3	30	-2	-297.3	-503.5	113.4	-84.0	-11.8
12TH	151.93	.0	-13.2	1197	2063	.0	-6.4	30	-0	-297.3	-490.2	107.0	-80.2	-11.5
13TH	164.76	-.5	-13.4	1197	2063	-.5	-6.5	29	2	-296.7	-476.8	100.8	-76.3	-11.2
14TH	177.59	-1.1	-13.6	1197	2063	-.9	-6.6	29	4	-295.6	-463.2	94.8	-72.5	-10.9
15TH	190.42	-1.7	-13.8	1197	2063	-1.4	-6.7	29	6	-293.9	-449.4	89.0	-68.8	-10.6
16TH	203.25	-2.3	-14.0	1197	2063	-1.9	-6.8	29	8	-291.7	-435.4	83.3	-65.0	-10.2
17TH	216.08	-2.4	-14.2	1197	2063	-2.0	-6.9	31	9	-289.2	-421.1	77.8	-61.3	-9.9
18TH	228.66	-3.1	-13.9	1174	2023	-2.7	-6.9	32	12	-286.1	-407.2	72.6	-57.7	-9.6
19TH	241.24	-4.0	-13.9	1174	2023	-3.4	-6.9	33	16	-282.1	-393.3	67.5	-54.1	-9.2
20TH	253.82	-4.9	-13.8	1174	2023	-4.1	-6.8	35	21	-277.3	-379.6	62.7	-50.6	-8.9
21ST	266.40	-5.7	-13.7	1174	2023	-4.9	-6.8	37	26	-271.5	-365.8	58.0	-47.1	-8.6
22ND	278.98	-6.6	-13.6	1174	2023	-5.6	-6.7	40	33	-264.9	-352.2	53.5	-43.7	-8.2
23RD	291.56	-7.5	-13.6	1174	2023	-6.4	-6.7	44	41	-257.4	-338.6	49.1	-40.5	-7.9
24TH	304.14	-8.1	-13.5	1174	2023	-6.9	-6.7	47	48	-249.3	-325.1	45.0	-37.3	-7.6
25TH	316.72	-8.5	-13.7	1174	2023	-7.2	-6.8	49	52	-240.8	-311.4	40.9	-34.2	-7.2
		-8.6	-13.5	1151	1983	-7.5	-6.8	51	56					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 0 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-232.2	-297.9	37.2	-31.3	-6.9
27TH	341.38	-8.9	-13.7	1151	1983	-7.8	-6.9	54	60	-223.3	-284.2	33.6	-28.5	-6.6
28TH	353.71	-9.2	-13.8	1151	1983	-8.0	-7.0	56	64	-214.0	-270.4	30.2	-25.8	-6.2
29TH	366.04	-9.6	-13.9	1151	1983	-8.3	-7.0	59	69	-204.5	-256.4	26.9	-23.2	-5.9
30TH	378.12	-9.7	-13.8	1127	1943	-8.6	-7.1	64	77	-194.8	-242.6	23.9	-20.8	-5.5
31ST	390.20	-9.9	-14.0	1127	1943	-8.8	-7.2	66	79	-184.9	-228.6	21.1	-18.5	-5.2
32ND	402.28	-10.1	-14.3	1127	1943	-8.9	-7.4	64	77	-174.9	-214.3	18.4	-16.3	-4.8
33RD	414.36	-10.2	-14.6	1127	1943	-9.1	-7.5	63	75	-164.6	-199.7	15.9	-14.3	-4.4
34TH	426.44	-10.4	-14.9	1127	1943	-9.3	-7.7	62	74	-154.2	-184.8	13.6	-12.3	-4.0
35TH	438.52	-10.6	-15.2	1127	1943	-9.4	-7.8	60	72	-143.6	-169.7	11.4	-10.5	-3.7
36TH	450.60	-10.8	-15.5	1127	1943	-9.6	-8.0	59	71	-132.8	-154.2	9.5	-8.9	-3.3
37TH	462.68	-10.9	-15.7	1127	1943	-9.7	-8.1	58	69	-121.9	-138.5	7.7	-7.3	-2.9
38TH	474.76	-11.2	-15.6	1127	1943	-10.0	-8.0	62	76	-110.6	-122.9	6.1	-5.9	-2.5
39TH	486.84	-11.6	-15.4	1127	1943	-10.3	-7.9	68	87	-99.0	-107.6	4.7	-4.7	-2.2
40TH	498.92	-11.9	-15.1	1127	1943	-10.6	-7.8	76	102	-87.1	-92.5	3.5	-3.5	-1.8
41ST	511.00	-12.3	-14.9	1127	1943	-10.9	-7.7	88	123	-74.8	-77.5	2.5	-2.5	-1.5
42ND	523.08	-12.7	-14.7	1127	1943	-11.2	-7.6	106	155	-62.2	-62.8	1.7	-1.7	-1.2
43RD	535.66	-13.8	-15.1	1174	2023	-11.7	-7.5	162	252	-48.4	-47.7	1.0	-1.0	-.8
44TH	548.58	-15.0	-15.6	1206	2078	-12.4	-7.5	331	541	-33.4	-32.2	.4	-.5	-.5
MR	566.58	-21.5	-22.8	1680	2895	-12.8	-7.9	185	297	-11.9	-9.3	.1	-.1	-.2
TOP	581.67	-11.9	-9.3	1085	2065	-11.0	-4.5	-35	-75	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 19 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-199.6	-389.8	128.0	-89.5	-8.1
2ND	23.00	-.3	-7.4	2147	3699	-.1	-2.0	5	0	-199.3	-382.4	119.1	-84.9	-8.1
3RD	35.92	-.2	-5.2	1206	2078	-.1	-2.5	11	1	-199.1	-377.2	114.2	-82.3	-8.0
4TH	48.84	-.2	-4.4	1206	2078	-.2	-2.1	14	1	-198.9	-372.8	109.3	-79.7	-8.0
5TH	61.76	-.3	-4.1	1206	2078	-.2	-2.0	16	2	-198.6	-368.7	104.5	-77.2	-7.9
6TH	74.68	-.2	-4.6	1206	2078	-.2	-2.2	18	2	-198.4	-364.1	99.8	-74.6	-7.8
7TH	87.60	-.2	-5.0	1206	2078	-.1	-2.4	19	1	-198.2	-359.1	95.1	-72.0	-7.8
8TH	100.52	-.1	-5.4	1206	2078	-.1	-2.6	21	1	-198.1	-353.7	90.5	-69.5	-7.7
9TH	113.44	-.1	-5.9	1206	2078	-.0	-2.8	22	0	-198.0	-347.8	86.0	-66.9	-7.6
10TH	126.27	.0	-6.3	1197	2063	.0	-3.0	23	-0	-198.0	-341.6	81.6	-64.4	-7.5
11TH	139.10	.0	-6.7	1197	2063	.0	-3.2	24	-0	-198.0	-334.9	77.2	-61.8	-7.3
12TH	151.93	-.2	-7.1	1197	2063	-.1	-3.4	25	1	-197.9	-327.8	73.0	-59.3	-7.2
13TH	164.76	-.3	-7.5	1197	2063	-.3	-3.6	27	2	-197.6	-320.3	68.8	-56.8	-7.0
14TH	177.59	-.5	-7.9	1197	2063	-.4	-3.8	28	3	-197.1	-312.3	64.8	-54.2	-6.8
15TH	190.42	-.7	-8.3	1197	2063	-.6	-4.0	29	4	-196.4	-304.0	60.8	-51.7	-6.7
16TH	203.25	-.8	-8.8	1197	2063	-.7	-4.2	31	5	-195.5	-295.2	57.0	-49.2	-6.4
17TH	216.08	-.8	-9.2	1197	2063	-.7	-4.4	34	5	-194.7	-286.1	53.2	-46.7	-6.2
18TH	228.66	-1.1	-9.1	1174	2023	-.9	-4.5	34	7	-193.6	-277.0	49.7	-44.2	-5.9
19TH	241.24	-1.4	-9.2	1174	2023	-1.2	-4.5	35	9	-192.2	-267.8	46.3	-41.8	-5.7
20TH	253.82	-1.8	-9.3	1174	2023	-1.5	-4.6	35	12	-190.4	-258.5	43.0	-39.4	-5.4
21ST	266.40	-2.1	-9.3	1174	2023	-1.8	-4.6	36	14	-188.3	-249.1	39.8	-37.0	-5.2
22ND	278.98	-2.5	-9.4	1174	2023	-2.1	-4.7	36	16	-185.8	-239.7	36.7	-34.7	-4.9
23RD	291.56	-2.9	-9.5	1174	2023	-2.4	-4.7	37	19	-182.9	-230.3	33.7	-32.3	-4.7
24TH	304.14	-3.2	-9.5	1174	2023	-2.7	-4.7	38	22	-179.7	-220.7	30.9	-30.1	-4.4
25TH	316.72	-3.5	-9.6	1174	2023	-3.0	-4.7	38	24	-176.2	-211.2	28.2	-27.8	-4.2
		-3.8	-9.4	1151	1983	-3.3	-4.7	38	26					

TABLE 7. SHEAR AND MOMENT DIAGRAMS NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 10 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-172.4	-201.7	25.6	-25.7	-3.9
27TH	341.38	-4.1	-9.5	1151	1983	-3.5	-4.8	39	28	-168.4	-192.3	23.2	-23.6	-3.7
28TH	353.71	-4.4	-9.5	1151	1983	-3.8	-4.8	39	31	-164.0	-182.8	20.9	-21.5	-3.5
29TH	366.04	-4.7	-9.5	1151	1983	-4.1	-4.8	40	33	-159.3	-173.2	18.7	-19.5	-3.2
30TH	378.12	-5.1	-9.4	1127	1943	-4.5	-4.8	43	39	-154.3	-163.9	16.7	-17.6	-3.0
31ST	390.20	-5.6	-9.4	1127	1943	-4.9	-4.9	46	46	-148.7	-154.4	14.7	-15.8	-2.8
32ND	402.28	-6.1	-9.5	1127	1943	-5.4	-4.9	49	53	-142.6	-144.9	12.9	-14.1	-2.5
33RD	414.36	-6.6	-9.6	1127	1943	-5.9	-4.9	54	63	-136.0	-135.3	11.2	-12.4	-2.3
34TH	426.44	-7.1	-9.7	1127	1943	-6.3	-5.0	60	75	-128.9	-125.7	9.7	-10.8	-2.1
35TH	438.52	-7.6	-9.7	1127	1943	-6.8	-5.0	69	93	-121.3	-115.9	8.2	-9.3	-1.9
36TH	450.60	-8.2	-9.8	1127	1943	-7.2	-5.1	84	119	-113.1	-106.1	6.9	-7.8	-1.7
37TH	462.68	-8.7	-9.9	1127	1943	-7.7	-5.1	110	164	-104.5	-96.3	5.6	-6.5	-1.5
38TH	474.76	-9.0	-9.9	1127	1943	-8.0	-5.1	137	211	-95.5	-86.3	4.5	-5.3	-1.3
39TH	486.84	-9.3	-9.9	1127	1943	-8.2	-5.1	200	320	-86.2	-76.5	3.6	-4.2	-1.1
40TH	498.92	-9.6	-9.9	1127	1943	-8.5	-5.1	416	688	-76.6	-66.6	2.7	-3.2	-.9
41ST	511.00	-9.9	-9.9	1127	1943	-8.8	-5.1	$$$$	-3369	-66.7	-56.7	1.9	-2.4	-.8
42ND	523.08	-10.2	-9.8	1127	1943	-9.1	-5.1	-264	-466	-56.5	-46.9	1.3	-1.6	-.6
43RD	535.66	-11.4	-10.2	1174	2023	-9.7	-5.1	-86	-162	-45.1	-36.6	.8	-1.0	-.4
44TH	548.58	-13.0	-10.8	1206	2078	-10.8	-5.2	-40	-82	-32.1	-25.9	.4	-.5	-.3
MR	566.58	-19.9	-16.3	1680	2895	-11.8	-5.6	-32	-66	-12.2	-9.6	.1	-.1	-.1
TOP	581.67	-12.2	-9.6	1085	2065	-11.2	-4.6	-18	-38	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 20 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-237.9	-126.0	49.0	-108.1	-2.2
2ND	23.00	-1.0	-1.6	2147	3699	-.4	-.4	-122	-128	-236.9	-124.4	46 1	-102.6	-2.3
3RD	35.92	-.3	-1.4	1206	2078	-.3	-.7	-23	-10	-236.6	-123.1	44.5	-99.5	-2.3
4TH	48.84	-.2	-.7	1206	2078	-.2	-.3	-39	-23	-236.4	-122.4	42.9	-96.5	-2.3
5TH	61.76	-.2	-.4	1206	2078	-.2	-.2	-101	-101	-236.1	-122.0	41.3	-93.4	-2.4
6TH	74.68	-.3	-.6	1206	2078	-.2	-.3	-78	-68	-235.8	-121.4	39.8	-90.4	-2.4
7TH	87.60	-.3	-.7	1206	2078	-.3	-.3	-66	-54	-235.5	-120.7	38.2	-87.3	-2.4
8TH	100.52	-.4	-.9	1206	2078	-.3	-.4	-60	-46	-235.1	-119.8	36.6	-84.3	-2.4
9TH	113.44	-.4	-1.0	1206	2078	-.4	-.5	-56	-41	-234.7	-118.8	35.1	-81.3	-2.5
10TH	126.27	-.5	-1.1	1197	2063	-.4	-.6	-53	-38	-234.2	-117.7	33.6	-78.3	-2.5
11TH	139.10	-.5	-1.3	1197	2063	-.5	-.6	-49	-35	-233.6	-116.4	32.1	-75.3	-2.6
12TH	151.93	-.6	-1.4	1197	2063	-.5	-.7	-37	-27	-233.0	-115.0	30.6	-72.3	-2.6
13TH	164.76	-.7	-1.5	1197	2063	-.6	-.7	-26	-20	-232.4	-113.5	29.1	-69.3	-2.6
14TH	177.59	-.7	-1.7	1197	2063	-.6	-.8	-17	-13	-231.6	-111.8	27.7	-66.3	-2.6
15TH	190.42	-.8	-1.8	1197	2063	-.7	-.9	-9	-7	-230.8	-110.0	26.3	-63.3	-2.6
16TH	203.25	-.9	-1.9	1197	2063	-.7	-.9	-2	-1	-229.9	-108.1	24.9	-60.4	-2.6
17TH	216.08	-.9	-2.0	1197	2063	-.8	-1.0	6	5	-229.0	-106.1	23.5	-57.4	-2.6
18TH	228.66	-1.1	-2.1	1174	2023	-1.0	-1.0	13	12	-227.9	-104.1	22.2	-54.6	-2.6
19TH	241.24	-1.4	-2.1	1174	2023	-1.2	-1.1	22	24	-226.5	-101.9	20.9	-51.7	-2.6
20TH	253.82	-1.6	-2.2	1174	2023	-1.4	-1.1	35	44	-224.8	-99.7	19.6	-48.9	-2.6
21ST	266.40	-1.9	-2.3	1174	2023	-1.6	-1.1	59	83	-223.0	-97.4	18.4	-46.1	-2.5
22ND	278.98	-2.1	-2.4	1174	2023	-1.8	-1.2	118	180	-220.8	-95.0	17.1	-43.3	-2.5
23RD	291.56	-2.4	-2.5	1174	2023	-2.0	-1.2	494	820	-218.4	-92.6	16.0	-40.5	-2.5
24TH	304.14	-2.7	-2.4	1174	2023	-2.3	-1.2	-127	-238	-215.7	-90.1	14.8	-37.8	-2.4
25TH	316.72	-3.0	-2.4	1174	2023	-2.5	-1.2	-49	-104	-212.7	-87.8	13.7	-35.1	-2.3
		-3.2	-2.3	1151	1983	-2.8	-1.1	-29	-71					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 20 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-209.5	-85.5	12.6	-32.5	-2.3
27TH	341.38	-3.5	-2.2	1151	1983	-3.1	-1.1	-20	-55	-206.0	-83.3	11.6	-29.9	-2.2
28TH	353.71	-3.8	-2.1	1151	1983	-3.3	-1.1	-15	-47	-202.2	-81.2	10.6	-27.4	-2.2
29TH	366.04	-4.1	-2.1	1151	1983	-3.6	-1.1	-12	-41	-198.0	-79.1	9.6	-24.9	-2.1
30TH	378.12	-4.9	-2.0	1127	1943	-4.3	-1.0	-7	-31	-193.2	-77.1	8.6	-22.6	-2.1
31ST	390.20	-5.8	-2.3	1127	1943	-5.1	-1.2	-7	-30	-187.4	-74.8	7.7	-20.3	-2.0
32ND	402.28	-6.7	-2.7	1127	1943	-5.9	-1.4	-8	-33	-180.7	-72.1	6.8	-18.0	-1.9
33RD	414.36	-7.5	-3.2	1127	1943	-6.7	-1.6	-9	-35	-173.2	-68.9	6.0	-15.9	-1.8
34TH	426.44	-8.4	-3.7	1127	1943	-7.4	-1.9	-10	-37	-164.8	-65.2	5.2	-13.9	-1.7
35TH	438.52	-9.3	-4.2	1127	1943	-8.2	-2.1	-10	-39	-155.5	-61.1	4.4	-11.9	-1.5
36TH	450.60	-10.1	-4.6	1127	1943	-9.0	-2.4	-11	-41	-145.4	-56.4	3.7	-10.1	-1.4
37TH	462.68	-10.9	-5.1	1127	1943	-9.7	-2.6	-12	-43	-134.5	-51.3	3.1	-8.4	-1.2
38TH	474.76	-11.4	-5.2	1127	1943	-10.1	-2.7	-11	-40	-123.1	-46.1	2.5	-6.9	-1.1
39TH	486.84	-11.8	-5.2	1127	1943	-10.4	-2.7	-9	-36	-111.4	-40.9	1.9	-5.4	-.9
40TH	498.92	-12.2	-5.2	1127	1943	-10.8	-2.7	-8	-32	-99.2	-35.7	1.5	-4.2	-.7
41ST	511.00	-12.6	-5.2	1127	1943	-11.2	-2.7	-7	-29	-86.6	-30.5	1.1	-3.0	-.6
42ND	523.08	-13.0	-5.2	1127	1943	-11.5	-2.7	-6	-26	-73.6	-25.3	.7	-2.1	-.5
43RD	535.66	-15.0	-5.4	1174	2023	-12.8	-2.7	-5	-22	-58.6	-20.0	.5	-1.3	-.3
44TH	548.58	-18.0	-5.6	1206	2078	-14.9	-2.7	-3	-17	-40.6	-14.4	.2	-.6	-.2
MR	566.58	-25.7	-8.1	1680	2895	-15.3	-2.8	-3	-14	-14.8	-6.3	.0	-.1	-.1
TOP	581.67	-14.8	-6.3	1085	2065	-13.7	-3.0	-2	-10	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 30 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-497.3	260.5	-67.0	-202.2	1.5
2ND	23.00	-2.5	9.6	2147	3699	-1.2	2.6	50	-22	-494.8	251.0	-61.1	-190.8	1.1
3RD	35.92	-1.1	5.6	1206	2078	-.9	2.7	39	-13	-493.7	245.4	-57.9	-184.4	1.0
4TH	48.84	-1.1	5.9	1206	2078	-.9	2.8	35	-11	-492.6	239.5	-54.8	-178.0	.8
5TH	61.76	-1.3	6.1	1206	2078	-1.1	2.9	35	-12	-491.3	233.3	-51.7	-171.6	.7
6TH	74.68	-1.6	6.2	1206	2078	-1.3	3.0	36	-16	-489.7	227.1	-48.7	-165.3	.5
7TH	87.60	-1.9	6.4	1206	2078	-1.6	3.1	37	-19	-487.8	220.7	-45.9	-159.0	.3
8TH	100.52	-2.2	6.5	1206	2078	-1.8	3.1	39	-22	-485.6	214.2	-43.0	-152.7	.1
9TH	113.44	-2.5	6.6	1206	2078	-2.1	3.2	40	-26	-483.0	207.6	-40.3	-146.4	-.0
10TH	126.27	-2.8	6.7	1197	2063	-2.4	3.3	42	-30	-480.2	200.9	-37.7	-140.3	-.2
11TH	139.10	-3.2	6.9	1197	2063	-2.7	3.3	44	-35	-477.0	194.0	-35.2	-134.1	-.4
12TH	151.93	-3.7	7.0	1197	2063	-3.1	3.4	45	-40	-473.3	187.0	-32.7	-128.0	-.6
13TH	164.76	-4.2	7.2	1197	2063	-3.5	3.5	46	-46	-469.1	179.8	-30.4	-122.0	-.8
14TH	177.59	-4.7	7.3	1197	2063	-3.9	3.5	49	-53	-464.4	172.5	-28.1	-116.0	-.9
15TH	190.42	-5.2	7.4	1197	2063	-4.3	3.6	52	-62	-459.2	165.1	-25.9	-110.1	-1.1
16TH	203.25	-5.7	7.6	1197	2063	-4.8	3.7	58	-74	-453.5	157.5	-23.9	-104.2	-1.3
17TH	216.08	-6.6	7.7	1197	2063	-5.5	3.7	84	-122	-446.9	149.8	-21.9	-98.4	-1.4
18TH	228.66	-7.0	7.6	1174	2023	-6.0	3.8	141	-221	-439.9	142.2	-20.1	-92.9	-1.5
19TH	241.24	-7.5	7.6	1174	2023	-6.4	3.8	546	-912	-432.5	134.6	-18.3	-87.4	-1.6
20TH	253.82	-7.9	7.6	1174	2023	-6.7	3.8	-223	396	-424.5	127.0	-16.7	-82.0	-1.8
21ST	266.40	-8.4	7.6	1174	2023	-7.1	3.8	-83	156	-416.2	119.4	-15.1	-76.7	-1.9
22ND	278.98	-8.8	7.6	1174	2023	-7.5	3.8	-47	94	-407.3	111.8	-13.7	-71.5	-2.0
23RD	291.56	-9.3	7.6	1174	2023	-7.9	3.8	-31	65	-398.1	104.2	-12.3	-66.4	-2.1
24TH	304.14	-9.7	7.6	1174	2023	-8.3	3.7	-21	47	-388.4	96.6	-11.1	-61.5	-2.1
25TH	316.72	-10.1	7.2	1174	2023	-8.6	3.5	-10	24	-378.3	89.5	-9.9	-56.7	-2.2
		-10.2	6.7	1151	1983	-8.9	3.4	-4	10					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 30 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-368.1	82.8	-8.8	-52.1	-2.2
27TH	341.38	-10.6	6.3	1151	1983	-9.2	3.2	-0	0	-357.5	76.5	-7.8	-47.6	-2.2
28TH	353.71	-10.9	5.9	1151	1983	-9.5	3.0	2	-7	-346.5	70.6	-6.9	-43.3	-2.2
29TH	366.04	-11.3	5.6	1151	1983	-9.8	2.8	4	-13	-335.3	65.0	-6.1	-39.1	-2.2
30TH	378.12	-12.4	5.1	1127	1943	-11.0	2.6	4	-15	-322.8	59.9	-5.3	-35.1	-2.1
31ST	390.20	-13.7	4.9	1127	1943	-12.1	2.5	3	-16	-309.1	55.1	-4.6	-31.3	-2.0
32ND	402.28	-14.6	4.7	1127	1943	-13.0	2.4	3	-16	-294.5	50.3	-4.0	-27.6	-1.9
33RD	414.36	-15.6	4.6	1127	1943	-13.8	2.4	3	-17	-278.9	45.7	-3.4	-24.2	-1.8
34TH	426.44	-16.5	4.5	1127	1943	-14.6	2.3	3	-17	-262.4	41.3	-2.9	-20.9	-1.7
35TH	438.52	-17.5	4.3	1127	1943	-15.5	2.2	3	-17	-245.0	37.0	-2.4	-17.8	-1.5
36TH	450.60	-18.4	4.2	1127	1943	-16.3	2.2	2	-18	-226.6	32.8	-2.0	-15.0	-1.4
37TH	462.68	-19.2	4.0	1127	1943	-17.1	2.1	2	-19	-207.3	28.8	-1.6	-12.4	-1.2
38TH	474.76	-19.6	3.6	1127	1943	-17.4	1.9	2	-18	-187.7	25.1	-1.3	-10.0	-1.1
39TH	486.84	-20.0	3.4	1127	1943	-17.7	1.7	2	-16	-167.8	21.7	-1.0	-7.8	-.9
40TH	498.92	-20.3	3.1	1127	1943	-18.0	1.6	1	-15	-147.5	18.6	-.8	-5.9	-.8
41ST	511.00	-20.7	2.8	1127	1943	-18.3	1.5	1	-14	-126.8	15.8	-.6	-4.3	-.6
42ND	523.08	-21.0	2.6	1127	1943	-18.6	1.3	1	-13	-105.8	13.2	-.4	-2.9	-.5
43RD	535.66	-23.7	2.4	1174	2023	-20.2	1.2	1	-11	-82.1	10.9	-.3	-1.7	-.4
44TH	548.58	-27.4	2.5	1206	2078	-22.7	1.2	1	-11	-54.7	8.4	-.1	-.8	-.2
MR	566.58	-36.6	5.2	1680	2895	-21.8	1.8	1	-13	-18.1	3.2	-.0	-.1	-.0
TOP	581.67	-18.1	3.2	1085	2065	-16.7	1.5	0	-5	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 40 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-983.6	559.8	-120.2	-346.9	.5
2ND	23.00	-8.7	25.3	2147	3699	-4.0	6.8	49	-29	-974.9	534.5	-107.6	-324.4	-.3
3RD	35.92	-4.1	17.2	1206	2078	-3.4	8.3	39	-16	-970.8	517.3	-100.8	-311.8	-.8
4TH	48.84	-3.9	17.6	1206	2078	-3.3	8.5	35	-13	-966.9	499.7	-94.2	-299.3	-1.3
5TH	61.76	-4.8	18.1	1206	2078	-4.0	8.7	35	-16	-962.1	481.6	-87.9	-286.8	-1.8
6TH	74.68	-6.3	18.6	1206	2078	-5.2	9.0	35	-20	-955.8	463.0	-81.8	-274.4	-2.2
7TH	87.60	-7.8	19.2	1206	2078	-6.5	9.2	37	-25	-948.0	443.8	-75.9	-262.1	-2.7
8TH	100.52	-9.3	19.7	1206	2078	-7.7	9.5	38	-31	-938.7	424.2	-70.3	-249.9	-3.2
9TH	113.44	-10.8	20.2	1206	2078	-8.9	9.7	41	-37	-928.0	403.9	-64.9	-237.9	-3.7
10TH	126.27	-12.2	20.6	1197	2063	-10.2	10.0	44	-44	-915.8	383.4	-59.9	-226.0	-4.1
11TH	139.10	-13.6	20.9	1197	2063	-11.4	10.1	48	-53	-902.2	362.4	-55.1	-214.4	-4.6
12TH	151.93	-15.0	20.6	1197	2063	-12.5	10.0	54	-68	-887.1	341.9	-50.6	-202.9	-5.0
13TH	164.76	-16.4	20.2	1197	2063	-13.7	9.8	67	-93	-870.7	321.7	-46.3	-191.6	-5.4
14TH	177.59	-17.8	19.8	1197	2063	-14.9	9.6	104	-159	-853.0	301.8	-42.3	-180.6	-5.7
15TH	190.42	-19.2	19.5	1197	2063	-16.0	9.4	616	-1034	-833.8	282.4	-38.6	-169.8	-6.0
16TH	203.25	-20.6	19.1	1197	2063	-17.2	9.2	-91	168	-813.2	263.3	-35.1	-159.2	-6.2
17TH	216.08	-23.0	18.7	1197	2063	-19.2	9.1	-20	41	-790.2	244.6	-31.8	-148.9	-6.3
18TH	228.66	-23.2	17.6	1174	2023	-19.8	8.7	-11	24	-767.0	227.0	-28.9	-139.1	-6.5
19TH	241.24	-23.6	16.7	1174	2023	-20.1	8.3	-7	16	-743.4	210.3	-26.1	-129.6	-6.5
20TH	253.82	-23.9	15.9	1174	2023	-20.4	7.9	-4	10	-719.5	194.4	-23.6	-120.4	-6.6
21ST	266.40	-24.3	15.1	1174	2023	-20.7	7.4	-2	5	-695.2	179.3	-21.2	-111.5	-6.6
22ND	278.98	-24.6	14.2	1174	2023	-21.0	7.0	-0	1	-670.6	165.1	-19.1	-102.9	-6.6
23RD	291.56	-25.0	13.4	1174	2023	-21.3	6.6	1	-2	-645.7	151.7	-17.1	-94.6	-6.6
24TH	304.14	-25.2	12.6	1174	2023	-21.5	6.2	1	-4	-620.5	139.0	-15.2	-86.7	-6.6
25TH	316.72	-25.3	12.0	1174	2023	-21.5	5.9	2	-8	-595.2	127.1	-13.6	-79.0	-6.5
		-24.8	11.1	1151	1983	-21.6	5.6	3	-11					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 40 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-570.4	115.9	-12.1	-71.8	-6.4
27TH	341.38	-24.9	10.5	1151	1983	-21.6	5.3	3	-13	-545.6	105.4	-10.7	-65.0	-6.3
28TH	353.71	-24.9	9.9	1151	1983	-21.6	5.0	4	-16	-520.6	95.6	-9.5	-58.4	-6.1
29TH	366.04	-25.0	9.2	1151	1983	-21.7	4.7	4	-19	-495.7	86.3	-8.3	-52.1	-5.9
30TH	378.12	-26.2	8.5	1127	1943	-23.3	4.4	4	-21	-469.5	77.9	-7.3	-46.3	-5.7
31ST	390.20	-27.4	7.7	1127	1943	-24.3	4.0	4	-22	-442.0	70.2	-6.4	-40.8	-5.5
32ND	402.28	-27.9	6.9	1127	1943	-24.7	3.6	3	-23	-414.2	63.3	-5.6	-35.6	-5.2
33RD	414.36	-28.3	6.1	1127	1943	-25.1	3.2	3	-23	-385.9	57.1	-4.9	-30.8	-4.9
34TH	426.44	-28.7	5.4	1127	1943	-25.5	2.8	3	-24	-357.2	51.7	-4.3	-26.3	-4.6
35TH	438.52	-29.1	4.6	1127	1943	-25.8	2.4	2	-25	-328.0	47.1	-3.7	-22.2	-4.2
36TH	450.60	-29.6	3.8	1127	1943	-26.2	2.0	2	-26	-298.5	43.3	-3.1	-18.4	-3.9
37TH	462.68	-29.9	3.0	1127	1943	-26.5	1.6	2	-27	-268.6	40.3	-2.6	-14.9	-3.5
38TH	474.76	-29.6	3.1	1127	1943	-26.3	1.6	2	-27	-239.0	37.2	-2.1	-11.9	-3.1
39TH	486.84	-29.3	3.3	1127	1943	-26.0	1.7	2	-27	-209.7	33.9	-1.7	-9.2	-2.8
40TH	498.92	-29.1	3.5	1127	1943	-25.8	1.8	2	-27	-180.6	30.4	-1.3	-6.8	-2.4
41ST	511.00	-28.8	3.7	1127	1943	-25.5	1.9	2	-27	-151.8	26.7	-1.0	-4.8	-2.0
42ND	523.08	-28.5	3.9	1127	1943	-25.3	2.0	2	-27	-123.3	22.9	-.7	-3.1	-1.7
43RD	535.66	-30.8	4.2	1174	2023	-26.3	2.1	2	-26	-92.5	18.6	-.4	-1.8	-1.3
44TH	548.58	-33.7	4.8	1206	2078	-27.9	2.3	2	-27	-58.8	13.8	-.2	-.8	-.9
MR	566.58	-42.2	8.6	1680	2895	-25.1	3.0	4	-34	-16.6	5.2	-.0	-.1	-.3
TOP	581.67	-16.6	5.2	1085	2065	-15.3	2.5	7	-37	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 30 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-1207.7	822.6	-188.1	-402.3	8.1
2ND	23.00	-16.8	45.7	2147	3699	-7.8	12.3	41	-26	-1190.9	776.9	-169.7	-374.7	6.8
3RD	35.92	-7.9	28.2	1206	2078	-6.6	13.6	31	-15	-1182.9	748.7	-159.8	-359.4	6.1
4TH	48.84	-7.0	28.1	1206	2078	-5.8	13.5	27	-11	-1175.9	720.6	-150.3	-344.2	5.6
5TH	61.76	-7.8	28.1	1206	2078	-6.5	13.5	26	-13	-1168.1	692.5	-141.2	-329.0	5.0
6TH	74.68	-10.0	28.1	1206	2078	-8.3	13.5	28	-17	-1158.1	664.4	-132.4	-314.0	4.5
7TH	87.60	-12.2	28.2	1206	2078	-10.1	13.6	30	-22	-1145.9	636.2	-124.0	-299.1	3.9
8TH	100.52	-14.4	28.2	1206	2078	-11.9	13.6	33	-29	-1131.5	608.0	-116.0	-284.4	3.4
9TH	113.44	-16.6	28.3	1206	2078	-13.7	13.6	37	-37	-1115.0	579.7	-108.3	-269.9	2.8
10TH	126.27	-18.6	28.1	1197	2063	-15.5	13.6	43	-49	-1096.4	551.6	-101.1	-255.7	2.3
11TH	139.10	-20.6	27.9	1197	2063	-17.2	13.5	54	-68	-1075.7	523.7	-94.2	-241.8	1.7
12TH	151.93	-22.1	26.9	1197	2063	-18.5	13.0	73	-102	-1053.6	496.8	-87.6	-228.1	1.2
13TH	164.76	-23.6	25.8	1197	2063	-19.7	12.5	137	-212	-1030.0	471.0	-81.4	-214.7	.8
14TH	177.59	-25.1	24.8	1197	2063	-21.0	12.0	-874	1505	-1004.9	446.2	-75.5	-201.7	.3
15TH	190.42	-26.6	23.8	1197	2063	-22.2	11.5	-80	152	-978.3	422.4	-70.0	-189.0	-.9
16TH	203.25	-28.1	22.8	1197	2063	-23.5	11.0	-35	75	-950.2	399.6	-64.7	-176.6	-.4
17TH	216.08	-31.1	21.8	1197	2063	-26.0	10.5	-15	36	-919.0	377.9	-59.7	-164.6	-.7
18TH	228.66	-31.2	20.4	1174	2023	-26.6	10.1	-11	27	-887.8	357.4	-55.1	-153.2	-.9
19TH	241.24	-31.5	19.6	1174	2023	-26.8	9.7	-8	22	-856.3	337.9	-50.7	-142.3	-1.1
20TH	253.82	-31.7	18.7	1174	2023	-27.0	9.2	-6	18	-824.6	319.1	-46.6	-131.7	-1.3
21ST	266.40	-32.0	17.8	1174	2023	-27.3	8.8	-5	14	-792.6	301.3	-42.7	-121.5	-1.4
22ND	278.98	-32.3	17.0	1174	2023	-27.5	8.4	-3	11	-760.3	284.3	-39.0	-111.8	-1.5
23RD	291.56	-32.5	16.1	1174	2023	-27.7	8.0	-2	8	-727.8	268.2	-35.5	-102.4	-1.6
24TH	304.14	-32.6	15.3	1174	2023	-27.7	7.6	-2	6	-695.2	252.9	-32.2	-93.4	-1.7
25TH	316.72	-32.3	14.9	1174	2023	-27.5	7.3	-1	5	-663.0	238.0	-29.1	-84.9	-1.8
		-31.4	14.1	1151	1983	-27.3	7.1	-1	3					

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 50 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-631.6	223.9	-26.3	-76.9	-1.8
27TH	341.38	-31.1	13.7	1151	1983	-27.0	6.9	-0	2	-600.5	210.3	-23.6	-69.3	-1.8
28TH	353.71	-30.8	13.2	1151	1983	-26.8	6.7	-0	1	-569.7	197.1	-21.1	-62.1	-1.8
29TH	366.04	-30.5	12.7	1151	1983	-26.5	6.4	0	-1	-539.1	184.3	-18.8	-55.3	-1.8
30TH	378.12	-31.4	12.0	1127	1943	-27.8	6.2	1	-3	-507.8	172.3	-16.6	-49.0	-1.8
31ST	390.20	-32.1	11.8	1127	1943	-28.5	6.0	1	-4	-475.6	160.5	-14.6	-43.0	-1.7
32ND	402.28	-32.1	11.5	1127	1943	-28.5	5.9	1	-4	-443.5	149.0	-12.7	-37.5	-1.7
33RD	414.36	-32.1	11.3	1127	1943	-28.5	5.8	1	-5	-411.4	137.7	-11.0	-32.3	-1.6
34TH	426.44	-32.1	11.0	1127	1943	-28.5	5.7	1	-5	-379.3	126.7	-9.4	-27.5	-1.5
35TH	438.52	-32.1	10.8	1127	1943	-28.5	5.6	1	-5	-347.2	115.8	-7.9	-23.1	-1.5
36TH	450.60	-32.1	10.6	1127	1943	-28.5	5.4	1	-5	-315.1	105.3	-6.6	-19.1	-1.4
37TH	462.68	-31.9	10.3	1127	1943	-28.3	5.3	1	-6	-283.1	94.9	-5.4	-15.5	-1.3
38TH	474.76	-31.7	10.2	1127	1943	-28.1	5.3	1	-7	-251.4	84.7	-4.3	-12.3	-1.2
39TH	486.84	-31.5	10.2	1127	1943	-27.9	5.2	1	-8	-219.9	74.5	-3.3	-9.4	-1.1
40TH	498.92	-31.3	10.1	1127	1943	-27.7	5.2	2	-8	-188.7	64.4	-2.5	-7.0	-1.0
41ST	511.00	-31.1	10.1	1127	1943	-27.5	5.2	2	-9	-157.6	54.3	-1.8	-4.9	-.9
42ND	523.08	-30.8	10.0	1127	1943	-27.3	5.2	2	-10	-126.8	44.3	-1.2	-3.2	-.8
43RD	535.66	-33.0	10.4	1174	2023	-28.1	5.1	2	-11	-93.8	33.9	-.7	-1.8	-.6
44TH	548.58	-34.9	10.8	1206	2078	-29.0	5.2	2	-13	-58.9	23.1	-.3	-.8	-.4
MR	566.58	-42.8	16.2	1680	2895	-25.5	5.6	4	-18	-16.1	7.0	-.1	-.1	-.1
TOP	581.67	-16.1	7.0	1085	2065	-14.8	3.4	4	-17	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 60 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-1118.8	1161.1	-297.8	-370.3	17.5
2ND	23.00	-20.4	58.8	2147	3699	-9.5	15.9	34	-20	-1098.4	1102.2	-271.8	-344.8	16.1
3RD	35.92	-8.9	36.4	1206	2078	-7.4	17.5	23	-10	-1089.4	1065.9	-257.8	-330.7	15.5
4TH	48.84	-6.6	34.7	1206	2078	-5.4	16.7	21	-7	-1082.9	1031.2	-244.3	-316.7	14.9
5TH	61.76	-6.5	33.5	1206	2078	-5.4	16.1	20	-7	-1076.3	997.7	-231.1	-302.7	14.4
6TH	74.68	-8.6	33.1	1206	2078	-7.1	15.9	22	-9	-1067.8	964.6	-218.5	-288.9	13.9
7TH	87.60	-10.6	32.6	1206	2078	-8.8	15.7	23	-13	-1057.2	932.0	-206.2	-275.1	13.3
8TH	100.52	-12.6	32.1	1206	2078	-10.5	15.5	25	-17	-1044.6	899.9	-194.4	-261.6	12.8
9TH	113.44	-14.6	31.7	1206	2078	-12.1	15.2	28	-22	-1029.9	868.2	-183.0	-248.2	12.2
10TH	126.27	-16.5	31.0	1197	2063	-13.8	15.0	32	-29	-1013.4	837.2	-172.0	-235.1	11.7
11TH	139.10	-18.4	30.5	1197	2063	-15.4	14.8	37	-39	-994.9	806.7	-161.5	-222.2	11.1
12TH	151.93	-20.0	30.2	1197	2063	-16.7	14.6	41	-47	-974.9	776.6	-151.3	-209.5	10.5
13TH	164.76	-21.6	29.8	1197	2063	-18.0	14.5	47	-58	-953.3	746.7	-141.5	-197.2	10.0
14TH	177.59	-23.2	29.5	1197	2063	-19.4	14.3	56	-75	-930.1	717.2	-132.2	-185.1	9.5
15TH	190.42	-24.8	29.2	1197	2063	-20.7	14.2	74	-107	-905.4	688.0	-123.1	-173.3	9.0
16TH	203.25	-26.3	28.9	1197	2063	-22.0	14.0	120	-186	-879.0	659.1	-114.5	-161.9	8.5
17TH	216.08	-29.0	28.6	1197	2063	-24.2	13.8	-645	1113	-850.1	630.6	-106.2	-150.8	8.1
18TH	228.66	-29.1	27.4	1174	2023	-24.8	13.5	-139	252	-820.9	603.2	-98.5	-140.3	7.7
19TH	241.24	-29.5	26.7	1174	2023	-25.1	13.2	-85	159	-791.5	576.5	-91.0	-130.1	7.3
20TH	253.82	-29.8	26.0	1174	2023	-25.4	12.8	-59	116	-761.7	550.5	-84.0	-120.3	6.9
21ST	266.40	-30.2	25.3	1174	2023	-25.7	12.5	-45	91	-731.5	525.2	-77.2	-111.0	6.5
22ND	278.98	-30.5	24.6	1174	2023	-26.0	12.2	-36	75	-701.0	500.6	-70.7	-101.9	6.1
23RD	291.56	-30.8	23.9	1174	2023	-26.3	11.8	-29	64	-670.2	476.7	-64.6	-93.3	5.8
24TH	304.14	-30.9	23.4	1174	2023	-26.3	11.6	-26	59	-639.2	453.3	-58.7	-85.1	5.4
25TH	316.72	-30.5	23.2	1174	2023	-26.0	11.5	-26	58	-608.7	430.1	-53.2	-77.2	5.1
		-29.6	22.5	1151	1983	-25.7	11.4	-25	57					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 60 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-579.2	407.6	-48.0	-69.9	4.7
27TH	341.38	-29.2	22.3	1151	1983	-25.4	11.3	-25	56	-550.0	385.3	-43.1	-62.9	4.4
28TH	353.71	-28.8	22.1	1151	1983	-25.0	11.2	-25	54	-521.1	363.1	-38.5	-56.3	4.1
29TH	366.04	-28.5	21.9	1151	1983	-24.7	11.0	-24	53	-492.7	341.2	-34.2	-50.1	3.8
30TH	378.12	-28.6	21.3	1127	1943	-25.4	10.9	-19	44	-464.0	320.0	-30.2	-44.3	3.6
31ST	390.20	-29.2	21.1	1127	1943	-25.9	10.9	-17	39	-434.8	298.8	-26.4	-38.9	3.3
32ND	402.28	-29.5	21.0	1127	1943	-26.1	10.8	-16	39	-405.3	277.8	-23.0	-33.8	3.0
33RD	414.36	-29.7	20.9	1127	1943	-26.3	10.8	-16	38	-375.6	256.8	-19.7	-29.1	2.8
34TH	426.44	-29.9	20.8	1127	1943	-26.5	10.7	-15	37	-345.7	236.0	-16.8	-24.7	2.5
35TH	438.52	-30.2	20.7	1127	1943	-26.8	10.7	-15	37	-315.5	215.3	-14.0	-20.7	2.2
36TH	450.60	-30.4	20.6	1127	1943	-27.0	10.6	-14	36	-285.2	194.6	-11.6	-17.1	1.9
37TH	462.68	-30.4	20.5	1127	1943	-27.0	10.6	-14	35	-254.7	174.1	-9.3	-13.9	1.7
38TH	474.76	-29.8	20.3	1127	1943	-26.5	10.4	-14	35	-224.9	153.8	-7.3	-11.0	1.4
39TH	486.84	-29.2	20.0	1127	1943	-25.9	10.3	-14	35	-195.7	133.7	-5.6	-8.4	1.2
40TH	498.92	-28.6	19.8	1127	1943	-25.3	10.2	-14	34	-167.1	113.9	-4.1	-6.2	.9
41ST	511.00	-27.9	19.5	1127	1943	-24.8	10.1	-14	34	-139.2	94.4	-2.9	-4.4	.7
42ND	523.08	-27.3	19.3	1127	1943	-24.2	9.9	-14	34	-111.9	75.1	-1.8	-2.9	.5
43RD	535.66	-28.4	19.8	1174	2023	-24.2	9.8	-13	31	-83.5	55.3	-1.0	-1.6	.3
44TH	548.58	-29.5	20.2	1206	2078	-24.5	9.7	-10	25	-54.0	35.1	-.4	-.7	.1
MR	566.58	-38.3	28.3	1680	2895	-22.8	9.8	-4	9	-15.6	6.8	-.1	-.1	.0
TOP	581.67	-15.6	6.8	1085	2065	-14.4	3.3	-0	1	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 70 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00													
		-37.0	64.3	2147	3699	-17.2	17.4	49	-48	-1221.6	1476.6	-406.8	-388.9	28.2
2ND	23.00									-1184.7	1412.4	-373.6	-361.2	26.5
		-17.5	39.1	1206	2078	-14.5	18.8	29	-22					
3RD	35.92									-1167.1	1373.3	-355.6	-346.1	25.8
		-16.1	36.5	1206	2078	-13.4	17.6	26	-20					
4TH	48.84									-1151.0	1336.8	-338.1	-331.1	25.2
		-16.6	35.2	1206	2078	-13.7	16.9	27	-21					
5TH	61.76									-1134.4	1301.6	-321.1	-316.3	24.6
		-17.1	35.4	1206	2078	-14.2	17.0	28	-23					
6TH	74.68									-1117.3	1266.2	-304.5	-301.8	24.0
		-17.7	35.6	1206	2078	-14.7	17.1	29	-25					
7TH	87.60									-1099.6	1230.6	-288.4	-287.4	23.4
		-18.3	35.9	1206	2078	-15.2	17.3	30	-26					
8TH	100.52									-1081.3	1194.7	-272.7	-273.4	22.7
		-18.8	36.1	1206	2078	-15.6	17.4	32	-28					
9TH	113.44									-1062.5	1158.7	-257.5	-259.5	22.1
		-19.3	36.0	1197	2063	-16.1	17.5	33	-30					
10TH	126.27									-1043.2	1122.6	-242.8	-246.0	21.4
		-19.9	36.1	1197	2063	-16.6	17.5	35	-32					
11TH	139.10									-1023.3	1086.5	-228.7	-232.7	20.7
		-20.9	35.8	1197	2063	-17.4	17.3	36	-36					
12TH	151.93									-1002.4	1050.7	-215.0	-219.7	20.0
		-21.8	35.5	1197	2063	-18.2	17.2	38	-40					
13TH	164.76									-980.6	1015.2	-201.7	-207.0	19.3
		-22.7	35.1	1197	2063	-19.0	17.0	40	-44					
14TH	177.59									-957.9	980.1	-188.9	-194.6	18.7
		-23.7	34.8	1197	2063	-19.8	16.9	42	-50					
15TH	190.42									-934.2	945.3	-176.6	-182.5	18.0
		-24.6	34.5	1197	2063	-20.6	16.7	47	-57					
16TH	203.25									-909.6	910.8	-164.7	-170.6	17.4
		-26.7	34.2	1197	2063	-22.3	16.6	57	-76					
17TH	216.08									-882.9	876.6	-153.2	-159.1	16.8
		-27.2	33.1	1174	2023	-23.2	16.4	69	-97					
18TH	228.66									-855.7	843.5	-142.4	-148.2	16.2
		-28.0	32.8	1174	2023	-23.9	16.2	86	-125					
19TH	241.24									-827.6	810.7	-132.0	-137.6	15.6
		-28.9	32.4	1174	2023	-24.6	16.0	114	-173					
20TH	253.82									-798.7	778.3	-122.0	-127.4	15.0
		-29.7	32.0	1174	2023	-25.3	15.8	171	-270					
21ST	266.40									-769.0	746.3	-112.4	-117.5	14.4
		-30.6	31.7	1174	2023	-26.0	15.7	351	-576					
22ND	278.98									-738.4	714.6	-103.2	-108.0	13.7
		-31.4	31.3	1174	2023	-26.8	15.5	$$$$	7435					
23RD	291.56									-707.0	683.2	-94.4	-98.9	13.1
		-31.8	31.1	1174	2023	-27.1	15.4	-528	919					
24TH	304.14									-675.2	652.2	-86.0	-90.2	12.5
		-31.6	31.1	1174	2023	-26.9	15.3	-756	1309					
25TH	316.72									-643.6	621.1	-78.0	-81.9	11.9
		-30.7	30.4	1151	1983	-26.7	15.3	$$$$	2254					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 70 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-613.0	590.7	-70.5	-74.2	11.3
27TH	341.38	-30.4	30.4	1151	1983	-26.5	15.3	$$$$	7884	-582.5	560.3	-63.4	-66.8	10.6
28TH	353.71	-30.2	30.3	1151	1983	-26.2	15.3	3109	-5270	-552.3	530.0	-56.7	-59.8	10.0
29TH	366.04	-30.0	30.3	1151	1983	-26.0	15.3	1174	-1976	-522.3	499.7	-50.4	-53.2	9.4
30TH	378.12	-30.3	29.6	1127	1943	-26.9	15.3	-546	950	-492.0	470.1	-44.5	-47.1	8.8
31ST	390.20	-30.9	29.7	1127	1943	-27.4	15.3	-300	531	-461.1	440.4	-39.0	-41.3	8.2
32ND	402.28	-31.1	29.8	1127	1943	-27.6	15.4	-291	516	-430.0	410.5	-33.9	-35.9	7.6
33RD	414.36	-31.3	30.0	1127	1943	-27.7	15.4	-282	502	-398.7	380.6	-29.1	-30.9	7.0
34TH	426.44	-31.5	30.1	1127	1943	-27.9	15.5	-275	488	-367.2	350.5	-24.7	-26.3	6.4
35TH	438.52	-31.6	30.2	1127	1943	-28.1	15.6	-267	476	-335.6	320.2	-20.6	-22.1	5.8
36TH	450.60	-31.8	30.4	1127	1943	-28.2	15.6	-260	464	-303.8	289.9	-16.9	-18.2	5.2
37TH	462.68	-31.8	30.5	1127	1943	-28.2	15.7	-277	492	-272.0	259.4	-13.6	-14.7	4.5
38TH	474.76	-31.4	30.4	1127	1943	-27.9	15.7	-363	639	-240.5	229.0	-10.7	-11.6	3.9
39TH	486.84	-31.0	30.3	1127	1943	-27.5	15.6	-481	839	-209.5	198.7	-8.1	-8.9	3.3
40TH	498.92	-30.6	30.1	1127	1943	-27.1	15.5	-719	1244	-178.9	168.6	-5.9	-6.6	2.8
41ST	511.00	-30.2	30.0	1127	1943	-26.8	15.4	$$$$	2519	-148.7	138.7	-4.0	-4.6	2.2
42ND	523.08	-29.8	29.8	1127	1943	-26.4	15.3	$$$$$$$$$		-119.9	108.9	-2.5	-3.0	1.6
43RD	535.66	-31.2	30.9	1174	2023	-26.6	15.3	-959	1651	-87.7	78.0	-1.3	-1.7	1.0
44TH	548.58	-32.3	31.1	1206	2078	-26.8	15.0	-271	479	-55.4	46.9	-.5	-.8	.5
MR	566.58	-40.1	40.5	1680	2895	-23.9	14.0	703	-1185	-15.3	6.4	-.0	-.1	.1
TOP	581.67	-15.3	6.4	1085	2065	-14.1	3.1	-2	9	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-1099.3	1689.9	-489.7	-338.9	39.5
2ND	23.00	-42.3	61.6	2147	3699	-19.7	16.7	65	-76	-1057.1	1628.3	-451.5	-314.1	37.8
3RD	35.92	-20.2	38.1	1206	2078	-16.8	18.3	35	-32	-1036.9	1590.2	-430.7	-300.6	37.0
4TH	48.84	-19.5	36.0	1206	2078	-16.2	17.3	33	-31	-1017.4	1554.2	-410.4	-287.3	36.3
5TH	61.76	-20.0	35.0	1206	2078	-16.5	16.8	35	-34	-997.4	1519.2	-390.6	-274.3	35.7
6TH	74.68	-19.7	35.3	1206	2078	-16.4	17.0	36	-34	-977.7	1483.9	-371.2	-261.5	35.0
7TH	87.60	-19.5	35.6	1206	2078	-16.2	17.1	37	-34	-958.2	1448.3	-352.2	-249.0	34.2
8TH	100.52	-19.3	35.9	1206	2078	-16.0	17.3	38	-35	-938.9	1412.4	-333.8	-236.8	33.5
9TH	113.44	-19.1	36.2	1206	2078	-15.8	17.4	39	-35	-919.8	1376.2	-315.7	-224.8	32.7
10TH	126.27	-18.8	36.3	1197	2063	-15.7	17.6	39	-35	-901.0	1339.9	-298.3	-213.1	31.8
11TH	139.10	-18.7	36.6	1197	2063	-15.6	17.7	40	-35	-882.3	1303.3	-281.4	-201.7	31.0
12TH	151.93	-19.2	36.9	1197	2063	-16.1	17.9	40	-36	-863.1	1266.4	-264.9	-190.5	30.1
13TH	164.76	-19.7	37.2	1197	2063	-16.5	18.0	40	-36	-843.3	1229.2	-248.9	-179.5	29.2
14TH	177.59	-20.3	37.6	1197	2063	-16.9	18.2	40	-37	-823.1	1191.6	-233.3	-168.8	28.4
15TH	190.42	-20.8	37.9	1197	2063	-17.4	18.4	40	-38	-802.3	1153.7	-218.3	-158.4	27.5
16TH	203.25	-21.3	38.2	1197	2063	-17.8	18.5	41	-38	-780.9	1115.5	-203.7	-148.2	26.7
17TH	216.08	-22.4	38.6	1197	2063	-18.7	18.7	42	-41	-758.5	1076.9	-189.7	-138.4	25.8
18TH	228.66	-22.6	37.9	1174	2023	-19.2	18.7	43	-44	-735.9	1039.1	-176.4	-129.0	25.0
19TH	241.24	-23.1	37.8	1174	2023	-19.7	18.7	45	-47	-712.8	1001.2	-163.5	-119.9	24.1
20TH	253.82	-23.7	37.8	1174	2023	-20.1	18.7	47	-50	-689.1	963.5	-151.2	-111.0	23.2
21ST	266.40	-24.2	37.7	1174	2023	-20.6	18.6	49	-54	-665.0	925.7	-139.3	-102.5	22.4
22ND	278.98	-24.7	37.7	1174	2023	-21.0	18.6	52	-58	-640.3	888.1	-127.9	-94.3	21.5
23RD	291.56	-25.2	37.6	1174	2023	-21.5	18.6	54	-62	-615.0	850.4	-116.9	-86.4	20.6
24TH	304.14	-25.6	37.7	1174	2023	-21.8	18.6	56	-65	-589.4	812.7	-106.5	-78.8	19.7
25TH	316.72	-25.9	38.0	1174	2023	-22.1	18.8	57	-66	-563.5	774.8	-96.5	-71.6	18.7
		-25.6	37.5	1151	1983	-22.3	18.9	58	-67					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 80 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-537.9	737.3	-87.2	-64.8	17.8
27TH	341.38	-25.9	37.8	1151	1983	-22.5	19.0	58	-68	-512.0	699.5	-78.3	-58.3	16.9
28TH	353.71	-26.1	38.0	1151	1983	-22.7	19.2	59	-69	-485.9	661.5	-69.9	-52.2	15.9
29TH	366.04	-26.3	38.3	1151	1983	-22.9	19.3	60	-70	-459.6	623.2	-62.0	-46.3	15.0
30TH	378.12	-27.0	37.8	1127	1943	-23.9	19.4	64	-78	-432.6	585.4	-54.7	-41.0	14.0
31ST	390.20	-27.6	37.9	1127	1943	-24.5	19.5	67	-83	-405.0	547.5	-47.9	-35.9	13.1
32ND	402.28	-27.8	38.0	1127	1943	-24.6	19.5	68	-84	-377.2	509.6	-41.5	-31.2	12.1
33RD	414.36	-27.9	38.0	1127	1943	-24.8	19.6	69	-86	-349.3	471.6	-35.6	-26.8	11.2
34TH	426.44	-28.1	38.0	1127	1943	-24.9	19.6	69	-87	-321.1	433.5	-30.1	-22.7	10.2
35TH	438.52	-28.3	38.1	1127	1943	-25.1	19.6	70	-89	-292.8	395.5	-25.1	-19.0	9.2
36TH	450.60	-28.5	38.1	1127	1943	-25.3	19.6	71	-91	-264.4	357.4	-20.5	-15.7	8.3
37TH	462.68	-28.5	38.1	1127	1943	-25.3	19.6	71	-90	-235.9	319.3	-16.4	-12.6	7.3
38TH	474.76	-28.0	38.0	1127	1943	-24.8	19.6	67	-84	-207.9	281.3	-12.8	-10.0	6.4
39TH	486.84	-27.5	37.9	1127	1943	-24.4	19.5	64	-79	-180.4	243.4	-9.6	-7.6	5.5
40TH	498.92	-27.0	37.7	1127	1943	-23.9	19.4	61	-74	-153.4	205.7	-6.9	-5.6	4.6
41ST	511.00	-26.5	37.5	1127	1943	-23.5	19.3	58	-69	-126.9	168.1	-4.7	-3.9	3.7
42ND	523.08	-26.0	37.4	1127	1943	-23.0	19.2	55	-65	-100.9	130.8	-2.9	-2.5	2.9
43RD	535.66	-26.9	38.8	1174	2023	-22.9	19.2	54	-64	-74.0	92.0	-1.5	-1.4	2.0
44TH	548.58	-27.2	38.9	1206	2078	-22.6	18.7	53	-63	-46.8	53.1	-.5	-.6	1.2
MR	566.58	-33.4	49.8	1680	2895	-19.9	17.2	44	-50	-13.5	3.3	-.0	-.1	.2
TOP	581.67	-13.5	3.3	1085	2065	-12.4	1.6	-5	32	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-829.2	1912.2	-561.0	-244.0	40.9
2ND	23.00	-44.0	65.7	2147	3699	-20.5	17.7	57	-65	-785.2	1846.6	-517.8	-225.5	39.2
3RD	35.92	-20.5	40.1	1206	2078	-17.0	19.3	31	-27	-764.7	1806.5	-494.2	-215.4	38.5
4TH	48.84	-18.0	38.3	1206	2078	-15.0	18.4	28	-22	-746.7	1768.2	-471.1	-205.7	37.8
5TH	61.76	-17.2	37.6	1206	2078	-14.3	18.1	28	-22	-729.5	1730.7	-448.5	-196.1	37.2
6TH	74.68	-16.7	38.4	1206	2078	-13.9	18.5	28	-21	-712.8	1692.3	-426.3	-186.8	36.5
7TH	87.60	-16.2	39.1	1206	2078	-13.4	18.8	28	-20	-696.6	1653.1	-404.7	-177.7	35.8
8TH	100.52	-15.7	39.9	1206	2078	-13.0	19.2	28	-19	-680.9	1613.2	-383.6	-168.8	35.0
9TH	113.44	-15.1	40.7	1206	2078	-12.6	19.6	29	-18	-665.8	1572.5	-363.1	-160.1	34.2
10TH	126.27	-14.5	41.2	1197	2063	-12.1	20.0	29	-17	-651.3	1531.3	-343.1	-151.7	33.4
11TH	139.10	-14.2	41.9	1197	2063	-11.9	20.3	29	-17	-637.1	1489.4	-323.8	-143.4	32.5
12TH	151.93	-14.7	42.2	1197	2063	-12.3	20.4	29	-17	-622.4	1447.2	-304.9	-135.3	31.6
13TH	164.76	-15.2	42.4	1197	2063	-12.7	20.6	29	-17	-607.3	1404.8	-286.6	-127.4	30.8
14TH	177.59	-15.6	42.7	1197	2063	-13.1	20.7	29	-18	-591.6	1362.1	-268.9	-119.8	30.0
15TH	190.42	-16.1	43.0	1197	2063	-13.4	20.8	28	-18	-575.5	1319.1	-251.7	-112.3	29.1
16TH	203.25	-16.6	43.2	1197	2063	-13.8	21.0	28	-18	-558.9	1275.9	-235.0	-105.0	28.3
17TH	216.08	-17.2	43.5	1197	2063	-14.4	21.1	29	-19	-541.8	1232.4	-218.9	-97.9	27.4
18TH	228.66	-17.2	42.7	1174	2023	-14.6	21.1	30	-20	-524.6	1189.7	-203.7	-91.2	26.6
19TH	241.24	-17.4	42.7	1174	2023	-14.9	21.1	31	-21	-507.1	1147.0	-189.0	-84.7	25.7
20TH	253.82	-17.7	42.7	1174	2023	-15.1	21.1	32	-22	-489.4	1104.2	-174.9	-78.5	24.8
21ST	266.40	-18.0	42.7	1174	2023	-15.3	21.1	32	-23	-471.4	1061.5	-161.2	-72.4	23.9
22ND	278.98	-18.3	42.8	1174	2023	-15.6	21.1	34	-24	-453.2	1018.7	-148.1	-66.6	23.0
23RD	291.56	-18.5	42.8	1174	2023	-15.8	21.1	35	-25	-434.6	975.9	-135.6	-61.0	22.0
24TH	304.14	-18.7	42.9	1174	2023	-16.0	21.2	35	-26	-415.9	933.0	-123.6	-55.7	21.0
25TH	316.72	-18.9	43.0	1174	2023	-16.1	21.3	35	-26	-397.0	890.0	-112.1	-50.6	20.1
		-18.6	42.3	1151	1983	-16.2	21.3	35	-26					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-378.4	847.7	-101.4	-45.8	19.1
27TH	341.38	-18.7	42.5	1151	1983	-16.3	21.4	35	-26	-359.7	805.2	-91.2	-41.2	18.1
28TH	353.71	-18.9	42.6	1151	1983	-16.4	21.5	35	-27	-340.8	762.6	-81.6	-36.9	17.2
29TH	366.04	-19.0	42.8	1151	1983	-16.5	21.6	35	-27	-321.9	719.8	-72.4	-32.8	16.2
30TH	378.12	-19.1	42.0	1127	1943	-16.9	21.6	36	-28	-302.8	677.8	-64.0	-29.0	15.2
31ST	390.20	-19.2	42.2	1127	1943	-17.0	21.7	36	-28	-283.6	635.6	-56.0	-25.5	14.3
32ND	402.28	-19.2	42.5	1127	1943	-17.0	21.9	36	-28	-264.4	593.0	-48.6	-22.2	13.3
33RD	414.36	-19.2	42.8	1127	1943	-17.1	22.0	37	-28	-245.2	550.2	-41.7	-19.1	12.3
34TH	426.44	-19.3	43.1	1127	1943	-17.1	22.2	37	-28	-225.9	507.1	-35.3	-16.3	11.3
35TH	438.52	-19.3	43.4	1127	1943	-17.1	22.3	37	-28	-206.6	463.7	-29.5	-13.7	10.2
36TH	450.60	-19.4	43.7	1127	1943	-17.2	22.5	37	-28	-187.2	420.0	-24.1	-11.3	9.2
37TH	462.68	-19.3	44.0	1127	1943	-17.1	22.6	37	-27	-167.9	376.1	-19.3	-9.1	8.2
38TH	474.76	-19.2	44.1	1127	1943	-17.0	22.7	36	-26	-148.8	331.9	-15.0	-7.2	7.1
39TH	486.84	-19.0	44.3	1127	1943	-16.9	22.8	35	-25	-129.7	287.6	-11.3	-5.5	6.1
40TH	498.92	-18.9	44.4	1127	1943	-16.8	22.9	34	-24	-110.8	243.2	-8.1	-4.1	5.2
41ST	511.00	-18.8	44.6	1127	1943	-16.7	22.9	33	-23	-92.0	198.6	-5.4	-2.9	4.2
42ND	523.08	-18.7	44.7	1127	1943	-16.6	23.0	32	-23	-73.3	153.9	-3.3	-1.9	3.3
43RD	535.66	-19.3	46.7	1174	2023	-16.5	23.1	31	-22	-54.0	107.2	-1.7	-1.1	2.3
44TH	548.58	-19.2	46.9	1206	2078	-16.0	22.6	31	-22	-34.7	60.3	-.6	-.5	1.3
MR	566.58	-23.8	58.2	1680	2895	-14.2	20.1	29	-20	-10.9	2.1	-.0	-.1	.2
TOP	581.67	-10.9	2.1	1085	2065	-10.1	1.0	-5	43	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 180 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-415.8	2066.9	-611.8	-106.0	40.3
2ND	23.00	-37.0	69.4	2147	3699	-17.2	18.8	39	-35	-378.9	1997.5	-565.0	-96.9	38.7
3RD	35.92	-17.8	42.3	1206	2078	-14.8	20.4	24	-17	-361.1	1955.2	-539.5	-92.1	38.1
4TH	48.84	-14.5	40.3	1206	2078	-12.1	19.4	23	-14	-346.5	1914.9	-514.5	-87.5	37.4
5TH	61.76	-12.8	39.5	1206	2078	-10.7	19.0	24	-13	-333.7	1875.4	-490.0	-83.2	36.7
6TH	74.68	-12.0	40.2	1206	2078	-10.0	19.3	24	-12	-321.6	1835.3	-466.0	-78.9	36.0
7TH	87.60	-11.2	40.8	1206	2078	-9.3	19.6	25	-12	-310.4	1794.5	-442.6	-74.8	35.3
8TH	100.52	-10.4	41.5	1206	2078	-8.7	20.0	25	-11	-299.9	1752.9	-419.7	-70.9	34.5
9TH	113.44	-9.6	42.2	1206	2078	-8.0	20.3	26	-10	-290.3	1710.8	-397.3	-67.1	33.7
10TH	126.27	-8.8	42.6	1197	2063	-7.3	20.6	26	-9	-281.5	1668.2	-375.6	-63.4	32.8
11TH	139.10	-8.2	43.2	1197	2063	-6.8	21.0	26	-8	-273.4	1625.0	-354.5	-59.9	31.9
12TH	151.93	-8.2	44.0	1197	2063	-6.9	21.3	26	-8	-265.2	1581.0	-333.9	-56.4	31.1
13TH	164.76	-8.3	44.7	1197	2063	-6.9	21.7	25	-8	-256.9	1536.3	-313.9	-53.1	30.2
14TH	177.59	-8.3	45.5	1197	2063	-7.0	22.0	25	-8	-248.6	1490.8	-294.5	-49.8	29.3
15TH	190.42	-8.4	46.2	1197	2063	-7.0	22.4	24	-7	-240.2	1444.6	-275.7	-46.7	28.5
16TH	203.25	-8.4	46.9	1197	2063	-7.1	22.8	23	-7	-231.7	1397.6	-257.4	-43.6	27.6
17TH	216.08	-7.7	47.7	1197	2063	-6.5	23.1	24	-7	-224.0	1350.0	-239.8	-40.7	26.7
18TH	228.66	-7.6	46.9	1174	2023	-6.4	23.2	25	-7	-216.4	1303.0	-223.1	-38.0	25.8
19TH	241.24	-7.7	46.9	1174	2023	-6.6	23.2	25	-7	-208.7	1256.1	-207.0	-35.3	24.9
20TH	253.82	-7.8	46.9	1174	2023	-6.7	23.2	25	-7	-200.9	1209.2	-191.5	-32.7	24.0
21ST	266.40	-8.0	46.9	1174	2023	-6.8	23.2	26	-7	-192.9	1162.3	-176.6	-30.2	23.1
22ND	278.98	-8.1	46.9	1174	2023	-6.9	23.2	26	-8	-184.8	1115.4	-162.3	-27.8	22.1
23RD	291.56	-8.3	46.9	1174	2023	-7.0	23.2	26	-8	-176.5	1068.5	-148.5	-25.6	21.2
24TH	304.14	-8.3	47.0	1174	2023	-7.1	23.2	26	-8	-168.3	1021.5	-135.4	-23.4	20.2
25TH	316.72	-8.2	47.2	1174	2023	-7.0	23.3	26	-8	-160.1	974.3	-122.8	-21.3	19.3
		-7.9	46.4	1151	1983	-6.9	23.4	26	-8					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 100 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-152.2	927.9	-111.1	-19.4	18.3
27TH	341.38	-7.8	46.6	1151	1983	-6.8	23.5	26	-7	-144.4	881.3	-100.0	-17.6	17.4
28TH	353.71	-7.7	46.8	1151	1983	-6.7	23.6	26	-7	-136.7	834.5	-89.4	-15.9	16.5
29TH	366.04	-7.6	46.9	1151	1983	-6.6	23.7	25	-7	-129.0	787.5	-79.4	-14.2	15.5
30TH	378.12	-6.7	46.2	1127	1943	-6.0	23.8	26	-7	-122.3	741.4	-70.2	-12.7	14.6
31ST	390.20	-6.3	46.4	1127	1943	-5.6	23.9	27	-6	-116.0	695.0	-61.5	-11.3	13.6
32ND	402.28	-6.4	46.7	1127	1943	-5.7	24.0	27	-6	-109.6	648 3	-53.4	-9.9	12.6
33RD	414.36	-6.5	46.9	1127	1943	-5.8	24.2	27	-6	-103.0	601.4	-45.8	-8.6	11.6
34TH	426.44	-6.6	47.2	1127	1943	-5.9	24.3	27	-6	-96.4	554.2	-38.8	-7.4	10.6
35TH	438.52	-6.7	47.5	1127	1943	-6.0	24.4	27	-6	-89.7	506.7	-32.4	-6.3	9.6
36TH	450.60	-6.8	47.7	1127	1943	-6.1	24.6	26	-6	-82.8	459.0	-26.6	-5.2	8.7
37TH	462.68	-6.9	48.0	1127	1943	-6.1	24.7	26	-6	-75.9	411.0	-21.3	-4.3	7.7
38TH	474.76	-7.3	48.1	1127	1943	-6.5	24.8	26	-7	-68.6	362.9	-16.7	-3.4	6.7
39TH	486.84	-7.7	48.1	1127	1943	-6.9	24.7	25	-7	-60.9	314.8	-12.6	-2.6	5.7
40TH	498.92	-8.2	48.1	1127	1943	-7.3	24.7	25	-7	-52.7	266.7	-9.1	-1.9	4.8
41ST	511.00	-8.6	48.1	1127	1943	-7.7	24.7	24	-7	-44.0	218.6	-6.1	-1.4	3.9
42ND	523.08	-9.1	48.1	1127	1943	-8.0	24.7	23	-8	-35.0	170.6	-3.8	-.9	3.1
43RD	535.66	-9.6	50.1	1174	2023	-8.2	24.7	23	-8	-25.4	120.5	-2.0	-.5	2.2
44TH	548.58	-9.2	50.4	1206	2078	-7.6	24.3	23	-7	-16.2	70.1	-.7	-.2	1.2
MR	566.58	-10.8	64.7	1680	2895	-6.4	22.4	20	-6	-5.4	5.4	-.0	-.0	.3
TOP	581.67	-5.4	5.4	1085	2065	-5.0	2.6	****	6269	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 110 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									13.5	2293.8	-693.9	42.8	31.7
2ND	23.00	-29.2	73.8	2147	3699	-13.6	20.0	27	-18	42.7	2219.9	-641.9	42.1	30.3
3RD	35.92	-13.7	42.5	1206	2078	-11.4	20.5	18	-10	56.4	2177.4	-613.5	41.5	29.8
4TH	48.84	-11.5	41.6	1206	2078	-9.6	20.0	16	-8	67.9	2135.8	-585.7	40.7	29.3
5TH	61.76	-10.1	41.6	1206	2078	-8.4	20.0	17	-7	78.0	2094.2	-558.3	39.7	28.8
6TH	74.68	-8.8	42.7	1206	2078	-7.3	20.6	17	-6	86.8	2051.4	-531.6	38.7	28.2
7TH	87.60	-7.5	43.9	1206	2078	-6.2	21.1	17	-5	94.2	2007.6	-505.3	37.5	27.6
8TH	100.52	-6.2	45.0	1206	2078	-5.1	21.7	17	-4	100.4	1962.6	-479.7	36.2	27.0
9TH	113.44	-4.9	46.1	1206	2078	-4.1	22.2	17	-3	105.3	1916.5	-454.6	34.9	26.4
10TH	126.27	-3.6	46.9	1197	2063	-3.0	22.7	18	-2	108.9	1869.6	-430.4	33.5	25.7
11TH	139.10	-2.5	47.9	1197	2063	-2.1	23.2	18	-2	111.4	1821.7	-406.7	32.1	25.1
12TH	151.93	-2.2	48.1	1197	2063	-1.8	23.3	18	-1	113.6	1773.6	-383.6	30.7	24.4
13TH	164.76	-1.9	48.3	1197	2063	-1.6	23.4	18	-1	115.5	1725.3	-361.2	29.2	23.7
14TH	177.59	-1.6	48.6	1197	2063	-1.3	23.5	17	-1	117.0	1676.7	-339.3	27.7	23.0
15TH	190.42	-1.3	48.8	1197	2063	-1.1	23.6	17	-1	118.3	1627.9	-318.1	26.2	22.3
16TH	203.25	-1.0	49.0	1197	2063	-.8	23.7	17	-1	119.2	1578.9	-297.6	24.7	21.7
17TH	216.08	1.0	49.2	1197	2063	.8	23.9	19	1	118.3	1529.7	-277.6	23.2	20.9
18TH	228.66	1.5	48.7	1174	2023	1.3	24.1	19	1	116.8	1481.0	-258.7	21.7	20.2
19TH	241.24	1.8	49.2	1174	2023	1.6	24.3	19	1	114.9	1431.8	-240.4	20.2	19.4
20TH	253.82	2.1	49.7	1174	2023	1.8	24.6	19	1	112.8	1382.1	-222.7	18.8	18.7
21ST	266.40	2.4	50.2	1174	2023	2.1	24.8	19	2	110.3	1331.9	-205.6	17.4	17.9
22ND	278.98	2.8	50.7	1174	2023	2.3	25.1	19	2	107.6	1281.2	-189.2	16.0	17.1
23RD	291.56	3.1	51.2	1174	2023	2.6	25.3	19	2	104.5	1230.0	-173.4	14.7	16.4
24TH	304.14	3.3	51.8	1174	2023	2.8	25.6	18	2	101.2	1178.2	-158.2	13.4	15.6
25TH	316.72	3.5	52.3	1174	2023	2.9	25.8	18	2	97.8	1125.9	-143.7	12.1	14.9
		3.5	51.8	1151	1983	3.1	26.1	18	2					

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 110 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									94.2	1074.1	-130.2	10.9	14.1
		3.7	52.3	1151	1983	3.2	26.4	18	2					
27TH	341.38									90.6	1021.8	-117.2	9.8	13.4
		3.8	52.8	1151	1983	3.3	26.6	18	2					
28TH	353.71									86.8	969.0	-105.0	8.7	12.6
		3.9	53.3	1151	1983	3.4	26.9	18	2					
29TH	366.04									82.9	915.7	-93.3	7.7	11.9
		5.2	52.8	1127	1943	4.6	27.2	19	3					
30TH	378.12									77.7	863.0	-82.6	6.7	11.1
		5.9	53.1	1127	1943	5.3	27.3	20	4					
31ST	390.20									71.8	809.8	-72.5	5.8	10.3
		5.9	53.3	1127	1943	5.2	27.5	19	4					
32ND	402.28									65.9	756.5	-63.0	5.0	9.4
		5.9	53.6	1127	1943	5.2	27.6	19	4					
33RD	414.36									60.0	702.9	-54.2	4.2	8.6
		5.9	53.8	1127	1943	5.2	27.7	19	4					
34TH	426.44									54.1	649.1	-46.1	3.5	7.8
		5.9	54.1	1127	1943	5.2	27.8	19	3					
35TH	438.52									48.3	595.1	-38.5	2.9	7.0
		5.8	54.3	1127	1943	5.2	27.9	18	3					
36TH	450.60									42.4	540.8	-31.7	2.3	6.3
		5.8	54.5	1127	1943	5.2	28.1	18	3					
37TH	462.68									36.6	486.2	-25.5	1.9	5.5
		5.4	55.1	1127	1943	4.8	28.4	17	3					
38TH	474.76									31.2	431.2	-19.9	1.5	4.7
		4.9	55.7	1127	1943	4.3	28.7	16	2					
39TH	486.84									26.3	375.4	-15.1	1.1	4.0
		4.4	56.3	1127	1943	3.9	29.0	15	2					
40TH	498.92									22.0	319.1	-10.9	.8	3.3
		3.9	56.9	1127	1943	3.4	29.3	14	2					
41ST	511.00									18.1	262.2	-7.4	.6	2.7
		3.4	57.6	1127	1943	3.0	29.6	13	1					
42ND	523.08									14.8	204.6	-4.5	.4	2.1
		3.5	60.6	1174	2023	3.0	29.9	13	1					
43RD	535.66									11.2	144.0	-2.3	.2	1.4
		4.2	61.0	1206	2078	3.5	29.3	13	2					
44TH	548.58									7.0	83.1	-.9	.1	.8
		4.8	74.9	1680	2895	2.9	25.9	11	1					
MR	566.58									2.2	8.2	-.1	.0	.1
		2.2	8.2	1085	2065	2.0	4.0	24	11					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 120 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									281.5	2453.0	-748.5	122.1	21.6
2ND	23.00	-22.1	79.7	2147	3699	-10.3	21.5	16	-8	303.6	2373.3	-693.0	115.4	20.6
3RD	35.92	-10.3	46.5	1206	2078	-8.6	22.4	11	-4	313.9	2326.8	-662.7	111.4	20.2
4TH	48.84	-7.6	45.1	1206	2078	-6.3	21.7	12	-3	321.5	2281.7	-632.9	107.3	19.8
5TH	61.76	-5.2	44.6	1206	2078	-4.3	21.5	14	-3	326.7	2237.1	-603.7	103.1	19.3
6TH	74.68	-3.5	45.4	1206	2078	-2.9	21.8	14	-2	330.2	2191.7	-575.1	98.9	18.8
7TH	87.60	-1.8	46.2	1206	2078	-1.5	22.2	14	-1	332.0	2145.5	-547.1	94.6	18.3
8TH	100.52	-.1	46.9	1206	2078	-.1	22.6	15	-0	332.1	2098.6	-519.7	90.3	17.8
9TH	113.44	1.6	47.7	1206	2078	1.3	23.0	15	1	330.5	2050.9	-492.9	86.0	17.2
10TH	126.27	3.2	48.1	1197	2063	2.7	23.3	15	2	327.3	2002.7	-466.9	81.8	16.6
11TH	139.10	4.6	48.9	1197	2063	3.8	23.7	15	2	322.7	1953.8	-441.5	77.6	16.0
12TH	151.93	4.8	49.5	1197	2063	4.0	24.0	15	2	317.9	1904.3	-416.7	73.5	15.4
13TH	164.76	5.0	50.2	1197	2063	4.1	24.3	14	2	312.9	1854.1	-392.6	69.5	14.9
14TH	177.59	5.1	50.9	1197	2063	4.3	24.7	14	2	307.8	1803.2	-369.2	65.5	14.3
15TH	190.42	5.3	51.6	1197	2063	4.4	25.0	13	2	302.5	1751.6	-346.3	61.6	13.8
16TH	203.25	5.5	52.2	1197	2063	4.6	25.3	12	2	297.0	1699.4	-324.2	57.7	13.3
17TH	216.08	7.5	52.9	1197	2063	6.3	25.6	14	3	289.4	1646.5	-302.7	54.0	12.7
18TH	228.66	7.9	52.3	1174	2023	6.8	25.8	15	4	281.5	1594.2	-282.4	50.4	12.1
19TH	241.24	8.2	52.6	1174	2023	7.0	26.0	15	4	273.3	1541.7	-262.6	46.9	11.5
20TH	253.82	8.4	52.9	1174	2023	7.2	26.1	15	4	264.9	1488.8	-243.6	43.5	10.9
21ST	266.40	8.7	53.2	1174	2023	7.4	26.3	15	4	256.2	1435.7	-225.2	40.2	10.3
22ND	278.98	8.9	53.5	1174	2023	7.6	26.4	15	4	247.3	1382.2	-207.5	37.1	9.7
23RD	291.56	9.2	53.8	1174	2023	7.8	26.6	15	4	238.1	1328.4	-190.4	34.0	9.0
24TH	304.14	9.4	54.1	1174	2023	8.0	26.8	15	4	228.7	1274.3	-174.0	31.1	8.4
25TH	316.72	9.5	54.6	1174	2023	8.1	27.0	14	4	219.2	1219.7	-158.3	28.2	7.8
		9.4	54.0	1151	1983	8.1	27.2	13	4					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 120 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									209.9	1165.7	-143.6	25.6	7.3
27TH	341.38	9.5	54.4	1151	1983	8.2	27.5	12	4	200.4	1111.2	-129.6	23.1	6.8
28TH	353.71	9.6	54.9	1151	1983	8.3	27.7	11	3	190.8	1056.3	-116.2	20.7	6.3
29TH	366.04	9.6	55.4	1151	1983	8.4	27.9	10	3	181.2	1001.0	-103.6	18.4	5.9
30TH	378.12	10.8	54.7	1127	1943	9.6	28.1	11	4	170.4	946.3	-91.8	16.2	5.4
31ST	390.20	11.5	55.4	1127	1943	10.2	28.5	11	4	158.9	890.9	-80.7	14.3	4.9
32ND	402.28	11.4	56.2	1127	1943	10.1	28.9	11	4	147.5	834.7	-70.3	12.4	4.5
33RD	414.36	11.3	57.1	1127	1943	10.0	29.4	10	3	136.2	777.6	-60.5	10.7	4.0
34TH	426.44	11.2	57.9	1127	1943	9.9	29.8	10	3	125.0	719.7	-51.5	9.1	3.6
35TH	438.52	11.1	58.8	1127	1943	9.8	30.3	9	3	114.0	660.9	-43.2	7.7	3.2
36TH	450.60	10.9	59.6	1127	1943	9.7	30.7	9	3	103.1	601.2	-35.5	6.4	2.8
37TH	462.68	10.8	60.5	1127	1943	9.6	31.1	9	3	92.3	540.8	-28.6	5.2	2.4
38TH	474.76	10.5	61.1	1127	1943	9.3	31.4	8	2	81.7	479.7	-22.5	4.1	2.0
39TH	486.84	10.2	61.6	1127	1943	9.1	31.7	7	2	71.5	418.2	-17.0	3.2	1.6
40TH	498.92	9.9	62.0	1127	1943	8.8	31.9	7	2	61.6	356.1	-12.4	2.4	1.3
41ST	511.00	9.6	62.5	1127	1943	8.6	32.2	6	2	51.9	293.6	-8.4	1.7	1.0
42ND	523.08	9.3	63.0	1127	1943	8.3	32.4	5	1	42.6	230.5	-5.3	1.1	.7
43RD	535.66	10.0	66.2	1174	2023	8.5	32.7	5	1	32.5	164.3	-2.8	.7	.5
44TH	548.58	11.1	66.7	1206	2078	9.2	32.1	5	2	21.5	97.6	-1.1	.3	.2
MR	566.58	13.9	83.7	1680	2895	8.3	28.9	3	1	7.6	13.9	-.1	.1	-.0
TOP	581.67	7.6	13.9	1085	2065	7.0	6.7	-2	-2	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 130 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									334.6	2144.7	-668.8	118.9	15.4
2ND	23.00	-11.3	66.9	2147	3699	-5.3	18.1	17	-5	345.9	2077.7	-620.2	111.1	14.5
3RD	35.92	-4.8	39.2	1206	2078	-3.9	18.9	11	-2	350.6	2038.6	-593.7	106.6	14.1
4TH	48.84	-2.7	38.2	1206	2078	-2.3	18.4	12	-1	353.4	2000.4	-567.6	102.1	13.8
5TH	61.76	-.6	37.8	1206	2078	-.5	18.2	13	-0	354.0	1962.6	-542.0	97.5	13.4
6TH	74.68	.9	38.3	1206	2078	.7	18.4	14	1	353.1	1924.3	-516.9	92.9	13.0
7TH	87.60	2.3	38.8	1206	2078	1.9	18.7	15	2	350.7	1885.6	-492.2	88.4	12.5
8TH	100.52	3.8	39.2	1206	2078	3.2	18.9	15	3	346.9	1846.3	-468.1	83.9	12.0
9TH	113.44	5.3	39.7	1206	2078	4.4	19.1	16	4	341.6	1806.6	-444.5	79.4	11.5
10TH	126.27	6.7	39.9	1197	2063	5.6	19.3	17	5	334.9	1766.7	-421.6	75.1	11.0
11TH	139.10	7.9	40.4	1197	2063	6.6	19.6	18	6	327.0	1726.2	-399.2	70.8	10.5
12TH	151.93	7.9	41.0	1197	2063	6.6	19.9	17	5	319.2	1685.2	-377.3	66.7	9.9
13TH	164.76	7.8	41.6	1197	2063	6.5	20.1	15	5	311.3	1643.6	-356.0	62.7	9.4
14TH	177.59	7.8	42.1	1197	2063	6.5	20.4	15	5	303.5	1601.5	-335.2	58.7	9.0
15TH	190.42	7.8	42.7	1197	2063	6.5	20.7	14	4	295.7	1558.8	-314.9	54.9	8.5
16TH	203.25	7.8	43.3	1197	2063	6.5	21.0	13	4	287.9	1515.6	-295.2	51.1	8.1
17TH	216.08	9.6	43.8	1197	2063	8.0	21.2	15	5	278.2	1471.7	-276.0	47.5	7.6
18TH	228.66	9.9	43.6	1174	2023	8.5	21.5	15	6	268.3	1428.2	-257.8	44.1	7.1
19TH	241.24	10.1	44.1	1174	2023	8.6	21.8	14	6	258.2	1384.0	-240.1	40.7	6.6
20TH	253.82	10.3	44.7	1174	2023	8.7	22.1	14	5	248.0	1339.3	-222.9	37.6	6.2
21ST	266.40	10.4	45.3	1174	2023	8.9	22.4	14	5	237.5	1294.0	-206.4	34.5	5.7
22ND	278.98	10.6	45.9	1174	2023	9.0	22.7	13	5	226.9	1248.1	-190.4	31.6	5.2
23RD	291.56	10.8	46.5	1174	2023	9.2	23.0	13	5	216.2	1201.6	-175.0	28.8	4.8
24TH	304.14	10.8	47.1	1174	2023	9.2	23.3	13	5	205.4	1154.5	-160.2	26.1	4.3
25TH	316.72	10.5	47.7	1174	2023	8.9	23.6	11	4	194.9	1106.8	-145.9	23.6	3.9
		10.0	47.3	1151	1983	8.7	23.9	10	4					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 130 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									184.9	1059.5	-132.6	21.3	3.5
		9.7	47.8	1151	1983	8.5	24.1	9	3					
27TH	341.38									175.2	1011.6	-119.8	19.1	3.2
		9.5	48.4	1151	1983	8.2	24.4	8	3					
28TH	353.71									165.7	963.2	-107.6	17.0	2.9
		9.2	48.9	1151	1983	8.0	24.7	7	2					
29TH	366.04									156.5	914.3	-96.1	15.0	2.6
		10.0	48.5	1127	1943	8.8	25.0	8	3					
30TH	378.12									146.6	865.8	-85.3	13.1	2.3
		10.6	49.2	1127	1943	9.4	25.3	8	3					
31ST	390.20									136.0	816.6	-75.1	11.4	2.0
		10.5	50.1	1127	1943	9.3	25.8	7	3					
32ND	402.28									125.5	766.4	-65.6	9.9	1.7
		10.5	51.0	1127	1943	9.3	26.3	7	2					
33RD	414.36									115.0	715.4	-56.6	8.4	1.5
		10.4	51.9	1127	1943	9.3	26.7	6	2					
34TH	426.44									104.6	663.5	-48.3	7.1	1.2
		10.4	52.8	1127	1943	9.2	27.2	6	2					
35TH	438.52									94.2	610.7	-40.6	5.9	1.0
		10.4	53.7	1127	1943	9.2	27.6	6	2					
36TH	450.60									83.8	557.0	-33.6	4.8	.7
		10.3	54.6	1127	1943	9.1	28.1	5	2					
37TH	462.68									73.5	502.4	-27.2	3.9	.5
		9.7	55.2	1127	1943	8.6	28.4	4	1					
38TH	474.76									63.8	447.2	-21.4	3.0	.3
		9.2	55.9	1127	1943	8.1	28.8	4	1					
39TH	486.84									54.6	391.3	-16.4	2.3	.2
		8.6	56.5	1127	1943	7.6	29.1	3	1					
40TH	498.92									46.1	334.9	-12.0	1.7	.0
		8.0	57.1	1127	1943	7.1	29.4	2	1					
41ST	511.00									38.1	277.7	-8.3	1.2	-.1
		7.4	57.7	1127	1943	6.6	29.7	1	0					
42ND	523.08									30.7	220.0	-5.3	.8	-.1
		7.7	60.8	1174	2023	6.6	30.0	1	0					
43RD	535.66									22.9	159.2	-2.9	.4	-.2
		8.5	61.5	1206	2078	7.1	29.6	1	0					
44TH	548.58									14.4	97.8	-1.2	.2	-.2
		10.1	77.5	1680	2895	6.0	26.8	-1	-0					
MR	566.58									4.3	20.3	-.2	.0	-.2
		4.3	20.3	1085	2065	4.0	9.8	-12	-4					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 140 CONFIGURATION A REFERENCE PRESSURE 34 0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									163.5	1700.2	-563.9	76.7	10.0
2ND	23.00	-16.4	46.9	2147	3699	-7.6	12.7	24	-14	179.9	1653.4	-525.3	72.7	9.2
3RD	35.92	-7.8	26.9	1206	2078	-6.5	12.9	16	-8	187.8	1626.5	-504.1	70.4	8.9
4TH	48.84	-5.8	25.9	1206	2078	-4.8	12.5	16	-6	193.6	1600.6	-483.3	67.9	8.6
5TH	61.76	-4.2	25.6	1206	2078	-3.5	12.3	17	-5	197.8	1575.0	-462.8	65.4	8.3
6TH	74.68	-3.3	26.0	1206	2078	-2.7	12.5	18	-4	201.1	1549.0	-442.6	62.8	7.9
7TH	87.60	-2.4	26.5	1206	2078	-2.0	12.7	18	-3	203.5	1522.5	-422.8	60.2	7.5
8TH	100.52	-1.5	26.9	1206	2078	-1.2	12.9	19	-2	205.0	1495.6	-403.3	57.5	7.1
9TH	113.44	-.5	27.3	1206	2078	-.4	13.2	20	-1	205.5	1468.3	-384.1	54.9	6.7
10TH	126.27	.4	27.6	1197	2063	.3	13.4	21	0	205.1	1440.7	-365.4	52.2	6.2
11TH	139.10	1.2	28.0	1197	2063	1.0	13.6	21	1	203.9	1412.7	-347.1	49.6	5.7
12TH	151.93	1.4	28.4	1197	2063	1.2	13.7	20	2	202.5	1384.3	-329.2	47.0	5.3
13TH	164.76	1.7	28.7	1197	2063	1.4	13.9	19	2	200.8	1355.6	-311.6	44.4	4.9
14TH	177.59	1.9	29.1	1197	2063	1.6	14.1	17	2	198.9	1326.5	-294.4	41.9	4.5
15TH	190.42	2.2	29.4	1197	2063	1.8	14.2	16	2	196.7	1297.1	-277.6	39.3	4.1
16TH	203.25	2.5	29.7	1197	2063	2.0	14.4	15	2	194.3	1267.4	-261.1	36.8	3.7
17TH	216.08	4.0	30.1	1197	2063	3.3	14.6	17	4	190.2	1237.3	-245.1	34.4	3.3
18TH	228.66	4.7	30.2	1174	2023	4.0	14.9	16	4	185.5	1207.1	-229.7	32.0	3.0
19TH	241.24	5.3	31.0	1174	2023	4.5	15.3	15	4	180.2	1176.1	-214.7	29.7	2.6
20TH	253.82	5.9	31.8	1174	2023	5.0	15.7	15	5	174.3	1144.2	-200.1	27.5	2.2
21ST	266.40	6.5	32.7	1174	2023	5.6	16.1	14	5	167.8	1111.6	-185.9	25.3	1.9
22ND	278.98	7.1	33.5	1174	2023	6.1	16.5	13	5	160.7	1078.1	-172.1	23.2	1.6
23RD	291.56	7.7	34.3	1174	2023	6.6	16.9	12	5	152.9	1043.8	-158.8	21.3	1.2
24TH	304.14	7.9	35.1	1174	2023	6.8	17.4	11	4	145.0	1008.7	-145.9	19.4	.9
25TH	316.72	7.5	36.3	1174	2023	6.4	17.9	10	3	137.5	972.4	-133.4	17.6	.7
		7.0	36.7	1151	1983	6.1	18.5	8	3					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 140 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									130.5	935.7	-121.7	16.0	.4
		6.6	37.8	1151	1983	5.7	19.1	7	2					
27TH	341.38									123.9	897.8	-110.4	14.4	.2
		6.2	39.0	1151	1983	5.4	19.7	6	2					
28TH	353.71									117.7	858.9	-99.5	12.9	.0
		5.8	40.1	1151	1983	5.1	20.2	5	1					
29TH	366.04									111.9	818.8	-89.2	11.5	-.1
		6.2	40.4	1127	1943	5.5	20.8	5	1					
30TH	378.12									105.7	778.4	-79.5	10.2	-.3
		6.7	41.3	1127	1943	5.9	21.3	5	1					
31ST	390.20									99.0	737.1	-70.4	8.9	-.4
		6.7	42.3	1127	1943	5.9	21.8	4	1					
32ND	402.28									92.3	694.8	-61.7	7.8	-.6
		6.7	43.3	1127	1943	6.0	22.3	3	1					
33RD	414.36									85.6	651.5	-53.6	6.7	-.7
		6.8	44.3	1127	1943	6.0	22.8	3	1					
34TH	426.44									78.8	607.2	-46.0	5.7	-.8
		6.8	45.3	1127	1943	6.0	23.3	2	1					
35TH	438.52									72.0	562.0	-38.9	4.8	-.9
		6.8	46.2	1127	1943	6.1	23.8	2	0					
36TH	450.60									65.2	515.7	-32.4	4.0	-.9
		6.9	47.2	1127	1943	6.1	24.3	1	0					
37TH	462.68									58.3	468.5	-26.5	3.2	-1.0
		6.7	48.2	1127	1943	5.9	24.8	0	0					
38TH	474.76									51.6	420.4	-21.1	2.6	-1.0
		6.5	49.1	1127	1943	5.8	25.3	-0	-0					
39TH	486.84									45.1	371.3	-16.3	2.0	-1.0
		6.3	50.0	1127	1943	5.6	25.7	-1	-0					
40TH	498.92									38.8	321.3	-12.2	1.5	-.9
		6.1	50.9	1127	1943	5.4	26.2	-2	-0					
41ST	511.00									32.7	270.4	-8.6	1.0	-.8
		5.9	51.8	1127	1943	5.2	26.7	-3	-1					
42ND	523.08									26.8	218.6	-5.6	.7	-.7
		6.4	54.9	1174	2023	5.5	27.1	-3	-1					
43RD	535.66									20.4	163.7	-3.2	.4	-.6
		7.4	56.6	1206	2078	6.1	27.3	-3	-1					
44TH	548.58									13.0	107.0	-1.5	.2	-.5
		9.5	76.1	1680	2895	5.7	26.3	-2	-0					
MR	566.58									3.5	30.9	-.2	.0	-.3
		3.5	30.9	1085	2065	3.2	15.0	-13	-3					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 150 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									133.3	1169.2	-408.2	69.1	2.4
2ND	23.00	-10.0	25.2	2147	3699	-4.6	6.8	31	-21	143.3	1143.9	-381.6	65.9	1.9
3RD	35.92	-4.9	15.1	1206	2078	-4.1	7.3	19	-10	148.2	1128.8	-366.9	64.0	1.7
4TH	48.84	-4.3	14.3	1206	2078	-3.6	6.9	16	-8	152.5	1114.5	-352.4	62.1	1.5
5TH	61.76	-3.8	13.9	1206	2078	-3.2	6.7	17	-8	156.4	1100.5	-338.1	60.1	1.3
6TH	74.68	-3.3	14.1	1206	2078	-2.8	6.8	18	-7	159.7	1086.5	-324.0	58.0	1.1
7TH	87.60	-2.8	14.2	1206	2078	-2.3	6.8	20	-7	162.5	1072.2	-310.0	55.9	.9
8TH	100.52	-2.3	14.3	1206	2078	-1.9	6.9	22	-6	164.8	1057.9	-296.3	53.8	.7
9TH	113.44	-1.8	14.5	1206	2078	-1.5	7.0	23	-5	166.6	1043.4	-282.7	51.7	.4
10TH	126.27	-1.3	14.5	1197	2063	-1.1	7.0	25	-4	167.9	1028.9	-269.4	49.5	.1
11TH	139.10	-.8	14.8	1197	2063	-.7	7.2	26	-2	168.7	1014.1	-256.3	47.4	-.2
12TH	151.93	-.5	15.5	1197	2063	-.4	7.5	22	-1	169.1	998.6	-243.4	45.2	-.5
13TH	164.76	-.2	16.3	1197	2063	-.1	7.9	19	-0	169.3	982.4	-230.7	43.0	-.7
14TH	177.59	.1	17.0	1197	2063	.1	8.2	17	0	169.2	965.4	-218.2	40.9	-1.0
15TH	190.42	.4	17.8	1197	2063	.4	8.6	14	1	168.7	947.6	-205.9	38.7	-1.2
16TH	203.25	.8	18.5	1197	2063	.6	9.0	12	1	168.0	929.1	-193.9	36.5	-1.3
17TH	216.08	1.8	19.2	1197	2063	1.5	9.3	12	2	166.2	909.9	-182.1	34.4	-1.5
18TH	228.66	2.3	19.9	1174	2023	2.0	9.8	11	2	163.8	890.0	-170.8	32.3	-1.7
19TH	241.24	2.8	21.0	1174	2023	2.4	10.4	9	2	161.0	869.0	-159.7	30.3	-1.8
20TH	253.82	3.3	22.1	1174	2023	2.8	10.9	8	2	157.7	846.9	-148.9	28.3	-2.0
21ST	266.40	3.8	23.2	1174	2023	3.2	11.5	6	2	153.9	823.7	-138.4	26.3	-2.1
22ND	278.98	4.3	24.3	1174	2023	3.6	12.0	5	2	149.7	799.5	-128.2	24.4	-2.2
23RD	291.56	4.7	25.4	1174	2023	4.0	12.5	4	1	145.0	774.1	-118.3	22.6	-2.3
24TH	304.14	5.0	26.3	1174	2023	4.3	13.0	3	1	139.9	747.8	-108.7	20.8	-2.3
25TH	316.72	5.0	27.1	1174	2023	4.2	13.4	2	1	135.0	720.7	-99.5	19.0	-2.4
		4.8	27.3	1151	1983	4.2	13.8	1	0					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 150 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05	4.8	28.0	1151	1983	4.1	14.1	-0	-0	130.2	693.4	-90.8	17.4	-2.4
27TH	341.38	4.7	28.7	1151	1983	4.1	14.5	-1	-0	125.4	665.4	-82.4	15.8	-2.4
28TH	353.71	4.6	29.5	1151	1983	4.0	14.9	-2	-1	120.7	636.7	-74.4	14.3	-2.4
29TH	366.04	5.2	29.6	1127	1943	4.6	15.2	-2	-1	116.1	607.2	-66.7	12.8	-2.3
30TH	378.12	5.7	30.2	1127	1943	5.1	15.6	-2	-1	110.8	577.7	-59.5	11.5	-2.3
31ST	390.20	5.9	31.0	1127	1943	5.2	15.9	-3	-1	105.1	547.4	-52.7	10.2	-2.2
32ND	402.28	6.0	31.7	1127	1943	5.4	16.3	-3	-1	99.2	516.4	-46.3	8.9	-2.1
33RD	414.36	6.2	32.5	1127	1943	5.5	16.7	-3	-1	93.1	484.7	-40.3	7.8	-2.1
34TH	426.44	6.3	33.2	1127	1943	5.6	17.1	-4	-1	87.0	452.3	-34.6	6.7	-2.0
35TH	438.52	6.5	33.9	1127	1943	5.7	17.5	-4	-1	80.6	419.1	-29.3	5.7	-1.9
36TH	450.60	6.6	34.7	1127	1943	5.9	17.8	-5	-1	74.2	385.1	-24.5	4.7	-1.8
37TH	462.68	6.7	35.4	1127	1943	6.0	18.2	-5	-2	67.5	350.5	-20.0	3.9	-1.7
38TH	474.76	6.8	36.2	1127	1943	6.1	18.6	-5	-2	60.8	315.1	-16.0	3.1	-1.5
39TH	486.84	6.9	36.9	1127	1943	6.1	19.0	-6	-2	54.0	278.9	-12.4	2.4	-1.4
40TH	498.92	7.0	37.7	1127	1943	6.2	19.4	-6	-2	47.0	241.9	-9.3	1.8	-1.2
41ST	511.00	7.1	38.4	1127	1943	6.3	19.8	-6	-2	40.0	204.2	-6.6	1.3	-1.0
42ND	523.08	8.0	40.8	1174	2023	6.8	20.2	-6	-2	32.9	165.8	-4.4	.8	-.9
43RD	535.66	9.0	42.1	1206	2078	7.5	20.3	-5	-2	24.9	125.0	-2.5	.5	-.7
44TH	548.58	11.5	56.3	1680	2895	6.9	19.4	-5	-2	15.9	82.9	-1.2	.2	-.5
MR	566.58	4.4	26.6	1085	2065	4.0	12.9	-14	-4	4.4	26.6	-.2	.0	-.3
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 160 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									168.4	724.7	-273.6	69.5	-2.2
2ND	23.00	-4.6	11.5	2147	3699	-2.1	3.1	34	-23	173.0	713.1	-257.0	65.6	-2.4
3RD	35.92	-2.2	6.6	1206	2078	-1.8	3.2	18	-10	175.1	706.5	-247.9	63.4	-2.5
4TH	48.84	-1.4	6.5	1206	2078	-1.1	3.1	13	-5	176.5	700.0	-238.8	61.1	-2.6
5TH	61.76	-.8	6.4	1206	2078	-.6	3.1	13	-3	177.3	693.6	-229.8	58.8	-2.6
6TH	74.68	-.5	6.1	1206	2078	-.4	2.9	15	-2	177.8	687.5	-220.9	56.5	-2.7
7TH	87.60	-.2	5.9	1206	2078	-.2	2.8	18	-1	178.0	681.6	-212.0	54.2	-2.8
8TH	100.52	.0	5.6	1206	2078	.0	2.7	21	0	178.0	675.9	-203.2	51.9	-2.9
9TH	113.44	.3	5.4	1206	2078	.2	2.6	25	2	177.7	670.5	-194.5	49.6	-3.0
10TH	126.27	.5	5.1	1197	2063	.4	2.5	29	5	177.2	665.4	-186.0	47.3	-3.1
11TH	139.10	.8	5.0	1197	2063	.7	2.4	31	9	176.4	660.4	-177.5	45.1	-3.2
12TH	151.93	1.2	5.7	1197	2063	1.0	2.8	25	9	175.2	654.7	-169.0	42.8	-3.3
13TH	164.76	1.6	6.4	1197	2063	1.3	3.1	20	8	173.6	648.3	-160.7	40.6	-3.4
14TH	177.59	2.0	7.0	1197	2063	1.7	3.4	15	7	171.6	641.3	-152.4	38.4	-3.5
15TH	190.42	2.4	7.7	1197	2063	2.0	3.7	12	6	169.2	633.6	-144.2	36.2	-3.6
16TH	203.25	2.8	8.4	1197	2063	2.3	4.1	8	5	166.4	625.2	-136.1	34.0	-3.6
17TH	216.08	3.9	9.0	1197	2063	3.3	4.4	11	8	162.5	616.2	-128.2	31.9	-3.7
18TH	228.66	4.2	9.8	1174	2023	3.6	4.8	8	6	158.3	606.4	-120.5	29.9	-3.7
19TH	241.24	4.4	10.7	1174	2023	3.8	5.3	4	3	153.9	595.7	-112.9	27.9	-3.8
20TH	253.82	4.6	11.6	1174	2023	3.9	5.8	1	1	149.2	584.1	-105.5	26.0	-3.8
21ST	266.40	4.8	12.6	1174	2023	4.1	6.2	-2	-1	144.4	571.5	-98.2	24.2	-3.8
22ND	278.98	5.1	13.5	1174	2023	4.3	6.7	-4	-2	139.3	558.0	-91.1	22.4	-3.7
23RD	291.56	5.3	14.5	1174	2023	4.5	7.2	-6	-4	134.1	543.5	-84.2	20.7	-3.7
24TH	304.14	5.3	15.4	1174	2023	4.5	7.6	-7	-4	128.7	528.1	-77.5	19.0	-3.6
25TH	316.72	5.2	16.6	1174	2023	4.4	8.2	-8	-4	123.6	511.5	-70.9	17.4	-3.5
		4.9	17.4	1151	1983	4.2	8.8	-9	-4					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 160 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
										118.7	494.2	-64.7	15.9	-3.4
26TH	329.05	4.7	18.5	1151	1983	4.1	9.3	-9	-4	114.0	475.7	-58.7	14.5	-3.3
27TH	341.38	4.5	19.6	1151	1983	3.9	9.9	-10	-4	109.5	456.1	-53.0	13.1	-3.1
28TH	353.71	4.4	20.7	1151	1983	3.8	10.4	-10	-4	105.1	435.4	-47.5	11.8	-3.0
29TH	366.04	4.5	21.4	1127	1943	4.0	11.0	-10	-4	100.6	414.0	-42.4	10.6	-2.8
30TH	378.12	4.9	22.0	1127	1943	4.3	11.3	-10	-4	95.7	392.0	-37.5	9.4	-2.6
31ST	390.20	5.1	22.5	1127	1943	4.5	11.6	-10	-4	90.7	369.5	-32.9	8.3	-2.4
32ND	402.28	5.2	23.0	1127	1943	4.7	11.9	-10	-4	85.4	346.5	-28.6	7.2	-2.3
33RD	414.36	5.4	23.5	1127	1943	4.8	12.1	-10	-4	80.0	322.9	-24.5	6.2	-2.1
34TH	426.44	5.6	24.0	1127	1943	5.0	12.4	-9	-4	74.4	298.9	-20.8	5.3	-1.9
35TH	438.52	5.8	24.5	1127	1943	5.2	12.6	-9	-4	68.5	274.3	-17.3	4.4	-1.8
36TH	450.60	6.0	25.0	1127	1943	5.3	12.9	-9	-4	62.6	249.3	-14.2	3.6	-1.6
37TH	462.68	6.1	25.5	1127	1943	5.4	13.1	-9	-4	56.4	223.8	-11.3	2.9	-1.4
38TH	474.76	6.3	26.0	1127	1943	5.6	13.4	-9	-4	50.1	197.8	-8.8	2.2	-1.2
39TH	486.84	6.5	26.5	1127	1943	5.7	13.6	-9	-4	43.6	171.3	-6.5	1.7	-1.1
40TH	498.92	6.6	27.0	1127	1943	5.9	13.9	-9	-4	37.0	144.3	-4.6	1.2	-.9
41ST	511.00	6.8	27.4	1127	1943	6.0	14.1	-9	-4	30.2	116.9	-3.0	.8	-.7
42ND	523.08	7.4	29.1	1174	2023	6.3	14.4	-9	-4	22.9	87.9	-1.8	.5	-.5
43RD	535.66	7.9	29.9	1206	2078	6.5	14.4	-7	-3	15.0	57.9	-.8	.2	-.3
44TH	548.58	10.5	40.1	1680	2895	6.2	13.9	-5	-2	4.5	17.8	-.1	.0	-.2
MR	566.58	4.5	17.8	1085	2065	4.2	8.6	-13	-6	0.0	0.0	0.0	0.0	0.0
TOP	581.67													

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 170 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									243.3	827.9	-311.7	84.5	-6.9
2ND	23.00	2.8	8.5	2147	3699	1.3	2.3	44	25	240.5	819.4	-292.8	79.0	-7.1
3RD	35.92	1.6	4.7	1206	2078	1.3	2.3	24	13	238.9	814.7	-282.2	75.9	-7.2
4TH	48.84	2.0	4.0	1206	2078	1.7	1.9	22	19	236.9	810.7	-271.7	72.8	-7.3
5TH	61.76	2.6	3.7	1206	2078	2.2	1.8	26	32	234.3	807.0	-261.2	69.8	-7.3
6TH	74.68	2.9	3.9	1206	2078	2.4	1.9	13	17	231.3	803.2	-250.8	66.8	-7.3
7TH	87.60	3.2	4.1	1206	2078	2.7	2.0	-3	-4	228.1	799.1	-240.5	63.8	-7.3
8TH	100.52	3.5	4.2	1206	2078	2.9	2.0	-23	-33	224.6	794.9	-230.2	60.9	-7.3
9TH	113.44	3.8	4.4	1206	2078	3.2	2.1	-50	-74	220.8	790.4	-220.0	58.0	-7.3
10TH	126.27	4.1	4.6	1197	2063	3.4	2.2	-89	-134	216.8	785.9	-209.8	55.2	-7.2
11TH	139.10	4.3	4.9	1197	2063	3.6	2.4	-89	-132	212.5	780.9	-199.8	52.4	-7.1
12TH	151.93	4.2	6.3	1197	2063	3.5	3.0	-38	-44	208.2	774.7	-189.8	49.7	-7.0
13TH	164.76	4.2	7.6	1197	2063	3.5	3.7	-29	-27	204.1	767.1	-179.9	47.1	-6.9
14TH	177.59	4.1	8.9	1197	2063	3.4	4.3	-25	-20	200.0	758.2	-170.1	44.5	-6.7
15TH	190.42	4.0	10.2	1197	2063	3.4	4.9	-23	-15	196.0	748.0	-160.5	41.9	-6.6
16TH	203.25	4.0	11.5	1197	2063	3.3	5.6	-22	-13	192.0	736.5	-151.0	39.5	-6.4
17TH	216.08	4.3	12.8	1197	2063	3.6	6.2	-20	-11	187.7	723.6	-141.6	37.0	-6.2
18TH	228.66	4.4	14.0	1174	2023	3.8	6.9	-18	-10	183.3	709.6	-132.6	34.7	-6.0
19TH	241.24	4.5	15.5	1174	2023	3.8	7.6	-17	-8	178.7	694.2	-123.7	32.4	-5.8
20TH	253.82	4.6	16.9	1174	2023	3.9	8.4	-16	-7	174.1	677.2	-115.1	30.2	-5.6
21ST	266.40	4.7	18.4	1174	2023	4.0	9.1	-15	-7	169.4	658.9	-106.7	28.0	-5.4
22ND	278.98	4.8	19.8	1174	2023	4.1	9.8	-15	-6	164.5	639.0	-98.5	25.9	-5.2
23RD	291.56	4.9	21.3	1174	2023	4.2	10.5	-14	-6	159.6	617.8	-90.6	23.9	-5.0
24TH	304.14	5.1	22.4	1174	2023	4.4	11.1	-14	-5	154.5	595.3	-83.0	21.9	-4.8
25TH	316.72	5.4	23.3	1174	2023	4.6	11.5	-13	-5	149.1	572.1	-75.7	20.0	-4.5
		5.5	23.6	1151	1983	4.8	11.9	-13	-5					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 170 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									143.7	548.5	-68.8	18.2	-4.3
		5.7	24.4	1151	1983	5.0	12.3	-12	-5					
27TH	341.38									138.0	524.0	-62.1	16.5	-4.1
		5.9	25.2	1151	1983	5.2	12.7	-12	-5					
28TH	353.71									132.0	498.8	-55.8	14.8	-3.8
		6.2	26.0	1151	1983	5.3	13.1	-12	-5					
29TH	366.04									125.9	472.8	-49.9	13.2	-3.6
		6.4	26.3	1127	1943	5.7	13.5	-11	-4					
30TH	378.12									119.5	446.5	-44.3	11.7	-3.4
		6.7	26.6	1127	1943	5.9	13.7	-10	-4					
31ST	390.20									112.7	419.8	-39.1	10.3	-3.2
		6.9	26.7	1127	1943	6.1	13.8	-10	-5					
32ND	402.28									105.9	393.1	-34.2	9.0	-3.0
		7.1	26.8	1127	1943	6.3	13.8	-10	-5					
33RD	414.36									98.8	366.2	-29.6	7.8	-2.8
		7.3	26.9	1127	1943	6.5	13.9	-11	-5					
34TH	426.44									91.5	339.3	-25.3	6.6	-2.6
		7.5	27.0	1127	1943	6.6	13.9	-11	-5					
35TH	438.52									84.0	312.2	-21.4	5.6	-2.4
		7.7	27.1	1127	1943	6.8	14.0	-11	-5					
36TH	450.60									76.4	285.1	-17.8	4.6	-2.1
		7.8	27.2	1127	1943	6.9	14.0	-11	-5					
37TH	462.68									68.6	257.9	-14.5	3.7	-1.9
		7.8	27.4	1127	1943	6.9	14.1	-11	-5					
38TH	474.76									60.8	230.4	-11.5	2.9	-1.7
		7.8	27.6	1127	1943	6.9	14.2	-11	-5					
39TH	486.84									53.0	202.8	-8.9	2.2	-1.5
		7.7	27.8	1127	1943	6.9	14.3	-11	-5					
40TH	498.92									45.3	175.0	-6.6	1.7	-1.2
		7.7	28.0	1127	1943	6.8	14.4	-11	-5					
41ST	511.00									37.6	147.0	-4.7	1.2	-1.0
		7.7	28.2	1127	1943	6.8	14.5	-12	-5					
42ND	523.08									29.9	118.8	-3.1	.7	-.8
		8.0	29.6	1174	2023	6.8	14.6	-11	-5					
43RD	535.66									21.9	89.2	-1.8	.4	-.5
		8.1	30.3	1206	2078	6.7	14.6	-9	-4					
44TH	548.58									13.9	58.9	-.8	.2	-.3
		9.9	41.0	1680	2895	5.9	14.2	-5	-2					
MR	566.58									3.9	17.9	-.1	.0	-.2
		3.9	17.9	1085	2065	3.6	8.6	-12	-4					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 180 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									189.8	579.7	-229.2	69.3	-6.1
2ND	23.00	2.4	1.6	2147	3699	1.1	.4	-86	-221	187.4	578.1	-215.9	65.0	-6.3
3RD	35.92	1.4	.3	1206	2078	1.2	.1	-6	-49	186.0	577.8	-208.4	62.6	-6.3
4TH	48.84	1.5	.6	1206	2078	1.3	.3	-3	-12	184.4	577.2	-201.0	60.2	-6.3
5TH	61.76	1.8	.9	1206	2078	1.5	.4	2	8	182.7	576.3	-193.5	57.8	-6.3
6TH	74.68	1.9	.9	1206	2078	1.6	.5	5	18	180.7	575.4	-186.1	55.4	-6.3
7TH	87.60	2.1	1.0	1206	2078	1.7	.5	8	27	178.7	574.4	-178.7	53.1	-6.3
8TH	100.52	2.2	1.1	1206	2078	1.8	.5	10	34	176.4	573.3	-171.3	50.8	-6.3
9TH	113.44	2.4	1.2	1206	2078	2.0	.6	12	41	174.1	572.1	-163.9	48.6	-6.2
10TH	126.27	2.5	1.2	1197	2063	2.1	.6	13	47	171.5	570.9	-156.5	46.3	-6.2
11TH	139.10	2.6	1.5	1197	2063	2.2	.7	20	61	168.9	569.4	-149.2	44.2	-6.1
12TH	151.93	2.6	2.5	1197	2063	2.2	1.2	436	772	166.3	566.9	-141.9	42.0	-6.1
13TH	164.76	2.6	3.6	1197	2063	2.2	1.7	-71	-89	163.7	563.3	-134.7	39.9	-6.0
14TH	177.59	2.6	4.6	1197	2063	2.2	2.2	-46	-44	161.1	558.7	-127.5	37.8	-5.9
15TH	190.42	2.6	5.6	1197	2063	2.2	2.7	-38	-30	158.5	553.1	-120.3	35.8	-5.7
16TH	203.25	2.6	6.7	1197	2063	2.2	3.2	-34	-23	155.9	546.4	-113.3	33.7	-5.6
17TH	216.08	2.8	7.7	1197	2063	2.3	3.7	-31	-19	153.1	538.7	-106.3	31.8	-5.4
18TH	228.66	2.8	8.8	1174	2023	2.4	4.4	-27	-15	150.3	529.9	-99.6	29.9	-5.2
19TH	241.24	3.0	10.1	1174	2023	2.5	5.0	-24	-12	147.3	519.8	-93.0	28.0	-5.1
20TH	253.82	3.1	11.4	1174	2023	2.6	5.6	-21	-10	144.2	508.4	-86.5	26.1	-4.9
21ST	266.40	3.2	12.7	1174	2023	2.7	6.3	-20	-8	141.0	495.8	-80.2	24.4	-4.7
22ND	278.98	3.3	13.9	1174	2023	2.8	6.9	-18	-7	137.7	481.8	-74.1	22.6	-4.5
23RD	291.56	3.4	15.2	1174	2023	2.9	7.5	-17	-7	134.3	466.6	-68.1	20.9	-4.3
24TH	304.14	3.6	16.3	1174	2023	3.1	8.1	-17	-6	130.7	450.2	-62.3	19.2	-4.1
25TH	316.72	3.9	17.2	1174	2023	3.3	8.5	-17	-6	126.8	433.0	-56.8	17.6	-3.9
		4.1	17.8	1151	1983	3.6	9.0	-17	-6					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 180 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									122.7	415.3	-51.5	16.1	-3.7
		4.4	18.6	1151	1983	3.8	9.4	-17	-7					
27TH	341.38									118.4	396.6	-46.5	14.6	-3.4
		4.6	19.5	1151	1983	4.0	9.8	-17	-7					
28TH	353.71									113.7	377.2	-41.8	13.1	-3.2
		4.9	20.3	1151	1983	4.3	10.3	-16	-7					
29TH	366.04									108.9	356.8	-37.2	11.8	-2.9
		5.1	20.8	1127	1943	4.6	10.7	-14	-6					
30TH	378.12									103.7	336.0	-33.1	10.5	-2.7
		5.4	21.0	1127	1943	4.8	10.8	-13	-6					
31ST	390.20									98.3	315.1	-29.1	9.3	-2.5
		5.6	20.9	1127	1943	4.9	10.8	-12	-6					
32ND	402.28									92.7	294.2	-25.4	8.1	-2.3
		5.8	20.8	1127	1943	5.1	10.7	-12	-6					
33RD	414.36									87.0	273.4	-22.0	7.0	-2.1
		5.9	20.7	1127	1943	5.3	10.7	-11	-5					
34TH	426.44									81.0	252.6	-18.8	6.0	-2.0
		6.1	20.6	1127	1943	5.4	10.6	-11	-5					
35TH	438.52									74.9	232.0	-15.9	5.1	-1.8
		6.3	20.5	1127	1943	5.6	10.6	-10	-5					
36TH	450.60									68.6	211.5	-13.2	4.2	-1.7
		6.5	20.4	1127	1943	5.8	10.5	-9	-5					
37TH	462.68									62.1	191.0	-10.8	3.4	-1.5
		6.6	20.5	1127	1943	5.8	10.5	-10	-6					
38TH	474.76									55.5	170.6	-8.6	2.7	-1.4
		6.7	20.5	1127	1943	5.9	10.5	-11	-6					
39TH	486.84									48.8	150.1	-6.7	2.1	-1.2
		6.8	20.5	1127	1943	6.0	10.5	-12	-7					
40TH	498.92									42.0	129.6	-5.0	1.5	-1.0
		6.9	20.5	1127	1943	6.1	10.5	-13	-7					
41ST	511.00									35.1	109.2	-3.6	1.1	-.8
		7.0	20.5	1127	1943	6.2	10.5	-14	-8					
42ND	523.08									28.1	88.7	-2.4	.7	-.6
		7.5	21.3	1174	2023	6.4	10.5	-13	-8					
43RD	535.66									20.6	67.4	-1.4	.4	-.5
		7.8	22.0	1206	2078	6.5	10.6	-10	-6					
44TH	548.58									12.8	45.4	-.6	.2	-.3
		10.4	31.1	1680	2895	6.2	10.7	-6	-4					
MR	566.58									2.4	14.3	-.1	.0	-.2
		2.4	14.3	1085	2065	2.2	6.9	-15	-4					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 190 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									283.4	486.0	-206.0	108.3	-7.7
2ND	23.00	2.7	.6	2147	3699	1.3	.2	-16	-116	280.7	485.4	-194.8	101.8	-7.8
3RD	35.92	1.1	-.0	1206	2078	.9	-.0	0	-99	279.6	485.4	-188.6	98.2	-7.9
4TH	48.84	1.3	-.4	1206	2078	1.1	-.2	9	-50	278.3	485.8	-182.3	94.6	-7.9
5TH	61.76	1.6	-.6	1206	2078	1.4	-.3	4	-20	276.6	486.3	-176.0	91.0	-7.9
6TH	74.68	1.9	-.5	1206	2078	1.6	-.2	1	-5	274.8	486.8	-169.7	87.5	-7.9
7TH	87.60	2.1	-.4	1206	2078	1.8	-.2	-1	6	272.7	487.1	-163.4	83.9	-7.9
8TH	100.52	2.3	-.3	1206	2078	1.9	-.1	-1	14	270.3	487.4	-157.1	80.4	-7.9
9TH	113.44	2.6	-.1	1206	2078	2.1	-.1	-1	21	267.7	487.5	-150.8	76.9	-7.9
10TH	126.27	2.8	-.0	1197	2063	2.3	-.0	-0	26	264.9	487.6	-144.6	73.5	-7.9
11TH	139.10	3.0	.2	1197	2063	2.5	.1	1	32	261.9	487.4	-138.3	70.1	-7.8
12TH	151.93	3.2	.9	1197	2063	2.6	.4	7	44	258.7	486.5	-132.1	66.8	-7.7
13TH	164.76	3.3	1.5	1197	2063	2.8	.7	17	62	255.4	485.0	-125.9	63.5	-7.7
14TH	177.59	3.5	2.2	1197	2063	2.9	1.1	34	93	251.9	482.8	-119.7	60.3	-7.6
15TH	190.42	3.6	2.9	1197	2063	3.0	1.4	77	166	248.3	480.0	-113.5	57.0	-7.5
16TH	203.25	3.8	3.5	1197	2063	3.2	1.7	290	530	244.5	476.5	-107.3	53.9	-7.4
17TH	216.08	4.4	4.2	1197	2063	3.7	2.0	437	777	240.2	472.3	-101.3	50.8	-7.2
18TH	228.66	4.6	5.1	1174	2023	3.9	2.5	-188	-287	235.6	467.2	-95.3	47.8	-7.1
19TH	241.24	4.7	6.1	1174	2023	4.0	3.0	-85	-112	230.9	461.1	-89.5	44.9	-6.9
20TH	253.82	4.9	7.2	1174	2023	4.2	3.5	-61	-71	225.9	453.9	-83.7	42.0	-6.7
21ST	266.40	5.1	8.2	1174	2023	4.3	4.0	-50	-53	220.8	445.7	-78.1	39.2	-6.5
22ND	278.98	5.3	9.2	1174	2023	4.5	4.6	-44	-43	215.6	436.5	-72.5	36.4	-6.3
23RD	291.56	5.5	10.3	1174	2023	4.7	5.1	-40	-36	210.1	426.2	-67.1	33.7	-6.1
24TH	304.14	5.7	11.3	1174	2023	4.8	5.6	-37	-32	204.4	415.0	-61.8	31.1	-5.8
25TH	316.72	5.9	12.3	1174	2023	5.0	6.1	-34	-28	198.5	402.6	-56.7	28.6	-5.6
		6.0	13.1	1151	1983	5.2	6.6	-32	-25					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 190 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									192.5	389.5	-51.8	26.2	-5.3
		6.2	14.2	1151	1983	5.4	7.1	-30	-23					
27TH	341.38									186.3	375.3	-47.1	23.9	-5.0
		6.5	15.2	1151	1983	5.6	7.7	-29	-21					
28TH	353.71									179.8	360.1	-42.5	21.6	-4.7
		6.7	16.2	1151	1983	5.8	8.2	-28	-20					
29TH	366.04									173.2	343.9	-38.2	19.4	-4.4
		7.3	16.9	1127	1943	6.4	8.7	-24	-18					
30TH	378.12									165.9	327.0	-34.2	17.4	-4.1
		7.8	17.4	1127	1943	6.9	9.0	-23	-17					
31ST	390.20									158.1	309.6	-30.3	15.4	-3.9
		8.1	17.7	1127	1943	7.2	9.1	-23	-18					
32ND	402.28									150.0	291.9	-26.7	13.6	-3.6
		8.5	17.9	1127	1943	7.6	9.2	-22	-18					
33RD	414.36									141.5	274.0	-23.3	11.8	-3.4
		8.9	18.2	1127	1943	7.9	9.3	-22	-18					
34TH	426.44									132.6	255.8	-20.1	10.1	-3.1
		9.3	18.4	1127	1943	8.2	9.5	-22	-19					
35TH	438.52									123.3	237.4	-17.1	8.6	-2.9
		9.6	18.7	1127	1943	8.5	9.6	-22	-19					
36TH	450.60									113.7	218.7	-14.3	7.2	-2.7
		10.1	18.9	1127	1943	8.9	9.7	-22	-20					
37TH	462.68									103.6	199.8	-11.8	5.9	-2.4
		10.4	19.3	1127	1943	9.2	9.9	-23	-21					
38TH	474.76									93.2	180.5	-9.5	4.7	-2.2
		10.6	19.8	1127	1943	9.4	10.2	-24	-22					
39TH	486.84									82.6	160.8	-7.4	3.6	-1.9
		10.9	20.2	1127	1943	9.7	10.4	-25	-23					
40TH	498.92									71.7	140.6	-5.6	2.7	-1.6
		11.2	20.7	1127	1943	9.9	10.6	-26	-24					
41ST	511.00									60.5	119.9	-4.0	1.9	-1.3
		11.5	21.1	1127	1943	10.2	10.9	-27	-25					
42ND	523.08									49.0	98.8	-2.7	1.2	-1.0
		12.5	22.5	1174	2023	10.6	11.1	-26	-24					
43RD	535.66									36.5	76.3	-1.6	.7	-.7
		13.5	23.6	1206	2078	11.2	11.3	-19	-18					
44TH	548.58									23.0	52.7	-.8	.3	-.4
		18.1	33.7	1680	2895	10.8	11.6	-11	-10					
MR	566.58									4.9	19.1	-.1	.0	-.2
		4.9	19.1	1085	2065	4.5	9.2	-17	-7					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7 SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 200 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									345.6	300.3	-134.1	132.7	-5.8
2ND	23.00	1.5	-3.9	2147	3699	.7	-1.0	-54	36	344.1	304.2	-127.1	124.8	-6.0
3RD	35.92	-.1	-2.3	1206	2078	-.1	-1.1	-32	-2	344.1	306.4	-123.2	120.4	-6.0
4TH	48.84	.4	-2.4	1206	2078	.4	-1.2	-25	8	343.7	308.9	-119.2	115.9	-6.1
5TH	61.76	1.0	-2.5	1206	2078	.9	-1.2	-22	16	342.7	311.3	-115.2	111.5	-6.1
6TH	74.68	1.4	-2.3	1206	2078	1.2	-1.1	-21	22	341.2	313.6	-111.2	107.1	-6.1
7TH	87.60	1.8	-2.1	1206	2078	1.5	-1.0	-25	35	339.5	315.8	-107.1	102.7	-6.2
8TH	100.52	2.2	-2.0	1206	2078	1.8	-1.0	6	-11	337.3	317.7	-103.0	98.3	-6.2
9TH	113.44	2.5	-1.8	1206	2078	2.1	-.9	-8	18	334.8	319.6	-98.9	94.0	-6.2
10TH	126.27	2.9	-1.7	1197	2063	2.4	-.8	-8	24	331.9	321.2	-94.8	89.7	-6.1
11TH	139.10	3.2	-1.4	1197	2063	2.7	-.7	-6	26	328.7	322.6	-90.6	85.4	-6.1
12TH	151.93	3.6	-.7	1197	2063	3.0	-.3	-3	27	325.0	323.3	-86.5	81.2	-6.1
13TH	164.76	4.0	.1	1197	2063	3.4	.0	0	31	321.0	323.2	-82.4	77.1	-6.0
14TH	177.59	4.4	.8	1197	2063	3.7	.4	4	36	316.6	322.4	-78.2	73.0	-5.9
15TH	190.42	4.8	1.5	1197	2063	4.0	.7	8	42	311.8	320.9	-74.1	69.0	-5.8
16TH	203.25	5.2	2.3	1197	2063	4.3	1.1	13	50	306.7	318.6	-70.0	65.0	-5.7
17TH	216.08	6.4	3.0	1197	2063	5.4	1.4	12	44	300.2	315.7	-65.9	61.1	-5.6
18TH	228.66	6.7	3.7	1174	2023	5.7	1.8	17	54	293.5	311.9	-62.0	57.4	-5.5
19TH	241.24	7.0	4.5	1174	2023	5.9	2.2	27	72	286.5	307.4	-58.1	53.7	-5.4
20TH	253.82	7.2	5.3	1174	2023	6.2	2.6	43	100	279.3	302.1	-54.2	50.2	-5.2
21ST	266.40	7.5	6.1	1174	2023	6.4	3.0	73	151	271.8	295.9	-50.5	46.7	-5.1
22ND	278.98	7.7	6.9	1174	2023	6.6	3.4	147	278	264.1	289.0	-46.8	43.3	-4.9
23RD	291.56	8.0	7.8	1174	2023	6.8	3.8	645	1127	256.2	281.2	-43.2	40.1	-4.7
24TH	304.14	8.1	8.4	1174	2023	6.9	4.2	-438	-717	248.0	272.8	-39.7	36.9	-4.4
25TH	316.72	8.2	9.0	1174	2023	7.0	4.4	-182	-281	239.9	263.8	-36.3	33.8	-4.2
		8.1	9.4	1151	1983	7.0	4.7	-121	-177					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 200 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									231.8	254.4	-33.2	30.9	-4.0
27TH	341.38	8.1	9.9	1151	1983	7.1	5.0	-93	-130	223.7	244.5	-30.1	28.1	-3.7
28TH	353.71	8.2	10.4	1151	1983	7.1	5.3	-77	-103	215.5	234.1	-27.1	25.4	-3.5
29TH	366.04	8.2	11.0	1151	1983	7.1	5.5	-67	-85	207.3	223.1	-24.3	22.8	-3.2
30TH	378.12	9.0	11.3	1127	1943	8.0	5.8	-69	-94	198.3	211.8	-21.7	20.4	-3.0
31ST	390.20	9.7	11.6	1127	1943	8.6	6.0	-75	-107	188.6	200.2	-19.2	18.0	-2.8
32ND	402.28	10.1	11.8	1127	1943	9.0	6.1	-81	-118	178.5	188.4	-16.8	15.8	-2.6
33RD	414.36	10.6	12.1	1127	1943	9.4	6.2	-89	-133	167.9	176.4	-14.6	13.7	-2.4
34TH	426.44	11.1	12.3	1127	1943	9.8	6.3	-99	-152	156.9	164.1	-12.6	11.7	-2.2
35TH	438.52	11.5	12.5	1127	1943	10.2	6.4	-115	-180	145.3	151.6	-10.7	9.9	-2.0
36TH	450.60	12.0	12.8	1127	1943	10.6	6.6	-140	-224	133.4	138.8	-8.9	8.2	-1.8
37TH	462.68	12.6	13.0	1127	1943	11.2	6.7	-273	-450	120.8	125.8	-7.3	6.7	-1.7
38TH	474.76	12.7	12.9	1127	1943	11.3	6.7	-527	-883	108.0	112.9	-5.9	5.3	-1.5
39TH	486.84	12.8	13.0	1127	1943	11.4	6.7	-877	-1477	95.2	99.9	-4.6	4.1	-1.3
40TH	498.92	12.9	13.0	1127	1943	11.4	6.7	$$$$	-3803	82.3	87.0	-3.5	3.0	-1.1
41ST	511.00	13.0	13.0	1127	1943	11.5	6.7	5087	8674	69.3	74.0	-2.5	2.1	-.9
42ND	523.08	13.1	13.0	1127	1943	11.6	6.7	1262	2166	56.3	61.0	-1.7	1.3	-.7
43RD	535.66	14.4	13.5	1174	2023	12.3	6.7	132	239	41.9	47.5	-1.0	.7	-.5
44TH	548.58	16.2	14.3	1206	2078	13.5	6.9	41	78	25.6	33.2	-.5	.3	-.4
MR	566.58	22.2	22.5	1680	2895	13.2	7.8	-454	-763	3.5	10.7	-.1	.0	-.2
TOP	581.67	3.5	10.7	1085	2065	3.2	5.2	-25	-13	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 210 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00													
		4.1	-2.0	2147	3699	1.9	-.5	-0	1					
2ND	23.00									346.9	-174.2	55.7	128.5	1.9
		.5	-1.9	1206	2078	.4	-.9	2	-1					
3RD	35.92									342.9	-172.2	51.8	120.5	1.9
		1.2	-2.1	1206	2078	1.0	-1.0	-0	0					
4TH	48.84									342.4	-170.3	49.5	116.1	1.9
		1.9	-2.3	1206	2078	1.6	-1.1	-2	3					
5TH	61.76									341.2	-168.2	47.4	111.7	1.9
		2.3	-2.4	1206	2078	1.9	-1.2	-61	101					
6TH	74.68									339.3	-165.9	45.2	107.3	1.9
		2.7	-2.5	1206	2078	2.3	-1.2	27	-49					
7TH	87.60									336.9	-163.5	43.1	102.9	1.9
		3.1	-2.7	1206	2078	2.6	-1.3	17	-33					
8TH	100.52									334.2	-161.0	41.0	98.6	1.9
		3.5	-2.8	1206	2078	2.9	-1.4	13	-29					
9TH	113.44									331.0	-158.3	38.9	94.3	1.9
		3.9	-3.0	1197	2063	3.3	-1.4	12	-27					
10TH	126.27									327.5	-155.5	36.9	90.0	1.9
		4.3	-3.1	1197	2063	3.6	-1.5	11	-26					
11TH	139.10									323.6	-152.5	34.9	85.9	1.9
		4.5	-3.2	1197	2063	3.7	-1.5	9	-23					
12TH	151.93									319.3	-149.4	33.0	81.7	1.9
		4.7	-3.3	1197	2063	3.9	-1.6	8	-20					
13TH	164.76									314.8	-146.2	31.1	77.7	1.8
		4.9	-3.4	1197	2063	4.1	-1.7	7	-17					
14TH	177.59									310.1	-142.9	29.2	73.7	1.8
		5.1	-3.5	1197	2063	4.3	-1.7	6	-15					
15TH	190.42									305.2	-139.5	27.4	69.7	1.8
		5.4	-3.6	1197	2063	4.5	-1.8	5	-13					
16TH	203.25									300.1	-136.0	25.6	65.8	1.8
		6.5	-3.7	1197	2063	5.5	-1.8	4	-12					
17TH	216.08									294.7	-132.4	23.9	62.0	1.7
		6.8	-3.8	1174	2023	5.8	-1.9	5	-15					
18TH	228.66									288.2	-128.7	22.2	58.3	1.7
		7.1	-4.0	1174	2023	6.0	-2.0	6	-18					
19TH	241.24									281.3	-124.8	20.7	54.7	1.7
		7.3	-4.2	1174	2023	6.3	-2.1	7	-21					
20TH	253.82									274.3	-120.8	19.1	51.2	1.6
		7.6	-4.4	1174	2023	6.5	-2.2	8	-24					
21ST	266.40									266.9	-116.6	17.6	47.8	1.6
		7.9	-4.6	1174	2023	6.7	-2.3	9	-27					
22ND	278.98									259.3	-112.2	16.2	44.5	1.5
		8.1	-4.8	1174	2023	6.9	-2.4	10	-30					
23RD	291.56									251.4	-107.6	14.8	41.3	1.5
		8.2	-5.0	1174	2023	7.0	-2.5	11	-31					
24TH	304.14									243.3	-102.8	13.5	38.2	1.4
		8.2	-5.0	1174	2023	7.0	-2.5	11	-30					
25TH	316.72									235.1	-97.8	12.2	35.1	1.3
		7.9	-5.0	1151	1983	6.9	-2.5	10	-28					
										226.9	-92.8	11.0	32.2	1.3

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 210 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05	7.9	-5.0	1151	1983	6.8	-2.5	10	-27	218.9	-87.8	9.9	29.5	1.2
27TH	341.38	7.8	-5.0	1151	1983	6.8	-2.5	10	-25	211.1	-82.9	8.8	26.8	1.1
28TH	353.71	7.7	-5.1	1151	1983	6.7	-2.6	9	-23	203.3	-77.8	7.9	24.3	1.1
29TH	366.04	8.6	-5.0	1127	1943	7.6	-2.6	8	-23	195.5	-72.7	6.9	21.8	1.0
30TH	378.12	9.2	-5.0	1127	1943	8.2	-2.6	7	-22	186.9	-67.7	6.1	19.5	1.0
31ST	390.20	9.6	-4.9	1127	1943	8.5	-2.5	6	-21	177.7	-62.7	5.3	17.3	.9
32ND	402.28	9.9	-4.8	1127	1943	8.8	-2.5	6	-20	168.1	-57.8	4.6	15.2	.8
33RD	414.36	10.2	-4.7	1127	1943	9.1	-2.4	5	-19	158.2	-53.0	3.9	13.3	.8
34TH	426.44	10.5	-4.6	1127	1943	9.4	-2.3	5	-18	148.0	-48.3	3.3	11.4	.7
35TH	438.52	10.9	-4.4	1127	1943	9.6	-2.3	4	-17	137.5	-43.7	2.7	9.7	.6
36TH	450.60	11.3	-4.3	1127	1943	10.0	-2.2	3	-15	126.6	-39.3	2.2	8.1	.5
37TH	462.68	11.5	-4.3	1127	1943	10.2	-2.2	3	-14	115.3	-34.9	1.8	6.6	.5
38TH	474.76	11.6	-4.3	1127	1943	10.3	-2.2	3	-13	103.8	-30.6	1.4	5.3	.4
39TH	486.84	11.7	-4.3	1127	1943	10.4	-2.2	3	-13	92.2	-26.3	1.0	4.1	.3
40TH	498.92	11.8	-4.3	1127	1943	10.5	-2.2	3	-12	80.4	-22.0	.7	3.1	.3
41ST	511.00	12.0	-4.2	1127	1943	10.6	-2.2	2	-12	68.6	-17.8	.5	2.2	.2
42ND	523.08	13.4	-4.4	1174	2023	11.4	-2.2	2	-13	56.7	-13.5	.3	1.4	.2
43RD	535.66	15.7	-4.1	1206	2078	13.0	-2.0	2	-12	43.3	-9.2	.2	.8	.1
44TH	548.58	22.7	-2.9	1680	2895	13.5	-1.0	0	-4	27.6	-5.1	.1	.3	.0
MR	566.58	5.0	-2.2	1085	2065	4.6	-1.1	-4	16	5.0	-2.2	.0	.0	-.0
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS) NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 220 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									206.9	-445.5	153.3	85.0	6.2
2ND	23.00	-1.9	-5.6	2147	3699	-.9	-1.5	7	4	208.8	-439.9	143.1	80.2	6.2
3RD	35.92	-1.9	-4.2	1206	2078	-1.5	-2.0	4	3	210.6	-435.7	137.5	77.5	6.2
4TH	48.84	-1.6	-4.6	1206	2078	-1.3	-2.2	4	2	212.2	-431.1	131.9	74.7	6.2
5TH	61.76	-1.2	-5.0	1206	2078	-1.0	-2.4	3	1	213.4	-426.0	126.3	72.0	6.3
6TH	74.68	-.8	-5.3	1206	2078	-.7	-2.6	-0	-0	214.3	-420.7	120.9	69.2	6.3
7TH	87.60	-.5	-5.7	1206	2078	-.4	-2.7	-3	-0	214.7	-415.0	115.5	66.5	6.2
8TH	100.52	-.1	-6.0	1206	2078	-.1	-2.9	-5	-0	214.8	-409.1	110.1	63.7	6.2
9TH	113.44	.3	-6.3	1206	2078	.2	-3.0	-8	1	214.6	-402.8	104.9	60.9	6.2
10TH	126.27	.6	-6.5	1197	2063	.5	-3.2	-10	2	214.0	-396.3	99.8	58.2	6.1
11TH	139.10	1.0	-6.8	1197	2063	.8	-3.3	-12	3	213.0	-389.5	94.7	55.4	6.1
12TH	151.93	1.4	-7.1	1197	2063	1.2	-3.4	-14	5	211.5	-382.5	89.8	52.7	6.0
13TH	164.76	1.9	-7.4	1197	2063	1.6	-3.6	-16	7	209.6	-375.1	84.9	50.0	5.9
14TH	177.59	2.3	-7.6	1197	2063	1.9	-3.7	-18	9	207.3	-367.5	80.1	47.3	5.8
15TH	190.42	2.8	-7.9	1197	2063	2.3	-3.8	-20	12	204.5	-359.6	75.5	44.7	5.7
16TH	203.25	3.2	-8.2	1197	2063	2.7	-4.0	-22	15	201.3	-351.3	70.9	42.1	5.6
17TH	216.08	4.4	-8.5	1197	2063	3.7	-4.1	-27	24	196.9	-342.8	66.5	39.5	5.4
18TH	228.66	4.7	-8.6	1174	2023	4.0	-4.3	-30	28	192.2	-334.2	62.2	37.1	5.3
19TH	241.24	4.9	-8.9	1174	2023	4.2	-4.4	-31	30	187.3	-325.2	58.1	34.7	5.1
20TH	253.82	5.2	-9.3	1174	2023	4.4	-4.6	-33	31	182.1	-316.0	54.0	32.4	5.0
21ST	266.40	5.4	-9.6	1174	2023	4.6	-4.7	-34	33	176.6	-306.4	50.1	30.1	4.8
22ND	278.98	5.7	-9.9	1174	2023	4.8	-4.9	-36	35	171.0	-296.6	46.3	27.9	4.6
23RD	291.56	5.9	-10.2	1174	2023	5.0	-5.0	-37	37	165.1	-286.4	42.7	25.8	4.4
24TH	304.14	6.0	-10.5	1174	2023	5.1	-5.2	-37	36	159.1	-275.9	39.1	23.8	4.2
25TH	316.72	5.9	-10.8	1174	2023	5.0	-5.3	-34	32	153.2	-265.1	35.7	21.8	4.0
		5.7	-10.8	1151	1983	4.9	-5.4	-33	29					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 220 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05	5.5	-11.0	1151	1983	4.8	-5.6	-31	26	147.5	-254.3	32.5	20.0	3.8
27TH	341.38	5.4	-11.3	1151	1983	4.7	-5.7	-29	24	142.0	-243.3	29.4	18.2	3.6
28TH	353.71	5.3	-11.6	1151	1983	4.6	-5.8	-28	22	136.5	-232.0	26.5	16.5	3.4
29TH	366.04	5.9	-11.6	1127	1943	5.2	-6.0	-30	26	131.2	-220.4	23.7	14.8	3.2
30TH	378.12	6.3	-11.8	1127	1943	5.5	-6.1	-30	27	125.3	-208.9	21.1	13.3	3.0
31ST	390.20	6.4	-12.0	1127	1943	5.7	-6.2	-29	27	119.1	-197.1	18.7	11.8	2.8
32ND	402.28	6.6	-12.1	1127	1943	5.8	-6.2	-28	26	112.7	-185.1	16.4	10.4	2.6
33RD	414.36	6.7	-12.3	1127	1943	6.0	-6.3	-28	26	106.1	-173.0	14.2	9.1	2.4
34TH	426.44	6.9	-12.5	1127	1943	6.1	-6.4	-27	26	99.3	-160.7	12.2	7.8	2.2
35TH	438.52	7.1	-12.6	1127	1943	6.3	-6.5	-26	25	92.4	-148.3	10.3	6.7	2.0
36TH	450.60	7.3	-12.8	1127	1943	6.5	-6.6	-25	25	85.3	-135.6	8.6	5.6	1.8
37TH	462.68	7.5	-12.9	1127	1943	6.6	-6.6	-26	25	78.1	-122.8	7.0	4.6	1.6
38TH	474.76	7.6	-12.9	1127	1943	6.7	-6.6	-27	27	70.6	-109.9	5.6	3.7	1.5
39TH	486.84	7.7	-12.9	1127	1943	6.9	-6.7	-27	28	63.0	-97.0	4.4	2.9	1.3
40TH	498.92	7.9	-13.0	1127	1943	7.0	-6.7	-28	29	55.3	-84.1	3.3	2.2	1.1
41ST	511.00	8.0	-13.0	1127	1943	7.1	-6.7	-29	30	47.4	-71.1	2.4	1.6	.9
42ND	523.08	8.9	-13.6	1174	2023	7.6	-6.7	-30	34	39.4	-58.1	1.6	1.0	.7
43RD	535.66	10.2	-14.1	1206	2078	8.4	-6.8	-32	40	30.5	-44.5	.9	.6	.5
44TH	548.58	15.3	-20.0	1680	2895	9.1	-6.9	-34	44	20.3	-30.5	.4	.3	.4
MR	566.58	5.0	-10.5	1085	2065	4.6	-5.1	-22	18	5.0	-10.5	.1	.0	.1
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 230 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									194.2	-836.2	295 9	88.2	8.6
2ND	23.00	-1.9	-13.9	2147	3699	-.9	-3.8	24	6	196.1	-822.3	276.8	83.7	8.9
3RD	35.92	-1.9	-8.9	1206	2078	-1.5	-4.3	18	6	197.9	-813.4	266.2	81.1	9.0
4TH	48.84	-1.4	-8.9	1206	2078	-1.2	-4.3	15	4	199.4	-804.6	255.8	78.6	9.1
5TH	61.76	-.9	-9.0	1206	2078	-.8	-4.3	15	3	200.3	-795.5	245.4	76.0	9.2
6TH	74.68	-.8	-9.4	1206	2078	-.6	-4.5	13	2	201.0	-786.2	235.2	73.4	9.3
7TH	87.60	-.6	-9.7	1206	2078	-.5	-4.7	11	1	201.6	-776.5	225.1	70.8	9.4
8TH	100.52	-.4	-10.0	1206	2078	-.3	-4.8	9	1	202.0	-766.5	215.2	68.2	9.5
9TH	113.44	-.2	-10.4	1206	2078	-.2	-5.0	7	0	202.2	-756.1	205.3	65.6	9.5
10TH	126.27	-.0	-10.6	1197	2063	-.0	-5.1	6	0	202.3	-745.5	195.7	63.0	9.6
11TH	139.19	.1	-10.9	1197	2063	.1	-5.3	4	-0	202.1	-734.5	186.2	60.4	9.6
12TH	151.93	.3	-11.5	1197	2063	.2	-5.6	1	-0	201.8	-723.1	176.9	57.8	9.6
13TH	164.76	.4	-12.0	1197	2063	.3	-5.8	-2	0	201.4	-711.1	167.7	55.2	9.6
14TH	177.59	.5	-12.5	1197	2063	.4	-6.0	-4	0	200.9	-698.7	158.6	52.6	9.6
15TH	190.42	.7	-13.0	1197	2063	.6	-6.3	-7	1	200.2	-685.7	149.7	50.1	9.5
16TH	203.25	.8	-13.5	1197	2063	.7	-6.5	-9	1	199.4	-672.2	141.0	47.5	9.4
17TH	216.08	1.2	-14.0	1197	2063	1.0	-6.8	-10	1	198.2	-658.2	132.5	44.9	9.3
18TH	228.66	1.7	-14.3	1174	2023	1.4	-7.1	-11	2	196.5	-643.9	124.3	42.5	9.2
19TH	241.24	2.1	-14.9	1174	2023	1.8	-7.3	-13	3	194.5	-629.1	116.3	40.0	9.0
20TH	253.82	2.5	-15.4	1174	2023	2.2	-7.6	-14	4	191.9	-613.7	108.5	37.6	8.8
21ST	266.40	3.0	-16.0	1174	2023	2.5	-7.9	-16	5	188.9	-597.6	100.8	35.2	8.7
22ND	278.98	3.4	-16.6	1174	2023	2.9	-8.2	-17	6	185.5	-581.0	93.4	32.8	8.4
23RD	291.56	3.9	-17.2	1174	2023	3.3	-8.5	-18	7	181.7	-563.9	86.2	30.5	8.2
24TH	304.14	4.2	-17.8	1174	2023	3.6	-8.8	-19	8	177.5	-546.0	79.2	28.3	7.9
25TH	316.72	4.4	-18.7	1174	2023	3.7	-9.2	-20	8	173.1	-527.3	72 5	26.1	7.7
		4.5	-19.2	1151	1983	3.9	-9.7	-20	8					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 230 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05	4.6	-20.0	1151	1983	4.0	-10.1	-20	8	168.7	-508.2	66.1	23.9	7.4
27TH	341.38	4.8	-20.8	1151	1983	4.2	-10.5	-21	8	164.0	-488.2	60.0	21.9	7.1
28TH	353.71	5.0	-21.6	1151	1983	4.3	-10.9	-21	8	159.2	-467.4	54.1	19.9	6.7
29TH	366.04	5.3	-22.0	1127	1943	4.7	-11.3	-20	8	154.3	-445.7	48.5	18.0	6.4
30TH	378.12	5.8	-22.7	1127	1943	5.2	-11.7	-20	9	149.0	-423.7	43.2	16.1	6.1
31ST	390.20	6.3	-23.3	1127	1943	5.6	-12.0	-20	9	143.2	-401.0	38.2	14.4	5.7
32ND	402.28	6.9	-24.0	1127	1943	6.1	-12.3	-21	10	136.8	-377.7	33.5	12.7	5.4
33RD	414.36	7.4	-24.6	1127	1943	6.6	-12.6	-21	11	130.0	-353.7	29.1	11.1	5.0
34TH	426.44	7.9	-25.2	1127	1943	7.1	-13.0	-22	12	122.5	-329.1	25.0	9.5	4.6
35TH	438.52	8.5	-25.8	1127	1943	7.5	-13.3	-22	12	114.6	-303.9	21.1	8.1	4.2
36TH	450.60	9.1	-26.4	1127	1943	8.0	-13.6	-22	13	106.1	-278.1	17.6	6.8	3.8
37TH	462.68	9.4	-26.6	1127	1943	8.4	-13.7	-22	14	97.1	-251.7	14.4	5.6	3.4
38TH	474.76	9.8	-26.6	1127	1943	8.7	-13.7	-22	14	87.6	-225.2	11.6	4.4	3.0
39TH	486.84	10.1	-26.6	1127	1943	9.0	-13.7	-22	14	77.9	-198.6	9.0	3.4	2.6
40TH	498.92	10.4	-26.7	1127	1943	9.3	-13.7	-22	15	67.8	-172.0	6.8	2.6	2.2
41ST	511.00	10.8	-26.7	1127	1943	9.6	-13.7	-22	15	57.3	-145.3	4.8	1.8	1.8
42ND	523.08	11.8	-27.8	1174	2023	10.1	-13.7	-21	15	46.5	-118.6	3.2	1.2	1.4
43RD	535.66	12.6	-28.5	1206	2078	10.5	-13.7	-17	13	34.7	-90.8	1.9	.7	1.0
44TH	548.58	16.2	-39.5	1680	2895	9.6	-13.6	-13	9	22.1	-62.3	.9	.3	.7
MR	566.58	5.9	-22.8	1085	2065	5.5	-11.0	-20	9	5.9	-22.8	.2	.0	.3
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 240 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									131.2	-1509.5	516.7	83.1	8.0
2ND	23.00	-5.6	-30.5	2147	3699	-2.6	-8.3	16	5	136.7	-1478.9	482.4	80.0	8.4
3RD	35.92	-4.3	-18.2	1206	2078	-3.6	-8.8	14	5	141.1	-1460.7	463.4	78.2	8.6
4TH	48.84	-4.3	-17.4	1206	2078	-3.5	-8.4	13	5	145.3	-1443.3	444.6	76.3	8.7
5TH	61.76	-4.0	-17.3	1206	2078	-3.3	-8.3	12	5	149.4	-1426.0	426.1	74.4	8.9
6TH	74.68	-3.8	-17.9	1206	2078	-3.2	-8.6	10	4	153.2	-1408.1	407.8	72.5	9.0
7TH	87.60	-3.6	-18.5	1206	2078	-3.0	-8.9	8	3	156.8	-1389.6	389.7	70.5	9.1
8TH	100.52	-3.4	-19.1	1206	2078	-2.8	-9.2	7	2	160.3	-1370.5	371.9	68.4	9.2
9TH	113.44	-3.2	-19.7	1206	2078	-2.7	-9.5	6	2	163.5	-1350.8	354.3	66.3	9.3
10TH	126.27	-3.0	-20.2	1197	2063	-2.5	-9.8	4	1	166.5	-1330.6	337.1	64.2	9.4
11TH	139.10	-2.8	-20.9	1197	2063	-2.4	-10.1	3	1	169.3	-1309.7	320.2	62.1	9.4
12TH	151.93	-2.8	-22.0	1197	2063	-2.3	-10.7	1	0	172.1	-1287.7	303.5	59.9	9.5
13TH	164.76	-2.7	-23.1	1197	2063	-2.2	-11.2	-1	-0	174.8	-1264.6	287.1	57.6	9.4
14TH	177.59	-2.6	-24.3	1197	2063	-2.2	-11.8	-3	-1	177.4	-1240.3	271.1	55.4	9.4
15TH	190.42	-2.5	-25.4	1197	2063	-2.1	-12.3	-4	-1	179.9	-1214.9	255.3	53.1	9.3
16TH	203.25	-2.5	-26.6	1197	2063	-2.1	-12.9	-6	-1	182.4	-1188.3	239.9	50.8	9.2
17TH	216.08	-2.4	-27.7	1197	2063	-2.0	-13.4	-6	-1	184.8	-1160.6	224.8	48.4	9.0
18TH	228.66	-2.0	-28.4	1174	2023	-1.7	-14.0	-7	-1	186.8	-1132.2	210.4	46.1	8.9
19TH	241.24	-1.6	-29.7	1174	2023	-1.3	-14.7	-7	-1	188.3	-1102.4	196.3	43.7	8.7
20TH	253.82	-1.1	-31.0	1174	2023	-1.0	-15.3	-8	-1	189.5	-1071.4	182.7	41.3	8.5
21ST	266.40	-.7	-32.3	1174	2023	-.6	-16.0	-9	-0	190.2	-1039.1	169.4	38.9	8.3
22ND	278.98	-.3	-33.6	1174	2023	-.3	-16.6	-9	-0	190.5	-1005.5	156.5	36.6	8.0
23RD	291.56	.1	-34.9	1174	2023	.1	-17.3	-10	0	190.4	-970.6	144.1	34.2	7.8
24TH	304.14	.7	-36.2	1174	2023	.6	-17.9	-10	0	189.8	-934.4	132.1	31.8	7.5
25TH	316.72	1.5	-37.1	1174	2023	1.3	-18.3	-11	1	188.2	-897.3	120.6	29.4	7.2
		2.3	-37.2	1151	1983	2.0	-18.7	-11	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 240 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									186.0	-860.2	109.8	27.1	6.8
		3.1	-38.0	1151	1983	2.7	-19.2	-11	2					
27TH	341.38									182.9	-822.1	99.4	24.8	6.5
		3.8	-38.9	1151	1983	3.3	-19.6	-11	2					
28TH	353.71									179.1	-783.2	89.5	22.6	6.1
		4.6	-39.7	1151	1983	4.0	-20.0	-12	2					
29TH	366.04									174.4	-743.5	80.1	20.4	5.8
		5.1	-39.8	1127	1943	4.6	-20.5	-10	2					
30TH	378.12									169.3	-703.7	71.3	18.3	5.5
		5.9	-40.3	1127	1943	5.2	-20.8	-10	3					
31ST	390.20									163.4	-663.4	63.1	16.3	5.1
		6.7	-40.6	1127	1943	6.0	-20.9	-10	3					
32ND	402.28									156.6	-622.8	55.3	14.4	4.8
		7.6	-41.0	1127	1943	6.7	-21.1	-10	3					
33RD	414.36									149.0	-581.8	48.0	12.5	4.5
		8.4	-41.3	1127	1943	7.5	-21.3	-10	4					
34TH	426.44									140.6	-540.5	41.3	10.8	4.2
		9.3	-41.6	1127	1943	8.2	-21.4	-10	4					
35TH	438.52									131.3	-498.9	35.0	9.1	3.8
		10.1	-41.9	1127	1943	9.0	-21.6	-10	4					
36TH	450.60									121.2	-457.0	29.2	7.6	3.5
		10.9	-42.2	1127	1943	9.7	-21.7	-10	5					
37TH	462.68									110.3	-414.7	23.9	6.2	3.2
		11.2	-42.6	1127	1943	10.0	-21.9	-11	5					
38TH	474.76									99.0	-372.1	19.2	5.0	2.9
		11.5	-43.0	1127	1943	10.2	-22.1	-11	5					
39TH	486.84									87.5	-329.1	15.0	3.8	2.5
		11.8	-43.4	1127	1943	10.5	-22.3	-11	5					
40TH	498.92									75.7	-285.7	11.2	2.8	2.2
		12.1	-43.8	1127	1943	10.7	-22.5	-11	5					
41ST	511.00									63.6	-241.9	8.1	2.0	1.8
		12.4	-44.2	1127	1943	11.0	-22.7	-12	6					
42ND	523.08									51.2	-197.7	5.4	1.3	1.4
		13.3	-46.4	1174	2023	11.3	-22.9	-11	5					
43RD	535.66									37.9	-151.3	3.2	.7	1.0
		13.5	-47.7	1206	2078	11.2	-23.0	-8	4					
44TH	548.58									24.4	-103.6	1.6	.3	.7
		16.8	-65.3	1680	2895	10.0	-22.5	-5	2					
MR	566.58									7.5	-38.3	.3	.1	.5
		7.5	-38.3	1085	2065	6.9	-18.5	-16	5					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 250 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									486.5	-1779.0	576.8	197.7	4.1
2ND	23.00	.7	-39.2	2147	3699	3	-10.6	24	-1	485.8	-1739.7	536.3	186.6	4.9
3RD	35.92	-1.7	-23.8	1206	2078	-1.4	-11.5	18	2	487.4	-1715.9	514.0	180.3	5.2
4TH	48.84	-.8	-23.0	1206	2078	-.6	-11.0	15	1	488.2	-1692.9	492.0	174.0	5.5
5TH	61.76	.6	-23.0	1206	2078	.5	-11.1	14	-1	487.6	-1669.9	470.3	167.7	5.7
6TH	74.68	1.3	-24.2	1206	2078	1.0	-11.6	11	-1	486.4	-1645.8	448.8	161.4	6.0
7TH	87.60	1.9	-25.4	1206	2078	1.6	-12.2	9	-1	484.5	-1620.4	427.7	155.1	6.1
8TH	100.52	2.5	-26.6	1206	2078	2.1	-12.8	7	-1	481.9	-1593.7	407.0	148.9	6.3
9TH	113.44	3.2	-27.8	1206	2078	2.6	-13.4	5	-1	478.7	-1565.9	386.6	142.7	6.4
10TH	126.27	3.8	-28.8	1197	2063	3.2	-14.0	3	-1	474.9	-1537.1	366.7	136.5	6.5
11TH	139.10	4.3	-30.0	1197	2063	3.6	-14.5	2	-0	470.6	-1507.1	347.1	130.5	6.5
12TH	151.93	4.5	-31.4	1197	2063	3.8	-15.2	0	-0	466.1	-1475.7	328.0	124.5	6.5
13TH	164.76	4.7	-32.8	1197	2063	3.9	-15.9	-2	0	461.4	-1442.9	309.3	118.5	6.5
14TH	177.59	4.9	-34.2	1197	2063	4.1	-16.6	-3	1	456.4	-1408.7	291.0	112.6	6.4
15TH	190.42	5.1	-35.6	1197	2063	4.3	-17.3	-5	1	451.3	-1373.1	273.1	106.8	6.3
16TH	203.25	5.3	-37.1	1197	2063	4.4	-18.0	-6	1	446.0	-1336.0	255.8	101.0	6.1
17TH	216.08	6.5	-38.5	1197	2063	5.4	-18.6	-6	2	439.5	-1297.5	238.9	95.4	5.9
18TH	228.66	6.9	-38.8	1174	2023	5.9	-19.2	-6	2	432.7	-1258.7	222.8	89.9	5.8
19TH	241.24	7.2	-39.8	1174	2023	6.1	-19.7	-6	2	425.5	-1218.9	207.2	84.5	5.6
20TH	253.82	7.5	-40.8	1174	2023	6.4	-20.2	-7	2	417.9	-1178.1	192.1	79.2	5.4
21ST	266.40	7.9	-41.8	1174	2023	6.7	-20.7	-7	2	410.0	-1136.3	177.6	74.0	5.1
22ND	278.98	8.2	-42.8	1174	2023	7.0	-21.1	-7	2	401.8	-1093.5	163.5	68.9	4.9
23RD	291.56	8.6	-43.8	1174	2023	7.3	-21.6	-7	2	393.2	-1049.8	150.1	63.9	4.7
24TH	304.14	9.1	-44.6	1174	2023	7.7	-22.1	-8	3	384.2	-1005.1	137.1	59.0	4.4
25TH	316.72	9.8	-45.0	1174	2023	8.4	-22.2	-8	3	374.3	-960.1	124.8	54.2	4.1
		10.4	-44.4	1151	1983	9.0	-22.4	-8	3					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 250 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									364.0	-915.7	113.2	49.7	3.9
		11.1	-44.7	1151	1983	9.7	-22.6	-8	3					
27TH	341.38									352.9	-871.0	102.2	45.2	3.6
		11.8	-45.1	1151	1983	10.3	-22.7	-8	3					
28TH	353.71									341.0	-825.9	91.7	41.0	3.4
		12.6	-45.4	1151	1983	10.9	-22.9	-8	4					
29TH	366.04									328.4	-780.5	81.8	36.8	3.1
		13.6	-44.8	1127	1943	12.0	-23.1	-6	3					
30TH	378.12									314.9	-735.7	72.7	32.9	2.9
		14.6	-45.0	1127	1943	13.0	-23.1	-6	3					
31ST	390.20									300.2	-690.8	64.0	29.2	2.7
		15.4	-45.0	1127	1943	13.7	-23.2	-6	3					
32ND	402.28									284.8	-645.8	56.0	25.7	2.5
		16.2	-45.0	1127	1943	14.4	-23.2	-6	4					
33RD	414.36									268.6	-600.8	48.4	22.4	2.4
		17.0	-45.0	1127	1943	15.1	-23.2	-6	4					
34TH	426.44									251.5	-555.8	41.5	19.2	2.2
		17.8	-45.0	1127	1943	15.8	-23.2	-6	4					
35TH	438.52									233.7	-510.7	35.0	16.3	2.0
		18.6	-45.0	1127	1943	16.5	-23.2	-6	4					
36TH	450.60									215.1	-465.7	29.1	13.6	1.8
		19.4	-45.1	1127	1943	17.2	-23.2	-6	5					
37TH	462.68									195.7	-420.6	23.8	11.1	1.6
		19.9	-45.1	1127	1943	17.6	-23.2	-6	5					
38TH	474.76									175.8	-375.5	19.0	8.8	1.4
		20.3	-45.2	1127	1943	18.0	-23.3	-7	5					
39TH	486.84									155.5	-330.3	14.7	6.8	1.2
		20.8	-45.2	1127	1943	18.4	-23.3	-7	5					
40TH	498.92									134.7	-285.0	11.0	5.1	1.1
		21.2	-45.3	1127	1943	18.8	-23.3	-7	6					
41ST	511.00									113.5	-239.8	7.8	3.6	.9
		21.7	-45.3	1127	1943	19.2	-23.3	-7	6					
42ND	523.08									91.8	-194.4	5.2	2.4	.7
		23.5	-47.3	1174	2023	20.0	-23.4	-7	6					
43RD	535.66									68.3	-147.2	3.0	1.3	.5
		24.7	-48.2	1206	2078	20.4	-23.2	-4	3					
44TH	548.58									43.6	-99.0	1.5	.6	.4
		29.8	-65.2	1680	2895	17.7	-22.5	-1	1					
MR	566.58									13.9	-33.8	.3	.1	.3
		13.9	-33.8	1085	2065	12.8	-16.4	-14	10					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 260 CONFIGURATION A REFERENCE PRESSURE 24.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									308.2	-2101.2	665.7	118.1	6.1
2ND	23.00	3.7	-53.8	2147	3699	1.7	-14.5	21	-2	304.5	-2047.5	618.0	111.1	6.9
3RD	35.92	-1.2	-31.7	1206	2078	-1.0	-15.3	16	1	305.8	-2015.8	591.7	107.2	7.3
4TH	48.84	-.9	-31.0	1206	2078	-.7	-14.9	13	1	306.6	-1984.8	565.9	103.2	7.7
5TH	61.76	.3	-31.2	1206	2078	.3	-15.0	12	-0	306.3	-1953.6	540.4	99.2	8.0
6TH	74.68	1.1	-32.6	1206	2078	.9	-15.7	10	-1	305.2	-1921.0	515.4	95.3	8.2
7TH	87.60	1.9	-34.0	1206	2078	1.6	-16.4	8	-1	303.3	-1887.0	490.8	91.4	8.4
8TH	100.52	2.7	-35.4	1206	2078	2.2	-17.0	6	-1	300.6	-1851.6	466.7	87.5	8.6
9TH	113.44	3.4	-36.8	1206	2078	2.8	-17.7	4	-1	297.2	-1814.8	443.0	83.6	8.7
10TH	126.27	4.2	-37.9	1197	2063	3.5	-18.4	2	-0	293.1	-1777.0	419.9	79.8	8.8
11TH	139.10	4.8	-39.2	1197	2063	4.0	-19.0	1	-0	288.3	-1737.8	397.4	76.1	8.8
12TH	151.93	4.7	-40.1	1197	2063	4.0	-19.4	-1	0	283.6	-1697.7	375.3	72.4	8.8
13TH	164.76	4.7	-41.1	1197	2063	3.9	-19.9	-1	0	278.8	-1656.6	353.8	68.8	8.7
14TH	177.59	4.7	-42.1	1197	2063	3.9	-20.4	-2	0	274.1	-1614.5	332.8	65.3	8.6
15TH	190.42	4.7	-43.0	1197	2063	3.9	-20.9	-3	1	269.4	-1571.5	312.4	61.8	8.5
16TH	203.25	4.7	-44.0	1197	2063	3.9	-21.3	-4	1	264.7	-1527.5	292.5	58.3	8.4
17TH	216.08	5.9	-45.0	1197	2063	4.9	-21.8	-4	1	258.8	-1482.5	273.2	55.0	8.2
18TH	228.66	6.0	-44.8	1174	2023	5.1	-22.2	-4	1	252.8	-1437.6	254.8	51.8	8.1
19TH	241.24	6.1	-45.5	1174	2023	5.2	-22.5	-5	1	246.7	-1392.1	237.0	48.6	7.9
20TH	253.82	6.2	-46.2	1174	2023	5.2	-22.8	-5	1	240.5	-1346.0	219.8	45.6	7.7
21ST	266.40	6.2	-46.8	1174	2023	5.3	-23.1	-5	1	234.3	-1299.1	203.2	42.6	7.6
22ND	278.98	6.3	-47.5	1174	2023	5.3	-23.5	-5	1	228.1	-1251.7	187.1	39.7	7.4
23RD	291.56	6.3	-48.2	1174	2023	5.4	-23.8	-6	1	221.7	-1203.5	171.7	36.8	7.1
24TH	304.14	6.4	-48.9	1174	2023	5.4	-24.1	-6	1	215.4	-1154.6	156.9	34.1	6.9
25TH	316.72	6.4	-49.7	1174	2023	5.4	-24.5	-6	1	209.0	-1105.0	142.6	31.4	6.7
		6.2	-49.4	1151	1983	5.4	-24.9	-7	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 260 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									202.8	-1055.6	129.3	28.9	6.4
		6.2	-50.2	1151	1983	5.4	-25.3	-7	1					
27TH	341.38									196.5	-1005.3	116.6	26.4	6.2
		6.2	-51.0	1151	1983	5.4	-25.7	-7	1					
28TH	353.71									190.3	-954.4	104.5	24.0	5.9
		6.2	-51.7	1151	1983	5.4	-26.1	-7	2					
29TH	366.04									184.1	-902.6	93.1	21.7	5.6
		6.7	-51.4	1127	1943	6.0	-26.5	-7	2					
30TH	378.12									177.3	-851.2	82.5	19.5	5.3
		7.4	-51.9	1127	1943	6.5	-26.7	-7	2					
31ST	390.20									170.0	-799.3	72.5	17.4	5.0
		7.8	-52.3	1127	1943	6.9	-26.9	-7	2					
32ND	402.28									162.2	-747.0	63.2	15.4	4.7
		8.2	-52.6	1127	1943	7.3	-27.1	-7	2					
33RD	414.36									154.0	-694.4	54.5	13.5	4.4
		8.6	-52.9	1127	1943	7.6	-27.3	-7	2					
34TH	426.44									145.4	-641.4	46.4	11.7	4.0
		9.0	-53.3	1127	1943	8.0	-27.4	-7	2					
35TH	438.52									136.4	-588.1	39.0	10.0	3.7
		9.4	-53.6	1127	1943	8.3	-27.6	-7	2					
36TH	450.60									127.0	-534.5	32.2	8.4	3.4
		9.7	-54.0	1127	1943	8.6	-27.8	-8	2					
37TH	462.68									117.3	-480.5	26.1	7.0	3.1
		10.3	-54.0	1127	1943	9.1	-27.8	-8	3					
38TH	474.76									107.0	-426.5	20.6	5.6	2.8
		10.9	-54.0	1127	1943	9.7	-27.8	-8	3					
39TH	486.84									96.0	-372.5	15.8	4.4	2.5
		11.5	-54.1	1127	1943	10.2	-27.8	-9	3					
40TH	498.92									84.5	-318.4	11.6	3.3	2.1
		12.2	-54.1	1127	1943	10.8	-27.8	-9	3					
41ST	511.00									72.3	-264.4	8.1	2.3	1.7
		12.8	-54.1	1127	1943	11.3	-27.8	-9	4					
42ND	523.08									59.6	-210.3	5.2	1.5	1.4
		14.5	-56.4	1174	2023	12.3	-27.9	-9	4					
43RD	535.66									45.1	-153.9	2.9	.9	1.0
		16.0	-56.5	1206	2078	13.3	-27.2	-8	4					
44TH	548.58									29.0	-97.4	1.3	.4	.6
		20.4	-71.8	1680	2895	12.1	-24.8	-5	2					
MR	566.58									8.7	-25.6	.2	.1	.4
		8.7	-25.6	1085	2065	8.0	-12.4	-21	12					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 270 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									247.8	-2449.2	765.0	88.5	6.5
2ND	23.00	4.0	-66.2	2147	3699	1.9	-17.9	17	-2	243.8	-2383.0	709.5	82.8	7.4
3RD	35.92	-1.4	-39.3	1206	2078	-1.2	-18.9	15	1	245.3	-2343.7	678.9	79.7	7.8
4TH	48.84	-1.4	-37.1	1206	2078	-1.1	-17.8	12	1	246.6	-2306.6	648.9	76.5	8.2
5TH	61.76	-.2	-36.6	1206	2078	-.1	-17.6	11	0	246.8	-2270.0	619.3	73.3	8.5
6TH	74.68	.7	-38.4	1206	2078	.6	-18.5	9	-0	246.1	-2231.6	590.2	70.1	8.8
7TH	87.60	1.6	-40.2	1206	2078	1.3	-19.3	8	-1	244.5	-2191.4	561.7	66.9	9.1
8TH	100.52	2.5	-42.0	1206	2078	2.1	-20.2	6	-1	242.0	-2149.4	533.6	63.8	9.3
9TH	113.44	3.4	-43.8	1206	2078	2.8	-21.1	5	-1	238.6	-2105.6	506.1	60.7	9.4
10TH	126.27	4.3	-45.3	1197	2063	3.6	-21.9	4	-1	234.3	-2060.3	479.4	57.7	9.6
11TH	139.10	4.9	-47.0	1197	2063	4.1	-22.8	2	-0	229.4	-2013.4	453.3	54.7	9.6
12TH	151.93	4.9	-48.2	1197	2063	4.1	-23.4	1	-0	224.4	-1965.2	427.8	51.8	9.7
13TH	164.76	4.9	-49.5	1197	2063	4.1	-24.0	0	-0	219.5	-1915.7	402.9	48.9	9.7
14TH	177.59	4.9	-50.8	1197	2063	4.1	-24.6	-1	0	214.6	-1864.9	378.6	46.1	9.7
15TH	190.42	4.9	-52.0	1197	2063	4.1	-25.2	-2	0	209.6	-1812.9	355.0	43.4	9.6
16TH	203.25	4.9	-53.3	1197	2063	4.1	-25.8	-3	0	204.7	-1759.6	332.1	40.8	9.5
17TH	216.08	6.2	-54.6	1197	2063	5.2	-26.4	-3	1	198.5	-1705.0	309.9	38.2	9.3
18TH	228.66	6.3	-54.0	1174	2023	5.4	-26.7	-3	1	192.2	-1651.0	288.8	35.7	9.2
19TH	241.24	6.3	-54.4	1174	2023	5.4	-26.9	-3	1	185.8	-1596.6	268.3	33.3	9.1
20TH	253.82	6.4	-54.7	1174	2023	5.4	-27.0	-4	1	179.5	-1541.9	248.6	31.0	8.9
21ST	266.40	6.4	-55.0	1174	2023	5.4	-27.2	-4	1	173.1	-1486.9	229.5	28.8	8.7
22ND	278.98	6.4	-55.4	1174	2023	5.4	-27.4	-5	1	166.7	-1431.5	211.2	26.7	8.5
23RD	291.56	6.4	-55.7	1174	2023	5.4	-27.5	-5	1	160.4	-1375.8	193.5	24.6	8.3
24TH	304.14	6.3	-56.3	1174	2023	5.4	-27.8	-5	1	154.1	-1319.4	176.6	22.7	8.1
25TH	316.72	6.0	-57.4	1174	2023	5.1	-28.4	-6	1	148.0	-1262.0	160.3	20.8	7.8
		5.7	-57.3	1151	1983	4.9	-28.9	-6	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 270 CONFIGURATION A REFERENCE PRESSURE*34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05	5.4	-58.3	1151	1983	4.7	-29.4	-7	1	142.4	-1204.7	145.1	19.0	7.5
27TH	341.38	5.2	-59.4	1151	1983	4.5	-29.9	-7	1	136.9	-1146.3	130.6	17.2	7.2
28TH	353.71	4.9	-60.4	1151	1983	4.3	-30.5	-8	1	131.8	-1087.0	116.9	15.6	6.9
29TH	366.04	5.5	-60.2	1127	1943	4.9	-31.0	-8	1	126.9	-1026.5	103.8	14.0	6.5
30TH	378.12	6.1	-60.7	1127	1943	5.4	-31.2	-7	1	121.4	-966.4	91.8	12.5	6.1
31ST	390.20	6.3	-61.0	1127	1943	5.6	-31.4	-7	1	115.3	-905.7	80.5	11.1	5.8
32ND	402.28	6.5	-61.3	1127	1943	5.8	-31.5	-8	1	109.0	-844.7	69.9	9.7	5.4
33RD	414.36	6.7	-61.5	1127	1943	5.9	-31.7	-8	1	102.5	-783.5	60.1	8.4	5.0
34TH	426.44	6.9	-61.8	1127	1943	6.1	-31.8	-8	1	95.8	-721.9	51.0	7.2	4.7
35TH	438.52	7.1	-62.1	1127	1943	6.3	-32.0	-8	1	88.9	-660.1	42.7	6.1	4.3
36TH	450.60	7.2	-62.4	1127	1943	6.4	-32.1	-8	2	81.8	-598.0	35.1	5.1	3.9
37TH	462.68	7.4	-62.3	1127	1943	6.6	-32.1	-8	2	74.5	-535.6	28.2	4.1	3.6
38TH	474.76	7.7	-62.2	1127	1943	6.8	-32.0	-8	2	67.1	-473.3	22.1	3.3	3.2
39TH	486.84	7.9	-62.1	1127	1943	7.0	-32.0	-8	2	59.4	-411.1	16.8	2.5	2.8
40TH	498.92	8.2	-62.0	1127	1943	7.2	-31.9	-9	2	51.5	-349.0	12.2	1.9	2.4
41ST	511.00	8.4	-61.9	1127	1943	7.5	-31.8	-9	2	43.3	-287.0	8.3	1.3	1.9
42ND	523.08	9.4	-64.3	1174	2023	8.0	-31.8	-9	2	34.9	-225.1	5.2	.8	1.5
43RD	535.66	10.5	-63.9	1206	2078	8.7	-30.8	-8	2	25.5	-160.8	2.8	.4	1.1
44TH	548.58	13.1	-79.7	1680	2895	7.8	-27.5	-7	2	15.0	-96.9	1.2	.2	.7
MR	566.58	1.9	-17.2	1085	2065	1.8	-8.3	-20	4	1.9	-17.2	.1	.0	.3
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 280 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									134.7	-2376.7	763.6	62.7	3.9
2ND	23.00	-4.2	-57.6	2147	3699	-2.0	-15.6	19	2	139.0	-2319.1	709.6	59.5	4.7
3RD	35.92	-6.3	-34.3	1206	2078	-5.2	-16.5	17	5	145.2	-2284.8	679.8	57.7	5.2
4TH	48.84	-6.4	-32.8	1206	2078	-5.3	-15.8	15	5	151.6	-2252.0	650.5	55.8	5.6
5TH	61.76	-5.4	-32.6	1206	2078	-4.5	-15.7	14	4	157.1	-2219.3	621.6	53.8	5.9
6TH	74.68	-4.3	-34.1	1206	2078	-3.6	-16.4	12	3	161.4	-2185.2	593.2	51.7	6.2
7TH	87.60	-3.2	-35.6	1206	2078	-2.7	-17.1	11	2	164.6	-2149.6	565.2	49.6	6.5
8TH	100.52	-2.1	-37.1	1206	2078	-1.7	-17.9	9	1	166.7	-2112.5	537.6	47.5	6.8
9TH	113.44	-1.0	-38.6	1206	2078	-.8	-18.6	8	0	167.7	-2073.9	510.6	45.3	7.1
10TH	126.27	.1	-39.8	1197	2063	.1	-19.3	7	-0	167.6	-2034.1	484.2	43.2	7.3
11TH	139.10	1.0	-41.2	1197	2063	.9	-20.0	6	-0	166.6	-1992.9	458.4	41.0	7.5
12TH	151.93	1.2	-42.8	1197	2063	1.0	-20.7	5	-0	165.3	-1950.2	433.1	38.9	7.7
13TH	164.76	1.5	-44.3	1197	2063	1.2	-21.5	3	-0	163.9	-1905.9	408.4	36.8	7.8
14TH	177.59	1.7	-45.8	1197	2063	1.4	-22.2	2	-0	162.2	-1860.1	384.2	34.7	7.9
15TH	190.42	1.9	-47.4	1197	2063	1.6	-23.0	1	-0	160.2	-1812.7	360.6	32.6	7.9
16TH	203.25	2.1	-48.9	1197	2063	1.8	-23.7	-0	0	158.1	-1763.8	337.7	30.6	7.9
17TH	216.08	3.7	-50.4	1197	2063	3.1	-24.4	0	-0	154.4	-1713.4	315.4	28.6	7.9
18TH	228.66	4.2	-50.5	1174	2023	3.6	-25.0	-1	0	150.2	-1662.9	294.2	26.7	7.9
19TH	241.24	4.4	-51.4	1174	2023	3.8	-25.4	-2	0	145.8	-1611.5	273.6	24.8	7.8
20TH	253.82	4.7	-52.3	1174	2023	4.0	-25.8	-2	0	141.1	-1559.2	253.6	23.0	7.7
21ST	266.40	5.0	-53.2	1174	2023	4.3	-26.3	-3	1	136.1	-1506.0	234.3	21.2	7.6
22ND	278.98	5.3	-54.1	1174	2023	4.5	-26.7	-4	1	130.8	-1452.0	215.7	19.6	7.4
23RD	291.56	5.5	-55.0	1174	2023	4.7	-27.2	-5	1	125.3	-1397.0	197.8	18.0	7.1
24TH	304.14	5.6	-56.0	1174	2023	4.8	-27.7	-6	1	119.6	-1341.0	180.6	16.4	6.9
25TH	316.72	5.4	-57.1	1174	2023	4.6	-28.2	-6	1	114.3	-1283.9	164.1	14.9	6.6
		5.0	-57.1	1151	1983	4.4	-28.8	-6	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 280 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05	4.8	-58.1	1151	1983	4.2	-29.3	-6	1	109.2	-1226.8	148.6	13.6	6.3
27TH	341.38	4.6	-59.2	1151	1983	4.0	-29.9	-6	1	104.4	-1168.7	133.8	12.2	6.0
28TH	353.71	4.4	-60.3	1151	1983	3.8	-30.4	-7	1	99.8	-1109.5	119.8	11.0	5.7
29TH	366.04	5.1	-60.1	1127	1943	4.5	-30.9	-6	1	95.4	-1049.2	106.5	9.8	5.4
30TH	378.12	5.6	-60.8	1127	1943	5.0	-31.3	-6	1	90.3	-989.1	94.2	8.7	5.1
31ST	390.20	5.7	-61.3	1127	1943	5.0	-31.6	-6	1	84.7	-928.3	82.6	7.6	4.8
32ND	402.28	5.7	-61.9	1127	1943	5.0	-31.9	-6	1	79.0	-867.0	71.7	6.6	4.5
33RD	414.36	5.7	-62.5	1127	1943	5.1	-32.1	-6	1	73.3	-805.1	61.6	5.7	4.2
34TH	426.44	5.7	-63.0	1127	1943	5.1	-32.4	-7	1	67.6	-742.6	52.3	4.8	3.9
35TH	438.52	5.7	-63.6	1127	1943	5.1	-32.7	-7	1	61.9	-679.6	43.7	4.1	3.5
36TH	450.60	5.7	-64.1	1127	1943	5.0	-33.0	-7	1	56.2	-616.0	35.9	3.3	3.2
37TH	462.68	5.6	-64.2	1127	1943	5.0	-33.1	-7	1	50.5	-551.9	28.8	2.7	2.9
38TH	474.76	5.6	-64.3	1127	1943	5.0	-33.1	-6	1	44.8	-487.7	22.6	2.1	2.5
39TH	486.84	5.6	-64.4	1127	1943	4.9	-33.1	-6	1	39.2	-423.4	17.0	1.6	2.2
40TH	498.92	5.5	-64.5	1127	1943	4.9	-33.2	-6	1	33.7	-359.0	12.3	1.2	1.9
41ST	511.00	5.5	-64.6	1127	1943	4.9	-33.2	-6	1	28.2	-294.5	8.4	.8	1.6
42ND	523.08	6.3	-67.3	1174	2023	5.4	-33.3	-5	1	22.7	-229.9	5.2	.5	1.3
43RD	535.66	7.5	-67.9	1206	2078	6.2	-32.2	-5	1	16.3	-162.6	2.7	.3	1.0
44TH	548.58	8.2	-82.9	1680	2895	4.9	-28.6	-7	1	8.9	-95.7	1.1	.1	.7
MR	566.58	.7	-12.8	1085	2065	.6	-6.2	-22	2	.7	-12.8	.1	.0	.2
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 290 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									136.6	-2112.1	693.0	58.6	-1.6
2ND	23.00	-2.3	-49.8	2147	3699	-1.1	-13.5	23	2	138.9	-2062.3	645.0	55.5	-.6
3RD	35.92	-4.9	-29.9	1206	2078	-4.0	-14.4	19	5	143.8	-2032.5	618.6	53.6	-.2
4TH	48.84	-5.0	-28.5	1206	2078	-4.2	-13.7	17	5	148.8	-2004.0	592.5	51.7	.2
5TH	61.76	-4.2	-28.2	1206	2078	-3.5	-13.6	17	4	153.0	-1975.8	566.8	49.8	.5
6TH	74.68	-3.3	-29.4	1206	2078	-2.7	-14.1	16	3	156.3	-1946.4	541.4	47.8	.9
7TH	87.60	-2.4	-30.5	1206	2078	-2.0	-14.7	15	2	158.7	-1915.9	516.5	45.8	1.3
8TH	100.52	-1.5	-31.6	1206	2078	-1.3	-15.2	14	1	160.3	-1884.2	491.9	43.7	1.6
9TH	113.44	-.7	-32.8	1206	2078	-.6	-15.8	13	0	160.9	-1851.5	467.8	41.6	1.9
10TH	126.27	.2	-33.7	1197	2063	.2	-16.3	12	-0	160.7	-1817.8	444.3	39.6	2.3
11TH	139.10	1.0	-34.8	1197	2063	.8	-16.9	11	-1	159.7	-1783.0	421.2	37.5	2.6
12TH	151.93	1.4	-36.1	1197	2063	1.2	-17.5	9	-1	158.4	-1746.9	398.5	35.5	2.8
13TH	164.76	1.8	-37.4	1197	2063	1.5	-18.1	7	-1	156.5	-1709.5	376.4	33.4	3.0
14TH	177.59	2.2	-38.7	1197	2063	1.9	-18.8	5	-1	154.3	-1670.8	354.7	31.5	3.2
15TH	190.42	2.7	-40.0	1197	2063	2.2	-19.4	4	-0	151.6	-1630.7	333.5	29.5	3.3
16TH	203.25	3.1	-41.3	1197	2063	2.6	-20.0	2	-0	148.5	-1589.4	312.8	27.6	3.4
17TH	216.08	4.7	-42.6	1197	2063	3.9	-20.7	3	-1	143.8	-1546.8	292.7	25.7	3.5
18TH	228.66	4.9	-42.8	1174	2023	4.2	-21.1	2	-0	139.0	-1504.0	273.5	23.9	3.5
19TH	241.24	4.9	-43.7	1174	2023	4.2	-21.6	2	-0	134.1	-1460.3	254.9	22.2	3.6
20TH	253.82	4.9	-44.5	1174	2023	4.2	-22.0	1	-0	129.2	-1415.8	236.8	20.5	3.6
21ST	266.40	4.9	-45.4	1174	2023	4.2	-22.4	0	-0	124.3	-1370.4	219.3	18.9	3.6
22ND	278.98	4.9	-46.3	1174	2023	4.2	-22.9	-0	0	119.4	-1324.1	202.3	17.4	3.6
23RD	291.56	4.9	-47.2	1174	2023	4.2	-23.3	-1	0	114.5	-1276.9	186.0	15.9	3.6
24TH	304.14	4.9	-48.1	1174	2023	4.1	-23.8	-1	0	109.7	-1228.8	170.2	14.5	3.6
25TH	316.72	4.8	-49.1	1174	2023	4.1	-24.3	-2	0	104.9	-1179.7	155.0	13.2	3.5
		4.6	-49.0	1151	1983	4.0	-24.7	-2	0					

TABLE 7. SHEAR AND MOMENT DIAGRAMS NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 290 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
										100.3	-1130.7	140.8	11.9	3.4
26TH	329.05	4.5	-49.9	1151	1983	3.9	-25.2	-3	0	95.8	-1080.8	127.2	10.7	3.3
27TH	341.38	4.4	-50.9	1151	1983	3.9	-25.6	-3	0	91.3	-1029.9	114.2	9.6	3.2
28TH	353.71	4.3	-51.8	1151	1983	3.8	-26.1	-3	0	87.0	-978.2	101.8	8.5	3.1
29TH	366.04	5.0	-51.6	1127	1943	4.4	-26.6	-3	1	82.0	-926.5	90.3	7.4	2.9
30TH	378.12	5.5	-52.7	1127	1943	4.9	-27.1	-3	1	76.5	-873.8	79.4	6.5	2.8
31ST	390.20	5.5	-54.0	1127	1943	4.9	-27.8	-3	1	71.0	-819.8	69.2	5.6	2.7
32ND	402.28	5.6	-55.2	1127	1943	5.0	-28.4	-3	1	65.4	-764.6	59.6	4.8	2.5
33RD	414.36	5.6	-56.4	1127	1943	5.0	-29.1	-4	1	59.8	-708.2	50.7	4.0	2.3
34TH	426.44	5.7	-57.7	1127	1943	5.1	-29.7	-4	1	54.1	-650.5	42.5	3.3	2.2
35TH	438.52	5.8	-58.9	1127	1943	5.1	-30.3	-4	1	48.3	-591.6	35.0	2.7	2.0
36TH	450.60	5.8	-60.1	1127	1943	5.1	-31.0	-4	1	42.5	-531.4	28.2	2.1	1.8
37TH	462.68	5.6	-60.5	1127	1943	4.9	-31.1	-4	1	36.9	-471.0	22.2	1.7	1.6
38TH	474.76	5.3	-60.7	1127	1943	4.7	-31.3	-4	1	31.6	-410.3	16.8	1.3	1.4
39TH	486.84	5.1	-61.0	1127	1943	4.5	-31.4	-4	1	26.5	-349.3	12.2	.9	1.2
40TH	498.92	4.8	-61.2	1127	1943	4.3	-31.5	-4	1	21.7	-288.1	8.4	.6	1.0
41ST	511.00	4.6	-61.5	1127	1943	4.1	-31.7	-4	0	17.1	-226.6	5.3	.4	.8
42ND	523.08	5.0	-64.3	1174	2023	4.2	-31.8	-4	0	12.1	-162.2	2.8	.2	.7
43RD	535.66	5.5	-64.4	1206	2078	4.6	-31.0	-4	1	6.6	-97.9	1.2	.1	.5
44TH	548.58	5.8	-80.9	1680	2895	3.5	-27.9	-5	1	.8	-17.0	.1	.0	.2
MR	566.58	.8	-17.0	1085	2065	.7	-8.2	-14	1	0.0	0.0	0.0	0.0	0.0
TOP	581.67													

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 300 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									201.5	-2016.0	665.4	84.1	-10.3
2ND	23.00	-5.6	-42.9	2147	3699	-2.6	-11.6	24	5	207.1	-1973.1	619.5	79.4	-9.5
3RD	35.92	-4.9	-28.4	1206	2078	-4.1	-13.6	21	6	212.0	-1944.8	594.2	76.7	-9.0
4TH	48.84	-4.2	-27.5	1206	2078	-3.4	-13.2	21	5	216.1	-1917.3	569.2	73.9	-8.6
5TH	61.76	-3.0	-27.5	1206	2078	-2.5	-13.2	22	4	219.1	-1889.8	544.6	71.1	-8.1
6TH	74.68	-2.2	-28.5	1206	2078	-1.9	-13.7	21	3	221.4	-1861.3	520.4	68.3	-7.6
7TH	87.60	-1.5	-29.6	1206	2078	-1.2	-14.2	19	2	222.8	-1831.7	496.5	65.4	-7.2
8TH	100.52	-.7	-30.6	1206	2078	-.6	-14.7	18	1	223.5	-1801.1	473.1	62.5	-6.7
9TH	113.44	.1	-31.7	1206	2078	.1	-15.2	17	-0	223.4	-1769.5	450.0	59.6	-6.3
10TH	126.27	.9	-32.5	1197	2063	.7	-15.7	16	-1	222.6	-1737.0	427.5	56.8	-5.8
11TH	139.10	1.5	-33.5	1197	2063	1.3	-16.2	15	-1	221.0	-1703.5	405.4	53.9	-5.4
12TH	151.93	2.0	-34.5	1197	2063	1.6	-16.7	14	-1	219.1	-1668.9	383.8	51.1	-5.1
13TH	164.76	2.4	-35.6	1197	2063	2.0	-17.2	12	-1	216.7	-1633.4	362.6	48.3	-4.7
14TH	177.59	2.8	-36.6	1197	2063	2.3	-17.7	11	-1	213.9	-1596.8	341.9	45.6	-4.4
15TH	190.42	3.2	-37.6	1197	2063	2.7	-18.2	10	-1	210.6	-1559.2	321.7	42.8	-4.1
16TH	203.25	3.6	-38.6	1197	2063	3.0	-18.7	9	-1	207.0	-1520.6	301.9	40.2	-3.8
17TH	216.08	5.2	-39.6	1197	2063	4.3	-19.2	10	-2	201.8	-1481.0	282.7	37.5	-3.5
18TH	228.66	5.6	-39.7	1174	2023	4.8	-19.6	9	-2	196.2	-1441.3	264.3	35.0	-3.2
19TH	241.24	5.9	-40.5	1174	2023	5.0	-20.0	9	-2	190.4	-1400.7	246.4	32.6	-3.0
20TH	253.82	6.2	-41.4	1174	2023	5.3	-20.4	8	-2	184.2	-1359.4	229.0	30.2	-2.7
21ST	266.40	6.5	-42.2	1174	2023	5.5	-20.9	7	-2	177.8	-1317.2	212.2	28.0	-2.5
22ND	278.98	6.8	-43.0	1174	2023	5.7	-21.3	6	-2	171.0	-1274.2	195.9	25.8	-2.3
23RD	291.56	7.0	-43.9	1174	2023	6.0	-21.7	6	-2	164.0	-1230.3	180.1	23.7	-2.1
24TH	304.14	7.1	-44.9	1174	2023	6.1	-22.2	5	-1	156.8	-1185.4	164.9	21.6	-1.9
25TH	316.72	6.9	-46.1	1174	2023	5.9	-22.8	4	-1	149.9	-1139.3	150.3	19.7	-1.7
		6.5	-46.4	1151	1983	5.7	-23.4	4	-1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 300 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									143.4	-1092.9	136.6	17.9	-1.6
		6.3	-47.6	1151	1983	5.4	-24.0	3	-1					
27TH	341.38									137.2	-1045.3	123.4	16.2	-1.5
		6.0	-48.7	1151	1983	5.2	-24.6	3	-1					
28TH	353.71									131.1	-996.6	110.8	14.5	-1.4
		5.8	-49.9	1151	1983	5.0	-25.2	3	-1					
29TH	366.04									125.4	-946.7	98.8	12.9	-1.3
		6.5	-50.0	1127	1943	5.7	-25.8	3	-1					
30TH	378.12									118.9	-896.6	87.7	11.5	-1.1
		7.1	-51.1	1127	1943	6.3	-26.3	3	-1					
31ST	390.20									111.7	-845.5	77.2	10.1	-1.0
		7.3	-52.1	1127	1943	6.5	-26.8	3	-1					
32ND	402.28									104.4	-793.4	67.3	8.8	-.9
		7.5	-53.2	1127	1943	6.6	-27.4	3	-1					
33RD	414.36									97.0	-740.2	58.0	7.5	-.8
		7.6	-54.2	1127	1943	6.8	-27.9	3	-1					
34TH	426.44									89.4	-686.0	49.4	6.4	-.6
		7.8	-55.2	1127	1943	6.9	-28.4	3	-1					
35TH	438.52									81.6	-630.8	41.4	5.4	-.5
		7.9	-56.2	1127	1943	7.0	-29.0	3	-1					
36TH	450.60									73.7	-574.6	34.2	4.5	-.4
		8.1	-57.3	1127	1943	7.1	-29.5	3	-1					
37TH	462.68									65.6	-517.3	27.6	3.6	-.3
		7.8	-57.9	1127	1943	6.9	-29.8	2	-1					
38TH	474.76									57.8	-459.4	21.7	2.9	-.2
		7.5	-58.5	1127	1943	6.7	-30.1	2	-0					
39TH	486.84									50.3	-400.9	16.5	2.2	-.1
		7.2	-59.1	1127	1943	6.4	-30.4	2	-0					
40TH	498.92									43.1	-341.8	12.0	1.6	-.0
		6.9	-59.7	1127	1943	6.1	-30.7	1	-0					
41ST	511.00									36.2	-282.1	8.2	1.2	.1
		6.6	-60.3	1127	1943	5.9	-31.0	1	-0					
42ND	523.08									29.5	-221.9	5.2	.8	.1
		7.1	-63.4	1174	2023	6.1	-31.3	1	-0					
43RD	535.66									22.4	-158.5	2.8	.4	.2
		8.0	-63.4	1206	2078	6.6	-30.5	1	-0					
44TH	548.58									14.4	-95.1	1.1	.2	.2
		9.7	-78.5	1680	2895	5.8	-27.1	-1	0					
MR	566.58									4.7	-16.6	.1	.0	.1
		4.7	-16.6	1085	2065	4.3	-8.0	-11	5					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 310 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									186.6	-1871.2	624.0	84.1	-15.8
2ND	23.00	-6.8	-42.4	2147	3699	-3.2	-11.5	23	6	193.4	-1828.8	581.4	79.7	-15.1
3RD	35.92	-4.7	-25.9	1206	2078	-3.9	-12.5	20	6	198.1	-1802.9	558.0	77.2	-14.7
4TH	48.84	-3.9	-25.0	1206	2078	-3.2	-12.0	20	5	202.0	-1777.9	534.8	74.6	-14.3
5TH	61.76	-2.7	-24.9	1206	2078	-2.3	-12.0	20	4	204.7	-1753.0	512.0	72.0	-13.9
6TH	74.68	-2.0	-25.6	1206	2078	-1.7	-12.3	20	3	206.8	-1727.5	489.5	69.3	-13.5
7TH	87.60	-1.3	-26.3	1206	2078	-1.1	-12.6	19	2	208.1	-1701.2	467.4	66.7	-13.1
8TH	100.52	-.6	-27.0	1206	2078	-.5	-13.0	19	1	208.7	-1674.2	445.6	64.0	-12.7
9TH	113.44	.1	-27.7	1206	2078	.1	-13.3	18	-0	208.7	-1646.5	424.1	61.3	-12.3
10TH	126.27	.8	-28.2	1197	2063	.6	-13.7	18	-1	207.9	-1618.3	403.2	58.6	-11.9
11TH	139.10	1.3	-29.0	1197	2063	1.1	-14.1	17	-1	206.5	-1589.3	382.6	55.9	-11.5
12TH	151.93	1.4	-30.1	1197	2063	1.2	-14.6	16	-1	205.1	-1559.1	362.4	53.3	-11.1
13TH	164.76	1.5	-31.3	1197	2063	1.3	-15.2	14	-1	203.6	-1527.8	342.6	50.7	-10.7
14TH	177.59	1.6	-32.4	1197	2063	1.3	-15.7	13	-1	202.0	-1495.4	323.2	48.1	-10.4
15TH	190.42	1.7	-33.6	1197	2063	1.4	-16.3	12	-1	200.3	-1461.8	304.2	45.5	-10.1
16TH	203.25	1.8	-34.8	1197	2063	1.5	-16.8	11	-1	198.5	-1427.0	285.7	42.9	-9.8
17TH	216.08	2.8	-35.9	1197	2063	2.3	-17.4	11	-1	195.7	-1391.1	267.6	40.4	-9.5
18TH	228.66	3.2	-36.1	1174	2023	2.8	-17.8	11	-2	192.5	-1355.0	250.4	38.0	-9.2
19TH	241.24	3.6	-36.9	1174	2023	3.1	-18.3	11	-2	188.8	-1318.1	233.6	35.6	-8.8
20TH	253.82	4.0	-37.8	1174	2023	3.4	-18.7	10	-2	184.8	-1280.3	217.2	33.2	-8.5
21ST	266.40	4.4	-38.6	1174	2023	3.8	-19.1	10	-2	180.4	-1241.7	201.3	30.9	-8.2
22ND	278.98	4.8	-39.5	1174	2023	4.1	-19.5	9	-2	175.6	-1202.2	186.0	28.7	-7.9
23RD	291.56	5.2	-40.3	1174	2023	4.4	-19.9	9	-2	170.4	-1161.9	171.1	26.5	-7.6
24TH	304.14	5.4	-41.3	1174	2023	4.6	-20.4	9	-2	165.0	-1120.6	156.7	24.4	-7.4
25TH	316.72	5.4	-42.5	1174	2023	4.6	-21.0	9	-2	159.5	-1078.2	142.9	22.4	-7.1
		5.3	-42.8	1151	1983	4.6	-21.6	9	-2					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 310 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									154.2	-1035.4	129.9	20.4	-6.8
		5.3	-43.9	1151	1983	4.6	-22.1	9	-2					
27TH	341.38									148.8	-991.5	117.4	18.6	-6.5
		5.3	-45.0	1151	1983	4.6	-22.7	9	-2					
28TH	353.71									143.5	-946.6	105.4	16.8	-6.1
		5.3	-46.1	1151	1983	4.6	-23.2	9	-2					
29TH	366.04									138.2	-900.5	94.1	15.0	-5.8
		6.0	-46.2	1127	1943	5.3	-23.8	10	-2					
30TH	378.12									132.2	-854.2	83.5	13.4	-5.5
		6.7	-47.5	1127	1943	5.9	-24.5	10	-2					
31ST	390.20									125.5	-806.7	73.4	11.8	-5.1
		7.0	-48.8	1127	1943	6.2	-25.1	10	-2					
32ND	402.28									118.5	-757.9	64.0	10.4	-4.7
		7.4	-50.2	1127	1943	6.5	-25.8	10	-3					
33RD	414.36									111.1	-707.7	55.1	9.0	-4.3
		7.7	-51.5	1127	1943	6.8	-26.5	10	-3					
34TH	426.44									103.4	-656.2	46.9	7.7	-3.9
		8.1	-52.8	1127	1943	7.1	-27.2	10	-3					
35TH	438.52									95.3	-603.4	39.3	6.5	-3.5
		8.4	-54.2	1127	1943	7.5	-27.9	10	-3					
36TH	450.60									86.9	-549.2	32.3	5.4	-3.0
		8.7	-55.5	1127	1943	7.7	-28.5	10	-3					
37TH	462.68									78.2	-493.8	26.0	4.4	-2.6
		8.6	-56.0	1127	1943	7.7	-28.8	9	-2					
38TH	474.76									69.6	-437.8	20.4	3.5	-2.2
		8.5	-56.5	1127	1943	7.6	-29.1	9	-2					
39TH	486.84									61.0	-381.3	15.4	2.7	-1.8
		8.4	-57.0	1127	1943	7.5	-29.3	8	-2					
40TH	498.92									52.6	-324.3	11.2	2.0	-1.5
		8.3	-57.5	1127	1943	7.4	-29.6	7	-2					
41ST	511.00									44.3	-266.8	7.6	1.4	-1.1
		8.2	-57.9	1127	1943	7.3	-29.8	7	-2					
42ND	523.08									36.1	-208.9	4.7	.9	-.8
		9.0	-60.9	1174	2023	7.7	-30.1	7	-2					
43RD	535.66									27.2	-148.0	2.5	.5	-.5
		9.9	-60.9	1206	2078	8.3	-29.3	6	-2					
44TH	548.58									17.2	-87.1	1.0	.3	-.2
		11.3	-75.9	1680	2895	6.7	-26.2	3	-1					
MR	566.58									5.9	-11.2	.1	.0	.0
		5.9	-11.2	1085	2065	5.4	-5.4	-4	3					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 320 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									39.3	-1564.9	529.3	33.5	-21.0
2ND	23.00	-7.2	-34.7	2147	3699	-3.3	-9.4	25	9	46.4	-1530.2	493.7	32.5	-20.3
3RD	35.92	-4.8	-21.7	1206	2078	-3.9	-10.4	21	8	51.2	-1508.6	474.1	31.9	-20.0
4TH	48.84	-3.8	-21.0	1206	2078	-3.1	-10.1	22	7	55.0	-1487.6	454.8	31.2	-19.6
5TH	61.76	-3.1	-20.8	1206	2078	-2.6	-10.0	23	6	58.1	-1466.8	435.7	30.5	-19.2
6TH	74.68	-2.9	-21.3	1206	2078	-2.4	-10.2	23	5	60.9	-1445.5	416.9	29.7	-18.9
7TH	87.60	-2.7	-21.7	1206	2078	-2.2	-10.4	22	5	63.6	-1423.8	398.3	28.9	-18.5
8TH	100.52	-2.5	-22.2	1206	2078	-2.0	-10.7	21	4	66.1	-1401.7	380.1	28.1	-18.1
9TH	113.44	-2.3	-22.6	1206	2078	-1.9	-10.9	21	4	68.3	-1379.1	362.1	27.2	-17.8
10TH	126.27	-2.0	-22.9	1197	2063	-1.7	-11.1	20	3	70.4	-1356.1	344.6	26.3	-17.4
11TH	139.10	-1.9	-23.4	1197	2063	-1.6	-11.3	20	3	72.2	-1332.7	327.3	25.4	-17.0
12TH	151.93	-1.7	-24.1	1197	2063	-1.4	-11.7	18	2	74.0	-1308.7	310.4	24.4	-16.7
13TH	164.76	-1.6	-24.7	1197	2063	-1.3	-12.0	16	2	75.6	-1284.0	293.7	23.5	-16.4
14TH	177.59	-1.5	-25.4	1197	2063	-1.2	-12.3	15	1	77.0	-1258.6	277.4	22.5	-16.1
15TH	190.42	-1.3	-26.1	1197	2063	-1.1	-12.6	13	1	78.3	-1232.5	261.4	21.5	-15.8
16TH	203.25	-1.2	-26.7	1197	2063	-1.0	-12.9	12	1	79.5	-1205.8	245.8	20.5	-15.5
17TH	216.08	-.4	-27.4	1197	2063	-.3	-13.3	13	0	79.9	-1178.4	230.5	19.5	-15.2
18TH	228.66	-.2	-27.7	1174	2023	-.1	-13.7	14	0	80.1	-1150.7	215.8	18.5	-14.9
19TH	241.24	-.1	-28.6	1174	2023	-.1	-14.1	14	0	80.1	-1122.1	201.6	17.5	-14.6
20TH	253.82	.0	-29.5	1174	2023	.0	-14.6	14	-0	80.1	-1092.6	187.6	16.5	-14.3
21ST	266.40	.1	-30.4	1174	2023	.1	-15.0	14	-0	80.0	-1062.2	174.1	15.4	-13.9
22ND	278.98	.2	-31.3	1174	2023	.2	-15.5	14	-0	79.8	-1030.9	160.9	14.4	-13.6
23RD	291.56	.3	-32.2	1174	2023	.3	-15.9	14	-0	79.5	-998.7	148.1	13.4	-13.2
24TH	304.14	.4	-33.4	1174	2023	.4	-16.5	14	-0	79.0	-965.3	135.8	12.4	-12.8
25TH	316.72	.6	-34.9	1174	2023	.5	-17.2	14	-0	78.4	-930.5	123.9	11.5	-12.5
		.7	-35.6	1151	1983	.6	-17.9	14	-0					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 320 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									77.7	-894.9	112.6	10.5	-12.1
		.8	-37.0	1151	1983	.7	-18.7	14	-1					
27TH	341.38									76.9	-857.9	101.8	9.5	-11.6
		1.0	-38.4	1151	1983	.8	-19.4	14	-1					
28TH	353.71									75.9	-819.4	91.5	8.6	-11.2
		1.1	-39.8	1151	1983	1.0	-20.1	14	-1					
29TH	366.04									74.8	-779.6	81.6	7.7	-10.8
		2.2	-40.4	1127	1943	1.9	-20.8	15	-1					
30TH	378.12									72.6	-739.2	72.4	6.8	-10.3
		3.2	-41.5	1127	1943	2.8	-21.4	17	-2					
31ST	390.20									69.4	-697.7	63.7	5.9	-9.7
		3.7	-42.4	1127	1943	3.3	-21.8	17	-3					
32ND	402.28									65.7	-655.3	55.6	5.1	-9.1
		4.2	-43.3	1127	1943	3.8	-22.3	18	-3					
33RD	414.36									61.5	-612.0	47.9	4.3	-8.5
		4.8	-44.3	1127	1943	4.2	-22.8	18	-3					
34TH	426.44									56.7	-567.7	40.8	3.6	-7.9
		5.3	-45.2	1127	1943	4.7	-23.3	19	-4					
35TH	438.52									51.4	-522.6	34.2	3.0	-7.2
		5.8	-46.1	1127	1943	5.2	-23.7	19	-4					
36TH	450.60									45.6	-476.5	28.2	2.4	-6.6
		6.4	-47.0	1127	1943	5.7	-24.2	19	-4					
37TH	462.68									39.2	-429.4	22.7	1.9	-5.8
		6.0	-47.8	1127	1943	5.3	-24.6	19	-4					
38TH	474.76									33.2	-381.7	17.8	1.4	-5.1
		5.5	-48.5	1127	1943	4.9	-25.0	18	-3					
39TH	486.84									27.8	-333.1	13.5	1.1	-4.4
		5.0	-49.3	1127	1943	4.4	-25.4	18	-3					
40TH	498.92									22.8	-283.8	9.8	.8	-3.7
		4.5	-50.0	1127	1943	4.0	-25.8	17	-3					
41ST	511.00									18.3	-233.8	6.6	.5	-3.1
		4.0	-50.8	1127	1943	3.5	-26.2	17	-2					
42ND	523.08									14.3	-183.0	4.1	.3	-2.4
		4.4	-53.7	1174	2023	3.7	-26.5	17	-2					
43RD	535.66									10.0	-129.3	2.2	.2	-1.7
		5.0	-53.9	1206	2078	4.2	-25.9	17	-3					
44TH	548.58									4.9	-75.4	.8	.1	-.9
		3.8	-66.2	1680	2895	2.2	-22.9	14	-1					
MR	566.58									1.2	-9.2	.1	.0	-.2
		1.2	-9.2	1085	2065	1.1	-4.5	24	-5					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 330 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00													
		-4.1	-29.9	2147	3699	-1.9	-8.1	27	6	-215.8	-1250.9	421.5	-75.6	-25.3
2ND	23.00													
		-3.1	-18.3	1206	2078	-2.6	-8.8	23	7	-211.7	-1221.1	393.0	-70.7	-24.6
3RD	35.92													
		-2.6	-17.5	1206	2078	-2.1	-8.4	24	6	-208.6	-1202.8	377.4	-68.0	-24.3
4TH	48.84													
		-2.2	-17.2	1206	2078	-1.8	-8.3	26	6	-206.1	-1185.3	362 0	-65.3	-24.0
5TH	61.76													
		-2.1	-17.5	1206	2078	-1.7	-8.4	25	5	-203.9	-1168.1	346.8	-62.6	-23.6
6TH	74.68													
		-2.0	-17.8	1206	2078	-1.6	-8.6	25	5	-201.8	-1150.6	331.8	-60.0	-23.3
7TH	87.60													
		-1.8	-18.1	1206	2078	-1.5	-8.7	24	4	-199.8	-1132.8	317.0	-57.4	-22.9
8TH	100.52													
		-1.7	-18.4	1206	2078	-1.4	-8.8	24	4	-198.0	-1114.8	302.5	-54.9	-22.6
9TH	113.44													
		-1.6	-18.6	1197	2063	-1.3	-9.0	24	3	-196.3	-1096.4	288.2	-52.3	-22.2
10TH	126.27													
		-1.6	-18.9	1197	2063	-1.3	-9.2	23	3	-194.7	-1077.8	274.3	-49.8	-21.9
11TH	139.10													
		-2.0	-19.5	1197	2063	-1.7	-9.4	22	4	-193.1	-1058.9	260.6	-47.3	-21.5
12TH	151.93													
		-2.5	-20.1	1197	2063	-2.1	-9.7	21	4	-191.1	-1039.5	247.1	-44.8	-21.2
13TH	164.76													
		-2.9	-20.7	1197	2063	-2.4	-10.0	20	5	-188.6	-1019.4	233.9	-42.4	-20.8
14TH	177.59													
		-3.4	-21.2	1197	2063	-2.8	-10.3	20	5	-185.7	-998.8	221.0	-40.0	-20.5
15TH	190.42													
		-3.8	-21.8	1197	2063	-3.2	-10.6	19	6	-182.3	-977.5	208.3	-37.6	-20.2
16TH	203.25													
		-3.9	-22.4	1197	2063	-3.2	-10.9	20	6	-178.5	-955.7	195.9	-35.3	-19.9
17TH	216.08													
		-4.1	-22.5	1174	2023	-3.5	-11.1	21	7	-174.6	-933.2	183.8	-33.1	-19.5
18TH	228.66													
		-4.5	-23.0	1174	2023	-3.8	-11.3	22	7	-170 5	-910.8	172.2	-30.9	-19.2
19TH	241.24													
		-4.8	-23.4	1174	2023	-4.1	-11.6	22	8	-166.1	-887.8	160.8	-28.8	-18.8
20TH	253.82													
		-5.2	-23.9	1174	2023	-4.5	-11.8	23	9	-161.2	-864.4	149.8	-26.7	-18.4
21ST	266.40													
		-5.6	-24.4	1174	2023	-4.8	-12.0	24	9	-156.0	-840.5	139.1	-24.7	-18.0
22ND	278.98													
		-6.0	-24.8	1174	2023	-5.1	-12.3	25	10	-150.4	-816.1	128.7	-22.8	-17.5
23RD	291.56													
		-6.2	-25.6	1174	2023	-5.3	-12.6	25	10	-144.4	-791.3	118.6	-20.9	-17.0
24TH	304.14													
		-6.3	-26.7	1174	2023	-5.4	-13.2	25	10	-138.2	-765.7	108.8	-19.2	-16.6
25TH	316.72													
		-6.3	-27.2	1151	1983	-5.5	-13.7	26	10	-131.9	-739.0	99.3	-17.5	-16.1

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 330 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-125.6	-711.8	90.4	-15.9	-15.5
27TH	341.38	-6.4	-28.2	1151	1983	-5.6	-14.2	26	10	-119.2	-683.6	81.8	-14.4	-15.0
28TH	353.71	-6.5	-29.3	1151	1983	-5.7	-14.8	26	10	-112.6	-654.3	73.5	-12.9	-14.4
29TH	366.04	-6.6	-30.3	1151	1983	-5.7	-15.3	27	10	-106.0	-623.9	65.6	-11.6	-13.8
30TH	378.12	-5.9	-30.7	1127	1943	-5.2	-15.8	29	9	-100.1	-593.2	58.3	-10.3	-13.1
31ST	390.20	-5.5	-31.8	1127	1943	-4.8	-16.4	30	9	-94.7	-561.4	51.3	-9.2	-12.3
32ND	402.28	-5.5	-33.0	1127	1943	-4.9	-17.0	30	8	-89.2	-528.4	44.7	-8.1	-11.6
33RD	414.36	-5.5	-34.1	1127	1943	-4.9	-17.6	30	8	-83.6	-494.3	38.6	-7.0	-10.8
34TH	426.44	-5.6	-35.3	1127	1943	-4.9	-18.1	30	8	-78.1	-459.1	32.8	-6.0	-10.0
35TH	438.52	-5.6	-36.4	1127	1943	-5.0	-18.7	30	8	-72.5	-422.7	27.5	-5.1	-9.1
36TH	450.60	-5.6	-37.5	1127	1943	-5.0	-19.3	30	8	-66.8	-385.1	22.6	-4.3	-8.3
37TH	462.68	-5.6	-38.7	1127	1943	-5.0	-19.9	30	7	-61.2	-346.5	18.2	-3.5	-7.4
38TH	474.76	-5.9	-39.2	1127	1943	-5.2	-20.2	29	7	-55.4	-307.3	14.2	-2.8	-6.5
39TH	486.84	-6.2	-39.6	1127	1943	-5.5	-20.4	28	8	-49.2	-267.7	10.8	-2.2	-5.6
40TH	498.92	-6.5	-40.0	1127	1943	-5.8	-20.6	28	8	-42.7	-227.7	7.8	-1.6	-4.8
41ST	511.00	-6.8	-40.4	1127	1943	-6.1	-20.8	27	8	-35.8	-187.3	5.3	-1.1	-3.9
42ND	523.08	-7.1	-40.8	1127	1943	-6.3	-21.0	26	8	-28.7	-146.5	3.2	-.8	-3.1
43RD	535.66	-7.3	-43.0	1174	2023	-6.2	-21.2	27	8	-21.4	-103.5	1.7	-.4	-2.2
44TH	548.58	-6.7	-43.5	1206	2078	-5.6	-20.9	27	7	-14.7	-60.0	.6	-.2	-1.3
MR	566.58	-10.0	-56.1	1680	2895	-6.0	-19.4	23	7	-4.7	-4.0	.0	-.0	-.3
TOP	581.67	-4.7	-4.0	1085	2065	-4.3	-1.9	-232	-465	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 340 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-344.3	-1054.1	351.1	-137.2	-24.3
2ND	23.00	-2.6	-24.1	2147	3699	-1.2	-6.5	24	4	-341.7	-1030.0	327.1	-129.3	-23.8
3RD	35.92	-1.6	-14.7	1206	2078	-1.4	-7.1	21	4	-340.1	-1015.3	313.9	-124.9	-23.6
4TH	48.84	-1.5	-14.0	1206	2078	-1.3	-6.7	23	4	-338.5	-1001.3	300.9	-120.5	-23.3
5TH	61.76	-1.4	-13.8	1206	2078	-1.2	-6.6	25	4	-337.1	-987.6	288.0	-116.2	-23.1
6TH	74.68	-1.2	-14.2	1206	2078	-1.0	-6.8	26	4	-335.9	-973.3	275.3	-111.8	-22.8
7TH	87.60	-.9	-14.7	1206	2078	-.8	-7.1	26	3	-335.0	-958.6	262.9	-107.5	-22.5
8TH	100.52	-.7	-15.2	1206	2078	-.6	-7.3	27	2	-334.3	-943.5	250.6	-103.2	-22.1
9TH	113.44	-.5	-15.6	1206	2078	-.4	-7.5	28	1	-333.8	-927.8	238.5	-98.8	-21.8
10TH	126.27	-.2	-16.0	1197	2063	-.2	-7.7	28	1	-333.6	-911.9	226.7	-94.6	-21.4
11TH	139.10	-.2	-16.5	1197	2063	-.2	-8.0	29	1	-333.4	-895.4	215.1	-90.3	-21.1
12TH	151.93	-.8	-17.3	1197	2063	-.6	-8.4	28	2	-332.6	-878.1	203.7	-86.0	-20.7
13TH	164.76	-1.4	-18.1	1197	2063	-1.1	-8.8	27	3	-331.2	-860.0	192.6	-81.8	-20.3
14TH	177.59	-1.9	-18.9	1197	2063	-1.6	-9.2	26	5	-329.3	-841.1	181.7	-77.5	-19.9
15TH	190.42	-2.5	-19.7	1197	2063	-2.1	-9.6	25	6	-326.8	-821.3	171.0	-73.3	-19.5
16TH	203.25	-3.1	-20.6	1197	2063	-2.6	-10.0	25	6	-323.7	-800.8	160.6	-69.1	-19.1
17TH	216.08	-3.2	-21.4	1197	2063	-2.6	-10.4	26	7	-320.5	-779.4	150.4	-65.0	-18.7
18TH	228.66	-4.0	-21.3	1174	2023	-3.4	-10.5	27	9	-316.5	-758.1	140.8	-61.0	-18.2
19TH	241.24	-5.0	-21.4	1174	2023	-4.3	-10.6	27	11	-311.5	-736.7	131.4	-57.0	-17.8
20TH	253.82	-6.1	-21.6	1174	2023	-5.2	-10.7	28	13	-305.4	-715.1	122.2	-53.2	-17.3
21ST	266.40	-7.1	-21.8	1174	2023	-6.0	-10.8	28	16	-298.3	-693.3	113.4	-49.4	-16.9
22ND	278.98	-8.1	-21.9	1174	2023	-6.9	-10.8	29	18	-290.2	-671.4	104.8	-45.7	-16.5
23RD	291.56	-9.2	-22.1	1174	2023	-7.8	-10.9	30	21	-281.1	-649.3	96.5	-42.1	-16.0
24TH	304.14	-9.9	-22.6	1174	2023	-8.4	-11.1	31	23	-271.1	-626.7	88.5	-38.6	-15.6
25TH	316.72	-10.3	-23.2	1174	2023	-8.8	-11.5	32	24	-260.8	-603.5	80.7	-35.3	-15.1
		-10.5	-23.4	1151	1983	-9.1	-11.8	33	25					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 340 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-250.3	-580.2	73.4	-32.1	-14.6
		-10.9	-24.0	1151	1983	-9.5	-12.1	34	26					
27TH	341.38									-239.4	-556.2	66.4	-29.1	-14.1
		-11.3	-24.6	1151	1983	-9.8	-12.4	35	27					
28TH	353.71									-228.1	-531.6	59.7	-26.2	-13.6
		-11.7	-25.2	1151	1983	-10.2	-12.7	36	28					
29TH	366.04									-216.4	-506.4	53.3	-23.5	-13.0
		-11.5	-25.3	1127	1943	-10.2	-13.0	38	29					
30TH	378.12									-204.9	-481.2	47.4	-20.9	-12.4
		-11.4	-26.0	1127	1943	-10.1	-13.4	39	29					
31ST	390.20									-193.6	-455.1	41.7	-18.5	-11.7
		-11.5	-26.9	1127	1943	-10.2	-13.9	39	28					
32ND	402.28									-182.1	-428.2	36.4	-16.2	-11.0
		-11.6	-27.8	1127	1943	-10.3	-14.3	39	28					
33RD	414.36									-170.5	-400.4	31.4	-14.1	-10.3
		-11.7	-28.7	1127	1943	-10.4	-14.8	39	27					
34TH	426.44									-158.8	-371.7	26.7	-12.1	-9.6
		-11.8	-29.5	1127	1943	-10.5	-15.2	39	27					
35TH	438.52									-146.9	-342.2	22.4	-10.3	-8.8
		-11.9	-30.4	1127	1943	-10.6	-15.7	39	26					
36TH	450.60									-135.0	-311.8	18.4	-8.6	-8.0
		-11.9	-31.3	1127	1943	-10.5	-16.1	39	25					
37TH	462.68									-123.1	-280.5	14.9	-7.0	-7.2
		-12.2	-31.6	1127	1943	-10.9	-16.2	39	26					
38TH	474.76									-110.9	-249.0	11.7	-5.6	-6.3
		-12.7	-31.8	1127	1943	-11.2	-16.4	39	26					
39TH	486.84									-98.2	-217.2	8.8	-4.3	-5.5
		-13.1	-32.1	1127	1943	-11.6	-16.5	39	27					
40TH	498.92									-85.1	-185.1	6.4	-3.2	-4.7
		-13.5	-32.3	1127	1943	-12.0	-16.6	39	27					
41ST	511.00									-71.6	-152.8	4.4	-2.3	-3.8
		-13.9	-32.6	1127	1943	-12.4	-16.8	38	28					
42ND	523.08									-57.7	-120.2	2.7	-1.5	-3.0
		-14.6	-34.2	1174	2023	-12.4	-16.9	39	28					
43RD	535.66									-43.1	-86.1	1.4	-.9	-2.2
		-14.5	-34.8	1206	2078	-12.0	-16.8	38	27					
44TH	548.58									-28.6	-51.2	.5	-.4	-1.3
		-19.4	-46.6	1680	2895	-11.6	-16.1	32	22					
MR	566.58									-9.2	-4.7	.0	-.1	-.3
		-9.2	-4.7	1085	2065	-8.4	-2.3	-29	-96					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 350 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-352.6	-859.0	285.8	-144.0	-21.1
2ND	23.00	-.0	-19.7	2147	3699	-.0	-5.3	26	0	-352.5	-839.2	266.3	-135.9	-20.7
3RD	35.92	-.4	-11.4	1206	2078	-.4	-5.5	22	2	-352.1	-827.9	255.5	-131.3	-20.5
4TH	48.84	-.6	-11.0	1206	2078	-.5	-5.3	23	2	-351.5	-816.8	244.9	-126.8	-20.3
5TH	61.76	-.5	-11.0	1206	2078	-.4	-5.3	25	2	-351.0	-805.8	234.4	-122.2	-20.1
6TH	74.68	-.3	-11.5	1206	2078	-.3	-5.5	26	1	-350.6	-794.3	224.1	-117.7	-19.9
7TH	87.60	-.1	-11.9	1206	2078	-.1	-5.7	27	1	-350.5	-782.5	213.9	-113.2	-19.6
8TH	100.52	.1	-12.3	1206	2078	.0	-5.9	29	-0	-350.5	-770.1	203.8	-108.6	-19.3
9TH	113.44	.3	-12.7	1206	2078	.2	-6.1	30	-1	-350.8	-757.4	194.0	-104.1	-19.0
10TH	126.27	.5	-13.1	1197	2063	.4	-6.3	31	-2	-351.3	-744.3	184.3	-99.6	-18.7
11TH	139.10	.5	-13.5	1197	2063	.4	-6.6	32	-2	-351.7	-730.8	174.9	-95.1	-18.3
12TH	151.93	-.2	-14.2	1197	2063	-.2	-6.9	30	1	-351.5	-716.5	165.6	-90.6	-18.0
13TH	164.76	-.9	-14.9	1197	2063	-.8	-7.2	29	3	-350.5	-701.6	156.5	-86.1	-17.7
14TH	177.59	-1.7	-15.7	1197	2063	-1.4	-7.6	28	5	-348.9	-685.9	147.6	-81.6	-17.3
15TH	190.42	-2.4	-16.4	1197	2063	-2.0	-7.9	27	7	-346.5	-669.6	138.9	-77.1	-17.0
16TH	203.25	-3.1	-17.1	1197	2063	-2.6	-8.3	26	8	-343.4	-652.5	130.4	-72.7	-16.6
17TH	216.08	-3.4	-17.8	1197	2063	-2.8	-8.6	28	9	-349.1	-634.7	122.2	-68.3	-16.2
18TH	228.66	-4.4	-17.6	1174	2023	-3.7	-8.7	29	12	-335.7	-617.1	114.3	-64.1	-15.9
19TH	241.24	-5.6	-17.7	1174	2023	-4.8	-8.8	30	16	-330.1	-599.4	106.6	-59.9	-15.5
20TH	253.82	-6.8	-17.8	1174	2023	-5.8	-8.8	31	20	-323.3	-581.6	99.2	-55.8	-15.1
21ST	266.40	-8.0	-17.9	1174	2023	-6.8	-8.8	34	26	-315.3	-563.7	92.0	-51.8	-14.7
22ND	278.98	-9.2	-18.0	1174	2023	-7.8	-8.9	36	32	-306.2	-545.7	85.0	-47.9	-14.3
23RD	291.56	-10.4	-18.0	1174	2023	-8.8	-8.9	40	39	-295.8	-527.7	78.3	-44.1	-13.9
24TH	304.14	-11.2	-18.5	1174	2023	-9.5	-9.1	43	44	-284.6	-509.3	71.8	-40.4	-13.5
25TH	316.72	-11.4	-19.1	1174	2023	-9.7	-9.4	44	44	-273.2	-490.2	65.5	-36.9	-13.1
		-11.4	-19.3	1151	1983	-9.9	-9.7	44	45					

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
WIND DIRECTION 350 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
										-261.8	-470.9	59.5	-33.6	-12.7
26TH	329.05	-11.7	-19.9	1151	1983	-10.2	-10.0	45	45	-250.1	-451.1	53.9	-30.5	-12.2
27TH	341.38	-11.9	-20.4	1151	1983	-10.4	-10.3	46	46	-238.1	-430.6	48.4	-27.4	-11.7
28TH	353.71	-12.2	-21.0	1151	1983	-10.6	-10.6	47	46	-226.0	-409.6	43.2	-24.6	-11.2
29TH	366.04	-11.9	-21.2	1127	1943	-10.6	-10.9	48	46	-214.0	-388.4	38.4	-21.9	-10.6
30TH	378.12	-11.9	-21.7	1127	1943	-10.5	-11.1	49	46	-202.1	-366.8	33.9	-19.4	-10.0
31ST	390.20	-12.0	-22.1	1127	1943	-10.6	-11.4	49	45	-190.2	-344.6	29.6	-17.0	-9.4
32ND	402.28	-12.1	-22.6	1127	1943	-10.7	-11.6	49	44	-178.1	-322.0	25.5	-14.8	-8.8
33RD	414.36	-12.2	-23.1	1127	1943	-10.8	-11.9	48	43	-165.9	-298.9	21.8	-12.7	-8.1
34TH	426.44	-12.3	-23.6	1127	1943	-10.9	-12.1	48	43	-153.7	-275.3	18.3	-10.8	-7.5
35TH	438.52	-12.4	-24.1	1127	1943	-11.0	-12.4	48	42	-141.3	-251.2	15.1	-9.0	-6.8
36TH	450.60	-12.3	-24.6	1127	1943	-10.9	-12.6	48	41	-129.0	-226.6	12.3	-7.4	-6.1
37TH	462.68	-12.7	-24.9	1127	1943	-11.2	-12.8	48	42	-116.4	-201.8	9.7	-5.9	-5.4
38TH	474.76	-13.1	-25.1	1127	1943	-11.6	-12.9	48	43	-103.2	-176.7	7.4	-4.6	-4.7
39TH	486.84	-13.6	-25.4	1127	1943	-12.0	-13.1	48	44	-89.7	-151.2	5.4	-3.4	-4.0
40TH	498.92	-14.0	-25.7	1127	1943	-12.4	-13.2	48	45	-75.7	-125.6	3.7	-2.4	-3.3
41ST	511.00	-14.4	-26.0	1127	1943	-12.8	-13.4	49	46	-61.3	-99.6	2.4	-1.6	-2.6
42ND	523.08	-15.4	-27.3	1174	2023	-13.1	-13.5	49	47	-45.9	-72.3	1.3	-.9	-1.8
43RD	535.66	-15.6	-27.8	1206	2078	-13.0	-13.4	49	46	-30.3	-44.5	.5	-.4	-1.1
44TH	548.58	-20.6	-36.5	1680	2895	-12.3	-12.6	40	38	-9.6	-8.0	.1	-.1	-.3
MR	566.58	-9.6	-8.0	1085	2065	-8.9	-3.9	-105	-217	0.0	0.0	0.0	0.0	0.0
TOP	581.67													

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 0 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-290.1	-620.8	192.2	-124.8	-14.1
2ND	23.00	1.3	-15.7	2147	3699	.6	-4.3	28	-4	-291.4	-605.0	178.1	-118.1	-13.8
3RD	35.92	.6	-9.8	1206	2078	.5	-4.7	23	-3	-292.1	-595.2	170.3	-114.4	-13.6
4TH	48.84	.6	-10.0	1206	2078	.5	-4.8	24	-2	-292.7	-585.2	162.7	-110.6	-13.4
5TH	61.76	.6	-10.3	1206	2078	.5	-4.9	26	-3	-293.3	-575.0	155.2	-106.8	-13.2
6TH	74.68	.6	-10.8	1206	2078	.5	-5.2	27	-3	-293.9	-564.2	147.9	-103.0	-12.9
7TH	87.60	.7	-11.2	1206	2078	.5	-5.4	29	-3	-294.6	-553.0	140.6	-99.2	-12.7
8TH	100.52	.7	-11.7	1206	2078	.6	-5.6	30	-3	-295.3	-541.3	133.6	-95.4	-12.4
9TH	113.44	.7	-12.2	1206	2078	.6	-5.9	31	-3	-296.0	-529.1	126.7	-91.6	-12.1
10TH	126.27	.7	-12.6	1197	2063	.6	-6.1	32	-3	-296.7	-516.5	120.0	-87.8	-11.8
11TH	139.10	.6	-13.0	1197	2063	.5	-6.3	33	-3	-297.3	-503.5	113.4	-84.0	-11.4
12TH	151.93	.0	-13.2	1197	2063	.0	-6.4	32	-0	-297.3	-490.2	107.0	-80.2	-11.1
13TH	164.76	-.5	-13.4	1197	2063	-.5	-6.5	31	2	-296.7	-476.8	100.8	-76.3	-10.8
14TH	177.59	-1.1	-13.6	1197	2063	-.9	-6.6	31	4	-295.6	-463.2	94.8	-72.5	-10.4
15TH	190.42	-1.7	-13.8	1197	2063	-1.4	-6.7	30	6	-293.9	-449.4	89.0	-68.8	-10.1
16TH	203.25	-2.3	-14.0	1197	2063	-1.9	-6.8	30	8	-291.7	-435.4	83.3	-65.0	-9.8
17TH	216.08	-2.4	-14.2	1197	2063	-2.0	-6.9	32	9	-289.2	-421.1	77.8	-61.3	-9.4
18TH	228.66	-3.1	-13.9	1174	2023	-2.7	-6.9	33	13	-286.1	-407.2	72.6	-57.7	-9.1
19TH	241.24	-4.0	-13.9	1174	2023	-3.4	-6.9	34	17	-282.1	-393.3	67.5	-54.1	-8.7
20TH	253.82	-4.9	-13.8	1174	2023	-4.1	-6.8	35	21	-277.3	-379.6	62.7	-50.6	-8.4
21ST	266.40	-5.7	-13.7	1174	2023	-4.9	-6.8	37	26	-271.5	-365.8	58.0	-47.1	-8.0
22ND	278.98	-6.6	-13.6	1174	2023	-5.6	-6.7	39	32	-264.9	-352.2	53.5	-43.7	-7.7
23RD	291.56	-7.5	-13.6	1174	2023	-6.4	-6.7	43	40	-257.4	-338.6	49.1	-40.5	-7.4
24TH	304.14	-8.1	-13.5	1174	2023	-6.9	-6.7	46	47	-249.3	-325.1	45.0	-37.3	-7.1
25TH	316.72	-8.5	-13.7	1174	2023	-7.2	-6.8	48	50	-240.8	-311.4	40.9	-34.2	-6.8
		-8.6	-13.5	1151	1983	-7.5	-6.8	50	54					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 0 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-232.2	-297.9	37.2	-31.3	-6.4
27TH	341.38	-8.9	-13.7	1151	1983	-7.8	-6.9	52	57	-223.3	-284.2	33.6	-28.5	-6.1
28TH	353.71	-9.2	-13.8	1151	1983	-8.0	-7.0	54	61	-214.0	-270.4	30.2	-25.8	-5.8
29TH	366.04	-9.6	-13.9	1151	1983	-8.3	-7.0	56	65	-204.5	-256.4	26.9	-23.2	-5.5
30TH	378.12	-9.7	-13.8	1127	1943	-8.6	-7.1	61	73	-194.8	-242.6	23.9	-20.8	-5.1
31ST	390.20	-9.9	-14.0	1127	1943	-8.8	-7.2	63	75	-184.9	-228.6	21.1	-18.5	-4.8
32ND	402.28	-10.1	-14.3	1127	1943	-8.9	-7.4	61	73	-174.9	-214.3	18.4	-16.3	-4.4
33RD	414.36	-10.2	-14.6	1127	1943	-9.1	-7.5	60	71	-164.6	-199.7	15.9	-14.3	-4.0
34TH	426.44	-10.4	-14.9	1127	1943	-9.3	-7.7	59	70	-154.2	-184.8	13.6	-12.3	-3.7
35TH	438.52	-10.6	-15.2	1127	1943	-9.4	-7.8	57	68	-143.6	-169.7	11.4	-10.5	-3.3
36TH	450.60	-10.8	-15.5	1127	1943	-9.6	-8.0	56	67	-132.8	-154.2	9.5	-8.9	-3.0
37TH	462.68	-10.9	-15.7	1127	1943	-9.7	-8.1	55	65	-121.9	-138.5	7.7	-7.3	-2.6
38TH	474.76	-11.2	-15.6	1127	1943	-10.0	-8.0	58	71	-110.6	-122.9	6.1	-5.9	-2.3
39TH	486.84	-11.6	-15.4	1127	1943	-10.3	-7.9	63	81	-99.0	-107.6	4.7	-4.7	-1.9
40TH	498.92	-11.9	-15.1	1127	1943	-10.6	-7.8	70	94	-87.1	-92.5	3.5	-3.5	-1.6
41ST	511.00	-12.3	-14.9	1127	1943	-10.9	-7.7	80	113	-74.8	-77.5	2.5	-2.5	-1.3
42ND	523.08	-12.7	-14.7	1127	1943	-11.2	-7.6	97	141	-62.2	-62.8	1.7	-1.7	-1.0
43RD	535.66	-13.8	-15.1	1174	2023	-11.7	-7.5	146	227	-48.4	-47.7	1.0	-1.0	-.7
44TH	548.58	-15.0	-15.6	1206	2078	-12.4	-7.5	292	477	-33.4	-32.2	.4	-.5	-.4
MR	566.58	-21.5	-22.8	1680	2895	-12.8	-7.9	157	253	-11.9	-9.3	.1	-.1	-.1
TOP	581.67	-11.9	-9.3	1085	2065	-11.0	-4.5	-28	-60	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 10 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-199.6	-389.8	128.0	-89.5	-8.0
2ND	23.00	-.3	-7.4	2147	3699	-.1	-2.0	7	0	-199.3	-382.4	119.1	-84.9	-7.9
3RD	35.92	-.2	-5.2	1206	2078	-.1	-2.5	13	1	-199.1	-377.2	114.2	-82.3	-7.9
4TH	48.84	-.2	-4.4	1206	2078	-.2	-2.1	16	1	-198.9	-372.8	109.3	-79.7	-7.8
5TH	61.76	-.3	-4.1	1206	2078	-.2	-2.0	18	2	-198.6	-368.7	104.5	-77.2	-7.7
6TH	74.68	-.2	-4.6	1206	2078	-.2	-2.2	20	2	-198.4	-364.1	99.8	-74.6	-7.7
7TH	87.60	-.2	-5.0	1206	2078	-.1	-2.4	22	1	-198.2	-359.1	95.1	-72.0	-7.6
8TH	100.52	-.1	-5.4	1206	2078	-.1	-2.6	23	1	-198.1	-353.7	90.5	-69.5	-7.5
9TH	113.44	-.1	-5.9	1206	2078	-.0	-2.8	24	0	-198.0	-347.8	86.0	-66.9	-7.4
10TH	126.27	.0	-6.3	1197	2063	.0	-3.0	25	-0	-198.0	-341.6	81.6	-64.4	-7.3
11TH	139.10	.0	-6.7	1197	2063	.0	-3.2	26	-0	-198.0	-334.9	77.2	-61.8	-7.1
12TH	151.93	-.2	-7.1	1197	2063	-.1	-3.4	28	1	-197.9	-327.8	73.0	-59.3	-7.0
13TH	164.76	-.3	-7.5	1197	2063	-.3	-3.6	29	2	-197.6	-320.3	68.8	-56.8	-6.8
14TH	177.59	-.5	-7.9	1197	2063	-.4	-3.8	30	3	-197.1	-312.3	64.8	-54.2	-6.6
15TH	190.42	-.7	-8.3	1197	2063	-.6	-4.0	31	4	-196.4	-304.0	60.8	-51.7	-6.4
16TH	203.25	-.8	-8.8	1197	2063	-.7	-4.2	32	5	-195.5	-295.2	57.0	-49.2	-6.2
17TH	216.08	-.8	-9.2	1197	2063	-.7	-4.4	36	5	-194.7	-286.1	53.2	-46.7	-5.9
18TH	228.66	-1.1	-9.1	1174	2023	-.9	-4.5	36	7	-193.6	-277.0	49.7	-44.2	-5.6
19TH	241.24	-1.4	-9.2	1174	2023	-1.2	-4.5	36	10	-192.2	-267.8	46.3	-41.8	-5.4
20TH	253.82	-1.8	-9.3	1174	2023	-1.5	-4.6	37	12	-190.4	-258.5	43.0	-39.4	-5.1
21ST	266.40	-2.1	-9.3	1174	2023	-1.8	-4.6	37	14	-188.3	-249.1	39.8	-37.0	-4.9
22ND	278.98	-2.5	-9.4	1174	2023	-2.1	-4.7	37	17	-185.8	-239.7	36.7	-34.7	-4.6
23RD	291.56	-2.9	-9.5	1174	2023	-2.4	-4.7	38	19	-182.9	-230.3	33.7	-32.3	-4.3
24TH	304.14	-3.2	-9.5	1174	2023	-2.7	-4.7	38	22	-179.7	-220.7	30.9	-30.1	-4.1
25TH	316.72	-3.5	-9.6	1174	2023	-3.0	-4.7	39	24	-176.2	-211.2	28.2	-27.8	-3.8
		-3.8	-9.4	1151	1983	-3.3	-4.7	39	26					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 10 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-172.4	-201.7	25.6	-25.7	-3.6
27TH	341.38	-4.1	-9.5	1151	1983	-3.5	-4.8	39	28	-168.4	-192.3	23.2	-23.6	-3.3
28TH	353.71	-4.4	-9.5	1151	1983	-3.8	-4.8	39	31	-164.0	-182.8	20.9	-21.5	-3.1
29TH	366.04	-4.7	-9.5	1151	1983	-4.1	-4.8	40	33	-159.3	-173.2	18.7	-19.5	-2.9
30TH	378.12	-5.1	-9.4	1127	1943	-4.5	-4.8	42	38	-154.3	-163.9	16.7	-17.6	-2.6
31ST	390.20	-5.6	-9.4	1127	1943	-4.9	-4.9	44	44	-148.7	-154.4	14.7	-15.8	-2.4
32ND	402.28	-6.1	-9.5	1127	1943	-5.4	-4.9	47	51	-142.6	-144.9	12.9	-14.1	-2.2
33RD	414.36	-6.6	-9.6	1127	1943	-5.9	-4.9	51	60	-136.0	-135.3	11.2	-12.4	-2.0
34TH	426.44	-7.1	-9.7	1127	1943	-6.3	-5.0	57	71	-128.9	-125.7	9.7	-10.8	-1.8
35TH	438.52	-7.6	-9.7	1127	1943	-6.8	-5.0	65	86	-121.3	-115.9	8.2	-9.3	-1.6
36TH	450.60	-8.2	-9.8	1127	1943	-7.2	-5.1	77	110	-113.1	-106.1	6.9	-7.8	-1.4
37TH	462.68	-8.7	-9.9	1127	1943	-7.7	-5.1	100	149	-104.5	-96.3	5.6	-6.5	-1.2
38TH	474.76	-9.0	-9.9	1127	1943	-8.0	-5.1	123	190	-95.5	-86.3	4.5	-5.3	-1.1
39TH	486.84	-9.3	-9.9	1127	1943	-8.2	-5.1	178	284	-86.2	-76.5	3.6	-4.2	-.9
40TH	498.92	-9.6	-9.9	1127	1943	-8.5	-5.1	364	602	-76.6	-66.6	2.7	-3.2	-.7
41ST	511.00	-9.9	-9.9	1127	1943	-8.8	-5.1	$$$$	-2902	-66.7	-56.7	1.9	-2.4	-.6
42ND	523.08	-10.2	-9.8	1127	1943	-9.1	-5.1	-223	-395	-56.5	-46.9	1.3	-1.6	-.5
43RD	535.66	-11.4	-10.2	1174	2023	-9.7	-5.1	-70	-133	-45.1	-36.6	.8	-1.0	-.3
44TH	548.58	-13.0	-10.8	1206	2078	-10.8	-5.2	-31	-64	-32.1	-25.9	.4	-.5	-.2
MR	566.58	-19.9	-16.3	1680	2895	-11.8	-5.6	-23	-48	-12.2	-9.6	.1	-.1	-.1
TOP	581.67	-12.2	-9.6	1085	2065	-11.2	-4.6	-11	-23	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 20 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-237.9	-126.0	49.0	-108.1	-1.5
2ND	23.00	-1.0	-1.6	2147	3699	-.4	-.4	-124	-129	-236.9	-124.4	46.1	-102.6	-1.6
3RD	35.92	-.3	-1.4	1206	2078	-.3	-.7	-22	-9	-236.6	-123.1	44.5	-99.5	-1.6
4TH	48.84	-.2	-.7	1206	2078	-.2	-.3	-38	-22	-236.4	-122.4	42.9	-96.5	-1.6
5TH	61.76	-.2	-.4	1206	2078	-.2	-.2	-100	-100	-236.1	-122.0	41.3	-93.4	-1.7
6TH	74.68	-.3	-.6	1206	2078	-.2	-.3	-77	-68	-235.8	-121.4	39.8	-90.4	-1.7
7TH	87.60	-.3	-.7	1206	2078	-.3	-.3	-65	-53	-235.5	-120.7	38.2	-87.3	-1.7
8TH	100.52	-.4	-.9	1206	2078	-.3	-.4	-59	-46	-235.1	-119.8	36.6	-84.3	-1.7
9TH	113.44	-.4	-1.0	1206	2078	-.4	-.5	-55	-41	-234.7	-118.8	35 1	-81.3	-1.8
10TH	126.27	-.5	-1.1	1197	2063	-.4	-.6	-52	-37	-234.2	-117.7	33.6	-78.3	-1.8
11TH	139.10	-.5	-1.3	1197	2063	-.5	-.6	-48	-34	-233.6	-116.4	32.1	-75.3	-1.9
12TH	151.93	-.6	-1.4	1197	2063	-.5	-.7	-36	-27	-233.0	-115.0	30.6	-72.3	-1.9
13TH	164.76	-.7	-1.5	1197	2063	-.6	-.7	-26	-19	-232.4	-113.5	29.1	-69.3	-1.9
14TH	177.59	-.7	-1.7	1197	2063	-.6	-.8	-17	-13	-231.6	-111.8	27.7	-66.3	-1.9
15TH	190.42	-.8	-1.8	1197	2063	-.7	-.9	-9	-7	-230.8	-110.0	26.3	-63.3	-1.9
16TH	203.25	-.9	-1.9	1197	2063	-.7	-.9	-1	-1	-229.9	-108.1	24.9	-60.4	-1.9
17TH	216.08	-.9	-2.0	1197	2063	-.8	-1.0	6	5	-229.0	-106.1	23.5	-57.4	-1.9
18TH	228.66	-1.1	-2.1	1174	2023	-1.0	-1.0	13	12	-227.9	-104.1	22.2	-54.6	-1.9
19TH	241.24	-1.4	-2.1	1174	2023	-1.2	-1.1	21	23	-226.5	-101.9	20.9	-51.7	-1.9
20TH	253.82	-1.6	-2.2	1174	2023	-1.4	-1.1	33	41	-224.8	-99.7	19.6	-48.9	-1.9
21ST	266.40	-1.9	-2.3	1174	2023	-1.6	-1.1	55	77	-223.0	-97.4	18 4	-46.1	-1.8
22ND	278.98	-2.1	-2.4	1174	2023	-1.8	-1.2	108	166	-220.8	-95.0	17.1	-43.3	-1.8
23RD	291.56	-2.4	-2.5	1174	2023	-2.0	-1.2	452	749	-218.4	-92.6	16.0	-40.5	-1.8
24TH	304.14	-2.7	-2.4	1174	2023	-2.3	-1.2	-114	-214	-215.7	-90.1	14.8	-37.8	-1.7
25TH	316.72	-3.0	-2.4	1174	2023	-2.5	-1.2	-43	-92	-212.7	-87.8	13.7	-35.1	-1.7
		-3.2	-2.3	1151	1983	-2.8	-1.1	-25	-61					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 20 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-209.5	-85.5	12.6	-32.5	-1.6
27TH	341.38	-3.5	-2.2	1151	1983	-3.1	-1.1	-17	-47	-206.0	-83.3	11.6	-29.9	-1.6
28TH	353.71	-3.8	-2.1	1151	1983	-3.3	-1.1	-13	-39	-202.2	-81.2	10.6	-27.4	-1.5
29TH	366.04	-4.1	-2.1	1151	1983	-3.6	-1.1	-10	-33	-198.0	-79.1	9.6	-24.9	-1.5
30TH	378.12	-4.9	-2.0	1127	1943	-4.3	-1.0	-6	-23	-193.2	-77.1	8.6	-22.6	-1.4
31ST	390.20	-5.8	-2.3	1127	1943	-5.1	-1.2	-5	-22	-187.4	-74.8	7.7	-20.3	-1.4
32ND	402.28	-6.7	-2.7	1127	1943	-5.9	-1.4	-6	-25	-180.7	-72.1	6.8	-18.0	-1.3
33RD	414.36	-7.5	-3.2	1127	1943	-6.7	-1.6	-7	-27	-173.2	-68.9	6.0	-15.9	-1.2
34TH	426.44	-8.4	-3.7	1127	1943	-7.4	-1.9	-8	-29	-164.8	-65.2	5.2	-13.9	-1.1
35TH	438.52	-9.3	-4.2	1127	1943	-8.2	-2.1	-8	-31	-155.5	-61.1	4.4	-11.9	-1.0
36TH	450.60	-10.1	-4.6	1127	1943	-9.0	-2.4	-9	-32	-145.4	-56.4	3.7	-10.1	-.9
37TH	462.68	-10.9	-5.1	1127	1943	-9.7	-2.6	-9	-34	-134.5	-51.3	3.1	-8.4	-.8
38TH	474.76	-11.4	-5.2	1127	1943	-10.1	-2.7	-9	-32	-123.1	-46.1	2.5	-6.9	-.6
39TH	486.84	-11.8	-5.2	1127	1943	-10.4	-2.7	-7	-27	-111.4	-40.9	1.9	-5.4	-.5
40TH	498.92	-12.2	-5.2	1127	1943	-10.8	-2.7	-6	-24	-99.2	-35.7	1.5	-4.2	-.4
41ST	511.00	-12.6	-5.2	1127	1943	-11.2	-2.7	-5	-21	-86.6	-30.5	1.1	-3.0	-.3
42ND	523.08	-13.0	-5.2	1127	1943	-11.5	-2.7	-4	-18	-73.6	-25.3	.7	-2.1	-.2
43RD	535.66	-15.0	-5.4	1174	2023	-12.8	-2.7	-3	-13	-58.6	-20.0	.5	-1.3	-.1
44TH	548.58	-18.0	-5.6	1206	2078	-14.9	-2.7	-2	-9	-40.6	-14.4	.2	-.6	-.1
MR	566.58	-25.7	-8.1	1680	2895	-15.3	-2.8	-1	-5	-14.8	-6.3	.0	-.1	-.0
TOP	581.67	-14.8	-6.3	1085	2065	-13.7	-3.0	-0	-1	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 30 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-497.3	260.5	-67.0	-202.2	3.9
2ND	23.00	-2.5	9.6	2147	3699	-1.2	2.6	53	-24	-494.8	251.0	-61.1	-190.8	3.5
3RD	35.92	-1.1	5.6	1206	2078	-.9	2.7	42	-14	-493.7	245.4	-57.9	-184.4	3.4
4TH	48.84	-1.1	5.9	1206	2078	-.9	2.8	38	-12	-492.6	239.5	-54.8	-178.0	3.2
5TH	61.76	-1.3	6.1	1206	2078	-1.1	2.9	38	-13	-491.3	233.3	-51.7	-171.6	3.0
6TH	74.68	-1.6	6.2	1206	2078	-1.3	3.0	39	-17	-489.7	227.1	-48.7	-165.3	2.8
7TH	87.60	-1.9	6.4	1206	2078	-1.6	3.1	41	-21	-487.8	220.7	-45.9	-159.0	2.6
8TH	100.52	-2.2	6.5	1206	2078	-1.8	3.1	43	-25	-485.6	214.2	-43.0	-152.7	2.4
9TH	113.44	-2.5	6.6	1206	2078	-2.1	3.2	45	-29	-483.0	207.6	-40.3	-146.4	2.2
10TH	126.27	-2.8	6.7	1197	2063	-2.4	3.3	47	-34	-480.2	200.9	-37.7	-140.3	2.0
11TH	139.10	-3.2	6.9	1197	2063	-2.7	3.3	49	-39	-477.0	194.0	-35.2	-134.1	1.8
12TH	151.93	-3.7	7.0	1197	2063	-3.1	3.4	51	-46	-473.3	187.0	-32.7	-128.0	1.6
13TH	164.76	-4.2	7.2	1197	2063	-3.5	3.5	54	-54	-469.1	179.8	-30.4	-122.0	1.4
14TH	177.59	-4.7	7.3	1197	2063	-3.9	3.5	58	-63	-464.4	172.5	-28.1	-116.0	1.2
15TH	190.42	-5.2	7.4	1197	2063	-4.3	3.6	63	-75	-459.2	165.1	-25.9	-110.1	1.0
16TH	203.25	-5.7	7.6	1197	2063	-4.8	3.7	71	-91	-453.5	157.5	-23.9	-104.2	.8
17TH	216.08	-6.6	7.7	1197	2063	-5.5	3.7	107	-156	-446.9	149.8	-21.9	-98.4	.6
18TH	228.66	-7.0	7.6	1174	2023	-6.0	3.8	185	-290	-439.9	142.2	-20.1	-92.9	.5
19TH	241.24	-7.5	7.6	1174	2023	-6.4	3.8	736	-1229	-432.5	134.6	-18.3	-87.4	.3
20TH	253.82	-7.9	7.6	1174	2023	-6.7	3.8	-309	548	-424.5	127.0	-16.7	-82.0	.1
21ST	266.40	-8.4	7.6	1174	2023	-7.1	3.8	-118	222	-416.2	119.4	-15.1	-76.7	-.0
22ND	278.98	-8.8	7.6	1174	2023	-7.5	3.8	-70	138	-407.3	111.8	-13.7	-71.5	-.2
23RD	291.56	-9.3	7.6	1174	2023	-7.9	3.8	-48	99	-398.1	104.2	-12.3	-66.4	-.3
24TH	304.14	-9.7	7.6	1174	2023	-8.3	3.7	-34	75	-388.4	96.6	-11.1	-61.5	-.4
25TH	316.72	-10.1	7.2	1174	2023	-8.6	3.5	-19	46	-378.3	89.5	-9.9	-56.7	-.5
		-10.2	6.7	1151	1983	-8.9	3.4	-11	29					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 30 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-368.1	82.8	-8.8	-52.1	-.6
27TH	341.38	-10.6	6.3	1151	1983	-9.2	3.2	-6	16	-357.5	76.5	-7.8	-47.6	-.7
28TH	353.71	-10.9	5.9	1151	1983	-9.5	3.0	-2	7	-346.5	70.6	-6.9	-43.3	-.7
29TH	366.04	-11.3	5.6	1151	1983	-9.8	2.8	-0	0	-335.3	65.0	-6.1	-39.1	-.7
30TH	378.12	-12.4	5.1	1127	1943	-11.0	2.6	1	-3	-322.8	59.9	-5.3	-35.1	-.7
31ST	390.20	-13.7	4.9	1127	1943	-12.1	2.5	1	-5	-309.1	55.1	-4.6	-31.3	-.7
32ND	402.28	-14.6	4.7	1127	1943	-13.0	2.4	1	-6	-294.5	50.3	-4.0	-27.6	-.6
33RD	414.36	-15.6	4.6	1127	1943	-13.8	2.4	1	-6	-278.9	45.7	-3.4	-24.2	-.6
34TH	426.44	-16.5	4.5	1127	1943	-14.6	2.3	1	-7	-262.4	41.3	-2.9	-20.9	-.5
35TH	438.52	-17.5	4.3	1127	1943	-15.5	2.2	1	-7	-245.0	37.0	-2.4	-17.8	-.5
36TH	450.60	-18.4	4.2	1127	1943	-16.3	2.2	1	-8	-226.6	32.8	-2.0	-15.0	-.4
37TH	462.68	-19.2	4.0	1127	1943	-17.1	2.1	1	-9	-207.3	28.8	-1.6	-12.4	-.3
38TH	474.76	-19.6	3.6	1127	1943	-17.4	1.9	1	-8	-187.7	25.1	-1.3	-10.0	-.3
39TH	486.84	-20.0	3.4	1127	1943	-17.7	1.7	1	-7	-167.8	21.7	-1.0	-7.8	-.2
40TH	498.92	-20.3	3.1	1127	1943	-18.0	1.6	1	-6	-147.5	18.6	-.8	-5.9	-.1
41ST	511.00	-20.7	2.8	1127	1943	-18.3	1.5	0	-5	-126.8	15.8	-.6	-4.3	-.1
42ND	523.08	-21.0	2.6	1127	1943	-18.6	1.3	0	-4	-105.8	13.2	-.4	-2.9	-.1
43RD	535.66	-23.7	2.4	1174	2023	-20.2	1.2	0	-2	-82.1	10.9	-.3	-1.7	-.0
44TH	548.58	-27.4	2.5	1206	2078	-22.7	1.2	0	-1	-54.7	8.4	-.1	-.8	-.0
MR	566.58	-36.6	5.2	1680	2895	-21.8	1.8	0	-3	-18.1	3.2	-.0	-.1	.0
TOP	581.67	-18.1	3.2	1085	2065	-16.7	1.5	-0	4	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 40 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-983.6	559.8	-120.2	-346.9	5.5
2ND	23.00	-8.7	25.3	2147	3699	-4.0	6.8	53	-31	-974.9	534.5	-107.6	-324.4	4.6
3RD	35.92	-4.1	17.2	1206	2078	-3.4	8.3	42	-17	-970.8	517.3	-100.8	-311.8	4.0
4TH	48.84	-3.9	17.6	1206	2078	-3.3	8.5	38	-15	-966.9	499.7	-94.2	-299.3	3.5
5TH	61.76	-4.8	18.1	1206	2078	-4.0	8.7	38	-17	-962.1	481.6	-87.9	-286.8	3.0
6TH	74.68	-6.3	18.6	1206	2078	-5.2	9.0	40	-23	-955.8	463.0	-81.8	-274.4	2.5
7TH	87.60	-7.8	19.2	1206	2078	-6.5	9.2	42	-29	-948.0	443.8	-75.9	-262.1	2.0
8TH	100.52	-9.3	19.7	1206	2078	-7.7	9.5	44	-35	-938.7	424.2	-70.3	-249.9	1.4
9TH	113.44	-10.8	20.2	1206	2078	-8.9	9.7	47	-43	-928.0	403.9	-64.9	-237.9	.9
10TH	126.27	-12.2	20.6	1197	2063	-10.2	10.0	52	-52	-915.8	383.4	-59.9	-226.0	.3
11TH	139.10	-13.6	20.9	1197	2063	-11.4	10.1	58	-64	-902.2	362.4	-55.1	-214.4	-.2
12TH	151.93	-15.0	20.6	1197	2063	-12.5	10.0	67	-83	-887.1	341.9	-50.6	-202.9	-.7
13TH	164.76	-16.4	20.2	1197	2063	-13.7	9.8	86	-118	-870.7	321.7	-46.3	-191.6	-1.2
14TH	177.59	-17.8	19.8	1197	2063	-14.9	9.6	138	-211	-853.0	301.8	-42.3	-180.6	-1.6
15TH	190.42	-19.2	19.5	1197	2063	-16.0	9.4	869	-1457	-833.8	282.4	-38.6	-169.8	-2.0
16TH	203.25	-20.6	19.1	1197	2063	-17.2	9.2	-139	255	-813.2	263.3	-35.1	-159.2	-2.4
17TH	216.08	-23.0	18.7	1197	2063	-19.2	9.1	-36	76	-790.2	244.6	-31.8	-148.9	-2.6
18TH	228.66	-23.2	17.6	1174	2023	-19.8	8.7	-23	51	-767.0	227.0	-28.9	-139.1	-2.9
19TH	241.24	-23.6	16.7	1174	2023	-20.1	8.3	-16	39	-743.4	210.3	-26.1	-129.6	-3.1
20TH	253.82	-23.9	15.9	1174	2023	-20.4	7.9	-12	30	-719.5	194.4	-23.6	-120.4	-3.3
21ST	266.40	-24.3	15.1	1174	2023	-20.7	7.4	-8	23	-695.2	179.3	-21.2	-111.5	-3.4
22ND	278.98	-24.6	14.2	1174	2023	-21.0	7.0	-6	18	-670.6	165.1	-19.1	-102.9	-3.6
23RD	291.56	-25.0	13.4	1174	2023	-21.3	6.6	-4	13	-645.7	151.7	-17.1	-94.6	-3.7
24TH	304.14	-25.2	12.6	1174	2023	-21.5	6.2	-3	10	-620.5	139.0	-15.2	-86.7	-3.8
25TH	316.72	-25.3	12.0	1174	2023	-21.5	5.9	-2	6	-595.2	127.1	-13.6	-79.0	-3.8
		-24.8	11.1	1151	1983	-21.6	5.6	-1	2					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 40 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-570.4	115.9	-12.1	-71.8	-3.9
27TH	341.38	-24.9	10.5	1151	1983	-21.6	5.3	0	-1	-545.6	105.4	-10.7	-65.0	-3.9
28TH	353.71	-24.9	9.9	1151	1983	-21.6	5.0	1	-4	-520.6	95.6	-9.5	-58.4	-3.8
29TH	366.04	-25.0	9.2	1151	1983	-21.7	4.7	2	-7	-495.7	86.3	-8.3	-52.1	-3.7
30TH	378.12	-26.2	8.5	1127	1943	-23.3	4.4	2	-10	-469.5	77.9	-7.3	-46.3	-3.6
31ST	390.20	-27.4	7.7	1127	1943	-24.3	4.0	2	-11	-442.0	70.2	-6.4	-40.8	-3.5
32ND	402.28	-27.9	6.9	1127	1943	-24.7	3.6	2	-12	-414.2	63.3	-5.6	-35.6	-3.3
33RD	414.36	-28.3	6.1	1127	1943	-25.1	3.2	2	-13	-385.9	57.1	-4.9	-30.8	-3.2
34TH	426.44	-28.7	5.4	1127	1943	-25.5	2.8	2	-14	-357.2	51.7	-4.3	-26.3	-3.0
35TH	438.52	-29.1	4.6	1127	1943	-25.8	2.4	1	-15	-328.0	47.1	-3.7	-22.2	-2.8
36TH	450.60	-29.6	3.8	1127	1943	-26.2	2.0	1	-16	-298.5	43.3	-3.1	-18.4	-2.6
37TH	462.68	-29.9	3.0	1127	1943	-26.5	1.6	1	-18	-268.6	40.3	-2.6	-14.9	-2.3
38TH	474.76	-29.6	3.1	1127	1943	-26.3	1.6	1	-18	-239.0	37.2	-2.1	-11.9	-2.1
39TH	486.84	-29.3	3.3	1127	1943	-26.0	1.7	1	-18	-209.7	33.9	-1.7	-9.2	-1.8
40TH	498.92	-29.1	3.5	1127	1943	-25.8	1.8	1	-18	-180.6	30.4	-1.3	-6.8	-1.6
41ST	511.00	-28.8	3.7	1127	1943	-25.5	1.9	1	-17	-151.8	26.7	-1.0	-4.8	-1.4
42ND	523.08	-28.5	3.9	1127	1943	-25.3	2.0	1	-17	-123.3	22.9	-.7	-3.1	-1.1
43RD	535.66	-30.8	4.2	1174	2023	-26.3	2.1	1	-17	-92.5	18.6	-.4	-1.8	-.9
44TH	548.58	-33.7	4.8	1206	2078	-27.9	2.3	1	-17	-58.8	13.8	-.2	-.8	-.6
MR	566.58	-42.2	8.6	1680	2895	-25.1	3.0	3	-24	-16.6	5.2	-.0	-.1	-.2
TOP	581.67	-16.6	5.2	1085	2065	-15.3	2.5	5	-26	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-1207.7	822.6	-188.1	-402.3	14.5
2ND	23.00	-16.8	45.7	2147	3699	-7.8	12.3	45	-28	-1190.9	776.9	-169.7	-374.7	13.1
3RD	35.92	-7.9	28.2	1206	2078	-6.6	13.6	35	-17	-1182.9	748.7	-159.8	-359.4	12.3
4TH	48.84	-7.0	28.1	1206	2078	-5.8	13.5	30	-13	-1175.9	720.6	-150.3	-344.2	11.7
5TH	61.76	-7.8	28.1	1206	2078	-6.5	13.5	30	-14	-1168.1	692.5	-141.2	-329.0	11.1
6TH	74.68	-10.0	28.1	1206	2078	-8.3	13.5	32	-20	-1158.1	664.4	-132.4	-314.0	10.5
7TH	87.60	-12.2	28.2	1206	2078	-10.1	13.6	35	-26	-1145.9	636.2	-124.0	-299.1	9.8
8TH	100.52	-14.4	28.2	1206	2078	-11.9	13.6	39	-34	-1131.5	608.0	-116.0	-284.4	9.2
9TH	113.44	-16.6	28.3	1206	2078	-13.7	13.6	45	-45	-1115.0	579.7	-108.3	-269.9	8.5
10TH	126.27	-18.6	28.1	1197	2063	-15.5	13.6	53	-60	-1096.4	551.6	-101.1	-255.7	7.8
11TH	139.10	-20.6	27.9	1197	2063	-17.2	13.5	67	-84	-1075.7	523.7	-94.2	-241.8	7.1
12TH	151.93	-22.1	26.9	1197	2063	-18.5	13.0	93	-130	-1053.6	496.8	-87.6	-228.1	6.5
13TH	164.76	-23.6	25.8	1197	2063	-19.7	12.5	178	-277	-1030.0	471.0	-81.4	-214.7	5.9
14TH	177.59	-25.1	24.8	1197	2063	-21.0	12.0	$$$$	2023	-1004.9	446.2	-75.5	-201.7	5.3
15TH	190.42	-26.6	23.8	1197	2063	-22.2	11.5	-111	212	-978.3	422.4	-70.0	-189.0	4.8
16TH	203.25	-28.1	22.8	1197	2063	-23.5	11.0	-52	109	-950.2	399.6	-64.7	-176.6	4.3
17TH	216.08	-31.1	21.8	1197	2063	-26.0	10.5	-24	58	-919.0	377.9	-59.7	-164.6	3.9
18TH	228.66	-31.2	20.4	1174	2023	-26.6	10.1	-18	47	-887.8	357.4	-55.1	-153.2	3.5
19TH	241.24	-31.5	19.6	1174	2023	-26.8	9.7	-15	41	-856.3	337.9	-50.7	-142.3	3.1
20TH	253.82	-31.7	18.7	1174	2023	-27.0	9.2	-12	35	-824.6	319.1	-46.6	-131.7	2.8
21ST	266.40	-32.0	17.8	1174	2023	-27.3	8.8	-10	30	-792.6	301.3	-42.7	-121.5	2.4
22ND	278.98	-32.3	17.0	1174	2023	-27.5	8.4	-8	26	-760.3	284.3	-39.0	-111.8	2.2
23RD	291.56	-32.5	16.1	1174	2023	-27.7	8.0	-7	23	-727.8	268.2	-35.5	-102.4	1.9
24TH	304.14	-32.6	15.3	1174	2023	-27.7	7.6	-5	20	-695.2	252.9	-32.2	-93.4	1.7
25TH	316.72	-32.3	14.9	1174	2023	-27.5	7.3	-5	18	-663.0	238.0	-29.1	-84.9	1.4
		-31.4	14.1	1151	1983	-27.3	7.1	-4	17					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-631.6	223.9	-26.3	-76.9	1.2
27TH	341.38	-31.1	13.7	1151	1983	-27.0	6.9	-4	15	-600.5	210.3	-23.6	-69.3	1.1
28TH	353.71	-30.8	13.2	1151	1983	-26.8	6.7	-3	13	-569.7	197.1	-21.1	-62.1	.9
29TH	366.04	-30.5	12.7	1151	1983	-26.5	6.4	-3	12	-539.1	184.3	-18.8	-55.3	.8
30TH	378.12	-31.4	12.0	1127	1943	-27.8	6.2	-2	9	-507.8	172.3	-16.6	-49.0	.7
31ST	390.20	-32.1	11.8	1127	1943	-28.5	6.0	-2	8	-475.6	160.5	-14.6	-43.0	.6
32ND	402.28	-32.1	11.5	1127	1943	-28.5	5.9	-2	7	-443.5	149.0	-12.7	-37.5	.5
33RD	414.36	-32.1	11.3	1127	1943	-28.5	5.8	-1	7	-411.4	137.7	-11.0	-32.3	.4
34TH	426.44	-32.1	11.0	1127	1943	-28.5	5.7	-1	7	-379.3	126.7	-9.4	-27.5	.3
35TH	438.52	-32.1	10.8	1127	1943	-28.5	5.6	-1	6	-347.2	115.8	-7.9	-23.1	.2
36TH	450.60	-32.1	10.6	1127	1943	-28.5	5.4	-1	6	-315.1	105.3	-6.6	-19.1	.1
37TH	462.68	-31.9	10.3	1127	1943	-28.3	5.3	-1	5	-283.1	94.9	-5.4	-15.5	.0
38TH	474.76	-31.7	10.2	1127	1943	-28.1	5.3	-1	5	-251.4	84.7	-4.3	-12.3	-.0
39TH	486.84	-31.5	10.2	1127	1943	-27.9	5.2	-1	4	-219.9	74.5	-3.3	-9.4	-.1
40TH	498.92	-31.3	10.1	1127	1943	-27.7	5.2	-1	3	-188.7	64.4	-2.5	-7.0	-.1
41ST	511.00	-31.1	10.1	1127	1943	-27.5	5.2	-0	2	-157.6	54.3	-1.8	-4.9	-.1
42ND	523.08	-30.8	10.0	1127	1943	-27.3	5.2	-0	1	-126.8	44.3	-1.2	-3.2	-.2
43RD	535.66	-33.0	10.4	1174	2023	-28.1	5.1	-0	0	-93.8	33.9	-.7	-1.8	-.2
44TH	548.58	-34.9	10.8	1206	2078	-29.0	5.2	0	-2	-58.9	23.1	-.3	-.8	-.1
MR	566.58	-42.8	16.2	1680	2895	-25.5	5.6	1	-6	-16.1	7.0	-.1	-.1	-.0
TOP	581.67	-16.1	7.0	1085	2065	-14.8	3.4	1	-5	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 60 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-1118.8	1161.1	-297.8	-370.3	24.1
2ND	23.00	-20.4	58.8	2147	3699	-9.5	15.9	38	-23	-1098.4	1102.2	-271.8	-344.8	22.5
3RD	35.92	-8.9	36.4	1206	2078	-7.4	17.5	27	-11	-1089.4	1065.9	-257.8	-330.7	21.8
4TH	48.84	-6.6	34.7	1206	2078	-5.4	16.7	24	-8	-1082.9	1031.2	-244.3	-316.7	21.2
5TH	61.76	-6.5	33.5	1206	2078	-5.4	16.1	23	-8	-1076.3	997.7	-231.1	-302.7	20.6
6TH	74.68	-8.6	33.1	1206	2078	-7.1	15.9	25	-11	-1067.8	964.6	-218.5	-288.9	20.0
7TH	87.60	-10.6	32.6	1206	2078	-8.8	15.7	27	-15	-1057.2	932.0	-206.2	-275.1	19.3
8TH	100.52	-12.6	32.1	1206	2078	-10.5	15.5	30	-20	-1044.6	899.9	-194.4	-261.6	18.7
9TH	113.44	-14.6	31.7	1206	2078	-12.1	15.2	34	-27	-1029.9	868.2	-183.0	-248.2	18.0
10TH	126.27	-16.5	31.0	1197	2063	-13.8	15.0	39	-35	-1013.4	837.2	-172.0	-235.1	17.3
11TH	139.10	-18.4	30.5	1197	2063	-15.4	14.8	46	-47	-994.9	806.7	-161.5	-222.2	16.6
12TH	151.93	-20.0	30.2	1197	2063	-16.7	14.6	51	-58	-974.9	776.6	-151.3	-209.5	15.9
13TH	164.76	-21.6	29.8	1197	2063	-18.0	14.5	59	-73	-953.3	746.7	-141.5	-197.2	15.3
14TH	177.59	-23.2	29.5	1197	2063	-19.4	14.3	72	-97	-930.1	717.2	-132.2	-185.1	14.6
15TH	190.42	-24.8	29.2	1197	2063	-20.7	14.2	97	-140	-905.4	688.0	-123.1	-173.3	14.0
16TH	203.25	-26.3	28.9	1197	2063	-22.0	14.0	160	-249	-879.0	659.1	-114.5	-161.9	13.3
17TH	216.08	-29.0	28.6	1197	2063	-24.2	13.8	-901	1555	-850.1	630.6	-106.2	-150.8	12.7
18TH	228.66	-29.1	27.4	1174	2023	-24.8	13.5	-197	358	-820.9	603.2	-98.5	-140.3	12.2
19TH	241.24	-29.5	26.7	1174	2023	-25.1	13.2	-120	226	-791.5	576.5	-91.0	-130.1	11.6
20TH	253.82	-29.8	26.0	1174	2023	-25.4	12.8	-85	166	-761.7	550.5	-84.0	-120.3	11.0
21ST	266.40	-30.2	25.3	1174	2023	-25.7	12.5	-65	132	-731.5	525.2	-77.2	-111.0	10.5
22ND	278.98	-30.5	24.6	1174	2023	-26.0	12.2	-52	109	-701.0	500.6	-70.7	-101.9	9.9
23RD	291.56	-30.8	23.9	1174	2023	-26.3	11.8	-43	94	-670.2	476.7	-64.6	-93.3	9.4
24TH	304.14	-30.9	23.4	1174	2023	-26.3	11.6	-38	86	-639.2	453.3	-58.7	-85.1	8.9
25TH	316.72	-30.5	23.2	1174	2023	-26.0	11.5	-38	86	-608.7	430.1	-53.2	-77.2	8.4
		-29.6	22.5	1151	1983	-25.7	11.4	-38	85					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 60 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-579.2	407.6	-48.0	-69.9	7.9
27TH	341.38	-29.2	22.3	1151	1983	-25.4	11.3	-38	84	-550.0	385.3	-43.1	-62.9	7.4
28TH	353.71	-28.8	22.1	1151	1983	-25.0	11.2	-37	83	-521.1	363.1	-38.5	-56.3	6.9
29TH	366.04	-28.5	21.9	1151	1983	-24.7	11.0	-37	82	-492.7	341.2	-34.2	-50.1	6.5
30TH	378.12	-28.6	21.3	1127	1943	-25.4	10.9	-30	70	-464.0	320.0	-30.2	-44.3	6.1
31ST	390.20	-29.2	21.1	1127	1943	-25.9	10.9	-27	64	-434.8	298.8	-26.4	-38.9	5.6
32ND	402.28	-29.5	21.0	1127	1943	-26.1	10.8	-26	62	-405.3	277.8	-23.0	-33.8	5.2
33RD	414.36	-29.7	20.9	1127	1943	-26.3	10.8	-25	61	-375.6	256.8	-19.7	-29.1	4.8
34TH	426.44	-29.9	20.8	1127	1943	-26.5	10.7	-24	60	-345.7	236.0	-16.8	-24.7	4.4
35TH	438.52	-30.2	20.7	1127	1943	-26.8	10.7	-24	58	-315.5	215.3	-14.0	-20.7	3.9
36TH	450.60	-30.4	20.6	1127	1943	-27.0	10.6	-23	57	-285.2	194.6	-11.6	-17.1	3.5
37TH	462.68	-30.4	20.5	1127	1943	-27.0	10.6	-22	56	-254.7	174.1	-9.3	-13.9	3.0
38TH	474.76	-29.8	20.3	1127	1943	-26.5	10.4	-23	57	-224.9	153.8	-7.3	-11.0	2.6
39TH	486.84	-29.2	20.0	1127	1943	-25.9	10.3	-23	56	-195.7	133.7	-5.6	-8.4	2.2
40TH	498.92	-28.6	19.8	1127	1943	-25.3	10.2	-23	56	-167.1	113.9	-4.1	-6.2	1.8
41ST	511.00	-27.9	19.5	1127	1943	-24.8	10.1	-23	56	-139.2	94.4	-2.9	-4.4	1.4
42ND	523.08	-27.3	19.3	1127	1943	-24.2	9.9	-23	57	-111.9	75.1	-1.8	-2.9	1.1
43RD	535.66	-28.4	19.8	1174	2023	-24.2	9.8	-22	53	-83.5	55.3	-1.0	-1.6	.7
44TH	548.58	-29.5	20.2	1206	2078	-24.5	9.7	-19	46	-54.0	35.1	-.4	-.7	.4
MR	566.58	-38.3	28.3	1680	2895	-22.8	9.8	-15	34	-15.6	6.8	-.1	-.1	.1
TOP	581.67	-15.6	6.8	1085	2065	-14.4	3.3	-3	12	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 70 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-1221.6	1476.6	-406.8	-388.9	35.8
2ND	23.00	-37.0	64.3	2147	3699	-17.2	17.4	57	-56	-1184.7	1412.4	-373.6	-361.2	33.9
3RD	35.92	-17.5	39.1	1206	2078	-14.5	18.8	35	-27	-1167.1	1373.3	-355.6	-346.1	33.0
4TH	48.84	-16.1	36.5	1206	2078	-13.4	17.6	32	-24	-1151.0	1336.8	-338.1	-331.1	32.3
5TH	61.76	-16.6	35.2	1206	2078	-13.7	16.9	32	-26	-1134.4	1301.6	-321.1	-316.3	31.5
6TH	74.68	-17.1	35.4	1206	2078	-14.2	17.0	34	-28	-1117.3	1266.2	-304.5	-301.8	30.8
7TH	87.60	-17.7	35.6	1206	2078	-14.7	17.1	35	-30	-1099.6	1230.6	-288.4	-287.4	30.1
8TH	100.52	-18.3	35.9	1206	2078	-15.2	17.3	37	-32	-1081.3	1194.7	-272.7	-273.4	29.3
9TH	113.44	-18.8	36.1	1206	2078	-15.6	17.4	38	-34	-1062.5	1158.7	-257.5	-259.5	28.5
10TH	126.27	-19.3	36.0	1197	2063	-16.1	17.5	40	-36	-1043.2	1122.6	-242.8	-246.0	27.7
11TH	139.10	-19.9	36.1	1197	2063	-16.6	17.5	42	-39	-1023.3	1086.5	-228.7	-232.7	26.8
12TH	151.93	-20.9	35.8	1197	2063	-17.4	17.3	44	-43	-1002.4	1050.7	-215.0	-219.7	26.0
13TH	164.76	-21.8	35.5	1197	2063	-18.2	17.2	46	-49	-980.6	1015.2	-201.7	-207.0	25.2
14TH	177.59	-22.7	35.1	1197	2063	-19.0	17.0	50	-55	-957.9	980.1	-188.9	-194.6	24.4
15TH	190.42	-23.7	34.8	1197	2063	-19.8	16.9	54	-62	-934.2	945.3	-176.6	-182.5	23.6
16TH	203.25	-24.6	34.5	1197	2063	-20.6	16.7	59	-71	-909.6	910.8	-164.7	-170.6	22.8
17TH	216.08	-26.7	34.2	1197	2063	-22.3	16.6	73	-97	-882.9	876.6	-153.2	-159.1	22.0
18TH	228.66	-27.2	33.1	1174	2023	-23.2	16.4	89	-124	-855.7	843.5	-142.4	-148.2	21.2
19TH	241.24	-28.0	32.8	1174	2023	-23.9	16.2	111	-161	-827.6	810.7	-132.0	-137.6	20.5
20TH	253.82	-28.9	32.4	1174	2023	-24.6	16.0	147	-223	-798.7	778.3	-122.0	-127.4	19.7
21ST	266.40	-29.7	32.0	1174	2023	-25.3	15.8	221	-349	-769.0	746.3	-112.4	-117.5	18.9
22ND	278.98	-30.6	31.7	1174	2023	-26.0	15.7	455	-747	-738.4	714.6	-103.2	-108.0	18.1
23RD	291.56	-31.4	31.3	1174	2023	-26.8	15.5	$$$$	9673	-707.0	683.2	-94.4	-98.9	17.3
24TH	304.14	-31.8	31.1	1174	2023	-27.1	15.4	-686	1196	-675.2	652.2	-86.0	-90.2	16.5
25TH	316.72	-31.6	31.1	1174	2023	-26.9	15.3	-982	1699	-643.6	621.1	-79.0	-81.9	15.7
		-30.7	30.4	1151	1983	-26.7	15.3	$$$$	2919					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 70 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-613.0	590.7	-70.5	-74.2	14.9
		-30.4	30.4	1151	1983	-26.5	15.3	$$$$	10189					
27TH	341.38									-582.5	560.3	-63.4	-66.8	14.1
		-30.2	30.3	1151	1983	-26.2	15.3	4009	-6795					
28TH	353.71									-552.3	530.0	-56.7	-59.8	13.3
		-30.0	30.3	1151	1983	-26.0	15.3	1510	-2542					
29TH	366.04									-522.3	499.7	-50.4	-53.2	12.5
		-30.3	29.6	1127	1943	-26.9	15.3	-709	1234					
30TH	378.12									-492.0	470.1	-44.5	-47.1	11.7
		-30.9	29.7	1127	1943	-27.4	15.3	-391	692					
31ST	390.20									-461.1	440.4	-39.0	-41.3	10.9
		-31.1	29.8	1127	1943	-27.6	15.4	-379	673					
32ND	402.28									-430.0	410.5	-33.9	-35.9	10.1
		-31.3	30.0	1127	1943	-27.7	15.4	-368	654					
33RD	414.36									-398.7	380.6	-29.1	-30.9	9.3
		-31.5	30.1	1127	1943	-27.9	15.5	-358	637					
34TH	426.44									-367.2	350.5	-24.7	-26.3	8.5
		-31.6	30.2	1127	1943	-28.1	15.6	-349	621					
35TH	438.52									-335.6	320.2	-20.6	-22.1	7.7
		-31.8	30.4	1127	1943	-28.2	15.6	-340	606					
36TH	450.60									-303.8	289.9	-16.9	-18.2	6.9
		-31.8	30.5	1127	1943	-28.2	15.7	-362	643					
37TH	462.68									-272.0	259.4	-13.6	-14.7	6.1
		-31.4	30.4	1127	1943	-27.9	15.7	-475	836					
38TH	474.76									-240.5	229.0	-10.7	-11.6	5.3
		-31.0	30.3	1127	1943	-27.5	15.6	-629	1098					
39TH	486.84									-209.5	198.7	-8.1	-8.9	4.6
		-30.6	30.1	1127	1943	-27.1	15.5	-942	1631					
40TH	498.92									-178.9	168.6	-5.9	-6.6	3.8
		-30.2	30.0	1127	1943	-26.8	15.4	$$$$	3307					
41ST	511.00									-148.7	138.7	-4.0	-4.6	3.0
		-29.8	29.8	1127	1943	-26.4	15.3	$$$$$$$$$						
42ND	523.08									-118.9	108.9	-2.5	-3.0	2.3
		-31.2	30.9	1174	2023	-26.6	15.3	$$$$	2184					
43RD	535.66									-87.7	78.0	-1.3	-1.7	1.5
		-32.3	31.1	1206	2078	-26.8	15.0	-368	650					
44TH	548.58									-55.4	46.9	-.5	-.8	.8
		-40.1	40.5	1680	2895	-23.9	14.0	1069	-1802					
MR	566.58									-15.3	6.4	-.0	-.1	.1
		-15.3	6.4	1085	2065	-14.1	3.1	-5	20					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-1099.3	1689.9	-489.7	-338.9	46.9
2ND	23.00	-42.3	61.6	2147	3699	-19.7	16.7	76	-88	-1057.1	1628.3	-451.5	-314.1	45.0
3RD	35.92	-20.2	38.1	1206	2078	-16.8	18.3	42	-38	-1036.9	1590.2	-430.7	-300.6	44.0
4TH	48.84	-19.5	36.0	1206	2078	-16.2	17.3	40	-37	-1017.4	1554.2	-410.4	-287.3	43.2
5TH	61.76	-20.0	35.0	1206	2078	-16.5	16.8	43	-41	-997.4	1519.2	-390 6	-274.3	42.4
6TH	74.68	-19.7	35.3	1206	2078	-16.4	17.0	43	-41	-977.7	1483.9	-371.2	-261.5	41.6
7TH	87.60	-19.5	35.6	1206	2078	-16.2	17.1	44	-41	-958.2	1448.3	-352.2	-249.0	40.7
8TH	100.52	-19.3	35.9	1206	2078	-16.0	17.3	45	-41	-938.9	1412.4	-333.8	-236.8	39.8
9TH	113.44	-19.1	36.2	1206	2078	-15.8	17.4	45	-41	-919.8	1376.2	-315 7	-224.8	38.9
10TH	126.27	-18.8	36.3	1197	2063	-15.7	17.6	46	-40	-901.0	1339.9	-298.3	-213.1	37.9
11TH	139.10	-18.7	36.6	1197	2063	-15.6	17.7	46	-40	-882.3	1303.3	-281.4	-201.7	36.9
12TH	151.93	-19.2	36.9	1197	2063	-16.1	17.9	47	-41	-863.1	1266.4	-264 9	-190.5	35.9
13TH	164.76	-19.7	37.2	1197	2063	-16.5	18.0	47	-42	-843.3	1229.2	-248.9	-179.5	34.9
14TH	177.59	-20.3	37.6	1197	2063	-16.9	18.2	47	-43	-823.1	1191.6	-233.3	-168.8	33.9
15TH	190.42	-20.8	37.9	1197	2063	-17.4	18.4	47	-44	-802.3	1153.7	-218.3	-158.4	32.9
16TH	203.25	-21.3	38.2	1197	2063	-17.8	18.5	48	-45	-780.9	1115.5	-203.7	-148.2	31.9
17TH	216.08	-22.4	38.6	1197	2063	-18.7	18.7	49	-49	-758.5	1076.9	-189.7	-138.4	30.8
18TH	228.66	-22.6	37.9	1174	2023	-19.2	18.7	51	-52	-735.9	1039.1	-176.4	-129.0	29.8
19TH	241.24	-23.1	37.8	1174	2023	-19.7	18.7	54	-56	-712.8	1001.2	-163.5	-119.9	28.8
20TH	253.82	-23.7	37.8	1174	2023	-20.1	18.7	56	-60	-689.1	963.5	-151.2	-111.0	27.8
21ST	266.40	-24.2	37.7	1174	2023	-20.6	18.6	59	-64	-665.0	925.7	-139.3	-102.5	26.8
22ND	278.98	-24.7	37.7	1174	2023	-21.0	18.6	61	-68	-640.3	888.1	-127.9	-94.3	25.7
23RD	291.56	-25.2	37.6	1174	2023	-21.5	18.6	64	-74	-615.0	850.4	-116.9	-86.4	24.6
24TH	304.14	-25.6	37.7	1174	2023	-21.8	18.6	67	-77	-589.4	812.7	-106.5	-78.8	23.6
25TH	316.72	-25.9	38.0	1174	2023	-22.1	18.8	68	-79	-563.5	774.8	-96.5	-71.6	22.5
		-25.6	37.5	1151	1983	-22.3	18.9	68	-80					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE NEW YORK CASE 2
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-537.9	737.3	-87.2	-64.8	21.4
27TH	341.38	-25.9	37.8	1151	1983	-22.5	19.0	69	-81	-512.0	699.5	-78.3	-58.3	20.2
28TH	353.71	-26.1	38.0	1151	1983	-22.7	19.2	70	-82	-485.9	661.5	-69.9	-52.2	19.1
29TH	366.04	-26.3	38.3	1151	1983	-22.9	19.3	71	-83	-459.6	623.2	-62.0	-46.3	18.0
30TH	378.12	-27.0	37.8	1127	1943	-23.9	19.4	76	-93	-432.6	585.4	-54.7	-41.0	16.9
31ST	390.20	-27.6	37.9	1127	1943	-24.5	19.5	80	-99	-405.0	547.5	-47.9	-35.9	15.7
32ND	402.28	-27.8	38.0	1127	1943	-24.6	19.5	81	-101	-377.2	509.6	-41.5	-31.2	14.6
33RD	414.36	-27.9	38.0	1127	1943	-24.8	19.6	82	-102	-349.3	471.6	-35.6	-26.8	13.4
34TH	426.44	-28.1	38.0	1127	1943	-24.9	19.6	83	-104	-321.1	433.5	-30.1	-22.7	12.3
35TH	438.52	-28.3	38.1	1127	1943	-25.1	19.6	84	-106	-292.8	395.5	-25.1	-19.0	11.2
36TH	450.60	-28.5	38.1	1127	1943	-25.3	19.6	85	-108	-264.4	357.4	-20.5	-15.7	10.0
37TH	462.68	-28.5	38.1	1127	1943	-25.3	19.6	85	-108	-235.9	319.3	-16.4	-12.6	8.9
38TH	474.76	-28.0	38.0	1127	1943	-24.8	19.6	80	-101	-207.9	281.3	-12.8	-10.0	7.7
39TH	486.84	-27.5	37.9	1127	1943	-24.4	19.5	77	-95	-180.4	243.4	-9.6	-7.6	6.7
40TH	498.92	-27.0	37.7	1127	1943	-23.9	19.4	73	-89	-153.4	205.7	-6.9	-5.6	5.6
41ST	511.00	-26.5	37.5	1127	1943	-23.5	19.3	69	-83	-126.9	168.1	-4.7	-3.9	4.5
42ND	523.08	-26.0	37.4	1127	1943	-23.0	19.2	66	-78	-100.9	130.8	-2.9	-2.5	3.5
43RD	535.66	-26.9	38.8	1174	2023	-22.9	19.2	65	-77	-74.0	92.0	-1.5	-1.4	2.5
44TH	548.58	-27.2	38.9	1206	2078	-22.6	18.7	65	-77	-46.8	53.1	-.5	-.6	1.4
MR	566.58	-33.4	49.8	1680	2895	-19.9	17.2	54	-62	-13.5	3.3	-.0	-.1	.2
TOP	581.67	-13.5	3.3	1085	2065	-12.4	1.6	-6	41	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-829.2	1912.2	-561.0	-244.0	47.5
2ND	23.00	-44.0	65.7	2147	3699	-20.5	17.7	67	-76	-785.2	1846.6	-517.8	-225.5	45.6
3RD	35.92	-20.5	40.1	1206	2078	-17.0	19.3	37	-32	-764.7	1806.5	-494.2	-215.4	44.7
4TH	48.84	-18.0	38.3	1206	2078	-15.0	18.4	34	-27	-746.7	1768.2	-471.1	-205.7	43.9
5TH	61.76	-17.2	37.6	1206	2078	-14.3	18.1	33	-26	-729.5	1730.7	-448.5	-196.1	43.1
6TH	74.68	-16.7	38.4	1206	2078	-13.9	18.5	33	-25	-712.8	1692.3	-426.3	-186.8	42.3
7TH	87.60	-16.2	39.1	1206	2078	-13.4	18.8	33	-23	-696.6	1653.1	-404.7	-177.7	41.4
8TH	100.52	-15.7	39.9	1206	2078	-13.0	19.2	33	-22	-680.9	1613.2	-383.6	-168.8	40.5
9TH	113.44	-15.1	40.7	1206	2078	-12.6	19.6	33	-21	-665.8	1572.5	-363.1	-160.1	39.6
10TH	126.27	-14.5	41.2	1197	2063	-12.1	20.0	33	-20	-651.3	1531.3	-343.1	-151.7	38.6
11TH	139.10	-14.2	41.9	1197	2063	-11.9	20.3	33	-19	-637.1	1489.4	-323.8	-143.4	37.7
12TH	151.93	-14.7	42.2	1197	2063	-12.3	20.4	33	-20	-622.4	1447.2	-304.9	-135.3	36.7
13TH	164.76	-15.2	42.4	1197	2063	-12.7	20.6	33	-20	-607.3	1404.8	-286.6	-127.4	35.7
14TH	177.59	-15.6	42.7	1197	2063	-13.1	20.7	33	-21	-591.6	1362.1	-268.9	-119.8	34.7
15TH	190.42	-16.1	43.0	1197	2063	-13.4	20.8	33	-21	-575.5	1319.1	-251.7	-112.3	33.7
16TH	203.25	-16.6	43.2	1197	2063	-13.8	21.0	33	-22	-558.9	1275.9	-235.0	-105.0	32.8
17TH	216.08	-17.2	43.5	1197	2063	-14.4	21.1	34	-23	-541.8	1232.4	-218.9	-97.9	31.8
18TH	228.66	-17.2	42.7	1174	2023	-14.6	21.1	35	-24	-524.6	1189.7	-203.7	-91.2	30.8
19TH	241.24	-17.4	42.7	1174	2023	-14.9	21.1	36	-25	-507.1	1147.0	-189.0	-84.7	29.8
20TH	253.82	-17.7	42.7	1174	2023	-15.1	21.1	37	-26	-489.4	1104.2	-174.9	-78.5	28.7
21ST	266.40	-18.0	42.7	1174	2023	-15.3	21.1	38	-27	-471.4	1061.5	-161.2	-72.4	27.7
22ND	278.98	-18.3	42.8	1174	2023	-15.6	21.1	39	-28	-453.2	1018.7	-148.1	-66.6	26.6
23RD	291.56	-18.5	42.8	1174	2023	-15.8	21.1	40	-29	-434.6	975.9	-135.6	-61.0	25.5
24TH	304.14	-18.7	42.9	1174	2023	-16.0	21.2	41	-30	-415.9	933.0	-123.6	-55.7	24.4
25TH	316.72	-18.9	43.0	1174	2023	-16.1	21.3	41	-30	-397.0	890.0	-112.1	-50.6	23.2
		-18.6	42.3	1151	1983	-16.2	21.3	41	-30					

TABLE 7. SHEAR AND MOMENT DIAGRAMS NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-378.4	847.7	-101.4	-45.8	22.1
27TH	341.38	-18.7	42.5	1151	1983	-16.3	21.4	41	-31	-359.7	805.2	-91.2	-41.2	21.0
28TH	353.71	-18.9	42.6	1151	1983	-16.4	21.5	41	-31	-340.8	762.6	-81.6	-36.9	19.9
29TH	366.04	-19.0	42.8	1151	1983	-16.5	21.6	41	-31	-321.9	719.8	-72.4	-32.8	18.8
30TH	378.12	-19.1	42.0	1127	1943	-16.9	21.6	42	-32	-302.8	677.8	-64.0	-29.0	17.7
31ST	390.20	-19.2	42.2	1127	1943	-17.0	21.7	42	-32	-283.6	635.6	-56.0	-25.5	16.5
32ND	402.28	-19.2	42.5	1127	1943	-17.0	21.9	42	-32	-264.4	593.0	-48.6	-22.2	15.4
33RD	414.36	-19.2	42.8	1127	1943	-17.1	22.0	42	-32	-245.2	550.2	-41.7	-19.1	14.2
34TH	426.44	-19.3	43.1	1127	1943	-17.1	22.2	42	-32	-225.9	507.1	-35.3	-16.3	13.1
35TH	438.52	-19.3	43.4	1127	1943	-17.1	22.3	42	-32	-206.6	463.7	-29.5	-13.7	11.9
36TH	450.60	-19.4	43.7	1127	1943	-17.2	22.5	42	-32	-187.2	420.0	-24.1	-11.3	10.7
37TH	462.68	-19.3	44.0	1127	1943	-17.1	22.6	42	-32	-167.9	376.1	-19.3	-9.1	9.5
38TH	474.76	-19.2	44.1	1127	1943	-17.0	22.7	41	-30	-148.8	331.9	-15.0	-7.2	8.3
39TH	486.84	-19.0	44.3	1127	1943	-16.9	22.8	40	-29	-129.7	287.6	-11.3	-5.5	7.2
40TH	498.92	-18.9	44.4	1127	1943	-16.8	22.9	39	-28	-110.8	243.2	-8.1	-4.1	6.0
41ST	511.00	-18.8	44.6	1127	1943	-16.7	22.9	38	-27	-92.0	198.6	-5.4	-2.9	4.9
42ND	523.08	-18.7	44.7	1127	1943	-16.6	23.0	37	-26	-73.3	153.9	-3.3	-1.9	3.8
43RD	535.66	-19.3	46.7	1174	2023	-16.5	23.1	37	-26	-54.0	107.2	-1.7	-1.1	2.7
44TH	548.58	-19.2	46.9	1206	2078	-16.0	22.6	37	-26	-34.7	60.3	-.6	-.5	1.6
MR	566.58	-23.8	58.2	1680	2895	-14.2	20.1	34	-23	-10.9	2.1	-.0	-.1	.2
TOP	581.67	-10.9	2.1	1085	2065	-10.1	1.0	-6	50	0.0	0.0	0.0	0.0	0.0

TABLE 7 SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 100 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00													
2ND	23.00	-37.0	69.4	2147	3699	-17.2	18.8	46	-41	-415.8	2066.9	-611.8	-106.0	45.4
3RD	35.92	-17.8	42.3	1206	2078	-14.8	20.4	29	-21	-378.9	1997.5	-565.0	-96.9	43.6
4TH	48.84	-14.5	40.3	1206	2078	-12.1	19.4	28	-17	-361.1	1955.2	-539.5	-92.1	42.8
5TH	61.76	-12.8	39.5	1206	2078	-10.7	19.0	28	-16	-346.5	1914.9	-514.5	-87.5	42.0
6TH	74.68	-12.0	40.2	1206	2078	-10.0	19.3	28	-14	-333.7	1875.4	-490.0	-83.2	41.2
7TH	87.60	-11.2	40.8	1206	2078	-9.3	19.6	29	-13	-321.6	1835.3	-466.0	-78.9	40.4
8TH	100.52	-10.4	41.5	1206	2078	-8.7	20.0	29	-12	-310.4	1794.5	-442.6	-74.8	39.5
9TH	113.44	-9.6	42.2	1206	2078	-8.0	20.3	29	-11	-299.9	1752.9	-419.7	-70.9	38.6
10TH	126.27	-8.8	42.6	1197	2063	-7.3	20.6	29	-10	-290.3	1710.8	-397.3	-67.1	37.7
11TH	139.10	-8.2	43.2	1197	2063	-6.8	21.0	29	-9	-281.5	1668.2	-375.6	-63.4	36.7
12TH	151.93	-8.2	44.0	1197	2063	-6.9	21.3	29	-9	-273.4	1625.0	-354.5	-59.9	35.8
13TH	164.76	-8.3	44.7	1197	2063	-6.9	21.7	28	-9	-265.2	1581.0	-333.9	-56.4	34.8
14TH	177.59	-8.3	45.5	1197	2063	-7.0	22.0	28	-9	-256.9	1536.3	-313.9	-53.1	33.8
15TH	190.42	-8.4	46.2	1197	2063	-7.0	22.4	27	-8	-248.6	1490.8	-294.5	-49.8	32.8
16TH	203.25	-8.4	46.9	1197	2063	-7.1	22.8	27	-8	-240.2	1444.6	-275.7	-46.7	31.9
17TH	216.08	-7.7	47.7	1197	2063	-6.5	23.1	27	-7	-231.7	1397.6	-257.4	-43.6	30.9
18TH	228.66	-7.6	46.9	1174	2023	-6.4	23.2	27	-8	-224.0	1350.0	-239.8	-40.7	29.9
19TH	241.24	-7.7	46.9	1174	2023	-6.6	23.2	28	-8	-216.4	1303.0	-223.1	-38.0	28.9
20TH	253.82	-7.8	46.9	1174	2023	-6.7	23.2	28	-8	-208.7	1256.1	-207.0	-35.3	27.9
21ST	266.40	-8.0	46.9	1174	2023	-6.8	23.2	29	-8	-200.9	1209.2	-191.5	-32.7	26.8
22ND	278.98	-8.1	46.9	1174	2023	-6.9	23.2	29	-9	-192.9	1162.3	-176.6	-30.2	25.8
23RD	291.56	-8.3	46.9	1174	2023	-7.0	23.2	29	-9	-184.8	1115.4	-162.3	-27.8	24.8
24TH	304.14	-8.3	47.0	1174	2023	-7.1	23.2	29	-9	-176.5	1068.5	-148.5	-25.6	23.7
25TH	316.72	-8.2	47.2	1174	2023	-7.0	23.3	29	-9	-168.3	1021.5	-135.4	-23.4	22.6
		-7.9	46.4	1151	1983	-6.9	23.4	29	-8	-160.1	974.3	-122.8	-21.3	21.5

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 180 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-152.2	927.9	-111.1	-19.4	20.5
27TH	341.38	-7.8	46.6	1151	1983	-6.8	23.5	29	-8	-144.4	881.3	-100.0	-17.6	19.5
28TH	353.71	-7.7	46.8	1151	1983	-6.7	23.6	29	-8	-136.7	834.5	-89.4	-15.9	18.4
29TH	366.04	-7.6	46.9	1151	1983	-6.6	23.7	28	-8	-129.0	787.5	-79.4	-14.2	17.4
30TH	378.12	-6.7	46.2	1127	1943	-6.0	23.8	29	-7	-122.3	741.4	-70.2	-12.7	16.3
31ST	390.20	-6.3	46.4	1127	1943	-5.6	23.9	30	-7	-116.0	695.0	-61.5	-11.3	15.2
32ND	402.28	-6.4	46.7	1127	1943	-5.7	24.0	30	-7	-109.6	648.3	-53.4	-9.9	14.1
33RD	414.36	-6.5	46.9	1127	1943	-5.8	24.2	30	-7	-103.0	601.4	-45.8	-8.6	13.0
34TH	426.44	-6.6	47.2	1127	1943	-5.9	24.3	30	-7	-96.4	554.2	-38.8	-7.4	12.0
35TH	438.52	-6.7	47.5	1127	1943	-6.0	24.4	29	-7	-89.7	506.7	-32.4	-6.3	10.9
36TH	450.60	-6.8	47.7	1127	1943	-6.1	24.6	29	-7	-82.8	459.0	-26.6	-5.2	9.8
37TH	462.68	-6.9	48.0	1127	1943	-6.1	24.7	29	-7	-75.9	411.0	-21.3	-4.3	8.7
38TH	474.76	-7.3	48.1	1127	1943	-6.5	24.8	29	-7	-68.6	362.9	-16.7	-3.4	7.6
39TH	486.84	-7.7	48.1	1127	1943	-6.9	24.7	28	-8	-60.9	314.8	-12.6	-2.6	6.5
40TH	498.92	-8.2	48.1	1127	1943	-7.3	24.7	28	-8	-52.7	266.7	-9.1	-1.9	5.5
41ST	511.00	-8.6	48.1	1127	1943	-7.7	24.7	27	-8	-44.0	218.6	-6.1	-1.4	4.5
42ND	523.08	-9.1	48.1	1127	1943	-8.0	24.7	27	-9	-35.0	170.6	-3.8	-.9	3.5
43RD	535.66	-9.6	50.1	1174	2023	-8.2	24.7	27	-9	-25.4	120.5	-2.0	-.5	2.5
44TH	548.58	-9.2	50.4	1206	2078	-7.6	24.3	27	-8	-16.2	70.1	-.7	-.2	1.4
MR	566.58	-10.8	64.7	1680	2895	-6.4	22.4	23	-6	-5.4	5.4	-.0	-.0	.3
TOP	581.67	-5.4	5.4	1085	2065	-5.0	2.6	****	6713	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 110 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									13.5	2293.8	-693.9	42.8	35.3
2ND	23.00	-29.2	73.8	2147	3699	-13.6	20.0	32	-21	42.7	2219.9	-641.9	42.1	33.7
3RD	35.92	-13.7	42.5	1206	2078	-11.4	20.5	22	-12	56.4	2177.4	-613.5	41.5	33.0
4TH	48.84	-11.5	41.6	1206	2078	-9.6	20.0	20	-9	67.9	2135.8	-585 7	40.7	32.4
5TH	61.76	-10.1	41.6	1206	2078	-8.4	20.0	20	-8	78.0	2094.2	-558.3	39.7	31.8
6TH	74.68	-8.8	42.7	1206	2078	-7.3	20.6	20	-7	86.8	2051.4	-531.6	38.7	31.1
7TH	87.60	-7.5	43.9	1206	2078	-6.2	21.1	20	-6	94.2	2007.6	-505.3	37.5	30.5
8TH	100.52	-6.2	45.0	1206	2078	-5.1	21.7	20	-5	100.4	1962.6	-479.7	36.2	29.8
9TH	113.44	-4.9	46.1	1206	2078	-4.1	22.2	20	-4	105 3	1916.5	-454.6	34.9	29.0
10TH	126.27	-3.6	46.9	1197	2063	-3.0	22.7	20	-3	108.9	1869.6	-430.4	33.5	28.3
11TH	139.10	-2.5	47.9	1197	2063	-2.1	23.2	20	-2	111.4	1821.7	-406.7	32.1	27.5
12TH	151.93	-2.2	48.1	1197	2063	-1.8	23.3	20	-2	113.6	1773.6	-383.6	30.7	26.8
13TH	164.76	-1.9	48.3	1197	2063	-1.6	23.4	20	-1	115.5	1725.3	-361.2	29.2	26.0
14TH	177.59	-1.6	48.6	1197	2063	-1.3	23.5	20	-1	117.0	1676.7	-339.3	27.7	25.2
15TH	190.42	-1.3	48.8	1197	2063	-1.1	23.6	19	-1	118.3	1627.9	-318.1	26.2	24.5
16TH	203.25	-1.0	49.0	1197	2063	-.8	23.7	19	-1	119.2	1578.9	-297.6	24.7	23.7
17TH	216.08	1.0	49.2	1197	2063	.8	23.9	21	1	118.3	1529.7	-277.6	23.2	22.9
18TH	228.66	1.5	48.7	1174	2023	1.3	24.1	21	1	116.8	1481.0	-258.7	21.7	22.1
19TH	241.24	1.8	49.2	1174	2023	1.6	24.3	21	1	114.9	1431.8	-240.4	20.2	21.2
20TH	253.82	2.1	49.7	1174	2023	1.8	24.6	21	2	112.8	1382.1	-222.7	18.8	20.4
21ST	266.40	2.4	50.2	1174	2023	2.1	24.8	21	2	110.3	1331.9	-205.6	17.4	19.6
22ND	278.98	2.8	50.7	1174	2023	2.3	25.1	20	2	107.6	1281.2	-189.2	16.0	18.8
23RD	291.56	3.1	51.2	1174	2023	2.6	25.3	20	2	104.5	1230.0	-173.4	14.7	17.9
24TH	304.14	3.3	51.8	1174	2023	2.8	25.6	20	2	101.2	1178.2	-158.2	13.4	17.1
25TH	316.72	3.5	52.3	1174	2023	2.9	25.8	20	2	97.8	1125.9	-143.7	12.1	16.3
		3.5	51.8	1151	1983	3.1	26.1	20	2					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 110 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05	3.7	52.3	1151	1983	3.2	26.4	20	2	94.2	1074.1	-130.2	10.9	15.5
27TH	341.38	3.8	52.8	1151	1983	3.3	26.6	19	2	90.6	1021.8	-117.2	9.8	14.7
28TH	353.71	3.9	53.3	1151	1983	3.4	26.9	19	2	86.8	969.0	-105.0	8.7	13.8
29TH	366.04	5.2	52.8	1127	1943	4.6	27.2	21	3	82.9	915.7	-93.3	7.7	13.0
30TH	378.12	5.9	53.1	1127	1943	5.3	27.3	21	4	77.7	863.0	-82.6	6.7	12.2
31ST	390.20	5.9	53.3	1127	1943	5.2	27.5	21	4	71.8	809.8	-72.5	5.8	11.3
32ND	402.28	5.9	53.6	1127	1943	5.2	27.6	21	4	65.9	756.5	-63.0	5.0	10.4
33RD	414.36	5.9	53.8	1127	1943	5.2	27.7	20	4	60.0	702.9	-54.2	4.2	9.5
34TH	426.44	5.9	54.1	1127	1943	5.2	27.8	20	4	54.1	649.1	-46.1	3.5	8.7
35TH	438.52	5.8	54.3	1127	1943	5.2	27.9	20	4	48.3	595.1	-38.5	2.9	7.8
36TH	450.60	5.8	54.5	1127	1943	5.2	28.1	20	4	42.4	540.8	-31.7	2.3	6.9
37TH	462.68	5.4	55.1	1127	1943	4.8	28.4	19	3	36.6	486.2	-25.5	1.9	6.1
38TH	474.76	4.9	55.7	1127	1943	4.3	28.7	18	3	31.2	431.2	-19.9	1.5	5.3
39TH	486.84	4.4	56.3	1127	1943	3.9	29.0	17	2	26.3	375.4	-15.1	1.1	4.5
40TH	498.92	3.9	56.9	1127	1943	3.4	29.3	16	2	22.0	319.1	-10.9	.8	3.8
41ST	511.00	3.4	57.6	1127	1943	3.0	29.6	15	2	18.1	262.2	-7.4	.6	3.0
42ND	523.08	3.5	60.6	1174	2023	3.0	29.9	15	1	14.8	204.6	-4.5	.4	2.3
43RD	535.66	4.2	61.9	1206	2078	3.5	29.3	15	2	11.2	144.0	-2.3	.2	1.6
44TH	548.58	4.8	74.9	1680	2895	2.9	25.9	12	1	7.0	83.1	-.9	.1	.9
MR	566.58	2.2	8.2	1085	2065	2.0	4.0	23	10	2.2	8.2	-.1	.0	.1
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 120 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									281.5	2453.0	-748.5	122.1	24.3
2ND	23.00	-22.1	79.7	2147	3699	-10.3	21.5	20	-9	303.6	2373.3	-693.0	115.4	23.1
3RD	35.92	-10.3	46.5	1206	2078	-8.6	22.4	14	-5	313.9	2326.8	-662.7	111.4	22.6
4TH	48.84	-7.6	45.1	1206	2078	-6.3	21.7	15	-4	321.5	2281.7	-632.9	107.3	22.1
5TH	61.76	-5.2	44.6	1206	2078	-4.3	21.5	16	-3	326.7	2237.1	-603.7	103.1	21.5
6TH	74.68	-3.5	45.4	1206	2078	-2.9	21.8	16	-2	330.2	2191.7	-575.1	98.9	21.0
7TH	87.60	-1.8	46.2	1206	2078	-1.5	22.2	16	-1	332.0	2145.5	-547.1	94.6	20.4
8TH	100.52	-.1	46.9	1206	2078	-.1	22.6	17	-0	332.1	2098.6	-519.7	90.3	19.7
9TH	113.44	1.6	47.7	1206	2078	1.3	23.0	17	1	330.5	2050.9	-492.9	86.0	19.1
10TH	126.27	3.2	48.1	1197	2063	2.7	23.3	17	2	327.3	2002.7	-466.9	81.8	18.5
11TH	139.10	4.6	48.9	1197	2063	3.8	23.7	17	3	322.7	1953.8	-441.5	77.6	17.8
12TH	151.93	4.8	49.5	1197	2063	4.0	24.0	16	3	317.9	1904.3	-416.7	73.5	17.2
13TH	164.76	5.0	50.2	1197	2063	4.1	24.3	16	3	312.9	1854.1	-392.6	69.5	16.5
14TH	177.59	5.1	50.9	1197	2063	4.3	24.7	15	3	307.8	1803.2	-369.2	65.5	15.9
15TH	190.42	5.3	51.6	1197	2063	4.4	25.0	14	3	302.5	1751.6	-346.3	61.6	15.3
16TH	203.25	5.5	52.2	1197	2063	4.6	25.3	14	2	297.0	1699.4	-324.2	57.7	14.8
17TH	216.08	7.5	52.9	1197	2063	6.3	25.6	15	4	289.4	1646.5	-302.7	54.0	14.1
18TH	228.66	7.9	52.3	1174	2023	6.8	25.8	16	4	281.5	1594.2	-282.4	50.4	13.5
19TH	241.24	8.2	52.6	1174	2023	7.0	26.0	16	4	273.3	1541.7	-262.6	46.9	12.8
20TH	253.82	8.4	52.9	1174	2023	7.2	26.1	16	4	264.9	1488.8	-243.6	43.5	12.2
21ST	266.40	8.7	53.2	1174	2023	7.4	26.3	16	4	256.2	1435.7	-225.2	40.2	11.5
22ND	278.98	8.9	53.5	1174	2023	7.6	26.4	16	5	247.3	1382.2	-207.5	37.1	10.8
23RD	291.56	9.2	53.8	1174	2023	7.8	26.6	16	5	238.1	1328.4	-190.4	34.0	10.2
24TH	304.14	9.4	54.1	1174	2023	8.0	26.8	16	5	228.7	1274.3	-174.0	31.1	9.5
25TH	316.72	9.5	54.6	1174	2023	8.1	27.0	15	4	219.2	1219.7	-158.3	28.2	8.9
		9.4	54.0	1151	1983	8.1	27.2	14	4					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 120 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05	9.5	54.4	1151	1983	8.2	27.5	13	4	209.9	1165.7	-143.6	25.6	8.3
27TH	341.38	9.6	54.9	1151	1983	8.3	27.7	12	4	200.4	1111.2	-129.6	23.1	7.7
28TH	353.71	9.6	55.4	1151	1983	8.4	27.9	11	3	190.8	1056.3	-116.2	20.7	7.2
29TH	366.04	10.8	54.7	1127	1943	9.6	28.1	12	4	181.2	1001.0	-103.6	18.4	6.7
30TH	378.12	11.5	55.4	1127	1943	10.2	28.5	12	4	170.4	946.3	-91.8	16.2	6.2
31ST	390.20	11.4	56.2	1127	1943	10.1	28.9	12	4	158.9	890.9	-80.7	14.3	5.7
32ND	402.28	11.3	57.1	1127	1943	10.0	29.4	11	4	147.5	834.7	-70.3	12.4	5.2
33RD	414.36	11.2	57.9	1127	1943	9.9	29.8	11	4	136.2	777.6	-60.5	10.7	4.7
34TH	426.44	11.1	58.8	1127	1943	9.8	30.3	11	3	125.0	719.7	-51.5	9.1	4.2
35TH	438.52	10.9	59.6	1127	1943	9.7	30.7	10	3	114.0	660.9	-43.2	7.7	3.8
36TH	450.60	10.8	60.5	1127	1943	9.6	31.1	10	3	103.1	601.2	-35.5	6.4	3.3
37TH	462.68	10.5	61.1	1127	1943	9.3	31.4	9	3	92.3	540.8	-28.6	5.2	2.8
38TH	474.76	10.2	61.6	1127	1943	9.1	31.7	9	2	81.7	479.7	-22.5	4.1	2.4
39TH	486.84	9.9	62.0	1127	1943	8.8	31.9	8	2	71.5	418.2	-17.0	3.2	2.0
40TH	498.92	9.6	62.5	1127	1943	8.6	32.2	7	2	61.6	356.1	-12.4	2.4	1.6
41ST	511.00	9.3	63.0	1127	1943	8.3	32.4	7	2	51.9	293.6	-8.4	1.7	1.3
42ND	523.08	10.0	66.2	1174	2023	8.5	32.7	6	2	42.6	230.5	-5.3	1.1	.9
43RD	535.66	11.1	66.7	1206	2078	9.2	32.1	7	2	32.5	164.3	-2.8	.7	.6
44TH	548.58	13.9	83.7	1680	2895	8.3	28.9	4	1	21.5	97.6	-1.1	.3	.3
MR	566.58	7.6	13.9	1085	2065	7.0	6.7	-5	-5	7.6	13.9	-.1	.1	-.0
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 130 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									334.6	2144.7	-668.8	118.9	17.4
2ND	23.00	-11.3	66.9	2147	3699	-5.3	18.1	20	-6	345.9	2077.7	-620.2	111.1	16.4
3RD	35.92	-4.8	39.2	1206	2078	-3.9	18.9	14	-3	350.6	2038.6	-593.7	106.6	15.9
4TH	48.84	-2.7	38.2	1206	2078	-2.3	18.4	14	-2	353.4	2000.4	-567.6	102.1	15.5
5TH	61.76	-.6	37.8	1206	2078	-.5	18.2	15	-0	354.0	1962.6	-542.0	97.5	15.0
6TH	74.68	.9	38.3	1206	2078	.7	18.4	16	1	353.1	1924.3	-516.9	92.9	14.6
7TH	87.60	2.3	38.8	1206	2078	1.9	18.7	16	2	350.7	1885.6	-492.2	88.4	14.1
8TH	100.52	3.8	39.2	1206	2078	3.2	18.9	17	3	346.9	1846.3	-468.1	83.9	13.5
9TH	113.44	5.3	39.7	1206	2078	4.4	19.1	18	4	341.6	1806.6	-444.5	79.4	13.0
10TH	126.27	6.7	39.9	1197	2063	5.6	19.3	18	5	334.9	1766.7	-421.6	75.1	12.4
11TH	139.10	7.9	40.4	1197	2063	6.6	19.6	19	6	327.0	1726.2	-399.2	70.8	11.9
12TH	151.93	7.9	41.0	1197	2063	6.6	19.9	17	6	319.2	1685.2	-377.3	66.7	11.3
13TH	164.76	7.8	41.6	1197	2063	6.5	20.1	16	5	311.3	1643.6	-356.0	62.7	10.8
14TH	177.59	7.8	42.1	1197	2063	6.5	20.4	16	5	303.5	1601.5	-335.2	58.7	10.3
15TH	190.42	7.8	42.7	1197	2063	6.5	20.7	15	5	295.7	1558.8	-314.9	54.9	9.8
16TH	203.25	7.8	43.3	1197	2063	6.5	21.0	14	4	287.9	1515.6	-295.2	51.1	9.3
17TH	216.08	9.6	43.8	1197	2063	8.0	21.2	16	6	278.2	1471.7	-276.0	47.5	8.8
18TH	228.66	9.9	43.6	1174	2023	8.5	21.5	16	6	268.3	1428.2	-257.8	44.1	8.3
19TH	241.24	10.1	44.1	1174	2023	8.6	21.8	15	6	258.2	1384.0	-240.1	40.7	7.8
20TH	253.82	10.3	44.7	1174	2023	8.7	22.1	15	6	248.0	1339.3	-222.9	37.6	7.3
21ST	266.40	10.4	45.3	1174	2023	8.9	22.4	15	6	237.5	1294.0	-206.4	34.5	6.8
22ND	278.98	10.6	45.9	1174	2023	9.0	22.7	14	6	226.9	1248.1	-190.4	31.6	6.3
23RD	291.56	10.8	46.5	1174	2023	9.2	23.0	14	5	216.2	1201.6	-175.0	28.8	5.8
24TH	304.14	10.8	47.1	1174	2023	9.2	23.3	13	5	205.4	1154.5	-160.2	26.1	5.3
25TH	316.72	10.5	47.7	1174	2023	8.9	23.6	12	5	194.9	1106.8	-145.9	23.6	4.9
		10.0	47.3	1151	1983	8.7	23.9	11	4					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 130 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									184.9	1059.5	-132.6	21.3	4.5
		9.7	47.8	1151	1983	8.5	24.1	10	4					
27TH	341.38									175.2	1011.6	-119.8	19.1	4.1
		9.5	48.4	1151	1983	8.2	24.4	9	3					
28TH	353.71									165.7	963.2	-107.6	17.0	3.7
		9.2	48.9	1151	1983	8.0	24.7	8	3					
29TH	366.04									156.5	914.3	-96.1	15.0	3.4
		10.0	48.5	1127	1943	8.8	25.0	9	3					
30TH	378.12									146.6	865.8	-85.3	13.1	3.1
		10.6	49.2	1127	1943	9.4	25.3	9	3					
31ST	390.20									136.0	816.6	-75.1	11.4	2.8
		10.5	50.1	1127	1943	9.3	25.8	8	3					
32ND	402.28									125.5	766.4	-65.6	9.9	2.5
		10.5	51.0	1127	1943	9.3	26.3	8	3					
33RD	414.36									115.0	715.4	-56.6	8.4	2.2
		10.4	51.9	1127	1943	9.3	26.7	7	3					
34TH	426.44									104.6	663.5	-48.3	7.1	1.9
		10.4	52.8	1127	1943	9.2	27.2	7	2					
35TH	438.52									94.2	610.7	-40.6	5.9	1.6
		10.4	53.7	1127	1943	9.2	27.6	7	2					
36TH	450.60									83.8	557.0	-33.6	4.8	1.3
		10.3	54.6	1127	1943	9.1	28.1	6	2					
37TH	462.68									73.5	502.4	-27.2	3.9	1.0
		9.7	55.2	1127	1943	8.6	28.4	6	2					
38TH	474.76									63.8	447.2	-21.4	3.0	.8
		9.2	55.9	1127	1943	8.1	28.8	5	1					
39TH	486.84									54.6	391.3	-16.4	2.3	.6
		8.6	56.5	1127	1943	7.6	29.1	4	1					
40TH	498.92									46.1	334.9	-12.0	1.7	.4
		8.0	57.1	1127	1943	7.1	29.4	4	1					
41ST	511.00									38.1	277.7	-8.3	1.2	.2
		7.4	57.7	1127	1943	6.6	29.7	3	1					
42ND	523.08									30.7	220.0	-5.3	.8	.1
		7.7	60.8	1174	2023	6.6	30.0	3	1					
43RD	535.66									22.9	159.2	-2.9	.4	-.0
		8.5	61.5	1206	2070	7.1	29.6	2	1					
44TH	548.58									14.4	97.8	-1.2	.2	-.1
		10.1	77.5	1680	2895	6.0	26.8	1	0					
MR	566.58									4.3	20.3	-.2	.0	-.2
		4.3	20.3	1085	2065	4.0	9.8	-12	-4					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 140 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									163.5	1700.2	-563 9	76.7	12.1
2ND	23.00	-16.4	46.9	2147	3699	-7.6	12.7	29	-17	179.9	1653.4	-525.3	72.7	11.1
3RD	35.92	-7.8	26.9	1206	2078	-6.5	12.9	20	-10	187.8	1626.5	-504.1	70.4	10.7
4TH	48.84	-5.8	25.9	1206	2078	-4.8	12.5	19	-7	193.6	1600.6	-483.3	67.9	10.4
5TH	61.76	-4.2	25.6	1206	2078	-3.5	12.3	20	-6	197.8	1575.0	-462.8	65.4	10.0
6TH	74.68	-3.3	26.0	1206	2078	-2.7	12.5	20	-4	201.1	1549.0	-442.6	62.8	9.5
7TH	87.60	-2.4	26.5	1206	2078	-2.0	12.7	21	-3	203.5	1522.5	-422 8	60.2	9.1
8TH	100.52	-1.5	26.9	1206	2078	-1.2	12.9	21	-2	205.0	1495.6	-403.3	57.5	8.7
9TH	113.44	-.5	27.3	1206	2078	-.4	13.2	22	-1	205.5	1468.3	-384 1	54.9	8.2
10TH	126.27	.4	27.6	1197	2063	.3	13.4	23	1	205.1	1440.7	-365.4	52.2	7.7
11TH	139.10	1.2	28.0	1197	2063	1.0	13.6	23	2	203.9	1412.7	-347.1	49.6	7.2
12TH	151.93	1.4	28.4	1197	2063	1.2	13.7	22	2	202.5	1384.3	-329.2	47.0	6.7
13TH	164.76	1.7	28.7	1197	2063	1.4	13.9	20	2	200.8	1355.6	-311 6	44.4	6.2
14TH	177.59	1.9	29.1	1197	2063	1.6	14.1	19	2	198.9	1326.5	-294.4	41.9	5.8
15TH	190.42	2.2	29.4	1197	2063	1.8	14.2	18	2	196.7	1297.1	-277.6	39.3	5.4
16TH	203.25	2.5	29.7	1197	2063	2.0	14.4	17	2	194.3	1267.4	-261.1	36.8	5.0
17TH	216.08	4.0	30.1	1197	2063	3.3	14.6	18	4	190.2	1237.3	-245 1	34.4	4.5
18TH	228.66	4.7	30.2	1174	2023	4.0	14.9	18	5	185.5	1207.1	-229.7	32.0	4.1
19TH	241.24	5.3	31.0	1174	2023	4.5	15.3	17	5	180.2	1176.1	-214.7	29.7	3.7
20TH	253.82	5.9	31.8	1174	2023	5.0	15.7	16	5	174.3	1144.2	-200.1	27.5	3.4
21ST	266.40	6.5	32.7	1174	2023	5.6	16.1	15	5	167 8	1111.6	-185.9	25.3	3.0
22ND	278.98	7.1	33.5	1174	2023	6.1	16.5	14	5	160.7	1078.1	-172.1	23.2	2.6
23RD	291.56	7.7	34.3	1174	2023	6.6	16.9	13	5	152.9	1043.8	-158.8	21.3	2.3
24TH	304.14	7.9	35.1	1174	2023	6.8	17.4	12	5	145.0	1008.7	-145.9	19.4	2.0
25TH	316.72	7.5	36.3	1174	2023	6.4	17.9	11	4	137.5	972.4	-133.4	17.6	1.7
		7.0	36.7	1151	1983	6.1	18.5	9	3					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 140 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05	6.6	37.8	1151	1983	5.7	19.1	8	2	130.5	935.7	-121.7	16.0	1.4
27TH	341.38	6.2	39.0	1151	1983	5.4	19.7	7	2	123.9	897.8	-110.4	14.4	1.2
28TH	353.71	5.8	40.1	1151	1983	5.1	20.2	6	2	117.7	858.9	-99.5	12.9	1.0
29TH	366.04	6.2	40.4	1127	1943	5.5	20.8	6	2	111.9	818.8	-89.2	11.5	.8
30TH	378.12	6.7	41.3	1127	1943	5.9	21.3	6	2	105.7	778.4	-79.5	10.2	.6
31ST	390.20	6.7	42.3	1127	1943	5.9	21.8	5	1	99.0	737.1	-70.4	8.9	.4
32ND	402.28	6.7	43.3	1127	1943	6.0	22.3	5	1	92.3	694.8	-61.7	7.8	.2
33RD	414.36	6.8	44.3	1127	1943	6.0	22.8	4	1	85.6	651.5	-53.6	6.7	.0
34TH	426.44	6.8	45.3	1127	1943	6.0	23.3	4	1	78.8	607.2	-46.0	5.7	-.1
35TH	438.52	6.8	46.2	1127	1943	6.1	23.8	3	1	72.0	562.0	-38.9	4.8	-.2
36TH	450.60	6.9	47.2	1127	1943	6.1	24.3	2	1	65.2	515.7	-32.4	4.0	-.3
37TH	462.68	6.7	48.2	1127	1943	5.9	24.8	2	0	58.3	468.5	-26.5	3.2	-.4
38TH	474.76	6.5	49.1	1127	1943	5.8	25.3	1	0	51.6	420.4	-21.1	2.6	-.5
39TH	486.84	6.3	50.0	1127	1943	5.6	25.7	0	0	45.1	371.3	-16.3	2.0	-.5
40TH	498.92	6.1	50.9	1127	1943	5.4	26.2	-0	-0	38.8	321.3	-12.2	1.5	-.5
41ST	511.00	5.9	51.8	1127	1943	5.2	26.7	-1	-0	32.7	270.4	-8.6	1.0	-.5
42ND	523.08	6.4	54.9	1174	2023	5.5	27.1	-2	-0	26.8	218.6	-5.6	.7	-.5
43RD	535.66	7.4	56.6	1206	2078	6.1	27.3	-1	-0	20.4	163.7	-3.2	.4	-.4
44TH	548.58	9.5	76.1	1680	2895	5.7	26.3	-1	-0	13.0	107.0	-1.5	.2	-.3
MR	566.58	3.5	30.9	1085	2065	3.2	15.0	-12	-2	3.5	30.9	-.2	.0	-.3
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 150 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									133.3	1169.2	-408.2	69.1	3.6
2ND	23.00	-10.0	25.2	2147	3699	-4.6	6.8	36	-24	143.3	1143.9	-381.6	65.9	3.0
3RD	35.92	-4.9	15.1	1206	2078	-4.1	7.3	23	-12	148.2	1128.8	-366.9	64.0	2.8
4TH	48.84	-4.3	14.3	1206	2078	-3.6	6.9	20	-10	152.5	1114.5	-352.4	62.1	2.6
5TH	61.76	-3.8	13.9	1206	2078	-3.2	6.7	20	-10	156.4	1100.5	-338.1	60.1	2.4
6TH	74.68	-3.3	14.1	1206	2078	-2.8	6.8	22	-9	159.7	1086.5	-324.0	58.0	2.1
7TH	87.60	-2.8	14.2	1206	2078	-2.3	6.8	23	-8	162.5	1072.2	-310.0	55.9	1.9
8TH	100.52	-2.3	14.3	1206	2078	-1.9	6.9	25	-7	164.8	1057.9	-296.3	53.8	1.6
9TH	113.44	-1.8	14.5	1206	2078	-1.5	7.0	26	-5	166.6	1043.4	-282.7	51.7	1.3
10TH	126.27	-1.3	14.5	1197	2063	-1.1	7.0	27	-4	167.9	1028.9	-269.4	49.5	1.0
11TH	139.10	-.8	14.8	1197	2063	-.7	7.2	28	-3	168.7	1014.1	-256.3	47.4	.7
12TH	151.93	-.5	15.5	1197	2063	-.4	7.5	24	-1	169.1	998.6	-243.4	45.2	.4
13TH	164.76	-.2	16.3	1197	2063	-.1	7.9	21	-0	169.3	982.4	-230.7	43.0	.1
14TH	177.59	.1	17.0	1197	2063	.1	8.2	19	0	169.2	965.4	-218.2	40.9	-.2
15TH	190.42	.4	17.8	1197	2063	.4	8.6	16	1	168.7	947.6	-205.9	38.7	-.4
16TH	203.25	.8	18.5	1197	2063	.6	9.0	14	1	168.0	929.1	-193.9	36.5	-.6
17TH	216.08	1.8	19.2	1197	2063	1.5	9.3	14	2	166.2	909.9	-182.1	34.4	-.8
18TH	228.66	2.3	19.9	1174	2023	2.0	9.8	12	2	163.8	890.0	-170.8	32.3	-1.0
19TH	241.24	2.8	21.0	1174	2023	2.4	10.4	10	2	161.0	869.0	-159.7	30.3	-1.2
20TH	253.82	3.3	22.1	1174	2023	2.8	10.9	9	2	157.7	846.9	-148.9	28.3	-1.3
21ST	266.40	3.8	23.2	1174	2023	3.2	11.5	7	2	153.9	823.7	-138.4	26.3	-1.5
22ND	278.98	4.3	24.3	1174	2023	3.6	12.0	6	2	149.7	799.5	-128.2	24.4	-1.6
23RD	291.56	4.7	25.4	1174	2023	4.0	12.5	5	2	145.0	774.1	-118.3	22.6	-1.7
24TH	304.14	5.0	26.3	1174	2023	4.3	13.0	4	1	139.9	747.8	-108.7	20.8	-1.7
25TH	316.72	5.0	27.1	1174	2023	4.2	13.4	3	1	135.0	720.7	-99.5	19.0	-1.8
		4.8	27.3	1151	1983	4.2	13.8	2	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 150 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									130.2	693.4	-90.8	17.4	-1.8
		4.8	28.0	1151	1983	4.1	14.1	1	0					
27TH	341.38									125.4	665.4	-82.4	15.8	-1.9
		4.7	28.7	1151	1983	4.1	14.5	-0	-0					
28TH	353.71									120.7	636.7	-74.4	14.3	-1.8
		4.6	29.5	1151	1983	4.0	14.9	-1	-0					
29TH	366.04									116.1	607.2	-66.7	12.8	-1.8
		5.2	29.6	1127	1943	4.6	15.2	-1	-0					
30TH	378.12									110.8	577.7	-59.5	11.5	-1.8
		5.7	30.2	1127	1943	5.1	15.6	-1	-0					
31ST	390.20									105.1	547.4	-52.7	10.2	-1.8
		5.9	31.0	1127	1943	5.2	15.9	-2	-1					
32ND	402.28									99.2	516.4	-46.3	8.9	-1.7
		6.0	31.7	1127	1943	5.4	16.3	-2	-1					
33RD	414.36									93.1	484.7	-40.3	7.8	-1.7
		6.2	32.5	1127	1943	5.5	16.7	-2	-1					
34TH	426.44									87.0	452.3	-34.6	6.7	-1.6
		6.3	33.2	1127	1943	5.6	17.1	-3	-1					
35TH	438.52									80.6	419.1	-29.3	5.7	-1.6
		6.5	33.9	1127	1943	5.7	17.5	-3	-1					
36TH	450.60									74.2	385.1	-24.5	4.7	-1.5
		6.6	34.7	1127	1943	5.9	17.8	-4	-1					
37TH	462.68									67.5	350.5	-20.0	3.9	-1.4
		6.7	35.4	1127	1943	6.0	18.2	-4	-1					
38TH	474.76									60.8	315.1	-16.0	3.1	-1.3
		6.8	36.2	1127	1943	6.1	18.6	-4	-1					
39TH	486.84									54.0	278.9	-12.4	2.4	-1.2
		6.9	36.9	1127	1943	6.1	19.0	-5	-1					
40TH	498.92									47.0	241.9	-9.3	1.8	-1.0
		7.0	37.7	1127	1943	6.2	19.4	-5	-2					
41ST	511.00									40.0	204.2	-6.6	1.3	-.9
		7.1	38.4	1127	1943	6.3	19.8	-5	-2					
42ND	523.08									32.9	165.8	-4.4	.8	-.7
		8.0	40.8	1174	2023	6.8	20.2	-5	-2					
43RD	535.66									24.9	125.0	-2.5	.5	-.6
		9.0	42.1	1206	2078	7.5	20.3	-4	-2					
44TH	548.58									15.9	82.9	-1.2	.2	-.4
		11.5	56.3	1680	2895	6.9	19.4	-4	-1					
MR	566.58									4.4	26.6	-.2	.0	-.3
		4.4	26.6	1085	2065	4.0	12.9	-13	-4					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 160 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF COST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									168.4	724.7	-273.6	69.5	-1.9
2ND	23.00	-4.6	11.5	2147	3699	-2.1	3.1	38	-26	173.0	713.1	-257.0	65.6	-2.2
3RD	35.92	-2.2	6.6	1206	2078	-1.8	3.2	21	-12	175.1	706.5	-247.9	63.4	-2.3
4TH	48.84	-1.4	6.5	1206	2078	-1.1	3.1	15	-6	176.5	700.0	-238.8	61.1	-2.3
5TH	61.76	-.8	6.4	1206	2078	-.6	3.1	15	-3	177.3	693.6	-229.8	58.8	-2.4
6TH	74.68	-.5	6.1	1206	2078	-.4	2.9	17	-2	177.8	687.5	-220.9	56.5	-2.5
7TH	87.60	-.2	5.9	1206	2078	-.2	2.8	20	-1	178.0	681.6	-212.0	54.2	-2.6
8TH	100.52	.0	5.6	1206	2078	.0	2.7	22	0	178.0	675.9	-203.2	51.9	-2.7
9TH	113.44	.3	5.4	1206	2078	.2	2.6	26	2	177.7	670.5	-194.5	49.6	-2.8
10TH	126.27	.5	5.1	1197	2063	.4	2.5	29	5	177.2	665.4	-186.0	47.3	-2.9
11TH	139.10	.8	5.0	1197	2063	.7	2.4	32	9	176.4	660.4	-177.5	45.1	-3.0
12TH	151.93	1.2	5.7	1197	2063	1.0	2.8	25	9	175.2	654.7	-169.0	42.8	-3.2
13TH	164.76	1.6	6.4	1197	2063	1.3	3.1	20	8	173.6	648.3	-160.7	40.6	-3.2
14TH	177.59	2.0	7.0	1197	2063	1.7	3.4	15	7	171.6	641.3	-152.4	38.4	-3.3
15TH	190.42	2.4	7.7	1197	2063	2.0	3.7	11	6	169.2	633.6	-144.2	36.2	-3.4
16TH	203.25	2.8	8.4	1197	2063	2.3	4.1	8	4	166.4	625.2	-136.1	34.0	-3.4
17TH	216.08	3.9	9.0	1197	2063	3.3	4.4	10	7	162.5	616.2	-128.2	31.9	-3.5
18TH	228.66	4.2	9.8	1174	2023	3.6	4.8	7	5	158.3	606.4	-120.5	29.9	-3.5
19TH	241.24	4.4	10.7	1174	2023	3.8	5.3	3	2	153.9	595.7	-112.9	27.9	-3.6
20TH	253.82	4.6	11.6	1174	2023	3.9	5.8	0	0	149.2	584.1	-105.5	26.0	-3.6
21ST	266.40	4.8	12.6	1174	2023	4.1	6.2	-2	-2	144.4	571.5	-98.2	24.2	-3.5
22ND	278.98	5.1	13.5	1174	2023	4.3	6.7	-4	-3	139.3	558.0	-91.1	22.4	-3.5
23RD	291.56	5.3	14.5	1174	2023	4.5	7.2	-6	-4	134.1	543.5	-84.2	20.7	-3.4
24TH	304.14	5.3	15.4	1174	2023	4.5	7.6	-7	-4	128.7	528.1	-77.5	19.0	-3.4
25TH	316.72	5.2	16.6	1174	2023	4.4	8.2	-8	-4	123.6	511.5	-70.9	17.4	-3.3
		4.9	17.4	1151	1983	4.2	8.8	-8	-4					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 160 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05	4.7	18.5	1151	1983	4.1	9.3	-9	-4	118.7	494.2	-64.7	15.9	-3.2
27TH	341.38	4.5	19.6	1151	1983	3.9	9.9	-9	-4	114.0	475.7	-58.7	14.5	-3.0
28TH	353.71	4.4	20.7	1151	1983	3.8	10.4	-10	-3	109.5	456.1	-53.0	13.1	-2.9
29TH	366.04	4.5	21.4	1127	1943	4.0	11.0	-10	-3	105.1	435.4	-47.5	11.8	-2.7
30TH	378.12	4.9	22.0	1127	1943	4.3	11.3	-9	-3	100.6	414.0	-42.4	10.6	-2.6
31ST	390.20	5.1	22.5	1127	1943	4.5	11.6	-9	-3	95.7	392.0	-37.5	9.4	-2.4
32ND	402.28	5.2	23.0	1127	1943	4.7	11.9	-9	-3	90.7	369.5	-32.9	8.3	-2.3
33RD	414.36	5.4	23.5	1127	1943	4.8	12.1	-9	-3	85.4	346.5	-28.6	7.2	-2.1
34TH	426.44	5.6	24.0	1127	1943	5.0	12.4	-9	-3	80.0	322.9	-24.5	6.2	-2.0
35TH	438.52	5.8	24.5	1127	1943	5.2	12.6	-9	-3	74.4	298.9	-20.8	5.3	-1.8
36TH	450.60	6.0	25.0	1127	1943	5.3	12.9	-8	-3	68.5	274.3	-17.3	4.4	-1.6
37TH	462.68	6.1	25.5	1127	1943	5.4	13.1	-8	-3	62.6	249.3	-14.2	3.6	-1.5
38TH	474.76	6.3	26.0	1127	1943	5.6	13.4	-9	-4	56.4	223.8	-11.3	2.9	-1.3
39TH	486.84	6.5	26.5	1127	1943	5.7	13.6	-9	-4	50.1	197.8	-8.8	2.2	-1.1
40TH	498.92	6.6	27.0	1127	1943	5.9	13.9	-9	-4	43.6	171.3	-6.5	1.7	-1.0
41ST	511.00	6.8	27.4	1127	1943	6.0	14.1	-9	-4	37.0	144.3	-4.6	1.2	-.8
42ND	523.08	7.4	29.1	1174	2023	6.3	14.4	-8	-4	30.2	116.9	-3.0	.8	-.6
43RD	535.66'	7.9	29.9	1206	2078	6.5	14.4	-7	-3	22.9	87.9	-1.8	.5	-.5
44TH	548.58	10.5	40.1	1680	2895	6.2	13.9	-4	-2	15.0	57.9	-.8	.2	-.3
MR	566.58	4.5	17.8	1085	2065	4.2	8.6	-13	-6	4.5	17.8	-.1	.0	-.2
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 170 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									243.3	827.9	-311.7	84.5	-6.8
2ND	23.00	2.8	8.5	2147	3699	1.3	2.3	44	25	240.5	819.4	-292.8	79.0	-7.0
3RD	35.92	1.6	4.7	1206	2078	1.3	2.3	23	13	238.9	814.7	-282.2	75.9	-7.1
4TH	48.84	2.0	4.0	1206	2078	1.7	1.9	20	17	236.9	810.7	-271.7	72.8	-7.2
5TH	61.76	2.6	3.7	1206	2078	2.2	1.8	20	24	234.3	807.0	-261.2	69.8	-7.2
6TH	74.68	2.9	3.9	1206	2078	2.4	1.9	5	7	231.3	803.2	-250.8	66.8	-7.2
7TH	87.60	3.2	4.1	1206	2078	2.7	2.0	-13	-17	228.1	799.1	-240.5	63.8	-7.2
8TH	100.52	3.5	4.2	1206	2078	2.9	2.0	-35	-50	224.6	794.9	-230.2	60.9	-7.1
9TH	113.44	3.8	4.4	1206	2078	3.2	2.1	-65	-96	220.8	790.4	-220.0	58.0	-7.1
10TH	126.27	4.1	4.6	1197	2063	3.4	2.2	-109	-165	216.8	785.9	-209.8	55.2	-7.0
11TH	139.10	4.3	4.9	1197	2063	3.6	2.4	-105	-155	212.5	780.9	-199.8	52.4	-6.9
12TH	151.93	4.2	6.3	1197	2063	3.5	3.0	-43	-50	208.2	774.7	-189.8	49.7	-6.8
13TH	164.76	4.2	7.6	1197	2063	3.5	3.7	-32	-29	204.1	767.1	-179.9	47.1	-6.6
14TH	177.59	4.1	8.9	1197	2063	3.4	4.3	-27	-21	200.0	758.2	-170.1	44.5	-6.5
15TH	190.42	4.0	10.2	1197	2063	3.4	4.9	-24	-16	196.0	748.0	-160.5	41.9	-6.3
16TH	203.25	4.0	11.5	1197	2063	3.3	5.6	-22	-13	192.0	736.5	-151.0	39.5	-6.2
17TH	216.08	4.3	12.8	1197	2063	3.6	6.2	-20	-12	187.7	723.6	-141.6	37.0	-6.0
18TH	228.66	4.4	14.0	1174	2023	3.8	6.9	-18	-10	183.3	709.6	-132.6	34.7	-5.8
19TH	241.24	4.5	15.5	1174	2023	3.8	7.6	-17	-8	178.7	694.2	-123.7	32.4	-5.6
20TH	253.82	4.6	16.9	1174	2023	3.9	8.4	-16	-7	174.1	677.2	-115.1	30.2	-5.4
21ST	266.40	4.7	18.4	1174	2023	4.0	9.1	-15	-7	169.4	658.9	-106.7	28.0	-5.2
22ND	278.98	4.8	19.8	1174	2023	4.1	9.8	-14	-6	164.5	639.0	-98.5	25.9	-5.0
23RD	291.56	4.9	21.3	1174	2023	4.2	10.5	-14	-5	159.6	617.8	-90.6	23.9	-4.7
24TH	304.14	5.1	22.4	1174	2023	4.4	11.1	-13	-5	154.5	595.3	-83.0	21.9	-4.5
25TH	316.72	5.4	23.3	1174	2023	4.6	11.5	-13	-5	149.1	572.1	-75.7	20.0	-4.3
		5.5	23.6	1151	1983	4.8	11.9	-12	-5					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 170 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
										143.7	548.5	-68.8	18.2	-4.1
26TH	329.05	5.7	24.4	1151	1983	5.0	12.3	-12	-5	138.0	524.0	-62.1	16.5	-3.9
27TH	341.38	5.9	25.2	1151	1983	5.2	12.7	-11	-5	132.0	498.8	-55.8	14.8	-3.6
28TH	353.71	6.2	26.0	1151	1983	5.3	13.1	-11	-4	125.9	472.8	-49.9	13.2	-3.4
29TH	366.04	6.4	26.3	1127	1943	5.7	13.5	-10	-4	119.5	446.5	-44.3	11.7	-3.2
30TH	378.12	6.7	26.6	1127	1943	5.9	13.7	-10	-4	112.7	419.8	-39.1	10.3	-3.0
31ST	390.20	6.9	26.7	1127	1943	6.1	13.8	-10	-4	105.9	393.1	-34.2	9.0	-2.8
32ND	402.28	7.1	26.8	1127	1943	6.3	13.8	-10	-4	98.8	366.2	-29.6	7.8	-2.6
33RD	414.36	7.3	26.9	1127	1943	6.5	13.9	-10	-5	91.5	339.3	-25.3	6.6	-2.4
34TH	426.44	7.5	27.0	1127	1943	6.6	13.9	-10	-5	84.0	312.2	-21.4	5.6	-2.2
35TH	438.52	7.7	27.1	1127	1943	6.8	14.0	-10	-5	76.4	285.1	-17.8	4.6	-2.0
36TH	450.60	7.8	27.2	1127	1943	6.9	14.0	-11	-5	68.6	257.9	-14.5	3.7	-1.8
37TH	462.68	7.8	27.4	1127	1943	6.9	14.1	-11	-5	60.8	230.4	-11.5	2.9	-1.6
38TH	474.76	7.8	27.6	1127	1943	6.9	14.2	-11	-5	53.0	202.8	-8.9	2.2	-1.4
39TH	486.84	7.7	27.8	1127	1943	6.9	14.3	-11	-5	45.3	175.0	-6.6	1.7	-1.2
40TH	498.92	7.7	28.0	1127	1943	6.8	14.4	-11	-5	37.6	147.0	-4.7	1.2	-.9
41ST	511.00	7.7	28.2	1127	1943	6.8	14.5	-11	-5	29.9	118.8	-3.1	.7	-.7
42ND	523.08	8.0	29.6	1174	2023	6.8	14.6	-11	-5	21.9	89.2	-1.8	.4	-.5
43RD	535.66	8.1	30.3	1206	2078	6.7	14.6	-9	-4	13.9	58.9	-.8	.2	-.3
44TH	548.58	9.9	41.0	1680	2895	5.9	14.2	-4	-2	3.9	17.9	-.1	.0	-.2
MR	566.58	3.9	17.9	1085	2065	3.6	8.6	-11	-4	0.0	0.0	0.0	0.0	0.0
TOP	581.67													

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 180 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									189.8	579.7	-229.2	69.3	-6.3
2ND	23.00	2.4	1.6	2147	3699	1.1	.4	-77	-200	187.4	578.1	-215.9	65.0	-6.4
3RD	35.92	1.4	.3	1206	2079	1.2	.1	-4	-34	186.0	577.8	-208.4	62.6	-6.4
4TH	48.84	1.5	.6	1206	2078	1.3	.3	1	4	184.4	577.2	-201.0	60.2	-6.4
5TH	61.76	1.8	.9	1206	2078	1.5	.4	7	24	182.7	576.3	-193.5	57.8	-6.4
6TH	74.68	1.9	.9	1206	2078	1.6	.5	10	34	180.7	575.4	-186.1	55.4	-6.4
7TH	87.60	2.1	1.0	1206	2078	1.7	.5	12	42	178.7	574.4	-178.7	53.1	-6.4
8TH	100.52	2.2	1.1	1206	2078	1.8	.5	14	50	176.4	573.3	-171.3	50.8	-6.3
9TH	113.44	2.4	1.2	1206	2078	2.0	.6	16	56	174.1	572.1	-163.9	48.6	-6.3
10TH	126.27	2.5	1.2	1197	2063	2.1	.6	18	62	171.5	570.9	-156.5	46.3	-6.2
11TH	139.10	2.6	1.5	1197	2063	2.2	.7	26	77	168.9	569.4	-149.2	44.2	-6.2
12TH	151.93	2.6	2.5	1197	2063	2.2	1.2	510	903	166.3	566.9	-141.9	42.0	-6.1
13TH	164.76	2.6	3.6	1197	2063	2.2	1.7	-79	-99	163.7	563.3	-134.7	39.9	-6.0
14TH	177.59	2.6	4.6	1197	2063	2.2	2.2	-49	-48	161.1	558.7	-127.5	37.8	-5.8
15TH	190.42	2.6	5.6	1197	2063	2.2	2.7	-40	-31	158.5	553.1	-120.3	35.8	-5.7
16TH	203.25	2.6	6.7	1197	2063	2.2	3.2	-36	-24	155.9	546.4	-113.3	33.7	-5.5
17TH	216.08	2.8	7.7	1197	2063	2.3	3.7	-31	-19	153.1	538.7	-106.3	31.6	-5.4
18TH	228.66	2.8	8.8	1174	2023	2.4	4.4	-27	-15	150.3	529.9	-99.6	29.9	-5.2
19TH	241.24	3.0	10.1	1174	2023	2.5	5.0	-24	-12	147.3	519.8	-93.0	28.0	-5.0
20TH	253.82	3.1	11.4	1174	2023	2.6	5.6	-21	-10	144.2	508.4	-86.5	26.1	-4.8
21ST	266.40	3.2	12.7	1174	2023	2.7	6.3	-20	-8	141.0	495.8	-80.2	24.4	-4.7
22ND	278.98	3.3	13.9	1174	2023	2.8	6.9	-18	-7	137.7	481.8	-74.1	22.6	-4.5
23RD	291.56	3.4	15.2	1174	2023	2.9	7.5	-17	-6	134.3	466.6	-68.1	20.9	-4.3
24TH	304.14	3.6	16.3	1174	2023	3.1	8.1	-16	-6	130.7	450.2	-62.3	19.2	-4.1
25TH	316.72	3.9	17.2	1174	2023	3.3	8.5	-16	-6	126.8	433.0	-56.8	17.6	-3.9
		4.1	17.8	1151	1983	3.6	9.0	-16	-6					

TABLE 7 SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 180 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									122.7	415.3	-51.5	16.1	-3.6
		4.4	18.6	1151	1983	3.8	9.4	-16	-6					
27TH	341.38									118.4	396.6	-46.5	14.6	-3.4
		4.6	19.5	1151	1983	4.0	9.8	-16	-7					
28TH	353.71									113.7	377.2	-41.8	13.1	-3.2
		4.9	20.3	1151	1983	4.3	10.3	-16	-7					
29TH	366.04									108.9	356.8	-37.2	11.8	-2.9
		5.1	20.8	1127	1943	4.6	10.7	-14	-6					
30TH	378.12									103.7	336.0	-33.1	10.5	-2.7
		5.4	21.0	1127	1943	4.8	10.8	-13	-6					
31ST	390.20									98.3	315.1	-29.1	9.3	-2.5
		5.6	20.9	1127	1943	4.9	10.8	-12	-6					
32ND	402.28									92.7	294.2	-25.4	8.1	-2.3
		5.8	20.8	1127	1943	5.1	10.7	-12	-5					
33RD	414.36									87.0	273.4	-22.0	7.0	-2.1
		5.9	20.7	1127	1943	5.3	10.7	-11	-5					
34TH	426.44									81.0	252.6	-18.8	6.0	-2.0
		6.1	20.6	1127	1943	5.4	10.6	-11	-5					
35TH	438.52									74.9	232.0	-15.9	5.1	-1.8
		6.3	20.5	1127	1943	5.6	10.6	-10	-5					
36TH	450.60									68.6	211.5	-13.2	4.2	-1.7
		6.5	20.4	1127	1943	5.8	10.5	-9	-5					
37TH	462.68									62.1	191.0	-10.8	3.4	-1.5
		6.6	20.5	1127	1943	5.8	10.5	-10	-6					
38TH	474.76									55.5	170.6	-8.6	2.7	-1.4
		6.7	20.5	1127	1943	5.9	10.5	-11	-6					
39TH	486.84									48.8	150.1	-6.7	2.1	-1.2
		6.8	20.5	1127	1943	6.0	10.5	-12	-7					
40TH	498.92									42.0	129.6	-5.0	1.5	-1.0
		6.9	20.5	1127	1943	6.1	10.5	-13	-7					
41ST	511.00									35.1	109.2	-3.6	1.1	-.9
		7.0	20.5	1127	1943	6.2	10.5	-14	-8					
42ND	523.08									28 1	88.7	-2.4	.7	-.7
		7.5	21.3	1174	2023	6.4	10.5	-13	-8					
43RD	535.66									20.6	67.4	-1.4	.4	-.5
		7.8	22.0	1206	2078	6.5	10.6	-10	-6					
44TH	548.58									12.8	45.4	-.6	.2	-.3
		10.4	31.1	1680	2895	6.2	10.7	-7	-4					
MR	566.58									2.4	14.3	-.1	.0	-.2
		2.4	14.3	1085	2065	2.2	6.9	-14	-4					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 190 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									283.4	486.0	-206.0	108.3	-8.5
2ND	23.00	2.7	.6	2147	3699	1.3	.2	-14	-103	280.7	485.4	-194.8	101.8	-8.6
3RD	35.92	1.1	-.0	1206	2078	.9	-.0	0	-82	279.6	485.4	-188.6	98.2	-8.6
4TH	48.84	1.3	-.4	1206	2078	1.1	-.2	6	-33	278.3	485.8	-182.3	94.6	-8.6
5TH	61.76	1.6	-.6	1206	2078	1.4	-.3	1	-3	276.6	486.3	-176.0	91.0	-8.6
6TH	74.68	1.9	-.5	1206	2078	1.6	-.2	-2	10	274.8	486.8	-169.7	87.5	-8.6
7TH	87.60	2.1	-.4	1206	2078	1.8	-.2	-2	20	272.7	487.1	-163.4	83.9	-8.6
8TH	100.52	2.3	-.3	1206	2078	1.9	-.1	-2	28	270.3	487.4	-157.1	80.4	-8.6
9TH	113.44	2.6	-.1	1206	2078	2.1	-.1	-1	34	267.7	487.5	-150.8	76.9	-8.5
10TH	126.27	2.8	-.0	1197	2063	2.3	-.0	-0	39	264.9	487.6	-144.6	73.5	-8.5
11TH	139.10	3.0	.2	1197	2063	2.5	.1	2	44	261.9	487.4	-138.3	70.1	-8.4
12TH	151.93	3.2	.9	1197	2063	2.6	.4	9	56	258.7	486.5	-132.1	66.8	-8.4
13TH	164.76	3.3	1.5	1197	2063	2.8	.7	20	76	255.4	485.0	-125.9	63.5	-8.3
14TH	177.59	3.5	2.2	1197	2063	2.9	1.1	41	110	251.9	482.8	-119.7	60.3	-8.2
15TH	190.42	3.6	2.9	1197	2063	3.0	1.4	69	191	248.3	480.0	-113.5	57.0	-8.0
16TH	203.25	3.8	3.5	1197	2063	3.2	1.7	329	601	244.5	476.5	-107.3	53.9	-7.9
17TH	216.08	4.4	4.2	1197	2063	3.7	2.0	495	881	240.2	472.3	-101.3	50.8	-7.7
18TH	228.66	4.6	5.1	1174	2023	3.9	2.5	-211	-321	235.6	467.2	-95.3	47.8	-7.6
19TH	241.24	4.7	6.1	1174	2023	4.0	3.0	-94	-124	230.9	461.1	-89.5	44.9	-7.4
20TH	253.82	4.9	7.2	1174	2023	4.2	3.5	-66	-77	225.9	453.9	-83.7	42.0	-7.2
21ST	266.40	5.1	8.2	1174	2023	4.3	4.0	-54	-57	220.8	445.7	-78.1	39.2	-7.0
22ND	278.98	5.3	9.2	1174	2023	4.5	4.6	-47	-46	215.6	436.5	-72.5	36.4	-6.7
23RD	291.56	5.5	10.3	1174	2023	4.7	5.1	-42	-38	210.1	426.2	-67.1	33.7	-6.5
24TH	304.14	5.7	11.3	1174	2023	4.8	5.6	-39	-33	204.4	415.0	-61.8	31.1	-6.2
25TH	316.72	5.9	12.3	1174	2023	5.0	6.1	-36	-29	198.5	402.6	-56.7	28.6	-6.0
		6.0	13.1	1151	1983	5.2	6.6	-34	-26					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 190 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									192.5	389.5	-51.8	26.2	-5.7
		6.2	14.2	1151	1983	5.4	7.1	-32	-24					
27TH	341.38									186.3	375.3	-47.1	23.9	-5.4
		6.5	15.2	1151	1983	5.6	7.7	-30	-22					
28TH	353.71									179.8	360.1	-42.5	21.6	-5.1
		6.7	16.2	1151	1983	5.8	8.2	-29	-20					
29TH	366.04									173.2	343.9	-38.2	19.4	-4.8
		7.3	16.9	1127	1943	6.4	8.7	-26	-19					
30TH	378.12									165.9	327.0	-34.2	17.4	-4.5
		7.8	17.4	1127	1943	6.9	9.0	-24	-18					
31ST	390.20									158.1	309.6	-30.3	15.4	-4.2
		8.1	17.7	1127	1943	7.2	9.1	-24	-19					
32ND	402.28									150.0	291.9	-26.7	13.6	-3.9
		8.5	17.9	1127	1943	7.6	9.2	-24	-19					
33RD	414.36									141.5	274.0	-23.3	11.8	-3.7
		8.9	18.2	1127	1943	7.9	9.3	-24	-20					
34TH	426.44									132.6	255.8	-20.1	10.1	-3.4
		9.3	18.4	1127	1943	8.2	9.5	-24	-20					
35TH	438.52									123.3	237.4	-17.1	8.6	-3.2
		9.6	18.7	1127	1943	8.5	9.6	-23	-21					
36TH	450.60									113.7	218.7	-14.3	7.2	-2.9
		10.1	18.9	1127	1943	8.9	9.7	-24	-22					
37TH	462.68									103.6	199.8	-11.8	5.9	-2.6
		10.4	19.3	1127	1943	9.2	9.9	-25	-23					
38TH	474.76									93.2	180.5	-9.5	4.7	-2.4
		10.6	19.8	1127	1943	9.4	10.2	-26	-24					
39TH	486.84									82.6	160.8	-7.4	3.6	-2.1
		10.9	20.2	1127	1943	9.7	10.4	-27	-25					
40TH	498.92									71.7	140.6	-5.6	2.7	-1.8
		11.2	20.7	1127	1943	9.9	10.6	-28	-26					
41ST	511.00									60.5	119.9	-4.0	1.9	-1.4
		11.5	21.1	1127	1943	10.2	10.9	-29	-27					
42ND	523.08									49.0	98.8	-2.7	1.2	-1.1
		12.5	22.5	1174	2023	10.6	11.1	-28	-26					
43RD	535.66									36.5	76.3	-1.6	.7	-.7
		13.5	23.6	1206	2078	11.2	11.3	-21	-21					
44TH	548.58									23.0	52.7	-.8	.3	-.5
		18.1	33.7	1680	2895	10.8	11.6	-13	-12					
MR	566.58									4.9	19.1	-.1	.0	-.2
		4.9	19.1	1085	2065	4.5	9.2	-16	-7					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 200 CONFIGURATION A REFERENCE PRESSURE 34 0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									345.6	300.3	-134.1	132.7	-7.3
2ND	23.00	1.5	-3.9	2147	3699	.7	-1.0	-47	31	344.1	304.2	-127.1	124.8	-7.4
3RD	35.92	-.1	-2.3	1206	2078	-.1	-1.1	-28	-2	344.1	306.4	-123.2	120.4	-7.5
4TH	48.84	.4	-2.4	1206	2078	.4	-1.2	-20	6	343.7	308.9	-119.2	115.9	-7.5
5TH	61.76	1.0	-2.5	1206	2078	.9	-1.2	-15	10	342.7	311.3	-115.2	111.5	-7.5
6TH	74.68	1.4	-2.3	1206	2078	1.2	-1.1	-9	9	341.2	313.6	-111.2	107.1	-7.5
7TH	87.60	1.8	-2.1	1206	2078	1.5	-1.0	5	-8	339.5	315.9	-107.1	102.7	-7.5
8TH	100.52	2.2	-2.0	1206	2078	1.8	-1.0	-58	107	337.3	317.7	-103.0	98.3	-7.5
9TH	113.44	2.5	-1.8	1206	2078	2.1	-.9	-22	52	334.8	319.6	-98.9	94.0	-7.5
10TH	126.27	2.9	-1.7	1197	2063	2.4	-.8	-16	47	331.9	321.2	-94.8	89.7	-7.4
11TH	139.10	3.2	-1.4	1197	2063	2.7	-.7	-11	44	328.7	322.6	-90.6	85.4	-7.4
12TH	151.93	3.6	-.7	1197	2063	3.0	-.3	-4	42	325.0	323.3	-86.5	81.2	-7.3
13TH	164.76	4.0	.1	1197	2063	3.4	.0	0	44	321.0	323.2	-82.4	77.1	-7.2
14TH	177.59	4.4	.8	1197	2063	3.7	.4	5	48	316.6	322.4	-78.2	73.0	-7.1
15TH	190.42	4.8	1.5	1197	2063	4.0	.7	10	55	311.8	320.9	-74.1	69.0	-7.0
16TH	203.25	5.2	2.3	1197	2063	4.3	1.1	16	63	306.7	318.6	-70.0	65.0	-6.9
17TH	216.08	6.4	3.0	1197	2063	5.4	1.4	16	58	300.2	315.7	-65.9	61.1	-6.8
18TH	228.66	6.7	3.7	1174	2023	5.7	1.8	22	68	293.5	311.9	-62.0	57.4	-6.6
19TH	241.24	7.0	4.5	1174	2023	5.9	2.2	34	89	286.5	307.4	-58.1	53.7	-6.4
20TH	253.82	7.2	5.3	1174	2023	6.2	2.6	52	121	279.3	302.1	-54.2	50.2	-6.3
21ST	266.40	7.5	6.1	1174	2023	6.4	3.0	87	179	271.8	295.9	-50.5	46.7	-6.1
22ND	278.98	7.7	6.9	1174	2023	6.6	3.4	172	325	264.1	289.0	-46.8	43.3	-5.8
23RD	291.56	8.0	7.8	1174	2023	6.8	3.8	746	1302	256.2	281.2	-43.2	40.1	-5.6
24TH	304.14	8.1	8.4	1174	2023	6.9	4.2	-501	-821	248.0	272.8	-39.7	36.9	-5.3
25TH	316.72	8.2	9.0	1174	2023	7.0	4.4	-207	-320	239.9	263.8	-36.3	33.8	-5.1
		8.1	9.4	1151	1983	7.0	4.7	-136	-200					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 200 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									231.8	254.4	-33.2	30.9	-4.8
		8.1	9.9	1151	1983	7.1	5.0	-105	-146					
27TH	341.38									223.7	244.5	-30.1	28.1	-4.5
		8.2	10.4	1151	1983	7.1	5.3	-86	-115					
28TH	353.71									215.5	234.1	-27.1	25.4	-4.3
		8.2	11.0	1151	1983	7.1	5.5	-75	-95					
29TH	366.04									207.3	223.1	-24.3	22.8	-4.0
		9.0	11.3	1127	1943	8.0	5.8	-79	-107					
30TH	378.12									198.3	211.8	-21.7	20.4	-3.7
		9.7	11.6	1127	1943	8.6	6.0	-88	-125					
31ST	390.20									188.6	200.2	-19.2	18.0	-3.5
		10.1	11.8	1127	1943	9.0	6.1	-96	-140					
32ND	402.28									178.5	188.4	-16.8	15.8	-3.2
		10.6	12.1	1127	1943	9.4	6.2	-106	-159					
33RD	414.36									167.9	176.4	-14.6	13.7	-3.0
		11.1	12.3	1127	1943	9.8	6.3	-121	-185					
34TH	426.44									156.9	164.1	-12.6	11.7	-2.8
		11.5	12.5	1127	1943	10.2	6.4	-142	-222					
35TH	438.52									145.3	151.6	-10.7	9.9	-2.5
		12.0	12.8	1127	1943	10.6	6.6	-176	-281					
36TH	450.60									133.4	138.8	-8.9	8.2	-2.3
		12.6	13.0	1127	1943	11.2	6.7	-347	-574					
37TH	462.68									120.8	125.8	-7.3	6.7	-2.1
		12.7	12.9	1127	1943	11.3	6.7	-667	-1117					
38TH	474.76									108.0	112.9	-5.9	5.3	-1.9
		12.8	13.0	1127	1943	11.4	6.7	$$$$	-1853					
39TH	486.84									95.2	99.9	-4.6	4.1	-1.7
		12.9	13.0	1127	1943	11.4	6.7	$$$$	-4737					
40TH	498.92									82.3	87.0	-3.5	3.0	-1.4
		13.0	13.0	1127	1943	11.5	6.7	629	2107					
41ST	511.00									69.3	74.0	-2.5	2.1	-1.2
		13.1	13.0	1127	1943	11.6	6.7	1551	2662					
42ND	523.08									56.3	61.0	-1.7	1.3	-.9
		14.4	13.5	1174	2023	12.3	6.7	169	306					
43RD	535.66									41.9	47.5	-1.0	.7	-.7
		16.2	14.3	1206	2078	13.5	6.9	59	114					
44TH	548.58									25.6	33.2	-.5	.3	-.5
		22.2	22.5	1680	2895	13.2	7.8	-629	-1057					
MR	566.58									3.5	10.7	-.1	.0	-.2
		3.5	10.7	1085	2065	3.2	5.2	-26	-14					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 210 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									346.9	-174.2	55.7	128.5	-.3
2ND	23.00	4.1	-2.0	2147	3699	1.9	-.5	-6	21	342.9	-172.2	51.8	120.5	-.3
3RD	35.92	.5	-1.9	1206	2078	.4	-.9	9	-4	342.4	-170.3	49.5	116.1	-.3
4TH	48.84	1.2	-2.1	1206	2078	1.0	-1.0	11	-11	341.2	-168.2	47.4	111.7	-.3
5TH	61.76	1.9	-2.3	1206	2078	1.6	-1.1	36	-53	339.3	-165.9	45.2	107.3	-.3
6TH	74.68	2.3	-2.4	1206	2078	1.9	-1.2	181	-301	336.9	-163.5	43.1	102.9	-.2
7TH	87.60	2.7	-2.5	1206	2078	2.3	-1.2	-38	70	334.2	-161.0	41.0	98.6	-.2
8TH	100.52	3.1	-2.7	1206	2078	2.6	-1.3	-14	28	331.0	-158.3	38.9	94.3	-.2
9TH	113.44	3.5	-2.8	1206	2078	2.9	-1.4	-7	16	327.5	-155.5	36.9	90.0	-.2
10TH	126.27	3.9	-3.0	1197	2063	3.3	-1.4	-4	10	323.6	-152.5	34.9	85.9	-.2
11TH	139.10	4.3	-3.1	1197	2063	3.6	-1.5	-3	6	319.3	-149.4	33.0	81.7	-.2
12TH	151.93	4.5	-3.2	1197	2063	3.7	-1.5	-3	8	314.8	-146.2	31.1	77.7	-.2
13TH	164.76	4.7	-3.3	1197	2063	3.9	-1.6	-4	10	310.1	-142.9	29.2	73.7	-.2
14TH	177.59	4.9	-3.4	1197	2063	4.1	-1.7	-5	12	305.2	-139.5	27.4	69.7	-.2
15TH	190.42	5.1	-3.5	1197	2063	4.3	-1.7	-5	13	300.1	-136.0	25.6	65.8	-.1
16TH	203.25	5.4	-3.6	1197	2063	4.5	-1.8	-6	14	294.7	-132.4	23.9	62.0	-.1
17TH	216.08	6.5	-3.7	1197	2063	5.5	-1.8	-3	9	288.2	-128.7	22.2	58.3	-.1
18TH	228.66	6.8	-3.8	1174	2023	5.8	-1.9	-2	6	281.3	-124.8	20.7	54.7	-.1
19TH	241.24	7.1	-4.0	1174	2023	6.0	-2.0	-1	3	274.3	-120.8	19.1	51.2	-.1
20TH	253.82	7.3	-4.2	1174	2023	6.3	-2.1	0	-0	266.9	-116.6	17.6	47.8	-.1
21ST	266.40	7.6	-4.4	1174	2023	6.5	-2.2	1	-3	259.3	-112.2	16.2	44.5	-.1
22ND	278.98	7.9	-4.6	1174	2023	6.7	-2.3	2	-6	251.4	-107.6	14.8	41.3	-.1
23RD	291.56	8.1	-4.8	1174	2023	6.9	-2.4	3	-8	243.3	-102.8	13.5	38.2	-.1
24TH	304.14	8.2	-5.0	1174	2023	7.0	-2.5	3	-9	235.1	-97.8	12.2	35.1	-.1
25TH	316.72	8.2	-5.0	1174	2023	7.0	-2.5	2	-7	226.9	-92.8	11.0	32.2	-.2
		7.9	-5.0	1151	1983	6.9	-2.5	2	-5					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 210 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									218.9	-87.8	9.9	29.5	-.2
27TH	341.38	7.9	-5.0	1151	1983	6.8	-2.5	1	-2	211.1	-82.9	8.8	26.8	-.2
28TH	353.71	7.8	-5.0	1151	1983	6.8	-2.5	-0	0	203.3	-77.8	7.9	24.3	-.2
29TH	366.04	7.7	-5.1	1151	1983	6.7	-2.6	-1	3	195.5	-72.7	6.9	21.8	-.2
30TH	378.12	8.6	-5.0	1127	1943	7.6	-2.6	0	-1	186.9	-67.7	6.1	19.5	-.2
31ST	390.20	9.2	-5.0	1127	1943	8.2	-2.6	1	-2	177.7	-62.7	5.3	17.3	-.2
32ND	402.28	9.6	-4.9	1127	1943	8.5	-2.5	1	-2	168.1	-57.8	4.6	15.2	-.2
33RD	414.36	9.9	-4.8	1127	1943	8.8	-2.5	1	-2	158.2	-53.0	3.9	13.3	-.2
34TH	426.44	10.2	-4.7	1127	1943	9.1	-2.4	0	-2	148.0	-48.3	3.3	11.4	-.2
35TH	438.52	10.5	-4.6	1127	1943	9.4	-2.3	0	-2	137.5	-43.7	2.7	9.7	-.2
36TH	450.60	10.9	-4.4	1127	1943	9.6	-2.3	0	-2	126.6	-39.3	2.2	8.1	-.2
37TH	462.68	11.3	-4.3	1127	1943	10.0	-2.2	-0	0	115.3	-34.9	1.8	6.6	-.2
38TH	474.76	11.5	-4.3	1127	1943	10.2	-2.2	-0	2	103.8	-30.6	1.4	5.3	-.2
39TH	486.84	11.6	-4.3	1127	1943	10.3	-2.2	-0	2	92.2	-26.3	1.0	4.1	-.2
40TH	498.92	11.7	-4.3	1127	1943	10.4	-2.2	-0	2	80.4	-22.0	.7	3.1	-.2
41ST	511.00	11.8	-4.3	1127	1943	10.5	-2.2	-1	3	68.6	-17.8	.5	2.2	-.2
42ND	523.08	12.0	-4.2	1127	1943	10.6	-2.2	-1	3	56.7	-13.5	.3	1.4	-.2
43RD	535.66	13.4	-4.4	1174	2023	11.4	-2.2	-0	1	43.3	-9.2	.2	.8	-.2
44TH	548.58	15.7	-4.1	1206	2078	13.0	-2.0	-0	1	27.6	-5.1	.1	.3	-.2
MR	566.58	22.7	-2.9	1680	2895	13.5	-1.0	-1	8	5.0	-2.2	.0	.0	-.1
TOP	581.67	5.0	-2.2	1085	2065	4.6	-1.1	-9	36	0.0	0.0	0.0	0.0	0.0

TABLE 7 SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 220 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									206.9	-445.5	153.3	85.0	4.2
2ND	23.00	-1.9	-5.6	2147	3699	-.9	-1.5	9	5	208.8	-439.9	143.1	80 2	4.2
3RD	35.92	-1.9	-4.2	1206	2078	-1.5	-2.0	5	4	210.6	-435.7	137 5	77.5	4.2
4TH	48.84	-1.6	-4.6	1206	2078	-1.3	-2.2	6	3	212.2	-431.1	131.9	74.7	4.2
5TH	61.76	-1.2	-5.0	1206	2078	-1.0	-2.4	5	2	213.4	-426.0	126.3	72.0	4.3
6TH	74.68	-.8	-5.3	1206	2078	-.7	-2.6	2	1	214.3	-420.7	120.9	69.2	4.3
7TH	87 60	-.5	-5.7	1206	2078	-.4	-2.7	-0	-0	214.7	-415.0	115.5	66.5	4.3
8TH	100.52	-.1	-6.0	1206	2078	-.1	-2.9	-2	-0	214.8	-409.1	110.1	63.7	4.3
9TH	113.44	.3	-6.3	1206	2078	.2	-3.0	-4	0	214.6	-402.8	104.9	60.9	4.2
10TH	126.27	.6	-6.5	1197	2063	.5	-3.2	-6	1	214.0	-396.3	99.8	58.2	4.2
11TH	139.10	1.0	-6.8	1197	2063	.8	-3.3	-8	2	213.0	-389.5	94.7	55.4	4.2
12TH	151.93	1.4	-7.1	1197	2063	1.2	-3.4	-9	3	211.5	-382.5	89.8	52.7	4.1
13TH	164.76	1.9	-7.4	1197	2063	1.6	-3.6	-11	5	209.6	-375.1	84.9	50.0	4.1
14TH	177.59	2.3	-7.6	1197	2063	1.9	-3.7	-12	6	207.3	-367 5	80.1	47.3	4.0
15TH	190.42	2.8	-7.9	1197	2063	2.3	-3.8	-14	8	204.5	-359.6	75.5	44.7	3.9
16TH	203.25	3.2	-8.2	1197	2063	2.7	-4.0	-16	10	201.3	-351.3	70.9	42.1	3.8
17TH	216.08	4.4	-8.5	1197	2063	3.7	-4.1	-19	17	196.9	-342.8	66.5	39.5	3.7
18TH	228.66	4.7	-8.6	1174	2023	4.0	-4.3	-21	20	192.2	-334.2	62.2	37.1	3.6
19TH	241.24	4.9	-8.9	1174	2023	4.2	-4.4	-23	21	187.3	-325.2	58.1	34.7	3.5
20TH	253.82	5.2	-9.3	1174	2023	4.4	-4.6	-24	23	182.1	-316.0	54.0	32.4	3.4
21ST	266.40	5.4	-9.6	1174	2023	4.6	-4.7	-25	24	176.6	-306.4	50.1	30.1	3.3
22ND	278.98	5.7	-9.9	1174	2023	4.8	-4.9	-26	26	171.0	-296.6	46.3	27.9	3.1
23RD	291.56	5.9	-10.2	1174	2023	5.0	-5.0	-28	27	165.1	-286.4	42.7	25.8	3.0
24TH	304.14	6.0	-10.5	1174	2023	5.1	-5.2	-27	27	159.1	-275.9	39.1	23.8	2.8
25TH	316.72	5.9	-10.8	1174	2023	5.0	-5.3	-26	24	153.2	-265.1	35.7	21.8	2.7
		5.7	-10.8	1151	1983	4.9	-5.4	-24	22					

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 220 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									147.5	-254.3	32.5	20.0	2.5
27TH	341.38	5.5	-11.0	1151	1983	4.8	-5.6	-23	20	142.0	-243.3	29.4	18.2	2.4
28TH	353.71	5.4	-11.3	1151	1983	4.7	-5.7	-22	18	136.5	-232.0	26.5	16.5	2.2
29TH	366.04	5.3	-11.6	1151	1983	4.6	-5.8	-21	17	131.2	-220.4	23.7	14.8	2.1
30TH	378.12	5.9	-11.6	1127	1943	5.2	-6.0	-22	19	125.3	-208.9	21.1	13.3	1.9
31ST	390.20	6.3	-11.8	1127	1943	5.5	-6.1	-22	19	119.1	-197.1	18.7	11.8	1.8
32ND	402.28	6.4	-12.0	1127	1943	5.7	-6.2	-21	19	112.7	-185.1	16.4	10.4	1.6
33RD	414.36	6.6	-12.1	1127	1943	5.8	-6.2	-20	18	106.1	-173.0	14.2	9.1	1.5
34TH	426.44	6.7	-12.3	1127	1943	6.0	-6.3	-19	18	99.3	-160.7	12.2	7.8	1.4
35TH	438.52	6.9	-12.5	1127	1943	6.1	-6.4	-18	17	92.4	-148.3	10.3	6.7	1.2
36TH	450.60	7.1	-12.6	1127	1943	6.3	-6.5	-17	17	85.3	-135.6	8.6	5.6	1.1
37TH	462.68	7.3	-12.8	1127	1943	6.5	-6.6	-16	16	78.1	-122.8	7.0	4.6	1.0
38TH	474.76	7.5	-12.9	1127	1943	6.6	-6.6	-16	16	70.6	-109.9	5.6	3.7	.9
39TH	486.84	7.6	-12.9	1127	1943	6.7	-6.6	-17	17	63.0	-97.0	4.4	2.9	.8
40TH	498.92	7.7	-12.9	1127	1943	6.9	-6.7	-18	18	55.3	-84.1	3.3	2.2	.7
41ST	511.00	7.9	-13.0	1127	1943	7.0	-6.7	-18	19	47.4	-71.1	2.4	1.6	.5
42ND	523.08	8.0	-13.0	1127	1943	7.1	-6.7	-19	20	39.4	-58.1	1.6	1.0	.4
43RD	535.66	8.9	-13.6	1174	2023	7.6	-6.7	-19	21	30.5	-44.5	.9	.6	.3
44TH	548.58	10.2	-14.1	1206	2078	8.4	-6.8	-18	22	20.3	-30.5	.4	.3	.2
MR	566.58	15.3	-20.0	1680	2895	9.1	-6.9	-16	21	5.0	-10.5	.1	.0	.1
TOP	581.67	5.0	-10.5	1985	2065	4.6	-5.1	-14	12	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 230 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 90 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									194.2	-836.2	295.9	88.2	6.0
2ND	23.00	-1.9	-13.9	2147	3699	-.9	-3.8	26	6	196.1	-822.3	276.8	83.7	6.3
3RD	35.92	-1.9	-8.9	1206	2078	-1.5	-4.3	20	7	197.9	-813.4	266.2	81.1	6.4
4TH	48.84	-1.4	-8.9	1206	2078	-1.2	-4.3	17	5	199.4	-804.6	255.8	78.6	6.5
5TH	61.76	-.9	-9.0	1206	2078	-.8	-4.3	17	3	200.3	-795.5	245.4	76.0	6.7
6TH	74.68	-.8	-9.4	1206	2078	-.6	-4.5	15	2	201.0	-786.2	235.2	73.4	6.8
7TH	87.60	-.6	-9.7	1206	2078	-.5	-4.7	13	1	201.6	-776.5	225.1	70.8	6.9
8TH	100.52	-.4	-10.0	1206	2078	-.3	-4.8	12	1	202.0	-766.5	215.2	68.2	7.0
9TH	113.44	-.2	-10.4	1206	2078	-.2	-5.0	10	0	202.2	-756.1	205.3	65.6	7.0
10TH	126.27	-.0	-10.6	1197	2063	-.0	-5.1	8	0	202.3	-745.5	195.7	63.0	7.1
11TH	139.10	.1	-10.9	1197	2063	.1	-5.3	7	-0	202.1	-734.5	186.2	60.4	7.2
12TH	151.93	.3	-11.5	1197	2063	.2	-5.6	4	-0	201.8	-723.1	176.9	57.8	7.2
13TH	164.76	.4	-12.0	1197	2063	.3	-5.8	1	-0	201.4	-711.1	167.7	55.2	7.2
14TH	177.59	.5	-12.5	1197	2063	.4	-6.0	-2	0	200.9	-698.7	158.6	52.6	7.2
15TH	190.42	.7	-13.0	1197	2063	.6	-6.3	-4	0	200.2	-685.7	149.7	50.1	7.2
16TH	203.25	.8	-13.5	1197	2063	.7	-6.5	-6	1	199.4	-672.2	141.0	47.5	7.1
17TH	216.08	1.2	-14.0	1197	2063	1.0	-6.8	-7	1	198.2	-658.2	132.5	44.9	7.0
18TH	228.66	1.7	-14.3	1174	2023	1.4	-7.1	-8	2	196.5	-643.9	124.3	42.5	6.9
19TH	241.24	2.1	-14.9	1174	2023	1.8	-7.3	-9	2	194.5	-629.1	116.3	40.0	6.8
20TH	253.82	2.5	-15.4	1174	2023	2.2	-7.6	-11	3	191.9	-613.7	108.5	37.6	6.7
21ST	266.40	3.0	-16.0	1174	2023	2.5	-7.9	-12	4	188.9	-597.6	100.8	35.2	6.6
22ND	278.98	3.4	-16.6	1174	2023	2.9	-8.2	-13	5	185.5	-581.0	93.4	32.8	6.4
23RD	291.56	3.9	-17.2	1174	2023	3.3	-8.5	-14	5	181.7	-563.9	86.2	30.5	6.2
24TH	304.14	4.2	-17.8	1174	2023	3.6	-8.8	-15	6	177.5	-546.0	79.2	28.3	6.0
25TH	316.72	4.4	-18.7	1174	2023	3.7	-9.2	-16	6	173.1	-527.3	72.5	26.1	5.8
		4.5	-19.2	1151	1983	3.9	-9.7	-16	6					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 230 CONFIGURATION A REFERENCE PRESSURE 34 0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									168.7	-508.2	66.1	23.9	5.6
27TH	341.38	4.6	-20.9	1151	1983	4.0	-10.1	-16	6	164.0	-488.2	60.0	21.9	5.3
28TH	353.71	4.8	-20.8	1151	1983	4.2	-10.5	-17	6	159.2	-467.4	54.1	19.9	5.1
29TH	366.04	5.0	-21.6	1151	1983	4.3	-10.9	-17	7	154.3	-445.7	48.5	18.0	4.8
30TH	378.12	5.3	-22.0	1127	1943	4.7	-11.3	-16	6	149.0	-423.7	43.2	16.1	4.5
31ST	390.20	5.8	-22.7	1127	1943	5.2	-11.7	-15	7	143.2	-401.0	38.2	14.4	4.2
32ND	402.28	6.3	-23.3	1127	1943	5.6	-12.0	-16	7	136.8	-377.7	33.5	12.7	4.0
33RD	414.36	6.9	-24.0	1127	1943	6.1	-12.3	-16	8	130.0	-353.7	29.1	11.1	3.7
34TH	426.44	7.4	-24.6	1127	1943	6.6	-12.6	-16	8	122.5	-329.1	25.0	9.5	3.4
35TH	438.52	7.9	-25.2	1127	1943	7.1	-13.0	-17	9	114.6	-303.9	21.1	8.1	3.1
36TH	450.60	8.5	-25.8	1127	1943	7.5	-13.3	-17	10	106.1	-278.1	17.6	6.8	2.8
37TH	462.68	9.1	-26.4	1127	1943	8.0	-13.6	-17	10	97.1	-251.7	14.4	5.6	2.5
38TH	474.76	9.4	-26.6	1127	1943	8.4	-13.7	-17	10	87.6	-225.2	11.6	4.4	2.1
39TH	486.84	9.8	-26.6	1127	1943	8.7	-13.7	-17	11	77.9	-198.6	9.0	3.4	1.8
40TH	498.92	10.1	-26.6	1127	1943	9.0	-13.7	-17	11	67.8	-172.0	6.8	2.6	1.5
41ST	511.00	10.4	-26.7	1127	1943	9.3	-13.7	-17	11	57.3	-145.3	4.8	1.8	1.2
42ND	523.08	10.8	-26.7	1127	1943	9.6	-13.7	-17	11	46.5	-118.6	3.2	1.2	.9
43RD	535.66	11.8	-27.8	1174	2023	10.1	-13.7	-15	11	34.7	-90.8	1.9	.7	.6
44TH	548.58	12.6	-28.5	1206	2078	10.5	-13.7	-11	8	22.1	-62.3	.9	.3	.4
MR	566.58	16.2	-39.5	1680	2895	9.6	-13.6	-7	5	5.9	-22.8	.2	.0	.3
TOP	581.67	5.9	-22.8	1085	2065	5.5	-11.0	-15	7	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 240 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									131.2	-1509.5	516.7	83.1	4.5
2ND	23.00	-5.6	-30.5	2147	3699	-2.6	-8.3	17	5	136.7	-1478.9	482.4	80.0	4.9
3RD	35.92	-4.3	-18.2	1206	2078	-3.6	-8.8	15	6	141.1	-1460.7	463.4	78.2	5.1
4TH	48.84	-4.3	-17.4	1206	2078	-3.5	-8.4	14	6	145.3	-1443.3	444.6	76.3	5.3
5TH	61.76	-4.0	-17.3	1206	2078	-3.3	-8.3	13	5	149.4	-1426.0	426.1	74.4	5.5
6TH	74.68	-3.8	-17.9	1206	2078	-3.2	-8.6	11	4	153.2	-1408.1	407.8	72.5	5.6
7TH	87.60	-3.6	-18.5	1206	2078	-3.0	-8.9	10	3	156.8	-1389.6	389.7	70.5	5.8
8TH	100.52	-3.4	-19.1	1206	2078	-2.8	-9.2	8	3	160.3	-1370.5	371.9	68.4	5.9
9TH	113.44	-3.2	-19.7	1206	2078	-2.7	-9.5	7	2	163.5	-1350.8	354.3	66.3	6.0
10TH	126.27	-3.0	-20.2	1197	2063	-2.5	-9.8	6	2	166.5	-1330.6	337.1	64.2	6.1
11TH	139.10	-2.8	-20.9	1197	2063	-2.4	-10.1	5	1	169.3	-1309.7	320.2	62.1	6.2
12TH	151.93	-2.8	-22.0	1197	2063	-2.3	-10.7	3	1	172.1	-1287.7	303.5	59.9	6.2
13TH	164.76	-2.7	-23.1	1197	2063	-2.2	-11.2	1	0	174.8	-1264.6	287.1	57.6	6.2
14TH	177.59	-2.6	-24.3	1197	2063	-2.2	-11.8	-1	-0	177.4	-1240.3	271.1	55.4	6.2
15TH	190.42	-2.5	-25.4	1197	2063	-2.1	-12.3	-2	-0	179.9	-1214.9	255.3	53.1	6.2
16TH	203.25	-2.5	-26.6	1197	2063	-2.1	-12.9	-4	-1	182.4	-1188.3	239.9	50.8	6.1
17TH	216.08	-2.4	-27.7	1197	2063	-2.0	-13.4	-4	-1	184.8	-1160.6	224.8	48.4	6.0
18TH	228.66	-2.0	-28.4	1174	2023	-1.7	-14.0	-5	-1	186.8	-1132.2	210.4	46.1	5.9
19TH	241.24	-1.6	-29.7	1174	2023	-1.3	-14.7	-5	-0	188.3	-1102.4	196.3	43.7	5.8
20TH	253.82	-1.1	-31.0	1174	2023	-1.0	-15.3	-6	-0	189.5	-1071.4	182.7	41.3	5.6
21ST	266.40	-.7	-32.3	1174	2023	-.6	-16.0	-6	-0	190.2	-1039.1	169.4	38.9	5.4
22ND	278.98	-.3	-33.6	1174	2023	-.3	-16.6	-7	-0	190.5	-1005.5	156.5	36.6	5.3
23RD	291.56	.1	-34.9	1174	2023	.1	-17.3	-7	0	190.4	-970.6	144.1	34.2	5.0
24TH	304.14	.7	-36.2	1174	2023	.6	-17.9	-8	0	189.8	-934.4	132.1	31.8	4.8
25TH	316.72	1.5	-37.1	1174	2023	1.3	-18.3	-8	1	188.2	-897.3	120.6	29.4	4.6
		2.3	-37.2	1151	1983	2.0	-18.7	-8	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 240 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									186.0	-860.2	109.8	27.1	4.3
		3.1	-38.0	1151	1983	2.7	-19.2	-8	1					
27TH	341.38									182.9	-822.1	99.4	24.8	4.1
		3.8	-38.9	1151	1983	3.3	-19.6	-8	1					
28TH	353.71									179.1	-783.2	89.5	22.6	3.8
		4.6	-39.7	1151	1983	4.0	-20.0	-9	2					
29TH	366.04									174.4	-743.5	80.1	20.4	3.6
		5.1	-39.8	1127	1943	4.6	-20.5	-7	2					
30TH	378.12									169.3	-703.7	71.3	18.3	3.3
		5.9	-40.3	1127	1943	5.2	-20.8	-7	2					
31ST	390.20									163.4	-663.4	63.1	16.3	3.1
		6.7	-40.6	1127	1943	6.0	-20.9	-7	2					
32ND	402.28									156.6	-622.8	55.3	14.4	2.9
		7.6	-41.0	1127	1943	6.7	-21.1	-7	2					
33RD	414.36									149.0	-581.8	48.0	12.5	2.7
		8.4	-41.3	1127	1943	7.5	-21.3	-7	2					
34TH	426.44									140.6	-540.5	41.3	10.8	2.5
		9.3	-41.6	1127	1943	8.2	-21.4	-6	2					
35TH	438.52									131.3	-498.9	35.0	9.1	2.3
		10.1	-41.9	1127	1943	9.0	-21.6	-6	3					
36TH	450.60									121.2	-457.0	29.2	7.6	2.1
		10.9	-42.2	1127	1943	9.7	-21.7	-6	3					
37TH	462.68									110.3	-414.7	23.9	6.2	1.9
		11.2	-42.6	1127	1943	10.0	-21.9	-6	3					
38TH	474.76									99.0	-372.1	19.2	5.0	1.7
		11.5	-43.0	1127	1943	10.2	-22.1	-7	3					
39TH	486.84									87.5	-329.1	15.0	3.8	1.5
		11.8	-43.4	1127	1943	10.5	-22.3	-7	3					
40TH	498.92									75.7	-285.7	11.2	2.8	1.3
		12.1	-43.8	1127	1943	10.7	-22.5	-7	3					
41ST	511.00									63.6	-241.9	8.1	2.0	1.0
		12.4	-44.2	1127	1943	11.0	-22.7	-7	3					
42ND	523.08									51.2	-197.7	5.4	1.3	.8
		13.3	-46.4	1174	2023	11.3	-22.9	-7	3					
43RD	535.66									37.9	-151.3	3.2	.7	.6
		13.5	-47.7	1206	2078	11.2	-23.0	-4	2					
44TH	548.58									24.4	-103.6	1.6	.3	.4
		16.8	-65.3	1680	2895	10.0	-22.5	-1	1					
MR	566.58									7.5	-38.3	.3	.1	.4
		7.5	-38.3	1085	2065	6.9	-18.5	-12	4					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 250 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									486.5	-1779.0	576.8	197.7	-1.4
2ND	23.00	.7	-39.2	2147	3699	.3	-10.6	27	-1	485.8	-1739.7	536.3	186.6	-.6
3RD	35.92	-1.7	-23.8	1206	2078	-1.4	-11.5	20	2	487.4	-1715.9	514.0	180.3	-.2
4TH	48.84	-.8	-23.0	1206	2078	-.6	-11.0	17	1	488.2	-1692.9	492.0	174.0	.1
5TH	61.76	.6	-23.0	1206	2078	.5	-11.1	17	-1	487.6	-1669.9	470.3	167.7	.4
6TH	74.68	1.3	-24.2	1206	2078	1.0	-11.6	14	-1	486.4	-1645 8	448.8	161.4	.7
7TH	87.60	1.9	-25.4	1206	2078	1.6	-12.2	12	-2	484.5	-1620.4	427.7	155.1	.9
8TH	100.52	2.5	-26.6	1206	2078	2.1	-12.8	10	-2	481.9	-1593.7	407.0	148.9	1.2
9TH	113.44	3.2	-27.8	1206	2078	2.6	-13.4	8	-2	478.7	-1565.9	386.6	142.7	1.3
10TH	126.27	3.8	-28.8	1197	2063	3.2	-14.0	7	-1	474.9	-1537.1	366.7	136.5	1.5
11TH	139.10	4.3	-30.0	1197	2063	3.6	-14.5	5	-1	470.6	-1507.1	347.1	130.5	1.6
12TH	151.93	4.5	-31.4	1197	2063	3.8	-15.2	3	-1	466.1	-1475.7	328.0	124.5	1.7
13TH	164.76	4.7	-32.8	1197	2063	3.9	-15.9	2	-0	461.4	-1442.9	309.3	118.5	1.7
14TH	177.59	4.9	-34.2	1197	2063	4.1	-16.6	0	-0	456.4	-1408.7	291.0	112.6	1.7
15TH	190.42	5.1	-35.6	1197	2063	4.3	-17.3	-1	0	451.3	-1373.1	273.1	106.8	1.7
16TH	203.25	5.3	-37.1	1197	2063	4.4	-18.0	-3	1	446.0	-1336.0	255.8	101.0	1.6
17TH	216.08	6.5	-38.5	1197	2063	5.4	-18.6	-2	1	439.5	-1297.5	238.9	95.4	1.5
18TH	228.66	6.9	-38.8	1174	2023	5.9	-19.2	-2	1	432.7	-1258.7	222.8	89.9	1.5
19TH	241.24	7.2	-39.8	1174	2023	6.1	-19.7	-3	1	425.5	-1218.9	207.2	84.5	1.4
20TH	253.82	7.5	-40.8	1174	2023	6.4	-20.2	-3	1	417.9	-1178.1	192.1	79.2	1.3
21ST	266.40	7.9	-41.8	1174	2023	6.7	-20.7	-3	1	410.0	-1136.3	177.6	74.0	1.2
22ND	278.98	8.2	-42.8	1174	2023	7.0	-21.1	-4	1	401.8	-1093.5	163.5	68.9	1.1
23RD	291.56	8.6	-43.8	1174	2023	7.3	-21.6	-4	1	393.2	-1049.8	150.1	63.9	.9
24TH	304 14	9.1	-44.6	1174	2023	7.7	-22.1	-4	1	384.2	-1005.1	137.1	59.0	.8
25TH	316.72	9.8	-45.0	1174	2023	8.4	-22.2	-4	1	374.3	-960.1	124.8	54.2	.7
		10.4	-44.4	1151	1983	9.0	-22.4	-4	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 250 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									364.0	-915.7	113.2	49.7	.5
		11.1	-44.7	1151	1983	9.7	-22.6	-4	2					
27TH	341.38									352.9	-871.0	102.2	45.2	.4
		11.8	-45.1	1151	1983	10.3	-22.7	-3	2					
28TH	353.71									341.0	-825.9	91.7	41.0	.3
		12.6	-45.4	1151	1983	10.9	-22.9	-3	2					
29TH	366.04									328.4	-780.5	81.8	36.8	.2
		13.6	-44.8	1127	1943	12.0	-23.1	-2	1					
30TH	378.12									314.9	-735.7	72.7	32.9	.1
		14.6	-45.0	1127	1943	13.0	-23.1	-1	1					
31ST	390.20									300.2	-690.8	64.0	29.2	.1
		15.4	-45.0	1127	1943	13.7	-23.2	-1	1					
32ND	402.28									284.8	-645.8	56.0	25.7	.1
		16.2	-45.0	1127	1943	14.4	-23.2	-1	1					
33RD	414.36									268.6	-600.8	48.4	22.4	.0
		17.0	-45.0	1127	1943	15.1	-23.2	-1	1					
34TH	426.44									251.5	-555.8	41.5	19.2	.0
		17.8	-45.0	1127	1943	15.8	-23.2	-1	0					
35TH	438.52									233.7	-510.7	35.0	16.3	-.0
		18.6	-45.0	1127	1943	16.5	-23.2	-1	0					
36TH	450.60									215.1	-465.7	29.1	13.6	-.0
		19.4	-45.1	1127	1943	17.2	-23.2	-0	0					
37TH	462.68									195.7	-420.6	23.8	11.1	-.0
		19.9	-45.1	1127	1943	17.6	-23.2	-0	0					
38TH	474.76									175.8	-375.5	19.0	8.8	-.1
		20.3	-45.2	1127	1943	18.0	-23.3	-1	0					
39TH	486.84									155.5	-330.3	14.7	6.8	-.1
		20.8	-45.2	1127	1943	18.4	-23.3	-1	0					
40TH	498.92									134.7	-285.0	11.0	5.1	-.1
		21.2	-45.3	1127	1943	18.8	-23.3	-1	1					
41ST	511.00									113.5	-239.8	7.8	3.6	-.1
		21.7	-45.3	1127	1943	19.2	-23.3	-1	1					
42ND	523.08									91.8	-194.4	5.2	2.4	-.1
		23.5	-47.3	1174	2023	20.0	-23.4	0	-0					
43RD	535.66									68.3	-147.2	3.0	1.3	-.1
		24.7	-48.2	1206	2078	20.4	-23.2	3	-3					
44TH	548.58									43.6	-99.0	1.5	.6	-.0
		29.8	-65.2	1680	2895	17.7	-22.5	5	-4					
MR	566.58									13.9	-33.8	.3	.1	.2
		13.9	-33.8	1085	2065	12.8	-16.4	-9	6					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 260 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									308.2	-2101.2	665.7	118.1	.9
2ND	23.00	3.7	-53.8	2147	3699	1.7	-14.5	23	-3	304.5	-2047.5	618.0	111.1	1.9
3RD	35.92	-1.2	-31.7	1206	2078	-1.0	-15.3	18	1	305.8	-2015.8	591.7	107.2	2.3
4TH	48.84	-.9	-31.0	1206	2078	-.7	-14.9	15	1	306.6	-1984.8	565.9	103.2	2.7
5TH	61.76	.3	-31.2	1206	2078	.3	-15.0	15	-0	306.3	-1953.6	540.4	99.2	3.1
6TH	74.68	1.1	-32.6	1206	2078	.9	-15.7	12	-1	305.2	-1921.0	515.4	95.3	3.4
7TH	87.60	1.9	-34.0	1206	2078	1.6	-16.4	10	-1	303.3	-1887.0	490.8	91.4	3.7
8TH	100.52	2.7	-35.4	1206	2078	2.2	-17.0	8	-1	300.6	-1851.6	466.7	87.5	3.9
9TH	113.44	3.4	-36.8	1206	2078	2.8	-17.7	7	-1	297.2	-1814.8	443.0	83.6	4.1
10TH	126.27	4.2	-37.9	1197	2063	3.5	-18.4	5	-1	293.1	-1777.0	419.9	79.8	4.3
11TH	139.10	4.8	-39.2	1197	2063	4.0	-19.0	4	-1	288.3	-1737.8	397.4	76.1	4.4
12TH	151.93	4.7	-40.1	1197	2063	4.0	-19.4	2	-1	283.6	-1697.7	375.3	72.4	4.4
13TH	164.76	4.7	-41.1	1197	2063	3.9	-19.9	1	-0	278.8	-1656.6	353.8	68.8	4.5
14TH	177.59	4.7	-42.1	1197	2063	3.9	-20.4	1	-0	274.1	-1614.5	332.8	65.3	4.5
15TH	190.42	4.7	-43.0	1197	2063	3.9	-20.9	-0	0	269.4	-1571.5	312.4	61.8	4.5
16TH	203.25	4.7	-44.0	1197	2063	3.9	-21.3	-1	0	264.7	-1527.5	292.5	58.3	4.5
17TH	216.08	5.9	-45.0	1197	2063	4.9	-21.8	-1	0	258.8	-1482.5	273.2	55.0	4.4
18TH	228.66	6.0	-44.8	1174	2023	5.1	-22.2	-1	0	252.8	-1437.6	254.8	51.8	4.4
19TH	241.24	6.1	-45.5	1174	2023	5.2	-22.5	-1	0	246.7	-1392.1	237.0	48.6	4.3
20TH	253.82	6.2	-46.2	1174	2023	5.2	-22.8	-2	0	240.5	-1346.0	219.8	45.6	4.3
21ST	266.40	6.2	-46.8	1174	2023	5.3	-23.1	-2	0	234.3	-1299.1	203.2	42.6	4.2
22ND	278.98	6.3	-47.5	1174	2023	5.3	-23.5	-2	1	228.1	-1251.7	187.1	39.7	4.1
23RD	291.56	6.3	-48.2	1174	2023	5.4	-23.8	-3	1	221.7	-1203.5	171.7	36.8	4.0
24TH	304.14	6.4	-48.9	1174	2023	5.4	-24.1	-3	1	215.4	-1154.6	156.9	34.1	3.9
25TH	316.72	6.4	-49.7	1174	2023	5.4	-24.5	-3	1	209.0	-1105.0	142.6	31.4	3.8
		6.2	-49.4	1151	1983	5.4	-24.9	-4	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 260 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									202.8	-1055.6	129.3	28.9	3.6
		6.2	-50.2	1151	1983	5.4	-25.3	-4	1					
27TH	341.38									196.5	-1005.3	116.6	26.4	3.5
		6.2	-51.0	1151	1983	5.4	-25.7	-4	1					
28TH	353.71									190.3	-954.4	104.5	24.0	3.3
		6.2	-51.7	1151	1983	5.4	-26.1	-5	1					
29TH	366.04									184.1	-902.6	93.1	21.7	3.1
		6.7	-51.4	1127	1943	6.0	-26.5	-4	1					
30TH	378.12									177.3	-851.2	82.5	19.5	3.0
		7.4	-51.9	1127	1943	6.5	-26.7	-4	1					
31ST	390.20									170.0	-799.3	72 5	17.4	2.8
		7.8	-52.3	1127	1943	6.9	-26.9	-4	1					
32ND	402.28									162.2	-747.0	63.2	15.4	2.6
		8.2	-52.6	1127	1943	7.3	-27.1	-4	1					
33RD	414.36									154.0	-694.4	54.5	13.5	2.4
		8.6	-52.9	1127	1943	7.6	-27.3	-4	1					
34TH	426.44									145.4	-641.4	46.4	11.7	2.3
		9.0	-53.3	1127	1943	8.0	-27.4	-4	1					
35TH	438.52									136.4	-588.1	39.0	10.0	2.1
		9.4	-53.6	1127	1943	8.3	-27.6	-4	1					
36TH	450.60									127.0	-534.5	32.2	8.4	1.9
		9.7	-54.0	1127	1943	8.6	-27.8	-4	1					
37TH	462.68									117.3	-480.5	26.1	7.0	1.7
		10.3	-54.0	1127	1943	9.1	-27.8	-4	1					
38TH	474.76									107.0	-426 5	20.6	5.6	1.6
		10.9	-54.0	1127	1943	9.7	-27.8	-5	2					
39TH	486.84									96.0	-372.5	15.8	4.4	1.4
		11.5	-54.1	1127	1943	10.2	-27.8	-5	2					
40TH	498.92									84.5	-318.4	11.6	3.3	1.2
		12.2	-54.1	1127	1943	10.8	-27.8	-5	2					
41ST	511.00									72.3	-264.4	8.1	2.3	.9
		12.8	-54.1	1127	1943	11.3	-27.8	-5	2					
42ND	523.08									59.6	-210.3	5.2	1.5	.7
		14.5	-56.4	1174	2023	12.3	-27.9	-5	2					
43RD	535.66									45.1	-153.9	2.9	.9	.5
		16.0	-56.5	1206	2078	13.3	-27.2	-4	2					
44TH	548.58									29.0	-97.4	1.3	.4	.3
		20.4	-71.8	1680	2895	12.1	-24.8	-1	0					
MR	566.58									8.7	-25.6	.2	.1	.3
		8.7	-25.6	1085	2065	8.0	-12.4	-15	9					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 270 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									247.8	-2449.2	765.0	88.5	1.0
2ND	23.00	4.0	-66.2	2147	3699	1.9	-17.9	20	-2	243.8	-2383.0	709.5	82.8	2.1
3RD	35.92	-1.4	-39.3	1206	2078	-1.2	-18.9	17	1	245.3	-2343.7	678.9	79.7	2.6
4TH	48.84	-1.4	-37.1	1206	2078	-1.1	-17.8	14	1	246.6	-2306.6	648.9	76.5	3.0
5TH	61.76	-.2	-36.6	1206	2078	-.1	-17.6	14	0	246.8	-2270.0	619.3	73.3	3.4
6TH	74.68	.7	-38.4	1206	2078	.6	-18.5	12	-0	246.1	-2231.6	590.2	70.1	3.8
7TH	87.60	1.6	-40.2	1206	2078	1.3	-19.3	10	-1	244.5	-2191.4	561.7	66.9	4.1
8TH	100.52	2.5	-42.0	1206	2078	2.1	-20.2	9	-1	242.0	-2149.4	533.6	63.8	4.4
9TH	113.44	3.4	-43.8	1206	2078	2.8	-21.1	8	-1	238.6	-2105.6	506.1	60.7	4.6
10TH	126.27	4.3	-45.3	1197	2063	3.6	-21.9	6	-1	234.3	-2060.3	479.4	57.7	4.9
11TH	139.19	4.9	-47.0	1197	2063	4.1	-22.8	5	-1	229.4	-2013.4	453.3	54.7	5.1
12TH	151.93	4.9	-48.2	1197	2063	4.1	-23.4	4	-1	224.4	-1965.2	427.8	51.8	5.2
13TH	164.76	4.9	-49.5	1197	2063	4.1	-24.0	3	-1	219.5	-1915.7	402.9	48.9	5.3
14TH	177.59	4.9	-50.8	1197	2063	4.1	-24.6	2	-0	214.6	-1864.9	378.6	46.1	5.4
15TH	190.42	4.9	-52.0	1197	2063	4.1	-25.2	1	-0	209.6	-1812.9	355.0	43.4	5.5
16TH	203.25	4.9	-53.3	1197	2063	4.1	-25.8	-0	0	204.7	-1759.6	332.1	40.8	5.5
17TH	216.08	6.2	-54.6	1197	2063	5.2	-26.4	0	-0	198.5	-1705.0	309.9	38.2	5.5
18TH	228.66	6.3	-54.0	1174	2023	5.4	-26.7	-0	0	192.2	-1651.0	288.8	35.7	5.5
19TH	241.24	6.3	-54.4	1174	2023	5.4	-26.9	-0	0	185.8	-1596.6	268.3	33.3	5.4
20TH	253.82	6.4	-54.7	1174	2023	5.4	-27.0	-1	0	179.5	-1541.9	248.6	31.0	5.4
21ST	266.40	6.4	-55.0	1174	2023	5.4	-27.2	-1	0	173.1	-1486.9	229.5	28.8	5.3
22ND	278.98	6.4	-55.4	1174	2023	5.4	-27.4	-2	0	166.7	-1431.5	211.2	26.7	5.3
23RD	291.56	6.4	-55.7	1174	2023	5.4	-27.5	-2	0	160.4	-1375.8	193.5	24.6	5.2
24TH	304.14	6.3	-56.3	1174	2023	5.4	-27.8	-2	0	154.1	-1319.4	176.6	22.7	5.1
25TH	316.72	6.0	-57.4	1174	2023	5.1	-28.4	-3	1	148.0	-1262.0	160.3	20.8	4.9
		5.7	-57.3	1151	1983	4.9	-28.9	-4	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 270 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									142.4	-1204.7	145.1	19.0	4.8
27TH	341.38	5.4	-58.3	1151	1983	4.7	-29.4	-4	1	136.9	-1146.3	130.6	17.2	4.6
28TH	353.71	5.2	-59.4	1151	1983	4.5	-29.9	-5	1	131.8	-1087.0	116.9	15.6	4.4
29TH	366.04	4.9	-60.4	1151	1983	4.3	-30.5	-5	1	126.9	-1026.5	103 8	14.0	4.1
30TH	378.12	5.5	-60.2	1127	1943	4.9	-31.0	-5	1	121.4	-966.4	91.8	12.5	3.9
31ST	390.20	6.1	-60.7	1127	1943	5.4	-31.2	-5	1	115.3	-905.7	80.5	11.1	3.7
32ND	402.28	6.3	-61.0	1127	1943	5.6	-31.4	-5	1	109.0	-844.7	69.9	9.7	3.5
33RD	414.36	6.5	-61.3	1127	1943	5.8	-31.5	-5	1	102.5	-783.3	60.1	8.4	3.2
34TH	426.44	6.7	-61.5	1127	1943	5.9	-31.7	-5	1	95.8	-721.9	51.0	7.2	3.0
35TH	438.52	6.9	-61.8	1127	1943	6.1	-31.8	-5	1	88.9	-660.1	42 7	6.1	2.8
36TH	450.60	7.1	-62.1	1127	1943	6.3	-32.0	-5	1	81.8	-598.0	35.1	5.1	2.5
37TH	462.68	7.2	-62.4	1127	1943	6.4	-32.1	-5	1	74.5	-535.6	28.2	4.1	2.3
38TH	474.76	7.4	-62.3	1127	1943	6.6	-32.1	-5	1	67.1	-473.3	22.1	3.3	2.0
39TH	486.84	7.7	-62.2	1127	1943	6.8	-32.0	-5	1	59.4	-411.1	16.8	2.5	1.8
40TH	498.92	7.9	-62.1	1127	1943	7.0	-32.0	-5	1	51.5	-349.0	12.2	1.9	1.5
41ST	511.00	8.2	-62.0	1127	1943	7.2	-31.9	-6	1	43.3	-287.0	8.3	1.3	1.2
42ND	523.08	8.4	-61.9	1127	1943	7.5	-31.8	-6	1	34.9	-225.1	5.2	.8	1.0
43RD	535.66	9.4	-64.3	1174	2023	8 0	-31.8	-6	1	25.5	-160.8	2.8	.4	.7
44TH	548.58	10.5	-63.9	1206	2078	8.7	-30.8	-5	1	15.0	-96.9	1.2	.2	.4
MR	566.58	13.1	-79.7	1680	2895	7.8	-27.5	-3	1	1.9	-17.2	.1	.0	.2
TOP	581.67	1.9	-17.2	1085	2065	1.8	-8.3	-16	3	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 280 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									134.7	-2376.7	763.6	62.7	-1.0
2ND	23.00	-4.2	-57.6	2147	3699	-2.0	-15.6	21	3	139.0	-2319.1	709.6	59.5	-.0
3RD	35.92	-6.3	-34.3	1206	2078	-5.2	-16.5	18	6	145.2	-2284.8	679.8	57.7	.5
4TH	48.84	-6.4	-32.8	1206	2078	-5.3	-15.8	16	5	151.6	-2252.0	650.5	55.8	.9
5TH	61.76	-5.4	-32.6	1206	2078	-4.5	-15.7	16	4	157.1	-2219.3	621.6	53.8	1.3
6TH	74.68	-4.3	-34.1	1206	2078	-3.6	-16.4	14	3	161.4	-2185.2	593.2	51.7	1.7
7TH	87.60	-3.2	-35.6	1206	2078	-2.7	-17.1	13	2	164.6	-2149.6	565.2	49.6	2.0
8TH	100.52	-2.1	-37.1	1206	2078	-1.7	-17.9	12	1	166.7	-2112.5	537.6	47.5	2.4
9TH	113.44	-1.0	-38.6	1206	2078	-.8	-18.6	10	0	167.7	-2073.9	510.6	45.3	2.7
10TH	126.27	.1	-39.8	1197	2063	.1	-19.3	10	-0	167.6	-2034.1	484.2	43.2	3.0
11TH	139.10	1.0	-41.2	1197	2063	.9	-20.0	9	-0	166.6	-1992.9	458.4	41.0	3.3
12TH	151.93	1.2	-42.8	1197	2063	1.0	-20.7	7	-0	165.3	-1950.2	433.1	38.9	3.5
13TH	164.76	1.5	-44.3	1197	2063	1.2	-21.5	6	-0	163.9	-1905.9	408.4	36.8	3.7
14TH	177.59	1.7	-45.8	1197	2063	1.4	-22.2	4	-0	162.2	-1860.1	384.2	34.7	3.9
15TH	190.42	1.9	-47.4	1197	2063	1.6	-23.0	3	-0	160.2	-1812.7	360.6	32.6	4.0
16TH	203.25	2.1	-48.9	1197	2063	1.8	-23.7	2	-0	158.1	-1763.8	337.7	30.6	4.1
17TH	216.08	3.7	-50.4	1197	2063	3.1	-24.4	3	-0	154.4	-1713.4	315.4	28.6	4.2
18TH	228.66	4.2	-50.5	1174	2023	3.6	-25.0	2	-0	150.2	-1662.9	294.2	26.7	4.3
19TH	241.24	4.4	-51.4	1174	2023	3.8	-25.4	1	-0	145.8	-1611.5	273.6	24.8	4.3
20TH	253.82	4.7	-52.3	1174	2023	4.0	-25.8	0	-0	141.1	-1559.2	253.6	23.0	4.4
21ST	266.40	5.0	-53.2	1174	2023	4.3	-26.3	-1	0	136.1	-1506.0	234.3	21.2	4.3
22ND	278.98	5.3	-54.1	1174	2023	4.5	-26.7	-1	0	130.8	-1452.0	215.7	19.6	4.3
23RD	291.56	5.5	-55.0	1174	2023	4.7	-27.2	-2	0	125.3	-1397.0	197.8	18.0	4.2
24TH	304.14	5.6	-56.0	1174	2023	4.8	-27.7	-3	1	119.6	-1341.0	180.6	16.4	4.0
25TH	316.72	5.4	-57.1	1174	2023	4.6	-28.2	-3	1	114.3	-1283.9	164.1	14.9	3.9
		5.0	-57.1	1151	1983	4.4	-28.8	-3	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 280 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									109.2	-1226.8	148.6	13.6	3.7
27TH	341.38	4.8	-58.1	1151	1983	4.2	-29.3	-4	1	104.4	-1168.7	133.8	12.2	3.6
28TH	353.71	4.6	-59.2	1151	1983	4.0	-29.9	-4	1	99.8	-1109.5	119.8	11.0	3.4
29TH	366.04	4.4	-60.3	1151	1983	3.8	-30.4	-4	0	95.4	-1049.2	106.5	9.8	3.2
30TH	378.12	5.1	-60.1	1127	1943	4.5	-30.9	-4	1	90.3	-989.1	94.2	8.7	3.0
31ST	390.20	5.6	-60.8	1127	1943	5.0	-31.3	-4	1	84.7	-928.3	82.6	7.6	2.8
32ND	402.28	5.7	-61.3	1127	1943	5.0	-31.6	-4	1	79.0	-867.0	71.7	6.6	2.7
33RD	414.36	5.7	-61.9	1127	1943	5.0	-31.9	-4	1	73.3	-805.1	61.6	5.7	2.5
34TH	426.44	5.7	-62.5	1127	1943	5.1	-32.1	-4	1	67.6	-742.6	52.3	4.8	2.3
35TH	438.52	5.7	-63.0	1127	1943	5.1	-32.4	-4	1	61.9	-679.6	43.7	4.1	2.1
36TH	450.60	5.7	-63.6	1127	1943	5.1	-32.7	-4	1	56.2	-616.0	35.9	3.3	1.9
37TH	462.68	5.7	-64.1	1127	1943	5.0	-33.0	-4	1	50.5	-551.9	28.8	2.7	1.7
38TH	474.76	5.6	-64.2	1127	1943	5.0	-33.1	-4	1	44.8	-487.7	22.6	2.1	1.5
39TH	486.84	5.6	-64.3	1127	1943	5.0	-33.1	-4	1	39.2	-423.4	17.0	1.6	1.3
40TH	498.92	5.6	-64.4	1127	1943	4.9	-33.1	-4	1	33.7	-359.0	12.3	1.2	1.1
41ST	511.00	5.5	-64.5	1127	1943	4.9	-33.2	-3	1	28.2	-294.5	8.4	.8	.9
42ND	523.08	5.5	-64.6	1127	1943	4.9	-33.2	-3	0	22.7	-229.9	5.2	.5	.8
43RD	535.66	6.3	-67.3	1174	2023	5.4	-33.3	-3	0	16.3	-162.6	2.7	.3	.6
44TH	548.58	7.5	-67.0	1206	2078	6.2	-32.2	-2	0	8.9	-95.7	1.1	.1	.5
MR	566.58	8.2	-82.9	1680	2895	4.9	-28.6	-4	1	.7	-12.8	.1	.0	.2
TOP	581.67	.7	-12.8	1085	2065	.6	-6.2	-19	2	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 290 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									136.6	-2112.1	693.0	58.6	-6.0
2ND	23.00	-2.3	-49.8	2147	3699	-1.1	-13.5	26	2	138.9	-2062.3	645.0	55.5	-5.0
3RD	35.92	-4.9	-29.9	1206	2078	-4.0	-14.4	20	6	143.8	-2032.5	618.6	53.6	-4.5
4TH	48.84	-5.0	-28.5	1206	2078	-4.2	-13.7	18	6	148.8	-2004.0	592.5	51.7	-4.1
5TH	61.76	-4.2	-28.2	1206	2078	-3.5	-13.6	19	5	153.0	-1975.8	566.8	49.8	-3.7
6TH	74.68	-3.3	-29.4	1206	2078	-2.7	-14.1	17	3	156.3	-1946.4	541.4	47.8	-3.3
7TH	87.60	-2.4	-30.5	1206	2078	-2.0	-14.7	17	2	158.7	-1915.9	516.5	45.8	-2.9
8TH	100.52	-1.5	-31.6	1206	2078	-1.3	-15.2	16	1	160.3	-1884.2	491.9	43.7	-2.5
9TH	113.44	-.7	-32.8	1206	2078	-.6	-15.8	15	1	160.9	-1851.5	467.8	41.6	-2.1
10TH	126.27	.2	-33.7	1197	2063	.2	-16.3	14	-0	160.7	-1817.8	444.3	39.6	-1.7
11TH	139.10	1.0	-34.8	1197	2063	.8	-16.9	13	-1	159.7	-1783.0	421.2	37.5	-1.3
12TH	151.93	1.4	-36.1	1197	2063	1.2	-17.5	11	-1	158.4	-1746.9	398.5	35.5	-1.0
13TH	164.76	1.8	-37.4	1197	2063	1.5	-18.1	10	-1	156.5	-1709.5	376.4	33.4	-.7
14TH	177.59	2.2	-38.7	1197	2063	1.9	-18.8	8	-1	154.3	-1670.8	354.7	31.5	-.5
15TH	190.42	2.7	-40.0	1197	2063	2.2	-19.4	6	-1	151.6	-1630.7	333.5	29.5	-.3
16TH	203.25	3.1	-41.3	1197	2063	2.6	-20.0	5	-1	148.5	-1589.4	312.8	27.6	-.1
17TH	216.08	4.7	-42.6	1197	2063	3.9	-20.7	6	-1	143.8	-1546.8	292.7	25.7	.1
18TH	228.66	4.9	-42.8	1174	2023	4.2	-21.1	5	-1	139.0	-1504.0	273.5	23.9	.3
19TH	241.24	4.9	-43.7	1174	2023	4.2	-21.6	5	-1	134.1	-1460.3	254.9	22.2	.4
20TH	253.82	4.9	-44.5	1174	2023	4.2	-22.0	4	-1	129.2	-1415.8	236.8	20.5	.6
21ST	266.40	4.9	-45.4	1174	2023	4.2	-22.4	3	-1	124.3	-1370.4	219.3	18.9	.7
22ND	278.98	4.9	-46.3	1174	2023	4.2	-22.9	3	-0	119.4	-1324.1	202.3	17.4	.8
23RD	291.56	4.9	-47.2	1174	2023	4.2	-23.3	2	-0	114.5	-1276.9	186.0	15.9	.9
24TH	304.14	4.9	-48.1	1174	2023	4.1	-23.8	2	-0	109.7	-1228.8	170.2	14.5	.9
25TH	316.72	4.8	-49.1	1174	2023	4.1	-24.3	1	-0	104.9	-1179.7	155.0	13.2	1.0
		4.6	-49.0	1151	1983	4.0	-24.7	1	-0					

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 290 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
										100.3	-1130.7	140.8	11.9	1.0
26TH	329.05	4.5	-49.9	1151	1983	3.9	-25.2	0	-0	95.8	-1080.8	127.2	10.7	1.0
27TH	341.38	4.4	-50.9	1151	1983	3.9	-25.6	-0	0	91.3	-1029.9	114.2	9.6	1.0
28TH	353.71	4.3	-51.8	1151	1983	3.8	-26.1	-1	0	87.0	-978.2	101.8	8.5	1.0
29TH	366.04	5.0	-51.6	1127	1943	4.4	-26.6	-0	0	82.0	-926.5	90.3	7.4	1.0
30TH	378.12	5.5	-52.7	1127	1943	4.9	-27.1	-0	0	76.5	-873.8	79.4	6.5	.9
31ST	390.20	5.5	-54.0	1127	1943	4.9	-27.8	-1	0	71.0	-819.8	69.2	5.6	.9
32ND	402.28	5.6	-55.2	1127	1943	5.0	-28.4	-1	0	65.4	-764.6	59.6	4.8	.9
33RD	414.36	5.6	-56.4	1127	1943	5.0	-29.1	-1	0	59.8	-708.2	50.7	4.0	.8
34TH	426.44	5.7	-57.7	1127	1943	5.1	-29.7	-1	0	54.1	-650.5	42.5	3.3	.8
35TH	438.52	5.8	-58.9	1127	1943	5.1	-30.3	-1	0	48.3	-591.6	35.0	2.7	.7
36TH	450.60	5.8	-60.1	1127	1943	5.1	-31.0	-1	0	42.5	-531.4	28.2	2.1	.7
37TH	462.68	5.6	-60.5	1127	1943	4.9	-31.1	-1	0	36.9	-471.0	22.2	1.7	.6
38TH	474.76	5.3	-60.7	1127	1943	4.7	-31.3	-1	0	31.6	-410.3	16.8	1.3	.5
39TH	486.84	5.1	-61.0	1127	1943	4.5	-31.4	-1	0	26.5	-349.3	12.2	.9	.5
40TH	498.92	4.8	-61.2	1127	1943	4.3	-31.5	-1	0	21.7	-288.1	8.4	.6	.4
41ST	511.00	4.6	-61.5	1127	1943	4.1	-31.7	-1	0	17.1	-226.6	5.3	.4	.4
42ND	523.08	5.0	-64.3	1174	2023	4.2	-31.8	-1	0	12.1	-162.2	2.8	.2	.3
43RD	535.66	5.5	-64.4	1206	2078	4.6	-31.0	-1	0	6.6	-97.9	1.2	.1	.3
44TH	548.58	5.8	-80.9	1680	2895	3.5	-27.9	-2	0	.8	-17.0	.1	.0	.1
MR	566.58	.8	-17.0	1085	2065	.7	-8.2	-10	1	0.0	0.0	0.0	0.0	0.0
TOP	581.67													

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 300 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									201.5	-2016.0	665.4	84.1	-14.8
2ND	23.00	-5.6	-42.9	2147	3699	-2.6	-11.6	26	6	207.1	-1973.1	619.5	79.4	-14.0
3RD	35.92	-4.9	-28.4	1206	2078	-4.1	-13.6	22	7	212.0	-1944.8	594.2	76.7	-13.5
4TH	48.84	-4.2	-27.5	1206	2078	-3.4	-13.2	23	6	216.1	-1917.3	569.2	73.9	-13.0
5TH	61.76	-3.0	-27.5	1206	2078	-2.5	-13.2	24	4	219.1	-1889.8	544.6	71.1	-12.5
6TH	74.68	-2.2	-28.5	1206	2078	-1.9	-13.7	23	3	221.4	-1861.3	520.4	68.3	-11.9
7TH	87.60	-1.5	-29.6	1206	2078	-1.2	-14.2	21	2	222.8	-1831.7	496.5	65.4	-11.4
8TH	100.52	-.7	-30.6	1206	2078	-.6	-14.7	20	1	223.5	-1801.1	473.1	62.5	-10.9
9TH	113.44	.1	-31.7	1206	2078	.1	-15.2	20	-0	223.4	-1769.5	450.0	59.6	-10.4
10TH	126.27	.9	-32.5	1197	2063	.7	-15.7	19	-1	222.6	-1737.0	427.5	56.8	-10.0
11TH	139.10	1.5	-33.5	1197	2063	1.3	-16.2	18	-1	221.0	-1703.5	405.4	53.9	-9.5
12TH	151.93	2.0	-34.5	1197	2063	1.6	-16.7	16	-2	219.1	-1668.9	383.8	51.1	-9.0
13TH	164.76	2.4	-35.6	1197	2063	2.0	-17.2	15	-2	216.7	-1633.4	362.6	48.3	-8.6
14TH	177.59	2.8	-36.6	1197	2063	2.3	-17.7	14	-2	213.9	-1596.8	341.9	45.6	-8.2
15TH	190.42	3.2	-37.6	1197	2063	2.7	-18.2	13	-2	210.6	-1559.2	321.7	42.8	-7.8
16TH	203.25	3.6	-38.6	1197	2063	3.0	-18.7	12	-2	207.0	-1520.6	301.9	40.2	-7.5
17TH	216.08	5.2	-39.6	1197	2063	4.3	-19.2	13	-3	201.8	-1481.0	282.7	37.5	-7.1
18TH	228.66	5.6	-39.7	1174	2023	4.8	-19.6	12	-3	196.2	-1441.3	264.3	35.0	-6.7
19TH	241.24	5.9	-40.5	1174	2023	5.0	-20.0	12	-3	190.4	-1400.7	246.4	32.6	-6.3
20TH	253.82	6.2	-41.4	1174	2023	5.3	-20.4	11	-3	184.2	-1359.4	229.0	30.2	-5.9
21ST	266.40	6.5	-42.2	1174	2023	5.5	-20.9	10	-3	177.8	-1317.2	212.2	28.0	-5.6
22ND	278.98	6.8	-43.0	1174	2023	5.7	-21.3	10	-3	171.0	-1274.2	195.9	25.8	-5.3
23RD	291.56	7.0	-43.9	1174	2023	6.0	-21.7	9	-2	164.0	-1230.3	180.1	23.7	-5.0
24TH	304.14	7.1	-44.9	1174	2023	6.1	-22.2	8	-2	156.8	-1185.4	164.9	21.6	-4.7
25TH	316.72	6.9	-46.1	1174	2023	5.9	-22.8	8	-2	149.9	-1139.3	150.3	19.7	-4.4
		6.5	-46.4	1151	1983	5.7	-23.4	7	-2					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 300 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									143.4	-1092.9	136.6	17.9	-4.2
		6.3	-47.6	1151	1983	5.4	-24.0	6	-1					
27TH	341.38									137.2	-1045.3	123.4	16.2	-3.9
		6.0	-48.7	1151	1983	5.2	-24.6	6	-1					
28TH	353.71									131.1	-996.6	110.8	14.5	-3.7
		5.8	-49.9	1151	1983	5.0	-25.2	6	-1					
29TH	366.04									125.4	-946.7	98.8	12.9	-3.5
		6.5	-50.0	1127	1943	5.7	-25.8	6	-1					
30TH	378.12									118.9	-896.6	87.7	11.5	-3.2
		7.1	-51.1	1127	1943	6.3	-26.3	6	-1					
31ST	390.20									111.7	-845.5	77.2	10.1	-3.0
		7.3	-52.1	1127	1943	6.5	-26.8	6	-1					
32ND	402.28									104.4	-793.4	67.3	8.8	-2.7
		7.5	-53.2	1127	1943	6.6	-27.4	6	-1					
33RD	414.36									97.0	-740.2	58.0	7.5	-2.5
		7.6	-54.2	1127	1943	6.8	-27.9	6	-1					
34TH	426.44									89.4	-686.0	49.4	6.4	-2.2
		7.8	-55.2	1127	1943	6.9	-28.4	6	-1					
35TH	438.52									81.6	-630.8	41.4	5.4	-2.0
		7.9	-56.2	1127	1943	7.0	-29.0	6	-1					
36TH	450.60									73.7	-574.6	34.2	4.5	-1.7
		8.1	-57.3	1127	1943	7.1	-29.5	6	-1					
37TH	462.68									65.6	-517.3	27.6	3.6	-1.5
		7.8	-57.9	1127	1943	6.9	-29.8	5	-1					
38TH	474.76									57.8	-459.4	21.7	2.9	-1.2
		7.5	-58.5	1127	1943	6.7	-30.1	5	-1					
39TH	486.84									50.3	-400.9	16.5	2.2	-1.0
		7.2	-59.1	1127	1943	6.4	-30.4	5	-1					
40TH	498.92									43.1	-341.8	12.0	1.6	-.8
		6.9	-59.7	1127	1943	6.1	-30.7	4	-1					
41ST	511.00									36.2	-282.1	8.2	1.2	-.6
		6.6	-60.3	1127	1943	5.9	-31.0	4	-1					
42ND	523.08									29.5	-221.9	5.2	.8	-.4
		7.1	-63.4	1174	2023	6.1	-31.3	4	-1					
43RD	535.66									22.4	-158.5	2.8	.4	-.2
		8.0	-63.4	1206	2078	6.6	-30.5	4	-1					
44TH	548.58									14.4	-95.1	1.1	.2	-.1
		9.7	-78.5	1680	2895	5.8	-27.1	2	-0					
MR	566.58									4.7	-16.6	.1	.0	.1
		4.7	-16.6	1085	2065	4.3	-8.0	-6	3					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 310 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									186.6	-1871.2	624.0	84.1	-20.1
2ND	23.00	-6.8	-42.4	2147	3699	-3.2	-11.5	25	7	193.4	-1828.8	581.4	79.7	-19.2
3RD	35.92	-4.7	-25.9	1206	2078	-3.9	-12.5	22	7	198.1	-1802.9	558.0	77.2	-18.8
4TH	48.84	-3.9	-25.0	1206	2078	-3.2	-12.0	21	6	202.0	-1777.9	534.8	74.6	-18.4
5TH	61.76	-2.7	-24.9	1206	2078	-2.3	-12.0	22	4	204.7	-1753.0	512.0	72.0	-18.0
6TH	74.68	-2.0	-25.6	1206	2078	-1.7	-12.3	22	3	206.8	-1727.5	489.5	69.3	-17.5
7TH	87.60	-1.3	-26.3	1206	2078	-1.1	-12.6	21	2	208.1	-1701.2	467.4	66.7	-17.1
8TH	100.52	-.6	-27.0	1206	2078	-.5	-13.0	21	1	208.7	-1674.2	445.6	64.0	-16.6
9TH	113.44	.1	-27.7	1206	2078	.1	-13.3	21	-0	208.7	-1646.5	424.1	61.3	-16.1
10TH	126.27	.8	-28.2	1197	2063	.6	-13.7	20	-1	207.9	-1618.3	403.2	58.6	-15.7
11TH	139.10	1.3	-29.0	1197	2063	1.1	-14.1	20	-2	206.5	-1589.3	382.6	55.9	-15.2
12TH	151.93	1.4	-30.1	1197	2063	1.2	-14.6	18	-1	205.1	-1559.1	362.4	53.3	-14.8
13TH	164.76	1.5	-31.3	1197	2063	1.3	-15.2	17	-1	203.6	-1527.8	342.6	50.7	-14.4
14TH	177.59	1.6	-32.4	1197	2063	1.3	-15.7	16	-1	202.0	-1495.4	323.2	48.1	-14.0
15TH	190.42	1.7	-33.6	1197	2063	1.4	-16.3	14	-1	200.3	-1461.8	304.2	45.5	-13.6
16TH	203.25	1.8	-34.8	1197	2063	1.5	-16.8	13	-1	198.5	-1427.0	285.7	42.9	-13.2
17TH	216.08	2.8	-35.9	1197	2063	2.3	-17.4	14	-2	195.7	-1391.1	267.6	40.4	-12.8
18TH	228.66	3.2	-36.1	1174	2023	2.8	-17.8	14	-2	192.5	-1355.0	250.4	38.0	-12.4
19TH	241.24	3.6	-36.9	1174	2023	3.1	-18.3	14	-2	188.8	-1318.1	233.6	35.6	-12.0
20TH	253.82	4.0	-37.8	1174	2023	3.4	-18.7	13	-2	184.8	-1280.3	217.2	33.2	-11.6
21ST	266.40	4.4	-38.6	1174	2023	3.8	-19.1	13	-2	180.4	-1241.7	201.3	30.9	-11.2
22ND	278.98	4.8	-39.5	1174	2023	4.1	-19.5	12	-3	175.6	-1202.2	186.0	28.7	-10.8
23RD	291.56	5.2	-40.3	1174	2023	4.4	-19.9	12	-3	170.4	-1161.9	171 1	26.5	-10.4
24TH	304.14	5.4	-41.3	1174	2023	4.6	-20.4	12	-3	165.0	-1120.6	156.7	24.4	-10.1
25TH	316.72	5.4	-42.5	1174	2023	4.6	-21.0	12	-3	159.5	-1078.2	142.9	22.4	-9.7
		5.3	-42.8	1151	1983	4.6	-21.6	12	-3					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 310 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									154.2	-1035.4	129.9	20.4	-9.3
		5.3	-43.9	1151	1983	4.6	-22.1	12	-2					
27TH	341.38									148.8	-991.5	117.4	18.6	-8.9
		5.3	-45.0	1151	1983	4.6	-22.7	12	-2					
28TH	353.71									143.5	-946.6	105.4	16.8	-8.4
		5.3	-46.1	1151	1983	4.6	-23.2	12	-2					
29TH	366.04									138.2	-900.5	94.1	15.0	-8.0
		6.0	-46.2	1127	1943	5.3	-23.8	13	-3					
30TH	378.12									132.2	-854.2	83.5	13.4	-7.6
		6.7	-47.5	1127	1943	5.9	-24.5	13	-3					
31ST	390.20									125.5	-806.7	73.4	11.8	-7.1
		7.0	-48.8	1127	1943	6.2	-25.1	13	-3					
32ND	402.28									118.5	-757.9	64.0	10.4	-6.6
		7.4	-50.2	1127	1943	6.5	-25.8	13	-3					
33RD	414.36									111.1	-707.7	55.1	9.0	-6.0
		7.7	-51.5	1127	1943	6.8	-26.5	13	-3					
34TH	426.44									103.4	-656.2	46.9	7.7	-5.5
		8.1	-52.8	1127	1943	7.1	-27.2	13	-3					
35TH	438.52									95.3	-603.4	39.3	6.5	-5.0
		8.4	-54.2	1127	1943	7.5	-27.9	13	-4					
36TH	450.60									86.9	-549.2	32.3	5.4	-4.4
		8.7	-55.5	1127	1943	7.7	-28.5	13	-4					
37TH	462.68									78.2	-493.8	26.0	4.4	-3.8
		8.6	-56.0	1127	1943	7.7	-28.8	13	-3					
38TH	474.76									69.6	-437.8	20.4	3.5	-3.3
		8.5	-56.5	1127	1943	7.6	-29.1	12	-3					
39TH	486.84									61.0	-381.3	15.4	2.7	-2.7
		8.4	-57.0	1127	1943	7.5	-29.3	11	-3					
40TH	498.92									52.6	-324.3	11.2	2.0	-2.3
		8.3	-57.5	1127	1943	7.4	-29.6	10	-3					
41ST	511.00									44.3	-266.8	7.6	1.4	-1.8
		8.2	-57.9	1127	1943	7.3	-29.8	10	-2					
42ND	523.08									36.1	-208.9	4.7	.9	-1.3
		9.0	-60.9	1174	2023	7.7	-30.1	10	-2					
43RD	535.66									27.2	-148.0	2.5	.5	-.9
		9.9	-60.9	1206	2078	8.3	-29.3	10	-3					
44TH	548.58									17.2	-87.1	1.0	.3	-.4
		11.3	-75.9	1680	2895	6.7	-26.2	6	-2					
MR	566.58									5.9	-11.2	.1	.0	-.0
		5.9	-11.2	1085	2065	5.4	-5.4	5	-4					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 320 CONFIGURATION A REFERENCE PRESSURE 34 0 PSF GUST FACTOR 1 32
ECCENTRICITIES BASED ON 89 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									39.3	-1564.9	529.3	33.5	-24.0
2ND	23.00	-7.2	-34.7	2147	3699	-3.3	-9.4	26	9	46.4	-1530.2	493.7	32.5	-23.3
3RD	35.92	-4 8	-21.7	1206	2078	-3.9	-10.4	23	9	51.2	-1508.6	474.1	31.9	-23.0
4TH	48.84	-3.8	-21.0	1206	2078	-3.1	-10.1	23	7	55.0	-1487.6	454.8	31.2	-22.6
5TH	61.76	-3.1	-20.8	1206	2078	-2.6	-10.0	25	6	58.1	-1466.8	435.7	30.5	-22.2
6TH	74.68	-2 9	-21.3	1206	2078	-2 4	-10.2	24	6	60.9	-1445.5	416.9	29.7	-21.8
7TH	87.60	-2.7	-21.7	1206	2078	-2.2	-10.4	24	5	63.6	-1423.8	398.3	28.9	-21.4
8TH	100.52	-2.5	-22.2	1206	2078	-2.0	-10.7	23	4	66.1	-1401.7	380.1	28.1	-21.0
9TH	113.44	-2.3	-22.6	1206	2078	-1.9	-10.9	23	4	68.3	-1379.1	362.1	27.2	-20.6
10TH	126.27	-2.0	-22.9	1197	2063	-1.7	-11.1	22	3	70.4	-1356.1	344 6	26.3	-20.2
11TH	139.10	-1.9	-23.4	1197	2063	-1.6	-11.3	22	3	72.2	-1332.7	327.3	25.4	-19.8
12TH	151.93	-1.7	-24.1	1197	2063	-1.4	-11.7	20	2	74.0	-1308.7	310.4	24.4	-19.4
13TH	164.76	-1.6	-24.7	1197	2063	-1.3	-12.0	18	2	75.6	-1284.0	293.7	23.5	-19.0
14TH	177.59	-1.5	-25.4	1197	2063	-1.2	-12.3	17	2	77.0	-1258.6	277.4	22.5	-18.7
15TH	190.42	-1.3	-26.1	1197	2063	-1.1	-12.6	16	1	78.3	-1232.5	261.4	21.5	-18.3
16TH	203.25	-1.2	-26.7	1197	2063	-1.0	-12.9	14	1	79.5	-1205.8	245.8	20.5	-18.0
17TH	216.08	-.4	-27.4	1197	2063	-.3	-13.3	16	0	79.9	-1178.4	230.5	19.5	-17.7
18TH	228.66	-.2	-27.7	1174	2023	-.1	-13.7	16	0	80.1	-1150.7	215.8	18.5	-17.3
19TH	241.24	-.1	-28.6	1174	2023	-.1	-14.1	16	0	80 1	-1122.1	201.6	17.5	-17.0
20TH	253.82	.0	-29.5	1174	2023	.0	-14.6	16	-0	80.1	-1092.6	187 6	16.5	-16.6
21ST	266.40	.1	-30.4	1174	2023	.1	-15.0	16	-0	80.0	-1062.2	174.1	15.4	-16.2
22ND	278.98	.2	-31.3	1174	2023	.2	-15.5	17	-0	79.8	-1030.9	160.9	14.4	-15.8
23RD	291.56	.3	-32.2	1174	2023	.3	-15.9	17	-0	79.5	-998.7	148.1	13.4	-15.3
24TH	304.14	.4	-33.4	1174	2023	.4	-16.5	17	-0	79.0	-965.3	135.8	12.4	-14.9
25TH	316.72	.6	-34.9	1174	2023	5	-17 2	17	-0	78.4	-930.5	123.9	11.5	-14.4
		.7	-35.6	1151	1983	.6	-17.9	16	-1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 320 CONFIGURATION A REFERENCE PRESSURE 34 0 PSF GUST FACTOR 1 32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									77.7	-894.9	112 6	10.5	-14.0
		.8	-37.0	1151	1983	.7	-18.7	16	-1					
27TH	341.38									76.9	-857.9	101 8	9.5	-13.5
		1.0	-38.4	1151	1983	.8	-19.4	16	-1					
28TH	353.71									75.9	-819.4	91.5	8.6	-13.0
		1.1	-39.8	1151	1983	1.0	-20.1	16	-1					
29TH	366.04									74.8	-779.6	81 6	7.7	-12.5
		2.2	-40.4	1127	1943	1.9	-20.8	18	-2					
30TH	378.12									72.6	-739.2	72 4	6.8	-11.9
		3.2	-41.5	1127	1943	2.8	-21.4	19	-3					
31ST	390.20									69.4	-697.7	63.7	5.9	-11.3
		3.7	-42.4	1127	1943	3.3	-21 8	20	-3					
32ND	402.28									65.7	-655.3	55 6	5.1	-10.6
		4 2	-43.3	1127	1943	3.8	-22 3	20	-3					
33RD	414.36									61.5	-612.0	47.9	4.3	-9.9
		4.8	-44.3	1127	1943	4.2	-22.8	21	-4					
34TH	426.44									56.7	-567.7	40 8	3.6	-9.1
		5 3	-45.2	1127	1943	4.7	-23.3	21	-4					
35TH	438.52									51.4	-522.6	34 2	3.0	-8.4
		5.8	-46.1	1127	1943	5.2	-23.7	22	-5					
36TH	450.60									45.6	-476.5	28.2	2.4	-7.6
		6.4	-47.0	1127	1943	5.7	-24.2	22	-5					
37TH	462.68									39 2	-429.4	22.7	1.9	-6.8
		6.0	-47.8	1127	1943	5.3	-24.6	22	-5					
38TH	474.76									33.2	-381.7	17 8	1.4	-5.9
		5.5	-48.5	1127	1943	4 9	-25.0	21	-4					
39TH	486.84									27.8	-333.1	13.5	1.1	-5.1
		5.0	-49.3	1127	1943	4.4	-25.4	20	-4					
40TH	498.92									22 8	-283.8	9 8	.8	-4.3
		4.5	-50.0	1127	1943	4.0	-25.8	20	-3					
41ST	511.00									18.3	-233.8	6.6	.5	-3.6
		4.0	-50.8	1127	1943	3.5	-26.2	19	-3					
42ND	523.08									14 3	-183.0	4.1	.3	-2.8
		4 4	-53.7	1174	2023	3.7	-26.5	20	-3					
43RD	535.66									10.0	-129.3	2 2	2	-2.0
		5.0	-53.9	1206	2078	4.2	-25.9	20	-3					
44TH	548.58									4.9	-75.4	8	.1	-1.1
		3 8	-66.2	1680	2895	2.2	-22.9	17	-2					
	566.58									1 2	-9.2	.1	0	-.2
		1.2	-9.2	1085	2065	1.1	-4 5	28	-6					
	581.67									0.0	0.0	0 0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 330 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-215.8	-1250.9	421.5	-75.6	-26.6
2ND	23.00	-4.1	-29.9	2147	3699	-1.9	-8.1	29	7	-211.7	-1221.1	393.0	-70.7	-25.9
3RD	35.92	-3.1	-18.3	1206	2078	-2.6	-8.8	25	7	-208.6	-1202.8	377.4	-68.0	-25.6
4TH	48.84	-2.6	-17.5	1206	2078	-2.1	-8.4	26	6	-206.1	-1185.3	362.0	-65.3	-25.2
5TH	61.76	-2.2	-17.2	1206	2078	-1.8	-8.3	27	6	-203.9	-1168.1	346.8	-62.6	-24.9
6TH	74.68	-2.1	-17.5	1206	2078	-1.7	-8.4	27	6	-201.8	-1150.6	331.8	-60.0	-24.5
7TH	87.60	-2.0	-17.8	1206	2078	-1.6	-8.6	27	5	-199.8	-1132.8	317.0	-57.4	-24.1
8TH	100.52	-1.8	-18.1	1206	2078	-1.5	-8.7	26	5	-198.0	-1114.8	302.5	-54.9	-23.7
9TH	113.44	-1.7	-18.4	1206	2078	-1.4	-8.8	26	4	-196.3	-1096.4	288.2	-52.3	-23.4
10TH	126.27	-1.6	-18.6	1197	2063	-1.3	-9.0	26	4	-194.7	-1077.8	274.3	-49.8	-23.0
11TH	139.10	-1.6	-18.9	1197	2063	-1.3	-9.2	25	4	-193.1	-1058.9	260.6	-47.3	-22.6
12TH	151.93	-2.0	-19.5	1197	2063	-1.7	-9.4	24	4	-191.1	-1039.5	247.1	-44.8	-22.2
13TH	164.76	-2.5	-20.1	1197	2063	-2.1	-9.7	23	5	-188.6	-1019.4	233.9	-42.4	-21.9
14TH	177.59	-2.9	-20.7	1197	2063	-2.4	-10.0	22	5	-185.7	-998.8	221.0	-40.0	-21.5
15TH	190.42	-3.4	-21.2	1197	2063	-2.8	-10.3	21	6	-182.3	-977.5	208.3	-37.6	-21.1
16TH	203.25	-3.8	-21.8	1197	2063	-3.2	-10.6	20	6	-178.5	-955.7	195.9	-35.3	-20.8
17TH	216.08	-3.9	-22.4	1197	2063	-3.2	-10.9	22	6	-174.6	-933.2	183.8	-33.1	-20.4
18TH	228.66	-4.1	-22.5	1174	2023	-3.5	-11.1	22	7	-170.5	-910.8	172.2	-30.9	-20.0
19TH	241.24	-4.5	-23.0	1174	2023	-3.8	-11.3	23	8	-166.1	-887.8	160.8	-28.8	-19.6
20TH	253.82	-4.8	-23.4	1174	2023	-4.1	-11.6	24	8	-161.2	-864.4	149.8	-26.7	-19.2
21ST	266.40	-5.2	-23.9	1174	2023	-4.5	-11.8	24	9	-156.0	-840.5	139.1	-24.7	-18.8
22ND	278.98	-5.6	-24.4	1174	2023	-4.8	-12.0	25	10	-150.4	-816.1	128.7	-22.8	-18.3
23RD	291.56	-6.0	-24.8	1174	2023	-5.1	-12.3	26	11	-144.4	-791.3	118.6	-20.9	-17.8
24TH	304.14	-6.2	-25.6	1174	2023	-5.3	-12.6	26	11	-138.2	-765.7	108.8	-19.2	-17.3
25TH	316.72	-6.3	-26.7	1174	2023	-5.4	-13.2	26	11	-131.9	-739.0	99.3	-17.5	-16.8
		-6.3	-27.2	1151	1983	-5.5	-13.7	27	11					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 330 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-125.6	-711.8	90.4	-15.9	-16.2
		-6.4	-28.2	1151	1983	-5.6	-14.2	27	10					
27TH	341.38									-119.2	-683.6	81.8	-14.4	-15.6
		-6.5	-29.3	1151	1983	-5.7	-14.8	28	10					
28TH	353.71									-112.6	-654.3	73 5	-12.9	-15.0
		-6.6	-30.3	1151	1983	-5.7	-15.3	28	10					
29TH	366.04									-106.0	-623.9	65.6	-11.6	-14.4
		-5.9	-30.7	1127	1943	-5.2	-15.8	30	10					
30TH	378.12									-100.1	-593.2	58 3	-10.3	-13.7
		-5.5	-31.8	1127	1943	-4.8	-16.4	31	9					
31ST	390.20									-94.7	-561.4	51 3	-9.2	-12.9
		-5.5	-33.0	1127	1943	-4.9	-17.0	31	9					
32ND	402.28									-89.2	-528.4	44.7	-8.1	-12.1
		-5.5	-34.1	1127	1943	-4.9	-17.6	31	9					
33RD	414.36									-83.6	-494.3	38.6	-7.0	-11.3
		-5.6	-35.3	1127	1943	-4.9	-18.1	31	8					
34TH	426.44									-78.1	-459.1	32.8	-6.0	-10.4
		-5.6	-36.4	1127	1943	-5.0	-18.7	31	8					
35TH	438.52									-72.5	-422.7	27.5	-5.1	-9.6
		-5.6	-37.5	1127	1943	-5.0	-19.3	31	8					
36TH	450.60									-66.8	-385.1	22 6	-4.3	-8.6
		-5.6	-38.7	1127	1943	-5.0	-19.9	31	8					
37TH	462.68									-61.2	-346.5	18.2	-3.5	-7.7
		-5.9	-39.2	1127	1943	-5.2	-20.2	30	8					
38TH	474.76									-55.4	-307.3	14.2	-2.8	-6.8
		-6.2	-39.6	1127	1943	-5.5	-20.4	30	8					
39TH	486.84									-49.2	-267 7	10 8	-2.2	-5.9
		-6.5	-40.0	1127	1943	-5.8	-20.6	29	8					
40TH	498.92									-42.7	-227.7	7.8	-1.6	-5.0
		-6.8	-40.4	1127	1943	-6.1	-20.8	28	8					
41ST	511.00									-35.8	-187.3	5 3	-1.1	-4.1
		-7.1	-40.8	1127	1943	-6.3	-21.0	28	8					
42ND	523.08									-29.7	-146.5	3.2	-.8	-3.2
		-7.3	-43.0	1174	2023	-6.2	-21.2	28	8					
43RD	535.66									-21.4	-103.5	1.7	-.4	-2.3
		-6.7	-43.5	1206	2078	-5.6	-20.9	28	7					
44TH	548.58									-14.7	-60.0	.6	-.2	-1.3
		-10.0	-56.1	1680	2895	-6.0	-19.4	24	7					
MR	566.58									-4.7	-4.0	.0	-.0	-.3
		-4.7	-4.0	1085	2065	-4.3	-1.9	-228	-457					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 340 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-344.3	-1054.1	351.1	-137.2	-24.7
2ND	23.00	-2.6	-24.1	2147	3699	-1.2	-6.5	26	5	-341.7	-1030.0	327.1	-129.3	-24.2
3RD	35.92	-1.6	-14.7	1206	2078	-1.4	-7.1	23	4	-340.1	-1015.3	313.9	-124.9	-23.9
4TH	48.84	-1.5	-14.0	1206	2078	-1.3	-6.7	25	5	-338.5	-1001.3	300.9	-120.5	-23.7
5TH	61.76	-1.4	-13.8	1206	2078	-1.2	-6.6	27	5	-337.1	-987.6	288.0	-116.2	-23.4
6TH	74.68	-1.2	-14.2	1206	2078	-1.0	-6.8	28	4	-335.9	-973.3	275.3	-111.8	-23.1
7TH	87.60	-.9	-14.7	1206	2078	-.8	-7.1	28	3	-335.0	-958.6	262.9	-107.5	-22.7
8TH	100.52	-.7	-15.2	1206	2078	-.6	-7.3	29	2	-334.3	-943.5	250.6	-103.2	-22.4
9TH	113.44	-.5	-15.6	1206	2078	-.4	-7.5	30	2	-333.8	-927.8	238.5	-98.8	-22.0
10TH	126.27	-.2	-16.0	1197	2063	-.2	-7.7	31	1	-333.6	-911.9	226.7	-94.6	-21.6
11TH	139.10	-.2	-16.5	1197	2063	-.2	-8.0	31	1	-333.4	-895.4	215.1	-90.3	-21.2
12TH	151.93	-.8	-17.3	1197	2063	-.6	-8.4	30	2	-332.6	-878.1	203.7	-86.0	-20.8
13TH	164.76	-1.4	-18.1	1197	2063	-1.1	-8.8	29	4	-331.2	-860.0	192.6	-81.8	-20.4
14TH	177.59	-1.9	-18.9	1197	2063	-1.6	-9.2	28	5	-329.3	-841.1	181.7	-77.5	-20.0
15TH	190.42	-2.5	-19.7	1197	2063	-2.1	-9.6	27	6	-326.8	-821.3	171.0	-73.3	-19.5
16TH	203.25	-3.1	-20.6	1197	2063	-2.6	-10.0	26	7	-323.7	-800.8	160.6	-69.1	-19.1
17TH	216.08	-3.2	-21.4	1197	2063	-2.6	-10.4	28	7	-320.5	-779.4	150.4	-65.0	-18.6
18TH	228.66	-4.0	-21.3	1174	2023	-3.4	-10.5	28	9	-316.5	-758.1	140.8	-61.0	-18.2
19TH	241.24	-5.0	-21.4	1174	2023	-4.3	-10.6	28	11	-311.5	-736.7	131.4	-57.0	-17.7
20TH	253.82	-6.1	-21.6	1174	2023	-5.2	-10.7	28	14	-305.4	-715.1	122.2	-53.2	-17.3
21ST	266.40	-7.1	-21.8	1174	2023	-6.0	-10.8	29	16	-298.3	-693.3	113.4	-49.4	-16.8
22ND	278.98	-8.1	-21.9	1174	2023	-6.9	-10.8	29	19	-290.2	-671.4	104.8	-45.7	-16.4
23RD	291.56	-9.2	-22.1	1174	2023	-7.8	-10.9	30	21	-281.1	-649.3	96.5	-42.1	-15.9
24TH	304.14	-9.9	-22.6	1174	2023	-8.4	-11.1	30	23	-271.1	-626.7	88.5	-38.6	-15.5
25TH	316.72	-10.3	-23.2	1174	2023	-8.8	-11.5	32	24	-260.8	-603.5	80.7	-35.3	-15.0
		-10.5	-23.4	1151	1983	-9.1	-11.8	33	25					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 340 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
										-250.3	-580.2	73.4	-32.1	-14.5
26TH	329.05	-10.9	-24.0	1151	1983	-9.5	-12.1	34	26					
										-239.4	-556.2	66.4	-29.1	-14.0
27TH	341.38	-11.3	-24.6	1151	1983	-9.8	-12.4	35	27					
										-228.1	-531.6	59.7	-26.2	-13.5
28TH	353.71	-11.7	-25.2	1151	1983	-10.2	-12.7	36	28					
										-216.4	-506.4	53.3	-23.5	-12.9
29TH	366.04	-11.5	-25.3	1127	1943	-10.2	-13.0	38	29					
										-204.9	-481.2	47.4	-20.9	-12.3
30TH	378.12	-11.4	-26.0	1127	1943	-10.1	-13.4	39	29					
										-193.6	-455.1	41.7	-18.5	-11.7
31ST	390.20	-11.5	-26.9	1127	1943	-10.2	-13.9	39	28					
										-182.1	-428.2	36.4	-16.2	-11.0
32ND	402.28	-11.6	-27.8	1127	1943	-10.3	-14.3	39	28					
										-170.5	-400.4	31.4	-14.1	-10.3
33RD	414.36	-11.7	-28.7	1127	1943	-10.4	-14.8	39	27					
										-158.8	-371.7	26.7	-12.1	-9.5
34TH	426.44	-11.8	-29.5	1127	1943	-10.5	-15.2	39	27					
										-146.9	-342.2	22.4	-10.3	-8.7
35TH	438.52	-11.9	-30.4	1127	1943	-10.6	-15.7	39	26					
										-135.0	-311.8	18.4	-8.6	-7.9
36TH	450.60	-11.9	-31.3	1127	1943	-10.5	-16.1	39	25					
										-123.1	-280.5	14.9	-7.0	-7.1
37TH	462.68	-12.2	-31.6	1127	1943	-10.9	-16.2	39	26					
										-110.9	-249.0	11.7	-5.6	-6.3
38TH	474.76	-12.7	-31.8	1127	1943	-11.2	-16.4	39	26					
										-98.2	-217.2	8.8	-4.3	-5.4
39TH	486.84	-13.1	-32.1	1127	1943	-11.6	-16.5	39	27					
										-85.1	-185.1	6.4	-3.2	-4.6
40TH	498.92	-13.5	-32.3	1127	1943	-12.0	-16.6	38	27					
										-71.6	-152.8	4.4	-2.3	-3.8
41ST	511.00	-13.9	-32.6	1127	1943	-12.4	-16.8	38	28					
										-57.7	-120.2	2.7	-1.5	-3.0
42ND	523.08	-14.6	-34.2	1174	2023	-12.4	-16.9	39	28					
										-43.1	-86.1	1.4	-.9	-2.1
43RD	535.66	-14.5	-34.8	1206	2078	-12.0	-16.8	38	27					
										-28.6	-51.2	.5	-.4	-1.2
44TH	548.58	-19.4	-46.6	1680	2895	-11.6	-16.1	31	22					
										-9.2	-4.7	.0	-.1	-.3
MR	566.58	-9.2	-4.7	1085	2065	-8.4	-2.3	-26	-88					
										0.0	0.0	0.0	0.0	0.0
TOP	581.67													

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 350 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-352.6	-859.0	285.8	-144.0	-21.1
2ND	23.00	-.0	-19.7	2147	3699	-.0	-5.3	28	0	-352.5	-839.2	266.3	-135.9	-20.7
3RD	35.92	-.4	-11.4	1206	2078	-.4	-5.5	25	2	-352.1	-827.9	255.5	-131.3	-20.5
4TH	48.84	-.6	-11.0	1206	2078	-.5	-5.3	25	2	-351.5	-816.8	244.9	-126.8	-20.3
5TH	61.76	-.5	-11.0	1206	2078	-.4	-5.3	27	2	-351.0	-805.8	234.4	-122.2	-20.0
6TH	74.68	-.3	-11.5	1206	2078	-.3	-5.5	28	1	-350.6	-794.3	224.1	-117.7	-19.8
7TH	87.60	-.1	-11.9	1206	2078	-.1	-5.7	30	1	-350.5	-782.5	213.9	-113.2	-19.5
8TH	100.52	.1	-12.3	1206	2078	.0	-5.9	31	-0	-350.5	-770.1	203.8	-108.6	-19.2
9TH	113.44	.3	-12.7	1206	2078	.2	-6.1	33	-1	-350.8	-757.4	194.0	-104.1	-18.8
10TH	126.27	.5	-13.1	1197	2063	.4	-6.3	34	-2	-351.3	-744.3	184.3	-99.6	-18.5
11TH	139.10	.5	-13.5	1197	2063	.4	-6.6	35	-2	-351.7	-730.8	174.9	-95.1	-18.1
12TH	151.93	-.2	-14.2	1197	2063	-.2	-6.9	33	1	-351.5	-716.5	165.6	-90.6	-17.7
13TH	164.76	-.9	-14.9	1197	2063	-.8	-7.2	31	3	-350.5	-701.6	156.5	-86.1	-17.4
14TH	177.59	-1.7	-15.7	1197	2063	-1.4	-7.6	30	5	-348.9	-685.9	147.6	-81.6	-17.0
15TH	190.42	-2.4	-16.4	1197	2063	-2.0	-7.9	29	7	-346.5	-669.6	138.9	-77.1	-16.6
16TH	203.25	-3.1	-17.1	1197	2063	-2.6	-8.3	28	8	-343.4	-652.5	130.4	-72.7	-16.3
17TH	216.08	-3.4	-17.8	1197	2063	-2.8	-8.6	29	9	-340.1	-634.7	122.2	-68.3	-15.9
18TH	228.66	-4.4	-17.6	1174	2023	-3.7	-8.7	30	13	-335.7	-617.1	114.3	-64.1	-15.5
19TH	241.24	-5.6	-17.7	1174	2023	-4.8	-8.8	31	16	-330.1	-599.4	106.6	-59.9	-15.1
20TH	253.82	-6.8	-17.8	1174	2023	-5.8	-8.8	32	21	-323.3	-581.6	99.2	-55.8	-14.7
21ST	266.40	-8.0	-17.9	1174	2023	-6.8	-8.8	34	25	-315.3	-563.7	92.0	-51.8	-14.3
22ND	278.98	-9.2	-18.0	1174	2023	-7.8	-8.9	36	31	-306.2	-545.7	85.0	-47.9	-13.9
23RD	291.56	-10.4	-18.0	1174	2023	-8.8	-8.9	39	38	-295.8	-527.7	78.3	-44.1	-13.6
24TH	304.14	-11.2	-18.5	1174	2023	-9.5	-9.1	41	42	-284.6	-509.3	71.8	-40.4	-13.2
25TH	316.72	-11.4	-19.1	1174	2023	-9.7	-9.4	42	43	-273.2	-490.2	65.5	-36.9	-12.8
		-11.4	-19.3	1151	1983	-9.9	-9.7	43	43					

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
WIND DIRECTION 350 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-261.8	-470.9	59.5	-33.6	-12.3
27TH	341.38	-11.7	-19.9	1151	1983	-10.2	-10.0	44	44	-250.1	-451.1	53.9	-30.5	-11.9
28TH	353.71	-11.9	-20.4	1151	1983	-10.4	-10.3	44	44	-238.1	-430.6	48.4	-27.4	-11.4
29TH	366.04	-12.2	-21.0	1151	1983	-10.6	-10.6	45	44	-226.0	-409.6	43.2	-24.6	-10.9
30TH	378.12	-11.9	-21.2	1127	1943	-10.6	-10.9	47	45	-214.0	-388.4	38.4	-21.9	-10.4
31ST	390.20	-11.9	-21.7	1127	1943	-10.5	-11.1	48	45	-202.1	-366.8	33.9	-19.4	-9.8
32ND	402.28	-12.0	-22.1	1127	1943	-10.6	-11.4	48	44	-190.2	-344.6	29.6	-17.0	-9.2
33RD	414.36	-12.1	-22.6	1127	1943	-10.7	-11.6	47	43	-178.1	-322.0	25.5	-14.8	-8.6
34TH	426.44	-12.2	-23.1	1127	1943	-10.8	-11.9	47	42	-165.9	-298.9	21.8	-12.7	-7.9
35TH	438.52	-12.3	-23.6	1127	1943	-10.9	-12.1	47	42	-153.7	-275.3	18.3	-10.8	-7.3
36TH	450.60	-12.4	-24.1	1127	1943	-11.0	-12.4	47	41	-141.3	-251.2	15.1	-9.0	-6.6
37TH	462.68	-12.3	-24.6	1127	1943	-10.9	-12.6	47	40	-129.0	-226.6	12.3	-7.4	-5.9
38TH	474.76	-12.7	-24.9	1127	1943	-11.2	-12.8	47	41	-116.4	-201.8	9.7	-5.9	-5.2
39TH	486.84	-13.1	-25.1	1127	1943	-11.6	-12.9	47	42	-103.2	-176.7	7.4	-4.6	-4.5
40TH	498.92	-13.6	-25.4	1127	1943	-12.0	-13.1	47	43	-89.7	-151.2	5.4	-3.4	-3.8
41ST	511.00	-14.0	-25.7	1127	1943	-12.4	-13.2	47	44	-75.7	-125.6	3.7	-2.4	-3.2
42ND	523.08	-14.4	-26.0	1127	1943	-12.8	-13.4	47	45	-61.3	-99.6	2.4	-1.6	-2.5
43RD	535.66	-15.4	-27.3	1174	2023	-13.1	-13.5	48	46	-45.9	-72.3	1.3	-.9	-1.8
44TH	548.58	-15.6	-27.8	1206	2078	-13.0	-13.4	47	45	-30.3	-44.5	.5	-.4	-1.0
MR	566.58	-20.6	-36.5	1680	2895	-12.3	-12.6	38	37	-9.6	-8.0	.1	-.1	-.3
TOP	581.67	-9.6	-8.0	1085	2065	-8.9	-3.9	-97	-200	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 0 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-290.1	-620.8	192.2	-124.8	-15.4
2ND	23.00	1.3	-15.7	2147	3699	.6	-4.3	28	-4	-291.4	-605.0	178.1	-118.1	-15.1
3RD	35.92	.6	-9.8	1206	2078	.5	-4.7	22	-3	-292.1	-595.2	170.3	-114.4	-14.9
4TH	48.84	.6	-10.0	1206	2078	.5	-4.8	24	-2	-292.7	-585.2	162.7	-110.6	-14.7
5TH	61.76	.6	-10.3	1206	2078	.5	-4.9	26	-3	-293.3	-575.0	155 2	-106.8	-14.5
6TH	74.68	.6	-10.8	1206	2078	.5	-5.2	27	-3	-293.9	-564.2	147.9	-103.0	-14.3
7TH	87.60	.7	-11.2	1206	2078	.5	-5.4	28	-3	-294.6	-553.0	140.6	-99.2	-14.0
8TH	100.52	.7	-11.7	1206	2078	.6	-5.6	30	-3	-295.3	-541.3	133.6	-95.4	-13.7
9TH	113.44	.7	-12.2	1206	2078	.6	-5.9	31	-3	-296.0	-529.1	126.7	-91.6	-13.4
10TH	126.27	.7	-12.6	1197	2063	.6	-6.1	32	-3	-296.7	-516.5	120.0	-87.8	-13.1
11TH	139.10	.6	-13.0	1197	2063	.5	-6.3	33	-3	-297.3	-503.5	113.4	-84.0	-12.8
12TH	151.93	.0	-13.2	1197	2063	.0	-6.4	32	-0	-297.3	-490.2	107.0	-80.2	-12.4
13TH	164.76	-.5	-13.4	1197	2063	-.5	-6.5	32	2	-296.7	-476.8	100.8	-76.3	-12.1
14TH	177.59	-1.1	-13.6	1197	2063	-.9	-6.6	31	4	-295.6	-463.2	94.8	-72.5	-11.8
15TH	190.42	-1.7	-13.8	1197	2063	-1.4	-6.7	31	6	-293.9	-449.4	89.0	-68.8	-11.4
16TH	203.25	-2.3	-14.0	1197	2063	-1.9	-6.8	31	9	-291.7	-435.4	83.3	-65.0	-11.1
17TH	216.08	-2.4	-14.2	1197	2063	-2.0	-6.9	33	10	-289.2	-421.1	77.8	-61.3	-10.7
18TH	228.66	-3.1	-13.9	1174	2023	-2.7	-6.9	34	13	-286.1	-407.2	72.6	-57.7	-10.3
19TH	241.24	-4.0	-13.9	1174	2023	-3.4	-6.9	36	17	-282.1	-393.3	67.5	-54.1	-10.0
20TH	253.82	-4.9	-13.8	1174	2023	-4.1	-6.8	37	22	-277.3	-379.6	62.7	-50.6	-9.6
21ST	266.40	-5.7	-13.7	1174	2023	-4.9	-6.8	40	28	-271.5	-365.8	58 0	-47.1	-9.3
22ND	278.98	-6.6	-13.6	1174	2023	-5.6	-6.7	43	35	-264.9	-352.2	53.5	-43.7	-8.9
23RD	291.56	-7.5	-13.6	1174	2023	-6.4	-6.7	47	44	-257.4	-338.6	49.1	-40.5	-8.6
24TH	304.14	-8.1	-13.5	1174	2023	-6.9	-6.7	51	52	-249.3	-325.1	45.0	-37.3	-8.2
25TH	316.72	-8.5	-13.7	1174	2023	-7.2	-6.8	53	56	-240.8	-311.4	40.9	-34.2	-7.8
		-8.6	-13.5	1151	1983	-7.5	-6.8	56	60					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 0 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-232.2	-297.9	37.2	-31.3	-7.5
27TH	341.38	-8.9	-13.7	1151	1983	-7.8	-6.9	58	64	-223.3	-284.2	33.6	-28.5	-7.1
28TH	353.71	-9.2	-13.8	1151	1983	-8.0	-7.0	61	69	-214.0	-270.4	30.2	-25.8	-6.7
29TH	366.04	-9.6	-13.9	1151	1983	-8.3	-7.0	63	74	-204.5	-256.4	26.9	-23.2	-6.4
30TH	378.12	-9.7	-13.8	1127	1943	-8.6	-7.1	69	83	-194.8	-242.6	23.9	-20.8	-6.0
31ST	390.20	-9.9	-14.0	1127	1943	-8.8	-7.2	70	84	-184.9	-228.6	21.1	-18.5	-5.6
32ND	402.28	-10.1	-14.3	1127	1943	-8.9	-7.4	69	83	-174.9	-214.3	18.4	-16.3	-5.2
33RD	414.36	-10.2	-14.6	1127	1943	-9.1	-7.5	68	81	-164.6	-199.7	15.9	-14.3	-4.8
34TH	426.44	-10.4	-14.9	1127	1943	-9.3	-7.7	66	79	-154.2	-184.8	13.6	-12.3	-4.4
35TH	438.52	-10.6	-15.2	1127	1943	-9.4	-7.8	65	78	-143.6	-169.7	11.4	-10.5	-4.0
36TH	450.60	-10.8	-15.5	1127	1943	-9.6	-8.0	64	76	-132.8	-154.2	9.5	-8.9	-3.6
37TH	462.68	-10.9	-15.7	1127	1943	-9.7	-8.1	63	74	-121.9	-138.5	7.7	-7.3	-3.2
38TH	474.76	-11.2	-15.6	1127	1943	-10.0	-8.0	66	82	-110.6	-122.9	6.1	-5.9	-2.8
39TH	486.84	-11.6	-15.4	1127	1943	-10.3	-7.9	73	94	-99.0	-107.6	4.7	-4.7	-2.4
40TH	498.92	-11.9	-15.1	1127	1943	-10.6	-7.8	82	110	-87.1	-92.5	3.5	-3.5	-2.0
41ST	511.00	-12.3	-14.9	1127	1943	-10.9	-7.7	95	133	-74.8	-77.5	2.5	-2.5	-1.7
42ND	523.08	-12.7	-14.7	1127	1943	-11.2	-7.6	115	169	-62.2	-62.8	1.7	-1.7	-1.3
43RD	535.66	-13.8	-15.1	1174	2023	-11.7	-7.5	176	274	-48.4	-47.7	1.0	-1.0	-.9
44TH	548.58	-15.0	-15.6	1206	2078	-12.4	-7.5	361	590	-33.4	-32.2	.4	-.5	-.6
MR	566.58	-21.5	-22.8	1680	2895	-12.8	-7.9	206	332	-11.9	-9.3	.1	-.1	-.2
TOP	581.67	-11.9	-9.3	1085	2065	-11.0	-4.5	-39	-85	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 10 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-199.6	-389.8	128.0	-89.5	-8.9
2ND	23.00	-.3	-7.4	2147	3699	-.1	-2.0	7	1	-199.3	-382.4	119.1	-84.9	-8.8
3RD	35.92	-.2	-5.2	1206	2078	-.1	-2.5	13	1	-199.1	-377.2	114.2	-82.3	-8.8
4TH	48.84	-.2	-4.4	1206	2078	-.2	-2.1	16	1	-198.9	-372.8	109.3	-79.7	-8.7
5TH	61.76	-.3	-4.1	1206	2078	-.2	-2.0	18	2	-198.6	-368.7	104.5	-77.2	-8.6
6TH	74.68	-.2	-4.6	1206	2078	-.2	-2.2	20	2	-198.4	-364.1	99.8	-74.6	-8.6
7TH	87.60	-.2	-5.0	1206	2078	-.1	-2.4	22	1	-198.2	-359.1	95.1	-72.0	-8.5
8TH	100.52	-.1	-5.4	1206	2078	-.1	-2.6	23	1	-198.1	-353.7	90.5	-69.5	-8.4
9TH	113.44	-.1	-5.9	1206	2078	-.0	-2.8	24	0	-198.0	-347.8	86.0	-66.9	-8.3
10TH	126.27	.0	-6.3	1197	2063	.0	-3.0	25	-0	-198.0	-341.6	81.6	-64.4	-8.1
11TH	139.10	.0	-6.7	1197	2063	.0	-3.2	26	-0	-198.0	-334.9	77.2	-61.8	-8.0
12TH	151.93	-.2	-7.1	1197	2063	-.1	-3.4	28	1	-197.9	-327.8	73.0	-59.3	-7.8
13TH	164.76	-.3	-7.5	1197	2063	-.3	-3.6	29	2	-197.6	-320.3	68.8	-56.8	-7.7
14TH	177.59	-.5	-7.9	1197	2063	-.4	-3.8	31	3	-197.1	-312.3	64.8	-54.2	-7.5
15TH	190.42	-.7	-8.3	1197	2063	-.6	-4.0	32	4	-196.4	-304.0	60.8	-51.7	-7.3
16TH	203.25	-.8	-8.8	1197	2063	-.7	-4.2	33	5	-195.5	-295.2	57.0	-49.2	-7.0
17TH	216.08	-.8	-9.2	1197	2063	-.7	-4.4	36	5	-194.7	-286.1	53.2	-46.7	-6.8
18TH	228.66	-1.1	-9.1	1174	2023	-.9	-4.5	37	7	-193.6	-277.0	49.7	-44.2	-6.5
19TH	241.24	-1.4	-9.2	1174	2023	-1.2	-4.5	37	10	-192.2	-267.8	46.3	-41.8	-6.2
20TH	253.82	-1.8	-9.3	1174	2023	-1.5	-4.6	38	12	-190.4	-258.5	43.0	-39.4	-6.0
21ST	266.40	-2.1	-9.3	1174	2023	-1.8	-4.6	38	15	-188.3	-249.1	39.8	-37.0	-5.7
22ND	278.98	-2.5	-9.4	1174	2023	-2.1	-4.7	39	18	-185.8	-239.7	36.7	-34.7	-5.4
23RD	291.56	-2.9	-9.5	1174	2023	-2.4	-4.7	40	20	-182.9	-230.3	33.7	-32.3	-5.2
24TH	304.14	-3.2	-9.5	1174	2023	-2.7	-4.7	41	23	-179.7	-220.7	30.9	-30.1	-4.9
25TH	316.72	-3.5	-9.6	1174	2023	-3.0	-4.7	41	26	-176.2	-211.2	28.2	-27.8	-4.6
		-3.8	-9.4	1151	1983	-3.3	-4.7	41	28					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 10 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-172.4	-201.7	25.6	-25.7	-4.3
		-4.1	-9.5	1151	1983	-3.5	-4.8	42	31					
27TH	341.38									-168.4	-192.3	23.2	-23.6	-4.1
		-4.4	-9.5	1151	1983	-3.8	-4.8	43	33					
28TH	353.71									-164.0	-182.8	20.9	-21.5	-3.8
		-4.7	-9.5	1151	1983	-4.1	-4.8	43	36					
29TH	366.04									-159.3	-173.2	18.7	-19.5	-3.6
		-5.1	-9.4	1127	1943	-4.5	-4.8	46	42					
30TH	378.12									-154.3	-163.9	16.7	-17.6	-3.3
		-5.6	-9.4	1127	1943	-4.9	-4.9	49	50					
31ST	390.20									-148.7	-154.4	14.7	-15.8	-3.1
		-6.1	-9.5	1127	1943	-5.4	-4.9	53	58					
32ND	402.28									-142.6	-144.9	12.9	-14.1	-2.9
		-6.6	-9.6	1127	1943	-5.9	-4.9	58	68					
33RD	414.36									-136.0	-135.3	11.2	-12.4	-2.6
		-7.1	-9.7	1127	1943	-6.3	-5.0	66	82					
34TH	426.44									-128.9	-125.7	9.7	-10.8	-2.4
		-7.6	-9.7	1127	1943	-6.8	-5.0	76	102					
35TH	438.52									-121.3	-115.9	8.2	-9.3	-2.2
		-8.2	-9.8	1127	1943	-7.2	-5.1	93	131					
36TH	450.60									-113.1	-106.1	6.9	-7.8	-1.9
		-8.7	-9.9	1127	1943	-7.7	-5.1	121	181					
37TH	462.68									-104.5	-96.3	5.6	-6.5	-1.7
		-9.0	-9.9	1127	1943	-8.0	-5.1	152	234					
38TH	474.76									-95.5	-86.3	4.5	-5.3	-1.5
		-9.3	-9.9	1127	1943	-8.2	-5.1	222	356					
39TH	486.84									-86.2	-76.5	3.6	-4.2	-1.3
		-9.6	-9.9	1127	1943	-8.5	-5.1	464	767					
40TH	498.92									-76.6	-66.6	2.7	-3.2	-1.1
		-9.9	-9.9	1127	1943	-8.8	-5.1	$$$$	-3776					
41ST	511.00									-66.7	-56.7	1.9	-2.4	-.9
		-10.2	-9.8	1127	1943	-9.1	-5.1	-297	-525					
42ND	523.08									-56.5	-46.9	1.3	-1.6	-.7
		-11.4	-10.2	1174	2023	-9.7	-5.1	-97	-183					
43RD	535.66									-45.1	-36.6	.8	-1.0	-.5
		-13.0	-10.8	1206	2078	-10.8	-5.2	-46	-94					
44TH	548.58									-32.1	-25.9	.4	-.5	-.3
		-19.9	-16.3	1680	2895	-11.8	-5.6	-37	-77					
MR	566.58									-12.2	-9.6	.1	-.1	-.1
		-12.2	-9.6	1085	2065	-11.2	-4.6	-22	-48					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO 15 COLUMBUS CIRCLE NEW YORK CASE 3
WIND DIRECTION 20 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00													
		-1.0	-1.6	2147	3699	-.4	-.4	-118	-123	-237.9	-126.0	49.0	-108.1	-2.6
2ND	23.00									-236.9	-124.4	46.1	-102.6	-2.7
		-.3	-1.4	1206	2078	-.3	-.7	-21	-9					
3RD	35.92									-236.6	-123.1	44.5	-99.5	-2.7
		-.2	-.7	1206	2078	-.2	-.3	-36	-21					
4TH	48.84									-236.4	-122.4	42.9	-96.5	-2.7
		-.2	-.4	1206	2078	-.2	-.2	-95	-95					
5TH	61.76									-236.1	-122.0	41.3	-93.4	-2.7
		-.3	-.6	1206	2078	-.2	-.3	-73	-64					
6TH	74.68									-235.8	-121.4	39.8	-90.4	-2.7
		-.3	-.7	1206	2078	-.3	-.3	-62	-51					
7TH	87.60									-235.5	-120.7	38.2	-87.3	-2.8
		-.4	-.9	1206	2078	-.3	-.4	-56	-43					
8TH	100.52									-235.1	-119.8	36.6	-84.3	-2.8
		-.4	-1.0	1206	2078	-.4	-.5	-52	-38					
9TH	113.44									-234.7	-118.8	35.1	-81.3	-2.8
		-.5	-1.1	1197	2063	-.4	-.6	-49	-35					
10TH	126.27									-234.2	-117.7	33.6	-78.3	-2.9
		-.5	-1.3	1197	2063	-.5	-.6	-45	-32					
11TH	139.10									-233.6	-116.4	32.1	-75.3	-2.9
		-.6	-1.4	1197	2063	-.5	-.7	-33	-24					
12TH	151.93									-233.0	-115.0	30.6	-72.3	-2.9
		-.7	-1.5	1197	2063	-.6	-.7	-23	-17					
13TH	164.76									-232.4	-113.5	29.1	-69.3	-3.0
		-.7	-1.7	1197	2063	-.6	-.8	-13	-10					
14TH	177.59									-231.6	-111.8	27.7	-66.3	-3.0
		-.8	-1.8	1197	2063	-.7	-.9	-5	-4					
15TH	190.42									-230.8	-110.0	26.3	-63.3	-3.0
		-.9	-1.9	1197	2063	-.7	-.9	2	2					
16TH	203.25									-229.9	-108.1	24.9	-60.4	-3.0
		-.9	-2.0	1197	2063	-.8	-1.0	10	8					
17TH	216.08									-229.0	-106.1	23.5	-57.4	-3.0
		-1.1	-2.1	1174	2023	-1.0	-1.0	17	16					
18TH	228.66									-227.9	-104.1	22.2	-54.6	-2.9
		-1.4	-2.1	1174	2023	-1.2	-1.1	27	30					
19TH	241.24									-226.5	-101.9	20.9	-51.7	-2.9
		-1.6	-2.2	1174	2023	-1.4	-1.1	42	53					
20TH	253.82									-224.8	-99.7	19.6	-48.9	-2.9
		-1.9	-2.3	1174	2023	-1.6	-1.1	69	97					
21ST	266.40									-223.0	-97.4	18.4	-46.1	-2.8
		-2.1	-2.4	1174	2023	-1.8	-1.2	135	207					
22ND	278.98									-220.8	-95.0	17.1	-43.3	-2.8
		-2.4	-2.5	1174	2023	-2.0	-1.2	560	929					
23RD	291.56									-218.4	-92.6	16.0	-40.5	-2.7
		-2.7	-2.4	1174	2023	-2.3	-1.2	-143	-268					
24TH	304.14									-215.7	-90.1	14.8	-37.8	-2.7
		-3.0	-2.4	1174	2023	-2.5	-1.2	-55	-118					
25TH	316.72									-212.7	-87.8	13.7	-35.1	-2.6
		-3.2	-2.3	1151	1983	-2.8	-1.1	-33	-80					

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 20 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-209.5	-85.5	12.6	-32.5	-2.6
27TH	341.38	-3.5	-2.2	1151	1983	-3.1	-1.1	-23	-63	-206.0	-83.3	11.6	-29.9	-2.5
28TH	353.71	-3.8	-2.1	1151	1983	-3.3	-1.1	-17	-53	-202.2	-81.2	10.6	-27.4	-2.4
29TH	366.04	-4.1	-2.1	1151	1983	-3.6	-1.1	-14	-46	-198.0	-79.1	9.6	-24.9	-2.4
30TH	378.12	-4.9	-2.0	1127	1943	-4.3	-1.0	-8	-35	-193.2	-77.1	8.6	-22.6	-2.3
31ST	390.20	-5.8	-2.3	1127	1943	-5.1	-1.2	-8	-33	-187.4	-74.8	7.7	-20.3	-2.2
32ND	402.28	-6.7	-2.7	1127	1943	-5.9	-1.4	-9	-36	-180.7	-72.1	6.8	-18.0	-2.1
33RD	414.36	-7.5	-3.2	1127	1943	-6.7	-1.6	-10	-39	-173.2	-68.9	6.0	-15.9	-2.0
34TH	426.44	-8.4	-3.7	1127	1943	-7.4	-1.9	-11	-41	-164.8	-65.2	5.2	-13.9	-1.9
35TH	438.52	-9.3	-4.2	1127	1943	-8.2	-2.1	-11	-43	-155.5	-61.1	4.4	-11.9	-1.7
36TH	450.60	-10.1	-4.6	1127	1943	-9.0	-2.4	-12	-44	-145.4	-56.4	3.7	-10.1	-1.6
37TH	462.68	-10.9	-5.1	1127	1943	-9.7	-2.6	-13	-46	-134.5	-51.3	3.1	-8.4	-1.4
38TH	474.76	-11.4	-5.2	1127	1943	-10.1	-2.7	-12	-44	-123.1	-46.1	2.5	-6.9	-1.2
39TH	486.84	-11.8	-5.2	1127	1943	-10.4	-2.7	-10	-39	-111.4	-40.9	1.9	-5.4	-1.0
40TH	498.92	-12.2	-5.2	1127	1943	-10.8	-2.7	-9	-36	-99.2	-35.7	1.5	-4.2	-.8
41ST	511.00	-12.6	-5.2	1127	1943	-11.2	-2.7	-8	-32	-86.6	-30.5	1.1	-3.0	-.7
42ND	523.08	-13.0	-5.2	1127	1943	-11.5	-2.7	-7	-29	-73.6	-25.3	.7	-2.1	-.5
43RD	535.66	-15.0	-5.4	1174	2023	-12.8	-2.7	-5	-24	-58.6	-20.0	.5	-1.3	-.4
44TH	548.58	-18.0	-5.6	1206	2078	-14.9	-2.7	-4	-19	-40.6	-14.4	.2	-.6	-.2
MR	566.58	-25.7	-8.1	1680	2895	-15.3	-2.8	-3	-16	-14.8	-6.3	.0	-.1	-.1
TOP	581.67	-14.8	-6.3	1085	2065	-13.7	-3.0	-3	-13	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 30 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-497.3	260.5	-67.0	-202.2	1.7
2ND	23.00	-2.5	9.6	2147	3699	-1.2	2.6	52	-23	-494.8	251.0	-61.1	-190.8	1.3
3RD	35.92	-1.1	5.6	1206	2078	-.9	2.7	41	-14	-493.7	245.4	-57.9	-184.4	1.1
4TH	48.84	-1.1	5.9	1206	2078	-.9	2.8	37	-11	-492.6	239.5	-54.8	-178.0	1.0
5TH	61.76	-1.3	6.1	1206	2078	-1.1	2.9	37	-13	-491.3	233.3	-51.7	-171.6	.8
6TH	74.68	-1.6	6.2	1206	2078	-1.3	3.0	38	-16	-489.7	227.1	-48.7	-165.3	.6
7TH	87.60	-1.9	6.4	1206	2078	-1.6	3.1	39	-20	-487.8	220.7	-45.9	-159.0	.4
8TH	100.52	-2.2	6.5	1206	2078	-1.8	3.1	41	-24	-485.6	214.2	-43.0	-152.7	.2
9TH	113.44	-2.5	6.6	1206	2078	-2.1	3.2	42	-28	-483.0	207.6	-40.3	-146.4	.1
10TH	126.27	-2.8	6.7	1197	2063	-2.4	3.3	44	-32	-480.2	200.9	-37.7	-140.3	-.1
11TH	139.10	-3.2	6.9	1197	2063	-2.7	3.3	46	-36	-477.0	194.0	-35.2	-134.1	-.3
12TH	151.93	-3.7	7.0	1197	2063	-3.1	3.4	47	-42	-473.3	187.0	-32.7	-128.0	-.5
13TH	164.76	-4.2	7.2	1197	2063	-3.5	3.5	49	-49	-469.1	179.8	-30.4	-122.0	-.7
14TH	177.59	-4.7	7.3	1197	2063	-3.9	3.5	52	-56	-464.4	172.5	-28.1	-116.0	-.9
15TH	190.42	-5.2	7.4	1197	2063	-4.3	3.6	55	-66	-459.2	165.1	-25.9	-110.1	-1.1
16TH	203.25	-5.7	7.6	1197	2063	-4.8	3.7	61	-78	-453.5	157.5	-23.9	-104.2	-1.2
17TH	216.08	-6.6	7.7	1197	2063	-5.5	3.7	90	-130	-446.9	149.8	-21.9	-98.4	-1.4
18TH	228.66	-7.0	7.6	1174	2023	-6.0	3.8	151	-236	-439.9	142.2	-20.1	-92.9	-1.5
19TH	241.24	-7.5	7.6	1174	2023	-6.4	3.8	586	-980	-432.5	134.6	-18.3	-87.4	-1.6
20TH	253.82	-7.9	7.6	1174	2023	-6.7	3.8	-240	426	-424.5	127.0	-16.7	-82.0	-1.8
21ST	266.40	-8.4	7.6	1174	2023	-7.1	3.8	-90	168	-416.2	119.4	-15.1	-76.7	-1.9
22ND	278.98	-8.8	7.6	1174	2023	-7.5	3.8	-51	101	-407.3	111.8	-13.7	-71.5	-2.0
23RD	291.56	-9.3	7.6	1174	2023	-7.9	3.8	-34	71	-398.1	104.2	-12.3	-66.4	-2.1
24TH	304.14	-9.7	7.6	1174	2023	-8.3	3.7	-23	51	-388.4	96.6	-11.1	-61.5	-2.2
25TH	316.72	-10.1	7.2	1174	2023	-8.6	3.5	-11	27	-378.3	89.5	-9.9	-56.7	-2.2
		-10.2	6.7	1151	1983	-8.9	3.4	-5	12					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 30 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.65									-368.1	82.8	-8.8	-52.1	-2.3
27TH	341.38	-10.6	6.3	1151	1983	-9.2	3.2	-1	2	-357.5	76.5	-7.8	-47.6	-2.3
28TH	353.71	-10.9	5.9	1151	1983	-9.5	3.0	2	-6	-346.5	70.6	-6.9	-43.3	-2.3
29TH	366.04	-11.3	5.6	1151	1983	-9.8	2.8	4	-13	-335.3	65.0	-6.1	-39.1	-2.2
30TH	378.12	-12.4	5.1	1127	1943	-11.0	2.6	4	-15	-322.8	59.9	-5.3	-35.1	-2.1
31ST	390.20	-13.7	4.9	1127	1943	-12.1	2.5	3	-16	-309.1	55.1	-4.6	-31.3	-2.0
32ND	402.28	-14.6	4.7	1127	1943	-13.0	2.4	3	-16	-294.5	50.3	-4.0	-27.6	-1.9
33RD	414.36	-15.6	4.6	1127	1943	-13.8	2.4	3	-17	-278.9	45.7	-3.4	-24.2	-1.8
34TH	426.44	-16.5	4.5	1127	1943	-14.6	2.3	3	-17	-262.4	41.3	-2.9	-20.9	-1.7
35TH	438.52	-17.5	4.3	1127	1943	-15.5	2.2	3	-18	-245.0	37.0	-2.4	-17.8	-1.6
36TH	450.60	-18.4	4.2	1127	1943	-16.3	2.2	2	-18	-226.6	32.8	-2.0	-15.0	-1.4
37TH	462.68	-19.2	4.0	1127	1943	-17.1	2.1	2	-19	-207.3	28.8	-1.6	-12.4	-1.3
38TH	474.76	-19.6	3.6	1127	1943	-17.4	1.9	2	-18	-187.7	25.1	-1.3	-10.0	-1.1
39TH	486.84	-20.0	3.4	1127	1943	-17.7	1.7	2	-17	-167.8	21.7	-1.0	-7.8	-1.0
40TH	498.92	-20.3	3.1	1127	1943	-18.0	1.6	1	-16	-147.5	18.6	-.8	-5.9	-.8
41ST	511.00	-20.7	2.8	1127	1943	-18.3	1.5	1	-15	-126.8	15.8	-.6	-4.3	-.7
42ND	523.08	-21.0	2.6	1127	1943	-18.6	1.3	1	-13	-105.8	13.2	-.4	-2.9	-.5
43RD	535.66	-23.7	2.4	1174	2023	-20.2	1.2	1	-12	-82.1	10.9	-.3	-1.7	-.4
44TH	548.58	-27.4	2.5	1206	2078	-22.7	1.2	1	-11	-54.7	8.4	-.1	-.8	-.3
MR	566.58	-36.6	5.2	1680	2895	-21.8	1.8	1	-13	-18.1	3.2	-.0	-.1	-.0
TOP	581.67	-18.1	3.2	1085	2065	-16.7	1.5	1	-5	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 40 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-983.6	559.8	-120.2	-346.9	1.1
2ND	23.00	-8.7	25.3	2147	3699	-4.0	6.8	51	-30	-974.9	534.5	-107.6	-324.4	.2
3RD	35.92	-4.1	17.2	1206	2078	-3.4	8.3	41	-17	-970.8	517.3	-100.8	-311.8	-.3
4TH	48.84	-3.9	17.6	1206	2078	-3.3	8.5	37	-14	-966.9	499.7	-94.2	-299.3	-.8
5TH	61.76	-4.8	18.1	1206	2078	-4.0	8.7	37	-16	-962.1	481.6	-87.9	-286.8	-1.3
6TH	74.68	-6.3	18.6	1206	2078	-5.2	9.0	37	-22	-955.8	463.0	-81.8	-274.4	-1.8
7TH	87.60	-7.8	19.2	1206	2078	-6.5	9.2	39	-27	-948.0	443.8	-75.9	-262.1	-2.3
8TH	100.52	-9.3	19.7	1206	2078	-7.7	9.5	41	-33	-938.7	424.2	-70.3	-249.9	-2.8
9TH	113.44	-10.8	20.2	1206	2078	-8.9	9.7	43	-39	-928.0	403.9	-64.9	-237.9	-3.3
10TH	126.27	-12.2	20.6	1197	2063	-10.2	10.0	47	-47	-915.8	383.4	-59.9	-226.0	-3.8
11TH	139.10	-13.6	20.9	1197	2063	-11.4	10.1	51	-57	-902.2	362.4	-55.1	-214.4	-4.3
12TH	151.93	-15.0	20.6	1197	2063	-12.5	10.0	58	-72	-887.1	341.9	-50.6	-202.9	-4.7
13TH	164.76	-16.4	20.2	1197	2063	-13.7	9.8	72	-100	-870.7	321.7	-46.3	-191.6	-5.1
14TH	177.59	-17.8	19.8	1197	2063	-14.9	9.6	112	-172	-853.0	301.8	-42.3	-180.6	-5.5
15TH	190.42	-19.2	19.5	1197	2063	-16.0	9.4	674	-1130	-833.8	282.4	-38.6	-169.8	-5.8
16TH	203.25	-20.6	19.1	1197	2063	-17.2	9.2	-101	186	-813.2	263.3	-35.1	-159.2	-6.0
17TH	216.08	-23.0	18.7	1197	2063	-19.2	9.1	-23	47	-790.2	244.6	-31.8	-148.9	-6.2
18TH	228.66	-23.2	17.6	1174	2023	-19.8	8.7	-13	29	-767.0	227.0	-28.9	-139.1	-6.3
19TH	241.24	-23.6	16.7	1174	2023	-20.1	8.3	-8	19	-743.4	210.3	-26.1	-129.6	-6.4
20TH	253.82	-23.9	15.9	1174	2023	-20.4	7.9	-5	13	-719.5	194.4	-23.6	-120.4	-6.5
21ST	266.40	-24.3	15.1	1174	2023	-20.7	7.4	-3	8	-695.2	179.3	-21.2	-111.5	-6.6
22ND	278.98	-24.6	14.2	1174	2023	-21.0	7.0	-1	3	-670.6	165.1	-19.1	-102.9	-6.6
23RD	291.56	-25.0	13.4	1174	2023	-21.3	6.6	0	-0	-645.7	151.7	-17.1	-94.6	-6.6
24TH	304.14	-25.2	12.6	1174	2023	-21.5	6.2	1	-3	-620.5	139.0	-15.2	-86.7	-6.6
25TH	316.72	-25.3	12.0	1174	2023	-21.5	5.9	2	-6	-595.2	127.1	-13.6	-79.0	-6.5
		-24.8	11.1	1151	1983	-21.6	5.6	3	-10					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 40 CONFIGURATION A REFERENCE PRESSURE 34.6 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05	-24.9	10.5	1151	1983	-21.6	5.3	3	-13	-570.4	115.9	-12.1	-71.8	-6.4
27TH	341.38	-24.9	9.9	1151	1983	-21.6	5.0	4	-15	-545.6	105.4	-10.7	-65.0	-6.3
28TH	353.71	-25.0	9.2	1151	1983	-21.7	4.7	4	-18	-520.6	95.6	-9.5	-58.4	-6.2
29TH	366.04	-26.2	8.5	1127	1943	-23.3	4.4	4	-20	-495.7	86.3	-8.3	-52.1	-6.0
30TH	378.12	-27.4	7.7	1127	1943	-24.3	4.0	4	-22	-469.5	77.9	-7.3	-46.3	-5.7
31ST	390.20	-27.9	6.9	1127	1943	-24.7	3.6	3	-23	-442.0	70.2	-6.4	-40.8	-5.5
32ND	402.28	-28.3	6.1	1127	1943	-25.1	3.2	3	-23	-414.2	63.3	-5.6	-35.6	-5.2
33RD	414.36	-28.7	5.4	1127	1943	-25.5	2.8	3	-24	-385.9	57.1	-4.9	-30.8	-4.9
34TH	426.44	-29.1	4.6	1127	1943	-25.8	2.4	2	-25	-357.2	51.7	-4.3	-26.3	-4.6
35TH	438.52	-29.6	3.8	1127	1943	-26.2	2.0	2	-26	-328.0	47.1	-3.7	-22.2	-4.3
36TH	450.60	-29.9	3.0	1127	1943	-26.5	1.6	2	-27	-298.5	43.3	-3.1	-18.4	-3.9
37TH	462.68	-29.6	3.1	1127	1943	-26.3	1.6	2	-28	-268.6	40.3	-2.6	-14.9	-3.5
38TH	474.76	-29.3	3.3	1127	1943	-26.0	1.7	2	-27	-239.0	37.2	-2.1	-11.9	-3.2
39TH	486.84	-29.1	3.5	1127	1943	-25.8	1.8	2	-27	-209.7	33.9	-1.7	-9.2	-2.8
40TH	498.92	-28.8	3.7	1127	1943	-25.5	1.9	2	-27	-180.6	30.4	-1.3	-6.8	-2.4
41ST	511.00	-28.5	3.9	1127	1943	-25.3	2.0	2	-27	-151.8	26.7	-1.0	-4.8	-2.1
42ND	523.08	-30.8	4.2	1174	2023	-26.3	2.1	2	-26	-123.3	22.9	-.7	-3.1	-1.7
43RD	535.66	-33.7	4.8	1206	2078	-27.9	2.3	2	-27	-92.5	18.6	-.4	-1.8	-1.3
44TH	548.58	-42.2	8.6	1680	2895	-25.1	3.0	4	-34	-58.8	13.8	-.2	-.8	-.9
MR	566.58	-16.6	5.2	1085	2065	-15.3	2.5	7	-37	-16.6	5.2	-.0	-.1	-.3
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 5¢ CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-1207.7	822.6	-188.1	-402.3	9.1
2ND	23.00	-16.8	45.7	2147	3699	-7.8	12.3	43	-27	-1190.9	776.9	-169.7	-374.7	7.7
3RD	35.92	-7.9	28.2	1206	2079	-6.6	13.6	33	-16	-1182.9	748.7	-159.8	-359.4	7.0
4TH	48.84	-7.0	28.1	1206	2078	-5.8	13.5	29	-12	-1175.9	720.6	-150.3	-344.2	6.4
5TH	61.76	-7.8	28.1	1206	2078	-6.5	13.5	28	-13	-1168.1	692.5	-141.2	-329.0	5.8
6TH	74.68	-10.0	28.1	1206	2078	-8.3	13.5	30	-18	-1158.1	664.4	-132.4	-314.0	5.2
7TH	87.60	-12.2	28.2	1206	2078	-10.1	13.6	32	-24	-1145.9	636.2	-124.0	-299.1	4.7
8TH	100.52	-14.4	28.2	1206	2078	-11.9	13.6	35	-31	-1131.5	608.0	-116.0	-284.4	4.1
9TH	113.44	-16.6	28.3	1206	2078	-13.7	13.6	40	-40	-1115.0	579.7	-108.3	-269.9	3.5
10TH	126.27	-18.6	28.1	1197	2063	-15.5	13.6	46	-52	-1096.4	551.6	-101.1	-255.7	2.9
11TH	139.10	-20.6	27.9	1197	2063	-17.2	13.5	58	-73	-1075.7	523.7	-94.2	-241.8	2.3
12TH	151.93	-22.1	26.9	1197	2063	-18.5	13.0	78	-110	-1053.6	496.8	-87.6	-228.1	1.8
13TH	164.76	-23.6	25.8	1197	2063	-19.7	12.5	147	-228	-1030.0	471.0	-81.4	-214.7	1.3
14TH	177.59	-25.1	24.8	1197	2063	-21.0	12.0	-941	1621	-1004.9	446.2	-75.5	-201.7	.8
15TH	190.42	-26.6	23.8	1197	2063	-22.2	11.5	-86	164	-978.3	422.4	-70.0	-189.0	.4
16TH	203.25	-28.1	22.8	1197	2063	-23.5	11.0	-39	81	-950.2	399.6	-64.7	-176.6	.0
17TH	216.08	-31.1	21.8	1197	2063	-26.0	10.5	-16	40	-919.0	377.9	-59.7	-164.6	-.3
18TH	228.66	-31.2	20.4	1174	2023	-26.6	10.1	-12	30	-887.8	357.4	-55.1	-153.2	-.5
19TH	241.24	-31.5	19.6	1174	2023	-26.8	9.7	-9	25	-856.3	337.9	-50.7	-142.3	-.8
20TH	253.82	-31.7	18.7	1174	2023	-27.0	9.2	-7	20	-824.6	319.1	-46.6	-131.7	-1.0
21ST	266.40	-32.0	17.8	1174	2023	-27.3	8.8	-5	16	-792.6	301.3	-42.7	-121.5	-1.1
22ND	278.98	-32.3	17.0	1174	2023	-27.5	8.4	-4	13	-760.3	284.3	-39.0	-111.8	-1.3
23RD	291.56	-32.5	16.1	1174	2023	-27.7	8.0	-3	10	-727.8	268.2	-35.5	-102.4	-1.4
24TH	304.14	-32.6	15.3	1174	2023	-27.7	7.6	-2	7	-695.2	252.9	-32.2	-93.4	-1.5
25TH	316.72	-32.3	14.9	1174	2023	-27.5	7.3	-2	6	-663.0	238.0	-29.1	-84.9	-1.5
		-31.4	14.1	1151	1983	-27.3	7.1	-1	5					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 34 0 PSF GUST FACTOR 1 32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05	-31.1	13.7	1151	1983	-27.0	6.9	-1	3	-631.6	223.9	-26.3	-76.9	-1.6
27TH	341.38	-30.8	13.2	1151	1983	-26.8	6.7	-0	2	-600.5	210.3	-23.6	-69.3	-1.6
28TH	353.71	-30.5	12.7	1151	1983	-26.5	6.4	-0	0	-569.7	197.1	-21.1	-62.1	-1.7
29TH	366.04	-31.4	12.0	1127	1943	-27.8	6.2	0	-2	-539.1	184.3	-18.8	-55.3	-1.7
30TH	378.12	-32.1	11.8	1127	1943	-28.5	6.0	1	-3	-507.8	172.3	-16.6	-49.0	-1.6
31ST	390.20	-32.1	11.5	1127	1943	-28.5	5.9	1	-4	-475.6	160.5	-14.6	-43.0	-1.6
32ND	402.28	-32.1	11.3	1127	1943	-28.5	5.8	1	-4	-443.5	149.0	-12.7	-37.5	-1.5
33RD	414.36	-32.1	11.0	1127	1943	-28.5	5.7	1	-4	-411.4	137.7	-11.0	-32.3	-1.5
34TH	426.44	-32.1	10.8	1127	1943	-28.5	5.6	1	-4	-379.3	126.7	-9.4	-27.5	-1.4
35TH	438.52	-32.1	10.6	1127	1943	-28.5	5.4	1	-5	-347.2	115.8	-7.9	-23.1	-1.4
36TH	450.60	-31.9	10.3	1127	1943	-28.3	5.3	1	-5	-315.1	105.3	-6.6	-19.1	-1.3
37TH	462.68	-31.7	10.2	1127	1943	-28.1	5.3	1	-6	-283.1	94.9	-5.4	-15.5	-1.2
38TH	474.76	-31.5	10.2	1127	1943	-27.9	5.2	1	-7	-251.4	84.7	-4.3	-12.3	-1.2
39TH	486.84	-31.3	10.1	1127	1943	-27.7	5.2	1	-8	-219.9	74.5	-3.3	-9.4	-1.1
40TH	498.92	-31.1	10.1	1127	1943	-27.5	5.2	2	-9	-188.7	64.4	-2.5	-7.0	-1.0
41ST	511.00	-30.8	10.0	1127	1943	-27.3	5.2	2	-9	-157.6	54.3	-1.8	-4.9	-.9
42ND	523.08	-33.6	10.4	1174	2023	-28.1	5.1	2	-10	-126.8	44.3	-1.2	-3.2	-.7
43RD	535.66	-34.9	10.8	1206	2078	-29.0	5.2	2	-12	-93.8	33.9	-.7	-1.8	-.6
44TH	548.58	-42.8	16.2	1680	2895	-25.5	5.6	4	-17	-58.9	23.1	-.3	-.8	-.4
MR	566.58	-16.1	7.9	1085	2065	-14.8	3.4	4	-17	-16.1	7.0	-.1	-.1	-.1
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 60 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-1118.8	1161.1	-297.8	-370.3	19.1
2ND	23.00	-20.4	58.6	2147	3699	-9.5	15.9	36	-21	-1098.4	1102.2	-271.8	-344.8	17.6
3RD	35.92	-8.9	36.4	1206	2078	-7.4	17.5	25	-11	-1089.4	1065.9	-257.8	-330.7	16.9
4TH	48.84	-6.6	34.7	1206	2078	-5.4	16.7	22	-7	-1082.9	1031.2	-244.3	-316.7	16.3
5TH	61.76	-6.5	33.5	1206	2078	-5.4	16.1	22	-7	-1076.3	997.7	-231.1	-302.7	15.7
6TH	74.68	-8.6	33.1	1206	2078	-7.1	15.9	23	-10	-1067.8	964.6	-218.5	-288.9	15.2
7TH	87.60	-10.6	32.6	1206	2078	-8.8	15.7	25	-14	-1057.2	932.0	-206.2	-275.1	14.6
8TH	100.52	-12.6	32.1	1206	2078	-10.5	15.5	27	-18	-1044.6	899.9	-194.4	-261.6	14.0
9TH	113.44	-14.6	31.7	1206	2078	-12.1	15.2	30	-24	-1029.9	868.2	-183.0	-248.2	13.4
10TH	126.27	-16.5	31.0	1197	2063	-13.8	15.0	35	-31	-1013.4	837.2	-172.0	-235.1	12.8
11TH	139.10	-18.4	30.5	1197	2063	-15.4	14.8	40	-41	-994.9	806.7	-161.5	-222.2	12.1
12TH	151.93	-20.0	30.2	1197	2063	-16.7	14.6	44	-59	-974.9	776.6	-151.3	-209.5	11.5
13TH	164.76	-21.6	29.8	1197	2063	-18.0	14.5	50	-62	-953.3	746.7	-141.5	-197.2	11.0
14TH	177.59	-23.2	29.5	1197	2063	-19.4	14.3	61	-81	-930.1	717.2	-132.2	-185.1	10.4
15TH	190.42	-24.8	29.2	1197	2063	-20.7	14.2	80	-116	-905.4	688.0	-123.1	-173.3	9.9
16TH	203.25	-26.3	28.9	1197	2063	-22.0	14.0	130	-201	-879.0	659.1	-114.5	-161.9	9.4
17TH	216.08	-29.0	28.6	1197	2063	-24.2	13.8	-703	1214	-850.1	630.6	-106.2	-150.8	8.9
18TH	228.66	-29.1	27.4	1174	2023	-24.8	13.5	-152	276	-820.9	603.2	-98.5	-140.3	8.5
19TH	241.24	-29.5	26.7	1174	2023	-25.1	13.2	-92	173	-791.5	576.5	-91.0	-130.1	8.0
20TH	253.82	-29.8	26.0	1174	2023	-25.4	12.8	-65	126	-761.7	550.5	-84.0	-120.3	7.6
21ST	266.40	-30.2	25.3	1174	2023	-25.7	12.5	-49	99	-731.5	525.2	-77.2	-111.0	7.2
22ND	278.98	-30.5	24.6	1174	2023	-26.0	12.2	-39	82	-701.0	500.6	-70.7	-101.9	6.8
23RD	291.56	-30.8	23.9	1174	2023	-26.3	11.8	-32	70	-670.2	476.7	-64.6	-93.3	6.4
24TH	304.14	-30.9	23.4	1174	2023	-26.3	11.6	-28	64	-639.2	453.3	-58.7	-85.1	6.0
25TH	316.72	-30.5	23.2	1174	2023	-26.0	11.5	-28	63	-608.7	430.1	-53.2	-77.2	5.6
		-29.6	22.5	1151	1983	-25.7	11.4	-28	62					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 60 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-579.2	407.6	-48.0	-69.9	5.3
27TH	341.38	-29.2	22.3	1151	1983	-25.4	11.3	-27	61	-550.0	385.3	-43.1	-62.9	4.9
28TH	353.71	-28.8	22.1	1151	1983	-25.0	11.2	-27	60	-521.1	363.1	-38.5	-56.3	4.6
29TH	366.04	-28.5	21.9	1151	1983	-24.7	11.0	-26	58	-492.7	341.2	-34.2	-50.1	4.3
30TH	378.12	-28.6	21.3	1127	1943	-25.4	10.9	-21	48	-464.0	320.0	-30.2	-44.3	4.0
31ST	390.20	-29.2	21.1	1127	1943	-25.9	10.9	-19	44	-434.8	298.8	-26.4	-38.9	3.7
32ND	402.28	-29.5	21.0	1127	1943	-26.1	10.8	-18	43	-405.3	277.8	-23.0	-33.8	3.4
33RD	414.36	-29.7	20.9	1127	1943	-26.3	10.8	-17	42	-375.6	256.8	-19.7	-29.1	3.1
34TH	426.44	-29.9	20.8	1127	1943	-26.5	10.7	-17	41	-345.7	236.0	-16.8	-24.7	2.8
35TH	438.52	-30.2	20.7	1127	1943	-26.8	10.7	-16	40	-315.5	215.3	-14.0	-20.7	2.5
36TH	450.60	-30.4	20.6	1127	1943	-27.0	10.6	-16	40	-285.2	194.6	-11.6	-17.1	2.2
37TH	462.68	-30.4	20.5	1127	1943	-27.0	10.6	-15	39	-254.7	174.1	-9.3	-13.9	1.9
38TH	474.76	-29.9	20.3	1127	1943	-26.5	10.4	-15	39	-224.9	153.8	-7.3	-11.0	1.6
39TH	486.84	-29.2	20.0	1127	1943	-25.9	10.3	-15	38	-195.7	133.7	-5.6	-8.4	1.3
40TH	498.92	-28.6	19.8	1127	1943	-25.3	10.2	-16	38	-167.1	113.9	-4.1	-6.2	1.1
41ST	511.00	-27.9	19.5	1127	1943	-24.8	10.1	-16	38	-139.2	94.4	-2.9	-4.4	.8
42ND	523.08	-27.3	19.3	1127	1943	-24.2	9.9	-16	37	-111.9	75.1	-1.8	-2.9	.6
43RD	535.66	-28.4	19.8	1174	2023	-24.2	9.8	-14	35	-83.5	55.3	-1.0	-1.6	.3
44TH	548.58	-29.5	20.2	1206	2078	-24.5	9.7	-11	28	-54.0	35.1	-.4	-.7	.1
MR	566.58	-38.3	28.3	1680	2895	-22.8	9.8	-6	13	-15.6	6.8	-.1	-.1	.0
TOP	581.67	-15.6	6.8	1085	2065	-14.4	3.3	-0	1	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 70 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-1221.6	1476.6	-406.8	-388.9	30.3
2ND	23.00	-37.0	64.3	2147	3699	-17.2	17.4	52	-51	-1184.7	1412.4	-373.6	-361.2	28.5
3RD	35.92	-17.5	39.1	1206	2078	-14.5	18.8	32	-24	-1167.1	1373.3	-355.6	-346.1	27.7
4TH	48.84	-16.1	36.5	1206	2078	-13.4	17.6	28	-21	-1151.0	1336.8	-338.1	-331.1	27.1
5TH	61.76	-16.6	35.2	1206	2078	-13.7	16.9	29	-23	-1134.4	1301.6	-321.1	-316.3	26.4
6TH	74.68	-17.1	35.4	1206	2078	-14.2	17.0	30	-25	-1117.3	1266.2	-304.5	-301.8	25.8
7TH	87.60	-17.7	35.6	1206	2078	-14.7	17.1	31	-27	-1099.6	1230.6	-288.4	-287.4	25.1
8TH	100.52	-18.3	35.9	1206	2078	-15.2	17.3	33	-28	-1081.3	1194.7	-272.7	-273.4	24.4
9TH	113.44	-18.8	36.1	1206	2078	-15.6	17.4	34	-30	-1062.5	1158.7	-257.5	-259.5	23.7
10TH	126.27	-19.3	36.9	1197	2063	-16.1	17.5	35	-32	-1043.2	1122.6	-242.8	-246.0	23.0
11TH	139.10	-19.9	36.1	1197	2063	-16.6	17.5	37	-35	-1023.3	1086.5	-228.7	-232.7	22.2
12TH	151.93	-20.9	35.8	1197	2063	-17.4	17.3	39	-38	-1002.4	1050.7	-215.0	-219.7	21.5
13TH	164.76	-21.8	35.5	1197	2063	-18.2	17.2	41	-43	-980.6	1015.2	-201.7	-207.0	20.8
14TH	177.59	-22.7	35.1	1197	2063	-19.0	17.0	43	-48	-957.9	980.1	-188.9	-194.6	20.1
15TH	190.42	-23.7	34.8	1197	2063	-19.8	16.9	46	-54	-934.2	945.3	-176.6	-182.5	19.4
16TH	203.25	-24.6	34.5	1197	2063	-20.6	16.7	50	-61	-909.6	910.8	-164.7	-170.6	18.7
17TH	216.08	-26.7	34.2	1197	2063	-22.3	16.6	62	-82	-882.9	876.6	-153.2	-159.1	18.0
18TH	228.66	-27.2	33.1	1174	2023	-23.2	16.4	75	-104	-855.7	843.5	-142.4	-148.2	17.4
19TH	241.24	-28.0	32.8	1174	2023	-23.9	16.2	93	-135	-827.6	810.7	-132.0	-137.6	16.7
20TH	253.82	-28.9	32.4	1174	2023	-24.6	16.0	123	-186	-798.7	778.3	-122.0	-127.4	16.1
21ST	266.40	-29.7	32.0	1174	2023	-25.3	15.8	184	-290	-769.0	746.3	-112.4	-117.5	15.4
22ND	278.98	-30.6	31.7	1174	2023	-26.0	15.7	377	-618	-738.4	714.6	-103.2	-108.0	14.8
23RD	291.56	-31.4	31.3	1174	2023	-26.8	15.5	$$$$	7974	-707.0	683.2	-94.4	-98.9	14.1
24TH	304.14	-31.8	31.1	1174	2023	-27.1	15.4	-565	985	-675.2	652.2	-86.0	-90.2	13.4
25TH	316.72	-31.6	31.1	1174	2023	-26.9	15.3	-810	1402	-643.6	621.1	-78.0	-81.9	12.8
		-30.7	30.4	1151	1983	-26.7	15.3	$$$$	2413					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 70 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-613.0	590.7	-70.5	-74.2	12.1
27TH	341.38	-30.4	30.4	1151	1983	-26.5	15.3	$$$$	8441	-582.5	560.3	-63.4	-66.8	11.4
28TH	353.71	-30.2	30.3	1151	1983	-26.2	15.3	3328	-5641	-552.3	530.0	-56.7	-59.8	10.8
29TH	366.04	-30.0	30.3	1151	1983	-26.0	15.3	1256	-2114	-522.3	499.7	-50.4	-53.2	10.1
30TH	378.12	-30.3	29.6	1127	1943	-26.9	15.3	-585	1018	-492.0	470.1	-44.5	-47.1	9.5
31ST	390.20	-30.9	29.7	1127	1943	-27.4	15.3	-321	569	-461.1	440.4	-39.0	-41.3	8.8
32ND	402.28	-31.1	29.8	1127	1943	-27.6	15.4	-312	553	-430.0	410.5	-33.9	-35.9	8.2
33RD	414.36	-31.3	30.0	1127	1943	-27.7	15.4	-303	538	-398.7	380.6	-29.1	-30.9	7.5
34TH	426.44	-31.5	30.1	1127	1943	-27.9	15.5	-294	524	-367.2	350.5	-24.7	-26.3	6.9
35TH	438.52	-31.6	30.2	1127	1943	-28.1	15.6	-287	510	-335.6	320.2	-20.6	-22.1	6.2
36TH	450.60	-31.8	30.4	1127	1943	-28.2	15.6	-279	498	-303.8	289.9	-16.9	-18.2	5.6
37TH	462.68	-31.8	30.5	1127	1943	-28.2	15.7	-297	528	-272.0	259.4	-13.6	-14.7	4.9
38TH	474.76	-31.4	30.4	1127	1943	-27.9	15.7	-390	687	-240.5	229.0	-10.7	-11.6	4.3
39TH	486.84	-31.0	30.3	1127	1943	-27.5	15.6	-516	901	-209.5	198.7	-8.1	-8.9	3.6
40TH	498.92	-30.6	30.1	1127	1943	-27.1	15.5	-773	1338	-178.9	168.6	-5.9	-6.6	3.0
41ST	511.00	-30.2	30.0	1127	1943	-26.8	15.4	$$$$	2711	-148.7	138.7	-4.0	-4.6	2.4
42ND	523.08	-29.8	29.8	1127	1943	-26.4	15.3	$$$$$$$$$		-118.9	108.9	-2.5	-3.0	1.8
43RD	535.66	-31.2	30.9	1174	2023	-26.6	15.3	$$$$	1781	-87.7	78.0	-1.3	-1.7	1.1
44TH	548.58	-32.3	31.1	1206	2078	-26.8	15.0	-294	519	-55.4	46.9	-.5	-.8	.6
MR	566.58	-40.1	40.5	1680	2895	-23.9	14.0	792	-1334	-15.3	6.4	-.0	-.1	.1
TOP	581.67	-15.3	6.4	1085	2065	-14.1	3.1	-2	8	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT.) X	AREA (SQ FT.) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-1099.3	1689.9	-489.7	-338.9	42.0
2ND	23.00	-42.3	61.6	2147	3699	-19.7	16.7	68	-80	-1057.1	1628.3	-451.5	-314.1	40.2
3RD	35.92	-20.2	38.1	1206	2078	-16.8	18.3	38	-34	-1036.9	1590.2	-430.7	-300.6	39.4
4TH	48.84	-19.5	36.0	1206	2078	-16.2	17.3	36	-33	-1017.4	1554.2	-410.4	-287.3	38.6
5TH	61.76	-20.0	35.0	1206	2078	-16.5	16.8	38	-37	-997.4	1519.2	-390.6	-274.3	37.9
6TH	74.68	-19.7	35.3	1206	2078	-16.4	17.0	39	-37	-977.7	1483.9	-371.2	-261.5	37.2
7TH	87.60	-19.5	35.6	1206	2078	-16.2	17.1	39	-37	-958.2	1448.3	-352.2	-249.0	36.4
8TH	100.52	-19.3	35.9	1206	2078	-16.0	17.3	40	-37	-938.9	1412.4	-333.8	-236.8	35.6
9TH	113.44	-19.1	36.2	1206	2078	-15.8	17.4	41	-37	-919.8	1376.2	-315.7	-224.9	34.7
10TH	126.27	-18.8	36.3	1197	2063	-15.7	17.6	42	-37	-901.0	1339.9	-298.3	-213.1	33.8
11TH	139.10	-18.7	36.6	1197	2063	-15.6	17.7	42	-37	-882.3	1303.3	-281.4	-201.7	32.9
12TH	151.93	-19.2	36.9	1197	2063	-16.1	17.9	43	-38	-863.1	1266.4	-264.9	-190.5	32.0
13TH	164.76	-19.7	37.2	1197	2063	-16.5	18.0	43	-39	-843.3	1229.2	-248.9	-179.5	31.1
14TH	177.59	-20.3	37.6	1197	2063	-16.9	18.2	43	-39	-823.1	1191.6	-233.3	-168.8	30.2
15TH	190.42	-20.8	37.9	1197	2063	-17.4	18.4	43	-40	-802.3	1153.7	-218.3	-158.4	29.2
16TH	203.25	-21.3	38.2	1197	2063	-17.8	18.5	43	-41	-780.9	1115.5	-203.7	-148.2	28.3
17TH	216.08	-22.4	38.6	1197	2063	-18.7	18.7	44	-44	-758.5	1076.9	-189.7	-138.4	27.4
18TH	228.66	-22.6	37.9	1174	2023	-19.2	18.7	46	-47	-735.9	1039.1	-176.4	-129.0	26.5
19TH	241.24	-23.1	37.8	1174	2023	-19.7	18.7	48	-50	-712.8	1001.2	-163.5	-119.9	25.6
20TH	253.82	-23.7	37.8	1174	2023	-20.1	18.7	50	-53	-689.1	963.5	-151.2	-111.0	24.7
21ST	266.40	-24.2	37.7	1174	2023	-20.6	18.6	52	-57	-665.0	925.7	-139.3	-102.5	23.8
22ND	278.98	-24.7	37.7	1174	2023	-21.0	18.6	55	-61	-640.3	888.1	-127.9	-94.3	22.8
23RD	291.56	-25.2	37.6	1174	2023	-21.5	18.6	58	-66	-615.0	850.4	-116.9	-86.4	21.9
24TH	304.14	-25.6	37.7	1174	2023	-21.8	18.6	60	-69	-589.4	812.7	-106.5	-78.8	20.9
25TH	316.72	-25.9	38.0	1174	2023	-22.1	18.8	61	-70	-563.5	774.8	-96.5	-71.6	19.9
		-25.6	37.5	1151	1983	-22.3	18.9	61	-71					

TABLE 7. SHEAR AND MOMENT DIAGRAMS NO. 15 COLUMBUS CIRCLE NEW YORK CASE 3
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-537.9	737.3	-87.2	-64.8	18.9
27TH	341.38	-25.9	37.8	1151	1983	-22.5	19.0	62	-72	-512.0	699.5	-78.3	-58.3	17.9
28TH	353.71	-26.1	38.0	1151	1983	-22.7	19.2	63	-73	-485.9	661.5	-69.9	-52.2	16.9
29TH	366.04	-26.3	38.3	1151	1983	-22.9	19.3	63	-74	-459.6	623.2	-62.0	-46.3	15.9
30TH	378.12	-27.0	37.8	1127	1943	-23.9	19.4	68	-83	-432.6	585.4	-54.7	-41.0	14.9
31ST	390.20	-27.6	37.9	1127	1943	-24.5	19.5	71	-88	-405.0	547.5	-47.9	-35.9	13.9
32ND	402.28	-27.8	38.0	1127	1943	-24.6	19.5	72	-89	-377.2	509.6	-41.5	-31.2	12.9
33RD	414.36	-27.9	38.0	1127	1943	-24.8	19.6	73	-91	-349.3	471.6	-35.6	-26.8	11.9
34TH	426.44	-28.1	38.0	1127	1943	-24.9	19.6	74	-93	-321.1	433.5	-30.1	-22.7	10.8
35TH	438.52	-28.3	38.1	1127	1943	-25.1	19.6	75	-94	-292.8	395.5	-25.1	-19.0	9.8
36TH	450.60	-28.5	38.1	1127	1943	-25.3	19.6	76	-96	-264.4	357.4	-20.5	-15.7	8.8
37TH	462.68	-28.5	38.1	1127	1943	-25.3	19.6	75	-96	-235.9	319.3	-16.4	-12.6	7.8
38TH	474.76	-28.0	38.0	1127	1943	-24.8	19.6	71	-90	-207.9	281.3	-12.8	-10.0	6.8
39TH	486.84	-27.5	37.9	1127	1943	-24.4	19.5	68	-84	-180.4	243.4	-9.6	-7.6	5.8
40TH	498.92	-27.0	37.7	1127	1943	-23.9	19.4	65	-79	-153.4	205.7	-6.9	-5.6	4.9
41ST	511.00	-26.5	37.5	1127	1943	-23.5	19.3	62	-74	-126.9	168.1	-4.7	-3.9	4.0
42ND	523.08	-26.0	37.4	1127	1943	-23.0	19.2	59	-69	-100.9	130.8	-2.9	-2.5	3.1
43RD	535.66	-26.9	38.8	1174	2023	-22.9	19.2	58	-68	-74.0	92.0	-1.5	-1.4	2.1
44TH	548.58	-27.2	38.9	1206	2078	-22.6	18.7	57	-68	-46.8	53.1	-.5	-.6	1.2
MR	566.58	-33.4	49.8	1680	2895	-19.9	17.2	47	-54	-13.5	3.3	-.0	-.1	.2
TOP	581.67	-13.5	3.3	1085	2065	-12.4	1.6	-4	30	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-829.2	1912.2	-561.0	-244.0	43.8
2ND	23.00	-44.0	65.7	2147	3699	-20.5	17.7	60	-68	-785.2	1846.6	-517.8	-225.5	42.0
3RD	35.92	-20.5	40.1	1206	2078	-17.0	19.3	33	-29	-764.7	1806.5	-494.2	-215.4	41.3
4TH	48.84	-18.0	38.3	1206	2078	-15.0	18.4	30	-24	-746.7	1768.2	-471.1	-205.7	40.5
5TH	61.76	-17.2	37.6	1206	2078	-14.3	18.1	30	-23	-729.5	1730.7	-448.5	-196.1	39.8
6TH	74.68	-16.7	38.4	1206	2078	-13.9	18.5	30	-22	-712.8	1692.3	-426.3	-186.9	39.1
7TH	87.60	-16.2	39.1	1206	2078	-13.4	18.8	30	-21	-696.6	1653.1	-404.7	-177.7	38.3
8TH	100.52	-15.7	39.9	1206	2078	-13.0	19.2	30	-20	-680.9	1613.2	-383.6	-168.8	37.5
9TH	113.44	-15.1	40.7	1206	2078	-12.6	19.6	31	-19	-665.8	1572.5	-363.1	-160.1	36.6
10TH	126.27	-14.5	41.2	1197	2063	-12.1	20.0	31	-19	-651.3	1531.3	-343.1	-151.7	35.7
11TH	139.10	-14.2	41.9	1197	2063	-11.9	20.3	31	-18	-637.1	1489.4	-323.8	-143.4	34.8
12TH	151.93	-14.7	42.2	1197	2063	-12.3	20.4	31	-18	-622.4	1447.2	-304.9	-135.3	33.9
13TH	164.76	-15.2	42.4	1197	2063	-12.7	20.6	31	-19	-607.3	1404.8	-286.6	-127.4	33.0
14TH	177.59	-15.6	42.7	1197	2063	-13.1	20.7	31	-19	-591.6	1362.1	-268.9	-119.8	32.0
15TH	190.42	-16.1	43.0	1197	2063	-13.4	20.8	31	-20	-575.5	1319.1	-251.7	-112.3	31.1
16TH	203.25	-16.6	43.2	1197	2063	-13.8	21.0	30	-20	-558.9	1275.9	-235.0	-105.0	30.2
17TH	216.08	-17.2	43.5	1197	2063	-14.4	21.1	31	-21	-541.8	1232.4	-218.9	-97.9	29.3
18TH	228.66	-17.2	42.7	1174	2023	-14.6	21.1	32	-22	-524.6	1189.7	-203.7	-91.2	28.4
19TH	241.24	-17.4	42.7	1174	2023	-14.9	21.1	33	-23	-507.1	1147.0	-189.0	-84.7	27.5
20TH	253.82	-17.7	42.7	1174	2023	-15.1	21.1	34	-24	-489.4	1104.2	-174.9	-78.5	26.5
21ST	266.40	-18.0	42.7	1174	2023	-15.3	21.1	35	-25	-471.4	1061.5	-161.2	-72.4	25.6
22ND	278.98	-18.3	42.8	1174	2023	-15.6	21.1	36	-26	-453.2	1018.7	-148.1	-66.6	24.5
23RD	291.56	-18.5	42.8	1174	2023	-15.8	21.1	37	-27	-434.6	975.9	-135.6	-61.0	23.5
24TH	304.14	-18.7	42.9	1174	2023	-16.0	21.2	38	-28	-415.9	933.0	-123.6	-55.7	22.5
25TH	316.72	-18.9	43.0	1174	2023	-16.1	21.3	38	-28	-397.0	890.0	-112.1	-50.6	21.4
		-18.6	42.3	1151	1983	-16.2	21.3	38	-28					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-378.4	847.7	-101.4	-45.8	20.4
27TH	341.38	-18.7	42.5	1151	1983	-16.3	21.4	38	-28	-359.7	805.2	-91.2	-41.2	19.4
28TH	353.71	-18.9	42.6	1151	1983	-16.4	21.5	38	-28	-340.8	762.6	-81.6	-36.9	18.3
29TH	366.04	-19.0	42.8	1151	1983	-16.5	21.6	38	-28	-321.9	719.8	-72.4	-32.8	17.3
30TH	378.12	-19.1	42.0	1127	1943	-16.9	21.6	38	-30	-302.8	677.8	-64.0	-29.0	16.3
31ST	390.20	-19.2	42.2	1127	1943	-17.0	21.7	39	-30	-283.6	635.6	-56.0	-25.5	15.2
32ND	402.28	-19.2	42.5	1127	1943	-17.0	21.9	39	-30	-264.4	593.0	-48.6	-22.2	14.2
33RD	414.36	-19.2	42.8	1127	1943	-17.1	22.0	39	-30	-245.2	550.2	-41.7	-19.1	13.1
34TH	426.44	-19.3	43.1	1127	1943	-17.1	22.2	39	-30	-225.9	507.1	-35.3	-16.3	12.0
35TH	438.52	-19.3	43.4	1127	1943	-17.1	22.3	39	-30	-206.6	463.7	-29.5	-13.7	11.0
36TH	450.60	-19.4	43.7	1127	1943	-17.2	22.5	39	-30	-187.2	420.0	-24.1	-11.3	9.9
37TH	462.68	-19.3	44.0	1127	1943	-17.1	22.6	39	-29	-167.9	376.1	-19.3	-9.1	8.7
38TH	474.76	-19.2	44.1	1127	1943	-17.0	22.7	38	-28	-148.8	331.9	-15.0	-7.2	7.7
39TH	486.84	-19.0	44.3	1127	1943	-16.9	22.8	37	-27	-129.7	287.6	-11.3	-5.5	6.6
40TH	498.92	-18.9	44.4	1127	1943	-16.8	22.9	36	-26	-110.8	243.2	-8.1	-4.1	5.5
41ST	511.00	-18.8	44.6	1127	1943	-16.7	22.9	35	-25	-92.0	198.6	-5.4	-2.9	4.5
42ND	523.08	-18.7	44.7	1127	1943	-16.6	23.0	34	-24	-73.3	153.9	-3.3	-1.9	3.5
43RD	535.66	-19.3	46.7	1174	2023	-16.5	23.1	34	-24	-54.0	107.2	-1.7	-1.1	2.5
44TH	548.58	-19.2	46.9	1206	2078	-16.0	22.6	34	-24	-34.7	60.3	-.6	-.5	1.4
MR	566.59	-23.8	58.2	1680	2895	-14.2	20.1	31	-22	-10.9	2.1	-.0	-.1	.2
TOP	581.67	-10.9	2.1	1085	2065	-10.1	1.0	-4	40	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 100 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-415.8	2066.9	-611.8	-106.0	43.5
2ND	23.00	-37.0	69.4	2147	3699	-17.2	18.8	41	-30	-378.9	1997.5	-565.0	-96.9	41.9
3RD	35.92	-17.8	42.3	1206	2078	-14.8	20.4	26	-19	-361.1	1955.2	-539.5	-92.1	41.1
4TH	48.84	-14.5	40.3	1206	2078	-12.1	19.4	25	-16	-346.5	1914.9	-514.5	-87.5	40.4
5TH	61.76	-12.8	39.5	1206	2078	-10.7	19.0	26	-14	-333.7	1875.4	-490.0	-83.2	39.7
6TH	74.68	-12.0	40.2	1206	2078	-10.0	19.3	26	-14	-321.6	1835.3	-466.0	-78.9	38.9
7TH	87.60	-11.2	40.8	1206	2078	-9.3	19.6	27	-13	-310.4	1794.5	-442.6	-74.8	38.1
8TH	100.52	-10.4	41.5	1206	2078	-8.7	20.0	27	-12	-299.9	1752.9	-419.7	-70.9	37.3
9TH	113.44	-9.6	42.2	1206	2078	-8.0	20.3	28	-11	-290.3	1710.8	-397.3	-67.1	36.4
10TH	126.27	-8.8	42.6	1197	2063	-7.3	20.6	28	-10	-281.5	1668.2	-375.6	-63.4	35.5
11TH	139.10	-8.2	43.2	1197	2063	-6.8	21.0	28	-9	-273.4	1625.0	-354.5	-59.9	34.5
12TH	151.93	-8.2	44.0	1197	2063	-6.9	21.3	28	-9	-265.2	1581.0	-333.9	-56.4	33.6
13TH	164.76	-8.3	44.7	1197	2063	-6.9	21.7	27	-9	-256.9	1536.3	-313.9	-53.1	32.6
14TH	177.59	-8.3	45.5	1197	2063	-7.0	22.0	27	-8	-248.6	1490.8	-294.5	-49.8	31.7
15TH	190.42	-8.4	46.2	1197	2063	-7.0	22.4	26	-8	-240.2	1444.6	-275.7	-46.7	30.8
16TH	203.25	-8.4	46.9	1197	2063	-7.1	22.8	25	-8	-231.7	1397.6	-257.4	-43.6	29.9
17TH	216.08	-7.7	47.7	1197	2063	-6.5	23.1	26	-7	-224.0	1350.0	-239.8	-40.7	28.9
18TH	228.66	-7.6	46.9	1174	2023	-6.4	23.2	27	-7	-216.4	1303.0	-223.1	-38.0	27.9
19TH	241.24	-7.7	46.9	1174	2023	-6.6	23.2	27	-8	-208.7	1256.1	-207.0	-35.3	26.9
20TH	253.82	-7.8	46.9	1174	2023	-6.7	23.2	27	-8	-200.9	1209.2	-191.5	-32.7	25.9
21ST	266.40	-8.0	46.9	1174	2023	-6.8	23.2	28	-8	-192.9	1162.3	-176.6	-30.2	24.9
22ND	278.98	-8.1	46.9	1174	2023	-6.9	23.2	28	-8	-184.8	1115.4	-162.3	-27.8	23.9
23RD	291.56	-8.3	46.9	1174	2023	-7.0	23.2	28	-8	-176.5	1068.5	-148.5	-25.6	22.9
24TH	304.14	-8.3	47.0	1174	2023	-7.1	23.2	28	-9	-168.3	1021.5	-135.4	-23.4	21.9
25TH	316.72	-8.2	47.2	1174	2023	-7.0	23.3	28	-8	-160.1	974.3	-122.8	-21.3	20.8
		-7.9	46.4	1151	1983	-6.9	23.4	28	-8					

TABLE 7 SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 100 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-152.2	927.9	-111.1	-19.4	19.8
27TH	341.38	-7.8	46.6	1151	1983	-6.8	23.5	28	-8	-144.4	881.3	-100.0	-17.6	18.8
28TH	353.71	-7.7	46.8	1151	1983	-6.7	23.6	28	-8	-136.7	834.5	-89.4	-15.9	17.8
29TH	366.04	-7.6	46.9	1151	1983	-6.6	23.7	27	-8	-129.0	787.5	-79.4	-14.2	16.8
30TH	378.12	-6.7	46.2	1127	1943	-6.0	23.8	28	-7	-122.3	741.4	-70.2	-12.7	15.8
31ST	390.20	-6.3	46.4	1127	1943	-5.6	23.9	29	-7	-116.0	695.0	-61.5	-11.3	14.7
32ND	402.28	-6.4	46.7	1127	1943	-5.7	24.0	29	-7	-109.6	648.3	-53.4	-9.9	13.6
33RD	414.36	-6.5	46.9	1127	1943	-5.8	24.2	29	-7	-103.0	601.4	-45.8	-8.6	12.6
34TH	426.44	-6.6	47.2	1127	1943	-5.9	24.3	29	-7	-96.4	554.2	-38.8	-7.4	11.5
35TH	438.52	-6.7	47.5	1127	1943	-6.0	24.4	29	-7	-89.7	506.7	-32.4	-6.3	10.5
36TH	450.60	-6.8	47.7	1127	1943	-6.1	24.6	29	-7	-82.8	459.0	-26.6	-5.2	9.4
37TH	462.68	-6.9	48.0	1127	1943	-6.1	24.7	28	-7	-75.9	411.0	-21.3	-4.3	8.3
38TH	474.76	-7.3	48.1	1127	1943	-6.5	24.8	28	-7	-68.6	362.9	-16.7	-3.4	7.3
39TH	486.84	-7.7	48.1	1127	1943	-6.9	24.7	27	-7	-60.9	314.8	-12.6	-2.6	6.2
40TH	498.92	-8.2	48.1	1127	1943	-7.3	24.7	27	-8	-52.7	266.7	-9.1	-1.9	5.2
41ST	511.00	-8.6	48.1	1127	1943	-7.7	24.7	26	-8	-44.0	218.6	-6.1	-1.4	4.3
42ND	523.08	-9.1	48.1	1127	1943	-8.0	24.7	26	-8	-35.0	170.6	-3.8	-.9	3.3
43RD	535.66	-9.6	50.1	1174	2023	-8.2	24.7	26	-8	-25.4	120.5	-2.0	-.5	2.3
44TH	548.58	-9.2	50.4	1206	2078	-7.6	24.3	26	-8	-16.2	70.1	-.7	-.2	1.3
MR	566.58	-10.8	64.7	1680	2895	-6.4	22.4	22	-6	-5.4	5.4	-.0	-.0	.3
TOP	581.67	-5.4	5.4	1085	2065	-5.0	2.6	$$$$	6130	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 110 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									13.5	2293.8	-693.9	42.8	35.4
2ND	23.00	-29.2	73.8	2147	3699	-13.6	20.0	29	-20	42.7	2219.9	-641.9	42.1	33.9
3RD	35.92	-13.7	42.5	1206	2078	-11.4	20.5	20	-11	56.4	2177.4	-613.5	41.5	33.3
4TH	48.84	-11.5	41.6	1206	2078	-9.6	20.0	18	-9	67.9	2135.8	-585.7	40.7	32.7
5TH	61.76	-10.1	41.6	1206	2078	-8.4	20.0	19	-8	78.0	2094.2	-558.3	39.7	32.2
6TH	74.68	-8.8	42.7	1206	2078	-7.3	20.6	19	-7	86.8	2051.4	-531.6	38.7	31.5
7TH	87.60	-7.5	43.9	1206	2078	-6.2	21.1	19	-5	94.2	2007.6	-505.3	37.5	30.9
8TH	100.52	-6.2	45.0	1206	2078	-5.1	21.7	19	-4	100.4	1962.6	-479.7	36.2	30.2
9TH	113.44	-4.9	46.1	1206	2078	-4.1	22.2	19	-3	105.3	1916.5	-454.6	34.9	29.5
10TH	126.27	-3.6	46.9	1197	2063	-3.0	22.7	20	-3	108.9	1869.6	-430.4	33.5	28.8
11TH	139.10	-2.5	47.9	1197	2063	-2.1	23.2	20	-2	111.4	1821.7	-406.7	32.1	28.0
12TH	151.93	-2.2	48.1	1197	2063	-1.8	23.3	20	-2	113.6	1773.6	-383.6	30.7	27.3
13TH	164.76	-1.9	48.3	1197	2063	-1.6	23.4	20	-1	115.5	1725.3	-361.2	29.2	26.5
14TH	177.59	-1.6	48.6	1197	2063	-1.3	23.5	19	-1	117.0	1676.7	-339.3	27.7	25.8
15TH	190.42	-1.3	48.8	1197	2063	-1.1	23.6	19	-1	118.3	1627.9	-318.1	26.2	25.0
16TH	203.25	-1.0	49.0	1197	2063	-.8	23.7	19	-1	119.2	1578.9	-297.6	24.7	24.3
17TH	216.08	1.0	49.2	1197	2063	.8	23.9	21	1	118.3	1529.7	-277.6	23.2	23.4
18TH	228.66	1.5	48.7	1174	2023	1.3	24.1	21	1	116.8	1481.0	-258.7	21.7	22.6
19TH	241.24	1.8	49.2	1174	2023	1.6	24.3	21	1	114.9	1431.8	-240.4	20.2	21.8
20TH	253.82	2.1	49.7	1174	2023	1.8	24.6	21	2	112.8	1382.1	-222.7	18.8	20.9
21ST	266.40	2.4	50.2	1174	2023	2.1	24.8	21	2	110.3	1331.9	-205.6	17.4	20.1
22ND	278.98	2.8	50.7	1174	2023	2.3	25.1	21	2	107.6	1281.2	-189.2	16.0	19.3
23RD	291.56	3.1	51.2	1174	2023	2.6	25.3	21	2	104.5	1230.0	-173.4	14.7	18.4
24TH	304.14	3.3	51.8	1174	2023	2.8	25.6	20	2	101.2	1178.2	-158.2	13.4	17.6
25TH	316.72	3.5	52.3	1174	2023	2.9	25.8	20	2	97.8	1125.9	-143.7	12.1	16.7
		3.5	51.8	1151	1983	3.1	26.1	20	2					

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 110 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									94.2	1074.1	-130.2	10.9	15.9
		3.7	52.3	1151	1983	3.2	26.4	20	2					
27TH	341.38									90.6	1021.8	-117.2	9.8	15.1
		3.8	52.8	1151	1983	3.3	26.6	20	2					
28TH	353.71									86.8	969.0	-105.0	8.7	14.2
		3.9	53.3	1151	1983	3.4	26.9	20	2					
29TH	366.04									82.9	915.7	-93.3	7.7	13.4
		5.2	52.8	1127	1943	4.6	27.2	21	4					
30TH	378.12									77.7	863.0	-82.6	6.7	12.5
		5.9	53.1	1127	1943	5.3	27.3	22	4					
31ST	390.20									71.8	809.8	-72.5	5.8	11.6
		5.9	53.3	1127	1943	5.2	27.5	22	4					
32ND	402.28									65.9	756.5	-63.0	5.0	10.7
		5.9	53.6	1127	1943	5.2	27.6	21	4					
33RD	414.36									60.0	702.9	-54.2	4.2	9.8
		5.9	53.8	1127	1943	5.2	27.7	21	4					
34TH	426.44									54.1	649.1	-46.1	3.5	8.9
		5.9	54.1	1127	1943	5.2	27.8	21	4					
35TH	438.52									48.3	595.1	-38.5	2.9	8.0
		5.8	54.3	1127	1943	5.2	27.9	20	4					
36TH	450.60									42.4	540.8	-31.7	2.3	7.1
		5.8	54.5	1127	1943	5.2	28.1	20	4					
37TH	462.68									36.6	486.2	-25.5	1.9	6.3
		5.4	55.1	1127	1943	4.8	28.4	19	3					
38TH	474.76									31.2	431.2	-19.9	1.5	5.4
		4.9	55.7	1127	1943	4.3	28.7	18	3					
39TH	486.84									26.3	375.4	-15.1	1.1	4.6
		4.4	56.3	1127	1943	3.9	29.0	17	2					
40TH	498.92									22.0	319.1	-10.9	.8	3.9
		3.9	56.9	1127	1943	3.4	29.3	16	2					
41ST	511.00									18.1	262.2	-7.4	.6	3.1
		3.4	57.6	1127	1943	3.0	29.6	15	2					
42ND	523.08									14.8	204.6	-4.5	.4	2.4
		3.5	60.6	1174	2023	3.0	29.9	15	2					
43RD	535.66									11.2	144.0	-2.3	.2	1.7
		4.2	61.0	1206	2078	3.5	29.3	16	2					
44TH	548.58									7.0	83.1	-.9	.1	.9
		4.8	74.9	1680	2895	2.9	25.9	13	1					
MR	566.58									2.2	8.2	-.1	.0	.1
		2.2	8.2	1085	2065	2.0	4.0	24	11					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 120 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									281.5	2453.0	-748.5	122.1	25.6
2ND	23.00	-22.1	79.7	2147	3699	-10.3	21.5	18	-9	303.6	2373.3	-693.0	115.4	24.5
3RD	35.92	-10.3	46.5	1206	2078	-8.6	22.4	13	-5	313.9	2326.8	-662.7	111.4	24.1
4TH	48.84	-7.6	45.1	1206	2078	-6.3	21.7	14	-4	321.5	2281.7	-632.9	107.3	23.6
5TH	61.76	-5.2	44.6	1206	2078	-4.3	21.5	16	-3	326.7	2237.1	-603.7	103.1	23.0
6TH	74.68	-3.5	45.4	1206	2078	-2.9	21.8	16	-2	330.2	2191.7	-575.1	98.9	22.4
7TH	87.60	-1.8	46.2	1206	2078	-1.5	22.2	16	-1	332.0	2145.5	-547.1	94.6	21.8
8TH	100.52	-.1	46.9	1206	2078	-.1	22.6	17	-0	332.1	2098.6	-519.7	90.3	21.2
9TH	113.44	1.6	47.7	1206	2078	1.3	23.0	17	1	330.5	2050.9	-492.9	86.0	20.6
10TH	126.27	3.2	48.1	1197	2063	2.7	23.3	17	2	327.3	2002.7	-466.9	81.8	19.9
11TH	139.10	4.6	48.9	1197	2063	3.8	23.7	17	3	322.7	1953.8	-441.5	77.6	19.2
12TH	151.93	4.8	49.5	1197	2063	4.0	24.0	17	3	317.9	1904.3	-416.7	73.5	18.6
13TH	164.76	5.0	50.2	1197	2063	4.1	24.3	16	3	312.9	1854.1	-392.6	69.5	17.9
14TH	177.59	5.1	50.9	1197	2063	4.3	24.7	16	3	307.8	1803.2	-369.2	65.5	17.3
15TH	190.42	5.3	51.6	1197	2063	4.4	25.0	15	3	302.5	1751.6	-346.3	61.6	16.7
16TH	203.25	5.5	52.2	1197	2063	4.6	25.3	14	3	297.0	1699.4	-324.2	57.7	16.1
17TH	216.08	7.5	52.9	1197	2063	6.3	25.6	16	4	289.4	1646.5	-302.7	54.0	15.4
18TH	228.66	7.9	52.3	1174	2023	6.8	25.8	17	4	281.5	1594.2	-282.4	50.4	14.7
19TH	241.24	8.2	52.6	1174	2023	7.0	26.0	17	4	273.3	1541.7	-262.6	46.9	14.1
20TH	253.82	8.4	52.9	1174	2023	7.2	26.1	17	5	264.9	1488.8	-243.6	43.5	13.4
21ST	266.40	8.7	53.2	1174	2023	7.4	26.3	17	5	256.2	1435.7	-225.2	40.2	12.7
22ND	278.98	8.9	53.5	1174	2023	7.6	26.4	17	5	247.3	1382.2	-207.5	37.1	12.0
23RD	291.56	9.2	53.8	1174	2023	7.8	26.6	17	5	238.1	1328.4	-190.4	34.0	11.2
24TH	304.14	9.4	54.1	1174	2023	8.0	26.8	17	5	228.7	1274.3	-174.0	31.1	10.5
25TH	316.72	9.5	54.6	1174	2023	8.1	27.0	16	5	219.2	1219.7	-158.3	28.2	9.9
		9.4	54.0	1151	1983	8.1	27.2	15	4					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 120 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									209.9	1165.7	-143.6	25.6	9.2
		9.5	54.4	1151	1983	8.2	27.5	14	4					
27TH	341.38									200.4	1111.2	-129.6	23.1	8.6
		9.6	54.9	1151	1983	8.3	27.7	13	4					
28TH	353.71									190.8	1056.3	-116.2	20.7	8.1
		9.6	55.4	1151	1983	8.4	27.9	12	4					
29TH	366.04									181.2	1001.0	-103.6	18.4	7.5
		10.8	54.7	1127	1943	9.6	28.1	13	4					
30TH	378.12									170.4	946.3	-91.8	16.2	7.0
		11.5	55.4	1127	1943	10.2	28.5	13	5					
31ST	390.20									158.9	890.9	-80.7	14.3	6.4
		11.4	56.2	1127	1943	10.1	28.9	13	4					
32ND	402.28									147.5	834.7	-70.3	12.4	5.9
		11.3	57.1	1127	1943	10.0	29.4	12	4					
33RD	414.36									136.2	777.6	-60.5	10.7	5.3
		11.2	57.9	1127	1943	9.9	29.8	12	4					
34TH	426.44									125.0	719.7	-51.5	9.1	4.8
		11.1	58.8	1127	1943	9.8	30.3	12	4					
35TH	438.52									114.0	660.9	-43.2	7.7	4.3
		10.9	59.6	1127	1943	9.7	30.7	11	4					
36TH	450.60									103.1	601.2	-35.5	6.4	3.8
		10.8	60.5	1127	1943	9.6	31.1	11	3					
37TH	462.68									92.3	540.8	-28.6	5.2	3.2
		10.5	61.1	1127	1943	9.3	31.4	10	3					
38TH	474.76									81.7	479.7	-22.5	4.1	2.8
		10.2	61.6	1127	1943	9.1	31.7	10	3					
39TH	486.84									71.5	418.2	-17.0	3.2	2.3
		9.9	62.0	1127	1943	8.8	31.9	9	2					
40TH	498.92									61.6	356.1	-12.4	2.4	1.9
		9.6	62.5	1127	1943	8.6	32.2	8	2					
41ST	511.00									51.9	293.6	-8.4	1.7	1.5
		9.3	63.0	1127	1943	8.3	32.4	7	2					
42ND	523.08									42.6	230.5	-5.3	1.1	1.1
		10.0	66.2	1174	2023	8.5	32.7	7	2					
43RD	535.66									32.5	164.3	-2.8	.7	.7
		11.1	66.7	1206	2078	9.2	32.1	8	2					
44TH	548.59									21.5	97.6	-1.1	.3	.3
		13.9	83.7	1680	2895	8.3	28.9	5	2					
MR	566.58									7.6	13.9	-.1	.1	-.0
		7.6	13.9	1085	2065	7.0	6.7	-1	-1					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7 SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 130 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									334.6	2144.7	-668.8	118.9	18.9
2ND	23.00	-11.3	66.9	2147	3699	-5.3	18.1	19	-5	345.9	2077.7	-620.2	111.1	17.9
3RD	35.92	-4.8	39.2	1206	2078	-3.9	18.9	13	-3	350.6	2038.6	-593.7	106.6	17.5
4TH	48.84	-2.7	38.2	1206	2078	-2.3	18.4	13	-2	353.4	2000.4	-567.6	102.1	17.1
5TH	61.76	-.6	37.8	1206	2078	-.5	18.2	15	-0	354.0	1962.6	-542.0	97.5	16.6
6TH	74.68	.9	38.3	1206	2078	.7	18.4	16	1	353.1	1924.3	-516.9	92.9	16.2
7TH	87.60	2.3	38.8	1206	2078	1.9	18.7	17	2	350.7	1885.6	-492.2	88.4	15.6
8TH	100.52	3.8	39.2	1206	2078	3.2	18.9	17	3	346.9	1846.3	-468.1	83.9	15.1
9TH	113.44	5.3	39.7	1206	2078	4.4	19.1	18	4	341.6	1806.6	-444.5	79.4	14.5
10TH	126.27	6.7	39.9	1197	2063	5.6	19.3	19	5	334.9	1766.7	-421.6	75.1	13.9
11TH	139.10	7.9	40.4	1197	2063	6.6	19.6	20	7	327.0	1726.2	-399.2	70.8	13.3
12TH	151.93	7.9	41.0	1197	2063	6.6	19.9	19	6	319.2	1685.2	-377.3	66.7	12.7
13TH	164.76	7.8	41.6	1197	2063	6.5	20.1	18	6	311.3	1643.6	-356.0	62.7	12.2
14TH	177.59	7.8	42.1	1197	2063	6.5	20.4	17	5	303.5	1601.5	-335.2	58.7	11.6
15TH	190.42	7.8	42.7	1197	2063	6.5	20.7	16	5	295.7	1558.8	-314.9	54.9	11.1
16TH	203.25	7.8	43.3	1197	2063	6.5	21.0	15	5	287.9	1515.6	-295.2	51.1	10.6
17TH	216.08	9.6	43.8	1197	2063	8.0	21.2	17	6	278.2	1471.7	-276.0	47.5	10.1
18TH	228.66	9.9	43.6	1174	2023	8.5	21.5	17	7	268.3	1428.2	-257.8	44.1	9.5
19TH	241.24	10.1	44.1	1174	2023	8.6	21.8	17	6	258.2	1384.0	-240.1	40.7	8.9
20TH	253.82	10.3	44.7	1174	2023	8.7	22.1	16	6	248.0	1339.3	-222.9	37.6	8.4
21ST	266.40	10.4	45.3	1174	2023	8.9	22.4	16	6	237.5	1294.0	-206.4	34.5	7.8
22ND	278.98	10.6	45.9	1174	2023	9.0	22.7	16	6	226.9	1248.1	-190.4	31.6	7.3
23RD	291.56	10.8	46.5	1174	2023	9.2	23.0	15	6	216.2	1201.6	-175.0	28.8	6.8
24TH	304.14	10.8	47.1	1174	2023	9.2	23.3	15	6	205.4	1154.5	-160.2	26.1	6.2
25TH	316.72	10.5	47.7	1174	2023	8.9	23.6	14	5	194.9	1106.8	-145.9	23.6	5.7
		10.0	47.3	1151	1983	8.7	23.9	12	4					

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 130 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									184.9	1059.5	-132.6	21.3	5.3
		9.7	47.8	1151	1983	8.5	24.1	11	4					
27TH	341.38									175.2	1011.6	-119.8	19.1	4.9
		9.5	48.4	1151	1983	8.2	24.4	10	3					
28TH	353.71									165.7	963.2	-107.6	17.0	4.5
		9.2	48.9	1151	1983	8.0	24.7	9	3					
29TH	366.04									156.5	914.3	-96.1	15.0	4.1
		10.0	48.5	1127	1943	8.8	25.0	10	3					
30TH	378.12									146.6	865.8	-85.3	13.1	3.8
		10.6	49.2	1127	1943	9.4	25.3	10	4					
31ST	390.20									136.0	816.6	-75.1	11.4	3.4
		10.5	50.1	1127	1943	9.3	25.8	10	3					
32ND	402.28									125.5	766.4	-65.6	9.9	3.0
		10.5	51.0	1127	1943	9.3	26.3	9	3					
33RD	414.36									115.0	715.4	-56.6	8.4	2.7
		10.4	51.9	1127	1943	9.3	26.7	9	3					
34TH	426.44									104.6	663.5	-48.3	7.1	2.3
		10.4	52.8	1127	1943	9.2	27.2	8	3					
35TH	438.52									94.2	610.7	-40.6	5.9	2.0
		10.4	53.7	1127	1943	9.2	27.6	8	3					
36TH	450.60									83.8	557.0	-33.6	4.8	1.7
		10.3	54.6	1127	1943	9.1	28.1	7	2					
37TH	462.68									73.5	502.4	-27.2	3.9	1.4
		9.7	55.2	1127	1943	8.6	28.4	7	2					
38TH	474.76									63.8	447.2	-21.4	3.0	1.1
		9.2	55.9	1127	1943	8.1	28.8	6	2					
39TH	486.84									54.6	391.3	-16.4	2.3	.8
		8.6	56.5	1127	1943	7.6	29.1	5	1					
40TH	498.92									46.1	334.9	-12.0	1.7	.6
		8.0	57.1	1127	1943	7.1	29.4	4	1					
41ST	511.00									38.1	277.7	-8.3	1.2	.4
		7.4	57.7	1127	1943	6.6	29.7	4	1					
42ND	523.08									30.7	220.0	-5.3	.8	.2
		7.7	60.8	1174	2023	6.6	30.0	3	1					
43RD	535.66									22.9	159.2	-2.9	.4	.1
		8.5	61.5	1206	2078	7.1	29.6	3	1					
44TH	548.58									14.4	97.8	-1.2	.2	-.1
		10.1	77.5	1680	2895	6.0	26.8	2	0					
MR	566.58									4.3	20.3	-.2	.0	-.2
		4.3	20.3	1085	2065	4.0	9.8	-11	-4					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 140 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									163.5	1700.2	-563.9	76.7	12.8
2ND	23.00	-16.4	46.9	2147	3699	-7.6	12.7	26	-16	179.9	1653.4	-525.3	72.7	11.9
3RD	35.92	-7.8	26.9	1206	2078	-6.5	12.9	18	-9	187.8	1626.5	-504.1	70.4	11.6
4TH	48.84	-5.8	25.9	1206	2078	-4.8	12.5	18	-7	193.6	1600.6	-483.3	67.9	11.2
5TH	61.76	-4.2	25.6	1206	2078	-3.5	12.3	19	-5	197.8	1575.0	-462.8	65.4	10.9
6TH	74.68	-3.3	26.0	1206	2078	-2.7	12.5	19	-4	201.1	1549.0	-442.6	62.8	10.5
7TH	87.60	-2.4	26.5	1206	2078	-2.0	12.7	20	-3	203.5	1522.5	-422.8	60.2	10.0
8TH	100.52	-1.5	26.9	1206	2078	-1.2	12.9	21	-2	205.0	1495.6	-403.3	57.5	9.6
9TH	113.44	-.5	27.3	1206	2078	-.4	13.2	22	-1	205.5	1468.3	-384.1	54.9	9.1
10TH	126.27	.4	27.6	1197	2063	.3	13.4	23	1	205.1	1440.7	-365.4	52.2	8.6
11TH	139.10	1.2	28.0	1197	2063	1.0	13.6	23	2	203.9	1412.7	-347.1	49.6	8.1
12TH	151.93	1.4	28.4	1197	2063	1.2	13.7	22	2	202.5	1384.3	-329.2	47.0	7.6
13TH	164.76	1.7	28.7	1197	2063	1.4	13.9	21	2	200.8	1355.6	-311.6	44.4	7.1
14TH	177.59	1.9	29.1	1197	2063	1.6	14.1	19	2	198.9	1326.5	-294.4	41.9	6.7
15TH	190.42	2.2	29.4	1197	2063	1.8	14.2	18	2	196.7	1297.1	-277.6	39.3	6.2
16TH	203.25	2.5	29.7	1197	2063	2.0	14.4	17	2	194.3	1267.4	-261.1	36.8	5.8
17TH	216.08	4.0	30.1	1197	2063	3.3	14.6	19	4	190.2	1237.3	-245.1	34.4	5.4
18TH	228.66	4.7	30.2	1174	2023	4.0	14.9	18	5	185.5	1207.1	-229.7	32.0	5.0
19TH	241.24	5.3	31.0	1174	2023	4.5	15.3	17	5	180.2	1176.1	-214.7	29.7	4.5
20TH	253.82	5.9	31.8	1174	2023	5.0	15.7	17	5	174.3	1144.2	-200.1	27.5	4.1
21ST	266.40	6.5	32.7	1174	2023	5.6	16.1	16	5	167.8	1111.6	-185.9	25.3	3.7
22ND	278.98	7.1	33.5	1174	2023	6.1	16.5	15	5	160.7	1078.1	-172.1	23.2	3.4
23RD	291.56	7.7	34.3	1174	2023	6.6	16.9	14	5	152.9	1043.8	-158.8	21.3	3.0
24TH	304.14	7.9	35.1	1174	2023	6.8	17.4	13	5	145.0	1008.7	-145.9	19.4	2.6
25TH	316.72	7.5	36.3	1174	2023	6.4	17.9	12	4	137.5	972.4	-133.4	17.6	2.3
		7.0	36.7	1151	1983	6.1	18.5	11	3					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 140 CONFIGURATION A REFERENCE PRESSURE 34 0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									130.5	935.7	-121.7	16.0	2.0
27TH	341.38	6.6	37.8	1151	1983	5.7	19.1	9	3	123.9	897.8	-110.4	14.4	1.7
28TH	353.71	6.2	39.0	1151	1983	5.4	19.7	8	2	117.7	858.9	-99.5	12.9	1.5
29TH	366.04	5.8	40.1	1151	1983	5.1	20.2	7	2	111.9	818.8	-89.2	11.5	1.3
30TH	378.12	6.2	40.4	1127	1943	5.5	20.8	7	2	105.7	778.4	-79.5	10.2	1.0
31ST	390.20	6.7	41.3	1127	1943	5.9	21.3	7	2	99.0	737.1	-70.4	8.9	.8
32ND	402.28	6.7	42.3	1127	1943	5.9	21.8	6	2	92.3	694.8	-61.7	7.8	.6
33RD	414.36	6.7	43.3	1127	1943	6.0	22.3	6	1	85.6	651.5	-53.6	6.7	.4
34TH	426.44	6.8	44.3	1127	1943	6.0	22.8	5	1	78.8	607.2	-46.0	5.7	.2
35TH	438.52	6.8	45.3	1127	1943	6.0	23.3	4	1	72.0	562.0	-38.9	4.8	.1
36TH	450.60	6.8	46.2	1127	1943	6.1	23.8	4	1	65.2	515.7	-32.4	4.0	-.0
37TH	462.68	6.9	47.2	1127	1943	6.1	24.3	3	1	58.3	468.5	-26.5	3.2	-.2
38TH	474.76	6.7	48.2	1127	1943	5.9	24.8	3	1	51.6	420.4	-21.1	2.6	-.3
39TH	486.84	6.5	49.1	1127	1943	5.8	25.3	2	0	45.1	371.3	-16.3	2.0	-.3
40TH	498.92	6.3	50.0	1127	1943	5.6	25.7	1	0	38.8	321.3	-12.2	1.5	-.4
41ST	511.00	6.1	50.9	1127	1943	5.4	26.2	0	0	32.7	270.4	-8.6	1.0	-.4
42ND	523.08	5.9	51.8	1127	1943	5.2	26.7	-1	-0	26.8	218.6	-5.6	.7	-.4
43RD	535.66	6.4	54.9	1174	2023	5.5	27.1	-1	-0	20.4	163.7	-3.2	.4	-.3
44TH	548.58	7.4	56.6	1206	2078	6.1	27.3	-1	-0	13.0	107.0	-1.5	.2	-.3
MR	566.58	9.5	76.1	1680	2895	5.7	26.3	-0	-0	3.5	30.9	-.2	.0	-.3
TOP	581.67	3.5	30.9	1085	2065	3.2	15.0	-11	-2	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 150 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									133.3	1169.2	-408.2	69.1	4.2
2ND	23.00	-10.0	25.2	2147	3699	-4.6	6.8	33	-22	143.3	1143.9	-381.6	65.9	3.7
3RD	35.92	-4.9	15.1	1206	2078	-4.1	7.3	21	-11	148.2	1128.8	-366.9	64.0	3.5
4TH	48.84	-4.3	14.3	1206	2078	-3.6	6.9	18	-9	152.5	1114.5	-352.4	62.1	3.3
5TH	61.76	-3.8	13.9	1206	2078	-3.2	6.7	19	-9	156.4	1100.5	-338.1	60.1	3.1
6TH	74.68	-3.3	14.1	1206	2078	-2.8	6.8	20	-8	159.7	1086.5	-324.0	58.0	2.9
7TH	87.60	-2.8	14.2	1206	2078	-2.3	6.8	22	-7	162.5	1072.2	-310.0	55.9	2.6
8TH	100.52	-2.3	14.3	1206	2078	-1.9	6.9	24	-6	164.8	1057.9	-296.3	53.8	2.4
9TH	113.44	-1.8	14.5	1206	2078	-1.5	7.0	25	-5	166.6	1043.4	-282.7	51.7	2.1
10TH	126.27	-1.3	14.5	1197	2063	-1.1	7.0	27	-4	167.9	1028.9	-269.4	49.5	1.8
11TH	139.10	-.8	14.8	1197	2063	-.7	7.2	28	-3	168.7	1014.1	-256.3	47.4	1.4
12TH	151.93	-.5	15.5	1197	2063	-.4	7.5	24	-1	169.1	998.6	-243.4	45.2	1.1
13TH	164.76	-.2	16.3	1197	2063	-.1	7.9	21	-0	169.3	982.4	-230.7	43.0	.9
14TH	177.59	.1	17.0	1197	2063	.1	8.2	19	0	169.2	965.4	-218.2	40.9	.6
15TH	190.42	.4	17.8	1197	2063	.4	8.6	16	1	168.7	947.6	-205.9	38.7	.4
16TH	203.25	.8	18.5	1197	2063	.6	9.0	14	1	168.0	929.1	-193.9	36.5	.2
17TH	216.08	1.8	19.2	1197	2063	1.5	9.3	14	2	166.2	909.9	-182.1	34.4	-.1
18TH	228.66	2.3	19.9	1174	2023	2.0	9.8	13	3	163.8	890.0	-170.8	32.3	-.3
19TH	241.24	2.8	21.0	1174	2023	2.4	10.4	11	3	161.0	869.0	-159.7	30.3	-.4
20TH	253.82	3.3	22.1	1174	2023	2.8	10.9	10	2	157.7	846.9	-148.9	28.3	-.6
21ST	266.40	3.8	23.2	1174	2023	3.2	11.5	8	2	153.9	823.7	-138.4	26.3	-.8
22ND	278.98	4.3	24.3	1174	2023	3.6	12.0	7	2	149.7	799.5	-128.2	24.4	-.9
23RD	291.56	4.7	25.4	1174	2023	4.0	12.5	6	2	145.0	774.1	-118.3	22.6	-1.0
24TH	304.14	5.0	26.3	1174	2023	4.3	13.0	5	2	139.9	747.8	-108.7	20.8	-1.1
25TH	316.72	5.0	27.1	1174	2023	4.2	13.4	4	1	135.0	720.7	-99.5	19.0	-1.2
		4.8	27.3	1151	1983	4.2	13.8	3	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 150 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									130.2	693.4	-90.8	17.4	-1.2
		4.8	28.0	1151	1983	4.1	14.1	2	1					
27TH	341.38									125.4	665.4	-82.4	15.8	-1.3
		4.7	28.7	1151	1983	4.1	14.5	1	0					
28TH	353.71									120.7	636.7	-74.4	14.3	-1.3
		4.6	29.5	1151	1983	4.0	14.9	0	0					
29TH	366.04									116.1	607.2	-66.7	12.8	-1.3
		5.2	29.6	1127	1943	4.6	15.2	-0	-0					
30TH	378.12									110.8	577.7	-59.5	11.5	-1.3
		5.7	30.2	1127	1943	5.1	15.6	-0	-0					
31ST	390.20									105.1	547.4	-52.7	10.2	-1.3
		5.9	31.0	1127	1943	5.2	15.9	-1	-0					
32ND	402.28									99.2	516.4	-46.3	8.9	-1.3
		6.0	31.7	1127	1943	5.4	16.3	-1	-0					
33RD	414.36									93.1	484.7	-40.3	7.8	-1.3
		6.2	32.5	1127	1943	5.5	16.7	-1	-0					
34TH	426.44									87.0	452.3	-34.6	6.7	-1.2
		6.3	33.2	1127	1943	5.6	17.1	-2	-1					
35TH	438.52									80.6	419.1	-29.3	5.7	-1.2
		6.5	33.9	1127	1943	5.7	17.5	-2	-1					
36TH	450.60									74.2	385.1	-24.5	4.7	-1.1
		6.6	34.7	1127	1943	5.9	17.8	-2	-1					
37TH	462.68									67.5	350.5	-20.0	3.9	-1.1
		6.7	35.4	1127	1943	6.0	18.2	-3	-1					
38TH	474.76									60.8	315.1	-16.0	3.1	-1.0
		6.8	36.2	1127	1943	6.1	18.6	-3	-1					
39TH	486.84									54.0	278.9	-12.4	2.4	-.9
		6.9	36.9	1127	1943	6.1	19.0	-3	-1					
40TH	498.92									47.0	241.9	-9.3	1.8	-.8
		7.0	37.7	1127	1943	6.2	19.4	-4	-1					
41ST	511.00									40.0	204.2	-6.6	1.3	-.7
		7.1	38.4	1127	1943	6.3	19.8	-4	-1					
42ND	523.08									32.9	165.8	-4.4	.8	-.6
		8.0	40.8	1174	2023	6.8	20.2	-4	-1					
43RD	535.66									24.9	125.0	-2.5	.5	-.5
		9.0	42.1	1206	2078	7.5	20.3	-3	-1					
44TH	548.58									15.9	82.9	-1.2	.2	-.4
		11.5	56.3	1680	2895	6.9	19.4	-2	-1					
MR	566.58									4.4	26.6	-.2	.0	-.3
		4.4	26.6	1085	2065	4.0	12.9	-12	-3					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 160 CONFIGURATION H REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 60 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									168.4	724.7	-273.6	69.5	-1.1
2ND	23.00	-4.6	11.5	2147	3699	-2.1	3.1	36	-24	173.0	713.1	-257.0	65.6	-1.4
3RD	35.92	-2.2	6.6	1206	2078	-1.8	3.2	19	-11	175.1	706.5	-247.9	63.4	-1.5
4TH	48.84	-1.4	6.5	1206	2078	-1.1	3.1	14	-5	176.5	700.0	-238.8	61.1	-1.5
5TH	61.76	-.8	6.4	1206	2078	-.6	3.1	14	-3	177.3	693.6	-229.8	58.8	-1.6
6TH	74.68	-.5	6.1	1206	2078	-.4	2.9	17	-2	177.8	687.5	-220.9	56.5	-1.7
7TH	87.60	-.2	5.9	1206	2078	-.2	2.8	19	-1	178.0	681.6	-212.0	54.2	-1.8
8TH	100.52	.0	5.6	1206	2078	.0	2.7	22	0	178.0	675.9	-203.2	51.9	-1.9
9TH	113.44	.3	5.4	1206	2078	.2	2.6	26	2	177.7	670.5	-194.5	49.6	-2.0
10TH	126.27	.5	5.1	1197	2063	.4	2.5	30	5	177.2	665.4	-186.0	47.3	-2.1
11TH	139.10	.8	5.0	1197	2063	.7	2.4	33	9	176.4	660.4	-177.5	45.1	-2.3
12TH	151.93	1.2	5.7	1197	2063	1.0	2.8	26	10	175.2	654.7	-169.0	42.8	-2.4
13TH	164.76	1.6	6.4	1197	2063	1.3	3.1	21	9	173.6	648.3	-160.7	40.6	-2.5
14TH	177.59	2.0	7.0	1197	2063	1.7	3.4	17	8	171.6	641.3	-152.4	38.4	-2.6
15TH	190.42	2.4	7.7	1197	2063	2.0	3.7	13	7	169.2	633.6	-144.2	36.2	-2.6
16TH	203.25	2.8	8.4	1197	2063	2.3	4.1	10	6	166.4	625.2	-136.1	34.0	-2.7
17TH	216.08	3.9	9.0	1197	2063	3.3	4.4	13	10	162.5	616.2	-128.2	31.9	-2.8
18TH	228.66	4.2	9.8	1174	2023	3.6	4.8	10	7	158.3	606.4	-120.5	29.9	-2.8
19TH	241.24	4.4	10.7	1174	2023	3.8	5.3	6	4	153.9	595.7	-112.9	27.9	-2.9
20TH	253.82	4.6	11.6	1174	2023	3.9	5.8	3	2	149.2	584.1	-105.5	26.0	-2.9
21ST	266.40	4.8	12.6	1174	2023	4.1	6.2	0	0	144.4	571.5	-98.2	24.2	-2.9
22ND	278.98	5.1	13.5	1174	2023	4.3	6.7	-2	-1	139.3	558.0	-91.1	22.4	-2.9
23RD	291.56	5.3	14.5	1174	2023	4.5	7.2	-4	-2	134.1	543.5	-84.2	20.7	-2.8
24TH	304.14	5.3	15.4	1174	2023	4.5	7.6	-5	-3	128.7	528.1	-77.5	19.0	-2.8
25TH	316.72	5.2	16.6	1174	2023	4.4	8.2	-6	-3	123.6	511.5	-70.9	17.4	-2.7
		4.9	17.4	1151	1983	4.2	8.8	-7	-3					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 160 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									118.7	494.2	-64.7	15.9	-2.6
		4.7	18.5	1151	1983	4.1	9.3	-7	-3					
27TH	341 38									114.0	475.7	-58.7	14.5	-2.5
		4.5	19.6	1151	1983	3.9	9 9	-8	-3					
28TH	353.71									109.5	456.1	-53.0	13.1	-2.4
		4.4	20.7	1151	1983	3.8	10.4	-8	-3					
29TH	366.04									105.1	435.4	-47.5	11.8	-2.3
		4.5	21.4	1127	1943	4.0	11.0	-8	-3					
30TH	378.12									100.6	414.0	-42.4	10.6	-2.1
		4.9	22.0	1127	1943	4.3	11.3	-8	-3					
31ST	390.20									95.7	392.0	-37.5	9.4	-2.0
		5.1	22.5	1127	1943	4.5	11.6	-8	-3					
32ND	402.28									90.7	369.5	-32.9	8.3	-1.9
		5.2	23.0	1127	1943	4.7	11.9	-8	-3					
33RD	414.36									85.4	346.5	-28.6	7.2	-1.7
		5.4	23.5	1127	1943	4.8	12.1	-7	-3					
34TH	426.44									80.0	322.9	-24.5	6.2	-1.6
		5.6	24.0	1127	1943	5.0	12.4	-7	-3					
35TH	438.52									74.4	298.9	-20.8	5.3	-1.5
		5.8	24.5	1127	1943	5.2	12.6	-7	-3					
36TH	450.60									68.5	274.3	-17.3	4.4	-1.3
		6.0	25.0	1127	1943	5.3	12.9	-7	-3					
37TH	462.68									62.6	249.3	-14.2	3.6	-1.2
		6.1	25.5	1127	1943	5.4	13.1	-7	-3					
38TH	474.76									56.4	223.8	-11.3	2.9	-1.1
		6.3	26.0	1127	1943	5.6	13.4	-7	-3					
39TH	486.84									50.1	197.8	-8.8	2.2	-.9
		6.5	26.5	1127	1943	5.7	13.6	-7	-3					
40TH	498.92									43.6	171.3	-6.5	1.7	-.8
		6.6	27.0	1127	1943	5.9	13.9	-7	-3					
41ST	511.00									37.0	144.3	-4.6	1.2	-.6
		6.8	27.4	1127	1943	6.0	14.1	-7	-3					
42ND	523.08									30.2	116.9	-3.0	.8	-.5
		7.4	29.1	1174	2023	6.3	14.4	-7	-3					
43RD	535.66									22.9	87.9	-1.8	.5	-.3
		7.9	29.9	1206	2078	6.5	14.4	-5	-2					
44TH	548.58									15.0	57.9	-.8	.2	-.2
		10.5	40.1	1680	2895	6.2	13.9	-3	-1					
MR	566.58									4.5	17.8	-.1	.0	-.2
		4.5	17.8	1085	2065	4.2	8.6	-12	-5					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 170 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									243.3	827.9	-311.7	84.5	-5.7
2ND	23.00	2.8	8.5	2147	3699	1.3	2.3	46	26	240.5	819.4	-292.8	79.0	-5.9
3RD	35.92	1.6	4.7	1206	2078	1.3	2.3	25	14	238.9	814.7	-282.2	75.9	-6.0
4TH	48.84	2.0	4.0	1206	2078	1.7	1.9	24	21	236.9	810.7	-271.7	72.8	-6.1
5TH	61.76	2.6	3.7	1206	2078	2.2	1.8	28	34	234.3	807.0	-261.2	69.8	-6.1
6TH	74.68	2.9	3.9	1206	2078	2.4	1.9	15	19	231.3	803.2	-250.8	66.8	-6.1
7TH	87.60	3.2	4.1	1206	2078	2.7	2.0	-1	-1	228.1	799.1	-240.5	63.8	-6.1
8TH	100.52	3.5	4.2	1206	2078	2.9	2.0	-20	-29	224.6	794.9	-230.2	60.9	-6.1
9TH	113.44	3.8	4.4	1206	2078	3.2	2.1	-47	-68	220.8	790.4	-220.0	58.0	-6.1
10TH	126.27	4.1	4.6	1197	2063	3.4	2.2	-84	-128	216.8	785.9	-209.8	55.2	-6.0
11TH	139.10	4.3	4.9	1197	2063	3.6	2.4	-85	-126	212.5	780.9	-199.8	52.4	-5.9
12TH	151.93	4.2	6.3	1197	2063	3.5	3.0	-36	-42	208.2	774.7	-189.8	49.7	-5.8
13TH	164.76	4.2	7.6	1197	2063	3.5	3.7	-27	-25	204.1	767.1	-179.9	47.1	-5.7
14TH	177.59	4.1	8.9	1197	2063	3.4	4.3	-23	-18	200.0	758.2	-170.1	44.5	-5.6
15TH	190.42	4.0	10.2	1197	2063	3.4	4.9	-21	-14	196.0	748.0	-160.5	41.9	-5.4
16TH	203.25	4.0	11.5	1197	2063	3.7	5.6	-20	-12	192.0	736.5	-151.0	39.5	-5.3
17TH	216.08	4.3	12.8	1197	2063	3.6	6.2	-18	-10	187.7	723.6	-141.6	37.0	-5.1
18TH	228.66	4.4	14.0	1174	2023	3.8	6.9	-17	-9	183.3	709.6	-132.6	34.7	-5.0
19TH	241.24	4.5	15.5	1174	2023	3.8	7.6	-15	-8	178.7	694.2	-123.7	32.4	-4.8
20TH	253.82	4.6	16.9	1174	2023	3.9	8.4	-14	-7	174.1	677.2	-115.1	30.2	-4.6
21ST	266.40	4.7	18.4	1174	2023	4.0	9.1	-13	-6	169.4	658.9	-106.7	28.0	-4.4
22ND	278.98	4.8	19.8	1174	2023	4.1	9.8	-13	-5	164.5	639.0	-98.5	25.9	-4.2
23RD	291.56	4.9	21.3	1174	2023	4.2	10.5	-12	-5	159.6	617.8	-90.6	23.9	-4.0
24TH	304.14	5.1	22.4	1174	2023	4.4	11.1	-12	-5	154.5	595.3	-83.0	21.9	-3.8
25TH	316.72	5.4	23.3	1174	2023	4.6	11.5	-11	-4	149.1	572.1	-75.7	20.0	-3.6
		5.5	23.6	1151	1983	4.8	11.9	-11	-4					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 170 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									143.7	548.5	-68.8	18.2	-3.4
		5.7	24.4	1151	1983	5.0	12.3	-10	-4					
27TH	341.38									138.0	524.0	-62.1	16.5	-3.2
		5.9	25.2	1151	1983	5.2	12.7	-10	-4					
28TH	353.71									132.0	498.8	-55.8	14.8	-3.1
		6.2	26.0	1151	1983	5.3	13.1	-10	-4					
29TH	366.04									125.9	472.8	-49.9	13.2	-2.9
		6.4	26.3	1127	1943	5.7	13.5	-9	-4					
30TH	378.12									119.5	446.5	-44.3	11.7	-2.7
		6.7	26.6	1127	1943	5.9	13.7	-8	-3					
31ST	390.20									112.7	419.8	-39.1	10.3	-2.5
		6.9	26.7	1127	1943	6.1	13.8	-8	-4					
32ND	402.28									105.9	393.1	-34.2	9.0	-2.4
		7.1	26.8	1127	1943	6.3	13.8	-8	-4					
33RD	414.36									98.8	366.2	-29.6	7.8	-2.2
		7.3	26.9	1127	1943	6.5	13.9	-8	-4					
34TH	426.44									91.5	339.3	-25.3	6.6	-2.0
		7.5	27.0	1127	1943	6.6	13.9	-9	-4					
35TH	438.52									84.0	312.2	-21.4	5.6	-1.9
		7.7	27.1	1127	1943	6.8	14.0	-9	-4					
36TH	450.60									76.4	285.1	-17.8	4.6	-1.7
		7.8	27.2	1127	1943	6.9	14.0	-9	-4					
37TH	462.68									68.6	257.9	-14.5	3.7	-1.5
		7.8	27.4	1127	1943	6.9	14.1	-9	-4					
38TH	474.76									60.8	230.4	-11.5	2.9	-1.3
		7.8	27.6	1127	1943	6.9	14.2	-9	-4					
39TH	486.84									53.0	202.8	-8.9	2.2	-1.1
		7.7	27.8	1127	1943	6.9	14.3	-9	-4					
40TH	498.92									45.3	175.0	-6.6	1.7	-1.0
		7.7	28.0	1127	1943	6.8	14.4	-9	-4					
41ST	511.00									37.6	147.0	-4.7	1.2	-.8
		7.7	28.2	1127	1943	6.8	14.5	-9	-4					
42ND	523.08									29.9	118.8	-3.1	.7	-.6
		8.0	29.6	1174	2023	6.8	14.6	-9	-4					
43RD	535.66									21.9	89.2	-1.8	.4	-.4
		8.1	30.3	1206	2078	6.7	14.6	-7	-3					
44TH	548.58									13.9	58.9	-.8	.2	-.2
		9.9	41.0	1680	2895	5.9	14.2	-3	-1					
MR	566.58									3.9	17.9	-.1	.0	-.1
		3.9	17.9	1085	2065	3.6	8.6	-10	-4					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 180 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									189.8	579.7	-229.2	69.3	-5.4
2ND	23.00	2.4	1.6	2147	3699	1.1	.4	-84	-217	187.4	578.1	-215.9	65.0	-5.6
3RD	35.92	1.4	.3	1206	2078	1.2	.1	-5	-44	186.0	577.8	-208.4	62.6	-5.6
4TH	48.84	1.5	.6	1206	2078	1.3	.3	-2	-7	184.4	577.2	-201.0	60.2	-5.6
5TH	61.76	1.8	.9	1206	2078	1.5	.4	3	12	182.7	576.3	-193.5	57.8	-5.6
6TH	74.68	1.9	.9	1206	2078	1.6	.5	6	21	180.7	575.4	-186.1	55.4	-5.6
7TH	87.60	2.1	1.0	1206	2078	1.7	.5	9	30	178.7	574.4	-178.7	53.1	-5.6
8TH	100.52	2.2	1.1	1206	2078	1.8	.5	11	37	176.4	573.3	-171.3	50.8	-5.5
9TH	113.44	2.4	1.2	1206	2078	2.0	.6	13	44	174.1	572.1	-163.9	48.6	-5.5
10TH	126.27	2.5	1.2	1197	2063	2.1	.6	14	49	171.5	570.9	-156.5	46.3	-5.4
11TH	139.10	2.6	1.5	1197	2063	2.2	.7	21	63	168.9	569.4	-149.2	44.2	-5.4
12TH	151.93	2.6	2.5	1197	2063	2.2	1.2	438	776	166.3	566.9	-141.9	42.0	-5.3
13TH	164.76	2.6	3.6	1197	2063	2.2	1.7	-70	-88	163.7	563.3	-134.7	39.9	-5.2
14TH	177.59	2.6	4.6	1197	2063	2.2	2.2	-45	-43	161.1	558.7	-127.5	37.8	-5.1
15TH	190.42	2.6	5.6	1197	2063	2.2	2.7	-37	-29	158.5	553.1	-120.3	35.8	-5.0
16TH	203.25	2.6	6.7	1197	2063	2.2	3.2	-33	-22	155.9	546.4	-113.3	33.7	-4.8
17TH	216.08	2.8	7.7	1197	2063	2.3	3.7	-29	-18	153.1	538.7	-106.3	31.8	-4.7
18TH	228.66	2.8	8.8	1174	2023	2.4	4.4	-25	-14	150.3	529.9	-99.6	29.9	-4.5
19TH	241.24	3.0	10.1	1174	2023	2.5	5.0	-22	-11	147.3	519.8	-93.0	28.0	-4.4
20TH	253.82	3.1	11.4	1174	2023	2.6	5.6	-20	-9	144.2	508.4	-86.5	26.1	-4.2
21ST	266.40	3.2	12.7	1174	2023	2.7	6.3	-18	-8	141.0	495.8	-80.2	24.4	-4.0
22ND	278.98	3.3	13.9	1174	2023	2.8	6.9	-17	-7	137.7	481.8	-74.1	22.6	-3.8
23RD	291.56	3.4	15.2	1174	2023	2.9	7.5	-16	-6	134.3	466.6	-68.1	20.9	-3.7
24TH	304.14	3.6	16.3	1174	2023	3.1	8.1	-15	-6	130.7	450.2	-62.3	19.2	-3.5
25TH	316.72	3.9	17.2	1174	2023	3.3	8.5	-15	-6	126.8	433.0	-56.8	17.6	-3.3
		4.1	17.8	1151	1983	3.6	9.0	-15	-6					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 180 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05	4.4	18.6	1151	1983	3.8	9.4	-15	-6	122.7	415.3	-51.5	16.1	-3.1
27TH	341.38	4.6	19.5	1151	1983	4.0	9.8	-15	-6	118.4	396.6	-46.5	14.6	-2.9
28TH	353.71	4.9	20.3	1151	1983	4.3	10.3	-15	-6	113.7	377.2	-41.8	13.1	-2.7
29TH	366.04	5.1	20.8	1127	1943	4.6	10.7	-12	-5	108.9	356.8	-37.2	11.8	-2.4
30TH	378.12	5.4	21.0	1127	1943	4.8	10.8	-11	-5	103.7	336.0	-33.1	10.5	-2.2
31ST	390.20	5.6	20.9	1127	1943	4.9	10.8	-11	-5	98.3	315.1	-29.1	9.3	-2.1
32ND	402.28	5.8	20.8	1127	1943	5.1	10.7	-10	-5	92.7	294.2	-25.4	8.1	-1.9
33RD	414.36	5.9	20.7	1127	1943	5.3	10.7	-9	-5	87.0	273.4	-22.0	7.0	-1.8
34TH	426.44	6.1	20.6	1127	1943	5.4	10.6	-9	-4	81.0	252.6	-18.8	6.0	-1.6
35TH	438.52	6.3	20.5	1127	1943	5.6	10.6	-8	-4	74.9	232.0	-15.9	5.1	-1.5
36TH	450.60	6.5	20.4	1127	1943	5.8	10.5	-7	-4	68.6	211.5	-13.2	4.2	-1.4
37TH	462.68	6.6	20.5	1127	1943	5.8	10.5	-8	-5	62.1	191.0	-10.8	3.4	-1.3
38TH	474.76	6.7	20.5	1127	1943	5.9	10.5	-9	-5	55.5	170.6	-8.6	2.7	-1.1
39TH	486.84	6.8	20.5	1127	1943	6.0	10.5	-10	-6	48.8	150.1	-6.7	2.1	-1.0
40TH	498.92	6.9	20.5	1127	1943	6.1	10.5	-11	-6	42.0	129.6	-5.0	1.5	-.9
41ST	511.00	7.0	20.5	1127	1943	6.2	10.5	-12	-7	35.1	109.2	-3.6	1.1	-.7
42ND	523.08	7.5	21.3	1174	2023	6.4	10.5	-11	-7	28.1	88.7	-2.4	.7	-.5
43RD	535.66	7 8	22.0	1206	2078	6.5	10.6	-8	-5	20.6	67.4	-1.4	.4	-.4
44TH	548.58	10.4	31.1	1680	2895	6.2	10.7	-4	-3	12.8	45.4	-.6	.2	-.2
MR	566.58	2.4	14.3	1085	2065	2.2	6.9	-13	-4	2.4	14.3	-.1	.0	-.1
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7 SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 190 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									283.4	486.0	-206.0	108.3	-7.2
2ND	23.00	2.7	.6	2147	3699	1.3	.2	-16	-113	280.7	485.4	-194.8	101.8	-7.3
3RD	35.92	1.1	-.0	1206	2078	.9	-.0	0	-92	279.6	485.4	-188.6	98.2	-7.4
4TH	48.84	1.3	-.4	1206	2078	1.1	-.2	8	-43	278.3	485.8	-182.3	94.6	-7.4
5TH	61.76	1.6	-.6	1206	2078	1.4	-.3	3	-14	276.6	486.3	-176.0	91.0	-7.4
6TH	74.68	1.9	-.5	1206	2078	1.6	-.2	-0	0	274.8	486.8	-169.7	87.5	-7.4
7TH	87.60	2.1	-.4	1206	2078	1.8	-.2	-1	10	272.7	487.1	-163.4	83.9	-7.4
8TH	100 52	2.3	-.3	1206	2078	1.9	-.1	-1	18	270.3	487.4	-157.1	80.4	-7.4
9TH	113.44	2.6	-.1	1206	2078	2.1	-.1	-1	24	267.7	487.5	-150.8	76.9	-7.3
10TH	126.27	2.8	-.0	1197	2063	2.3	-.0	-0	29	264.9	487.6	-144.6	73.5	-7.3
11TH	139.10	3.0	.2	1197	2063	2.5	.1	1	35	261.9	487.4	-138.3	70.1	-7.3
12TH	151.93	3.2	.9	1197	2063	2.6	.4	7	46	258.7	486.5	-132.1	66.8	-7.2
13TH	164.76	3.3	1.5	1197	2063	2.8	.7	17	63	255.4	485.0	-125.9	63.5	-7.1
14TH	177.59	3.5	2.2	1197	2063	2.9	1.1	35	94	251.9	482.8	-119.7	60.3	-7.0
15TH	190.42	3.6	2.9	1197	2063	3.0	1.4	77	166	248.3	480.0	-113.5	57.0	-6.9
16TH	203.25	3.8	3.5	1197	2063	3.2	1.7	289	528	244.5	476.5	-107.3	53.9	-6.8
17TH	216.08	4.4	4.2	1197	2063	3.7	2.0	432	769	240.2	472.3	-101.3	50.8	-6.7
18TH	228.66	4.6	5.1	1174	2023	3.9	2.5	-185	-282	235.6	467.2	-95.3	47.8	-6.5
19TH	241.24	4.7	6.1	1174	2023	4.0	3.0	-83	-109	230.9	461.1	-89.5	44.9	-6.3
20TH	253.82	4.9	7.2	1174	2023	4.2	3.5	-59	-69	225.9	453.9	-83.7	42.0	-6.2
21ST	266.40	5.1	8.2	1174	2023	4.3	4.0	-48	-51	220.8	445.7	-78.1	39.2	-6.0
22ND	278.98	5.3	9.2	1174	2023	4.5	4.6	-42	-41	215.6	436.5	-72.5	36.4	-5.8
23RD	291.56	5.5	10.3	1174	2023	4.7	5.1	-38	-34	210.1	426.2	-67.1	33.7	-5.5
24TH	304.14	5.7	11.3	1174	2023	4.8	5.6	-35	-30	204.4	415.0	-61.8	31.1	-5.3
25TH	316.72	5.9	12.3	1174	2023	5.0	6.1	-32	-26	198.5	402.6	-56.7	28.6	-5.1
		6.0	13.1	1151	1983	5.2	6.6	-30	-24					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 190 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									192.5	389.5	-51.8	26.2	-4.8
27TH	341.38	6.2	14.2	1151	1983	5.4	7.1	-29	-21	186.3	375.3	-47.1	23.9	-4.5
28TH	353.71	6.5	15.2	1151	1983	5.6	7.7	-27	-20	179.8	360.1	-42.5	21.6	-4.3
29TH	366.04	6.7	16.2	1151	1983	5.8	8.2	-26	-18	173.2	343.9	-38.2	19.4	-4.0
30TH	378.12	7.3	16.9	1127	1943	6.4	8.7	-23	-17	165.9	327.0	-34.2	17.4	-3.7
31ST	390.20	7.8	17.4	1127	1943	6.9	9.0	-21	-16	158.1	309.6	-30.3	15.4	-3.5
32ND	402.28	8.1	17.7	1127	1943	7.2	9.1	-21	-16	150.0	291.9	-26.7	13.6	-3.3
33RD	414.36	8.5	17.9	1127	1943	7.6	9.2	-20	-17	141.5	274.0	-23.3	11.8	-3.0
34TH	426.44	8.9	18.2	1127	1943	7.9	9.3	-20	-17	132.6	255.8	-20.1	10.1	-2.8
35TH	438.52	9.3	18.4	1127	1943	8.2	9.5	-20	-17	123.3	237.4	-17.1	8.6	-2.6
36TH	450.60	9.6	18.7	1127	1943	8.5	9.6	-19	-17	113.7	218.7	-14.3	7.2	-2.4
37TH	462.68	10.1	18.9	1127	1943	8.9	9.7	-20	-18	103.6	199.8	-11.8	5.9	-2.2
38TH	474.76	10.4	19.3	1127	1943	9.2	9.9	-21	-19	93.2	180.5	-9.5	4.7	-2.0
39TH	486.84	10.6	19.8	1127	1943	9 4	10.2	-22	-20	82.6	160.8	-7.4	3.6	-1.7
40TH	498.92	10.9	20.2	1127	1943	9.7	10.4	-23	-21	71.7	140.6	-5.6	2.7	-1.4
41ST	511.00	11.2	20.7	1127	1943	9.9	10.6	-24	-22	60.5	119.9	-4.0	1.9	-1.2
42ND	523.08	11.5	21.1	1127	1943	10.2	10.9	-25	-23	49.0	98.8	-2.7	1.2	-.9
43RD	535.66	12.5	22.5	1174	2023	10.6	11.1	-23	-22	36.5	76.3	-1.6	.7	-.6
44TH	548.58	13.5	23.6	1206	2078	11.2	11.3	-17	-16	23.0	52.7	-.8	.3	-.4
MR	566.58	18.1	33.7	1680	2895	10.8	11.6	-8	-8	4.9	19.1	- 1	.0	-.2
TOP	581.67	4.9	19.1	1085	2065	4.5	9.2	-15	-7	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 200 CONFIGURATION A REFERENCE PRESSURE 34 0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									345.6	300.3	-134.1	132.7	-5.7
2ND	23.00	1.5	-3.9	2147	3699	.7	-1.0	-49	33	344.1	304.2	-127.1	124.8	-5.9
3RD	35.92	-.1	-2.3	1206	2078	-.1	-1.1	-28	-2	344.1	306.4	-123.2	120.4	-5.9
4TH	48.84	.4	-2.4	1206	2078	.4	-1.2	-21	7	343.7	308.9	-119.2	115.9	-5.9
5TH	61.76	1.0	-2.5	1206	2078	.9	-1.2	-17	13	342.7	311.3	-115.2	111.5	-6.0
6TH	74.68	1.4	-2.3	1206	2078	1.2	-1.1	-14	15	341.2	313.6	-111 2	107.1	-6.0
7TH	87.60	1 8	-2.1	1206	2078	1.5	-1.0	-10	14	339.5	315.8	-107.1	102.7	-6.0
8TH	100.52	2.2	-2.0	1206	2078	1.8	-1.0	-23	43	337.3	317.7	-103.0	98.3	-6.0
9TH	113.44	2.5	-1.8	1206	2078	2.1	-.9	-14	32	334.8	319.6	-98.9	94.0	-6.0
10TH	126.27	2.9	-1.7	1197	2063	2.4	-.8	-11	32	331.9	321.2	-94.8	89.7	-5.9
11TH	139.10	3.2	-1.4	1197	2063	2.7	-.7	-8	32	328.7	322.6	-90.6	85.4	-5.9
12TH	151.93	3.6	-.7	1197	2063	3.0	-.3	-3	32	325.0	323.3	-86.5	81.2	-5.8
13TH	164.76	4.0	.1	1197	2063	3.4	.0	0	34	321.0	323.2	-82.4	77.1	-5.8
14TH	177.59	4.4	.8	1197	2063	3.7	.4	4	38	316.6	322.4	-78.2	73.0	-5.7
15TH	190.42	4.8	1.5	1197	2063	4.0	.7	8	44	311.8	320.9	-74.1	69.0	-5.6
16TH	203.25	5.2	2.3	1197	2063	4.3	1.1	13	51	306.7	318.6	-70.0	65.0	-5.5
17TH	216.08	6.4	3.0	1197	2063	5.4	1.4	12	45	300.2	315.7	-65.9	61.1	-5.4
18TH	228.66	6.7	3.7	1174	2023	5.7	1.8	18	55	293.5	311.9	-62 0	57.4	-5.3
19TH	241.24	7.0	4.5	1174	2023	5.9	2.2	27	72	286.5	307.4	-58.1	53.7	-5.2
20TH	253.82	7.2	5.3	1174	2023	6.2	2.6	43	99	279.3	302.1	-54.2	50.2	-5.0
21ST	266.40	7.5	6.1	1174	2023	6.4	3.0	72	150	271.8	295.9	-50 5	46.7	-4.8
22ND	278.98	7.7	6.9	1174	2023	6.6	3.4	145	274	264.1	289.0	-46.8	43.3	-4.6
23RD	291.56	8.0	7.8	1174	2023	6.8	3.8	634	1107	256.2	281.2	-43.2	40.1	-4.4
24TH	304.14	8.1	8.4	1174	2023	6.9	4.2	-429	-702	248.0	272.8	-39.7	36.9	-4.2
25TH	316.72	8.2	9.0	1174	2023	7.0	4.4	-178	-275	239.9	263.8	-36.3	33.8	-4.0
		8.1	9.4	1151	1983	7.0	4.7	-118	-172					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 200 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									231.8	254.4	-33.2	30.9	-3.8
		8.1	9.9	1151	1983	7.1	5.0	-90	-126					
27TH	341.38									223.7	244.5	-30.1	28.1	-3.5
		8.2	10.4	1151	1983	7.1	5.3	-75	-100					
28TH	353.71									215.5	234.1	-27.1	25.4	-3.3
		8.2	11.0	1151	1983	7.1	5.5	-65	-83					
29TH	366.04									207.3	223.1	-24.3	22.8	-3.0
		9.0	11.3	1127	1943	8.0	5.8	-67	-91					
30TH	378.12									198.3	211.8	-21.7	20.4	-2.8
		9.7	11.6	1127	1943	8.6	6.0	-72	-103					
31ST	390.20									188.6	200.2	-19.2	18.0	-2.6
		10.1	11.8	1127	1943	9.0	6.1	-77	-113					
32ND	402.28									178.5	188.4	-16.8	15.8	-2.4
		10.6	12.1	1127	1943	9.4	6.2	-84	-126					
33RD	414.36									167.9	176.4	-14.6	13.7	-2.2
		11.1	12.3	1127	1943	9.8	6.3	-94	-144					
34TH	426.44									156.9	164.1	-12.6	11.7	-2.1
		11.5	12.5	1127	1943	10.2	6.4	-109	-170					
35TH	438.52									145.3	151.6	-10.7	9.9	-1.9
		12.0	12.8	1127	1943	10.6	6.6	-132	-210					
36TH	450.60									133.4	138.8	-8.9	8.2	-1.7
		12.6	13.0	1127	1943	11.2	6.7	-256	-422					
37TH	462.68									120.8	125.8	-7.3	6.7	-1.6
		12.7	12.9	1127	1943	11.3	6.7	-496	-831					
38TH	474.76									108.0	112.9	-5.9	5.3	-1.4
		12.8	13.0	1127	1943	11.4	6.7	-827	-1393					
39TH	486.84									95.2	99.9	-4.6	4.1	-1.2
		12.9	13.0	1127	1943	11.4	6.7	$$$$	-3595					
40TH	498.92									82.3	87.0	-3.5	3.0	-1.1
		13.0	13.0	1127	1943	11.5	6.7	4818	8216					
41ST	511.00									69.3	74.0	-2.5	2.1	-.9
		13.1	13.0	1127	1943	11.6	6.7	1198	2055					
42ND	523.08									56.3	61.0	-1.7	1.3	-.7
		14.4	13.5	1174	2023	12.3	6.7	124	225					
43RD	535.66									41.9	47.5	-1.0	.7	-.5
		16.2	14.3	1206	2078	13.5	6.9	37	71					
44TH	548.58									25.6	33.2	-.5	.3	-.4
		22.2	22.5	1680	2895	13.2	7.8	-403	-678					
MR	566.58									3.5	10.7	-.1	.0	-.2
		3.5	10.7	1085	2065	3.2	5.2	-24	-13					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 210 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									346.9	-174.2	55.7	128.5	1.2
2ND	23.00	4.1	-2.0	2147	3699	1.9	-.5	-3	9	342.9	-172.2	51.8	120.5	1.2
3RD	35.92	.5	-1.9	1206	2078	.4	-.9	8	-3	342.4	-170.3	49.5	116.1	1.3
4TH	48.84	1.2	-2.1	1206	2078	1.0	-1.0	7	-6	341.2	-168.2	47.4	111.7	1.3
5TH	61.76	1.9	-2.3	1206	2078	1.6	-1.1	17	-25	339.3	-165.9	45.2	107.3	1.3
6TH	74.68	2.3	-2.4	1206	2078	1.9	-1.2	50	-84	336.9	-163.5	43.1	102.9	1.3
7TH	87.60	2.7	-2.5	1206	2078	2.3	-1.2	-2	3	334.2	-161.0	41.0	98.6	1.3
8TH	100.52	3.1	-2.7	1206	2078	2.6	-1.3	4	-8	331.0	-158.3	38.9	94.3	1.3
9TH	113.44	3.5	-2.8	1206	2078	2.9	-1.4	5	-11	327.5	-155.5	36.9	90.0	1.3
10TH	126.27	3.9	-3.0	1197	2063	3.3	-1.4	6	-13	323.6	-152.5	34.9	85.9	1.3
11TH	139.10	4.3	-3.1	1197	2063	3.6	-1.5	6	-14	319.3	-149.4	33.0	81.7	1.2
12TH	151.93	4.5	-3.2	1197	2063	3.7	-1.5	5	-11	314.8	-146.2	31.1	77.7	1.2
13TH	164.76	4.7	-3.3	1197	2063	3.9	-1.6	4	-9	310.1	-142.9	29.2	73.7	1.2
14TH	177.59	4.9	-3.4	1197	2063	4.1	-1.7	3	-7	305.2	-139.5	27.4	69.7	1.2
15TH	190.42	5.1	-3.5	1197	2063	4.3	-1.7	2	-5	300.1	-136.0	25.6	65.8	1.2
16TH	203.25	5.4	-3.6	1197	2063	4.5	-1.8	1	-3	294.7	-132.4	23.9	62.0	1.2
17TH	216.08	6.5	-3.7	1197	2063	5.5	-1.8	2	-5	288.2	-128.7	22.2	58.3	1.2
18TH	228.66	6.8	-3.8	1174	2023	5.8	-1.9	3	-8	281.3	-124.8	20.7	54.7	1.2
19TH	241.24	7.1	-4.0	1174	2023	6.0	-2.0	4	-11	274.3	-120.8	19.1	51.2	1.1
20TH	253.82	7.3	-4.2	1174	2023	6.3	-2.1	5	-14	266.9	-116.6	17.6	47.8	1.1
21ST	266.40	7.6	-4.4	1174	2023	6.5	-2.2	6	-17	259.3	-112.2	16.2	44.5	1.1
22ND	278.98	7.9	-4.6	1174	2023	6.7	-2.3	7	-20	251.4	-107.6	14.8	41.3	1.0
23RD	291.56	8.1	-4.8	1174	2023	6.9	-2.4	8	-23	243.3	-102.8	13.5	38.2	1.0
24TH	304.14	8.2	-5.0	1174	2023	7.0	-2.5	9	-24	235.1	-97.8	12.2	35.1	.9
25TH	316.72	8.2	-5.0	1174	2023	7.0	-2.5	8	-22	226.9	-92.8	11.0	32.2	.9
		7.9	-5.0	1151	1983	6.9	-2.5	7	-20					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 210 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05													
		7.9	-5.0	1151	1983	6.8	-2.5	7	-18	218.9	-87.8	9.9	29.5	.8
27TH	341.38	7.8	-5.0	1151	1983	6.8	-2.5	6	-16	211.1	-82.9	8.8	26.8	.8
28TH	353.71	7.7	-5.1	1151	1983	6.7	-2.6	5	-14	203.3	-77.8	7.9	24.3	.7
29TH	366.04	8.6	-5.0	1127	1943	7.6	-2.6	5	-15	195.5	-72.7	6.9	21.8	.7
30TH	378.12	9.2	-5.0	1127	1943	8.2	-2.6	5	-16	186.9	-67.7	6.1	19.5	.7
31ST	390.20	9.6	-4.9	1127	1943	8.5	-2.5	5	-15	177.7	-62.7	5.3	17.3	.6
32ND	402.28	9.9	-4.8	1127	1943	8.8	-2.5	4	-15	168.1	-57.8	4.6	15.2	.6
33RD	414.36	10.2	-4.7	1127	1943	9.1	-2.4	4	-14	158.2	-53.0	3.9	13.3	.5
34TH	426.44	10.5	-4.6	1127	1943	9.4	-2.3	3	-13	148.0	-48.3	3.3	11.4	.5
35TH	438.52	10.9	-4.4	1127	1943	9.6	-2.3	3	-13	137.5	-43.7	2.7	9.7	.4
36TH	450.60	11.3	-4.3	1127	1943	10.0	-2.2	2	-11	126.6	-39.3	2.2	8.1	.4
37TH	462.68	11.5	-4.3	1127	1943	10.2	-2.2	2	-10	115.3	-34.9	1.8	6.6	.3
38TH	474.76	11.6	-4.3	1127	1943	10.3	-2.2	2	-9	103.8	-30.6	1.4	5.3	.3
39TH	486.84	11.7	-4.3	1127	1943	10.4	-2.2	2	-9	92.2	-26.3	1.0	4.1	.2
40TH	498.92	11.8	-4.3	1127	1943	10.5	-2.2	2	-8	80.4	-22.0	.7	3.1	.2
41ST	511.00	12.0	-4.2	1127	1943	10.6	-2.2	2	-8	68.6	-17.8	.5	2.2	.1
42ND	523.08	13.4	-4.4	1174	2023	11.4	-2.2	2	-9	56.7	-13.5	.3	1.4	.1
43RD	535.66	15.7	-4.1	1206	2078	13.0	-2.0	1	-9	43.3	-9.2	.2	.8	.0
44TH	548.58	22.7	-2.9	1680	2895	13.5	-1.0	0	-2	27.6	-5.1	.1	.3	-.0
MR	566.58	5.0	-2.2	1085	2065	4.6	-1.1	-6	24	5.0	-2.2	.0	.0	-.0
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 220 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									206.9	-445.5	153.3	85.0	5.1
2ND	23.00	-1.9	-5.6	2147	3699	-.9	-1.5	12	7	208.8	-439.9	143.1	80.2	5.2
3RD	35.92	-1.9	-4.2	1206	2078	-1.5	-2.0	8	6	210.6	-435.7	137.5	77.5	5.2
4TH	48.84	-1.6	-4.6	1206	2078	-1.3	-2.2	8	4	212.2	-431.1	131.9	74.7	5.2
5TH	61.76	-1.2	-5.0	1206	2078	-1.0	-2.4	6	3	213.4	-426.0	126.3	72.0	5.2
6TH	74.68	-.8	-5.3	1206	2078	-.7	-2.6	3	1	214.3	-420.7	120.9	69.2	5.2
7TH	87.60	-.5	-5.7	1206	2078	-.4	-2.7	0	0	214.7	-415.0	115.5	66.5	5.2
8TH	100.52	-.1	-6.0	1206	2078	-.1	-2.9	-2	0	214.8	-409.1	110.1	63.7	5.2
9TH	113.44	.3	-6.3	1206	2078	.2	-3.0	-4	0	214.6	-402.8	104.9	60.9	5.2
10TH	126.27	.6	-6.5	1197	2063	.5	-3.2	-6	1	214.0	-396.3	99.8	58.2	5.2
11TH	139.10	1.0	-6.8	1197	2063	.8	-3.3	-8	2	213.0	-389.5	94.7	55.4	5.1
12TH	151.93	1.4	-7.1	1197	2063	1.2	-3.4	-10	4	211.5	-382.5	89.8	52.7	5.1
13TH	164.76	1.9	-7.4	1197	2063	1.6	-3.6	-12	5	209.6	-375.1	84.9	50.0	5.0
14TH	177.59	2.3	-7.6	1197	2063	1.9	-3.7	-14	7	207.3	-367.5	80.1	47.3	4.9
15TH	190.42	2.8	-7.9	1197	2063	2.3	-3.8	-16	10	204.5	-359.6	75.5	44.7	4.8
16TH	203.25	3.2	-8.2	1197	2063	2.7	-4.0	-18	12	201.3	-351.3	70.9	42.1	4.7
17TH	216.08	4.4	-8.5	1197	2063	3.7	-4.1	-23	20	196.9	-342.8	66.5	39.5	4.6
18TH	228.66	4.7	-8.6	1174	2023	4.0	-4.3	-26	24	192.2	-334.2	62.2	37.1	4.5
19TH	241.24	4.9	-8.9	1174	2023	4.2	-4.4	-27	25	187.3	-325.2	58.1	34.7	4.4
20TH	253.82	5.2	-9.3	1174	2023	4.4	-4.6	-29	27	182.1	-316.0	54.0	32.4	4.2
21ST	266.40	5.4	-9.6	1174	2023	4.6	-4.7	-30	29	176.6	-306.4	50.1	30.1	4.1
22ND	278.98	5.7	-9.9	1174	2023	4.8	-4.9	-31	31	171.0	-296.6	46.3	27.9	3.9
23RD	291.56	5.9	-10.2	1174	2023	5.0	-5.0	-33	32	165.1	-286.4	42.7	25.8	3.7
24TH	304.14	6.0	-10.5	1174	2023	5.1	-5.2	-32	31	159.1	-275.9	39.1	23.8	3.5
25TH	316.72	5.9	-10.8	1174	2023	5.0	-5.3	-30	28	153.2	-265.1	35.7	21.8	3.4
		5.7	-10.8	1151	1983	4.9	-5.4	-28	25					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 220 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05	5.5	-11.0	1151	1983	4.8	-5.6	-27	23	147.5	-254.3	32.5	20.0	3.2
27TH	341.38	5.4	-11.3	1151	1983	4.7	-5.7	-26	21	142.0	-243.3	29.4	18.2	3.0
28TH	353.71	5.3	-11.6	1151	1983	4.6	-5.8	-24	19	136.5	-232.0	26.5	16.5	2.8
29TH	366.04	5.9	-11.6	1127	1943	5.2	-6.0	-26	22	131.2	-220.4	23.7	14.8	2.6
30TH	378.12	6.3	-11.8	1127	1943	5.5	-6.1	-26	23	125.3	-208.9	21.1	13.3	2.5
31ST	390.20	6.4	-12.0	1127	1943	5.7	-6.2	-25	23	119.1	-197.1	18.7	11.8	2.3
32ND	402.28	6.6	-12.1	1127	1943	5.8	-6.2	-24	22	112.7	-185.1	16.4	10.4	2.1
33RD	414.36	6.7	-12.3	1127	1943	6.0	-6.3	-23	22	106.1	-173.0	14.2	9.1	2.0
34TH	426.44	6.9	-12.5	1127	1943	6.1	-6.4	-23	21	99.3	-160.7	12.2	7.8	1.8
35TH	438.52	7.1	-12.6	1127	1943	6.3	-6.5	-22	21	92.4	-148.3	10.3	6.7	1.6
36TH	450.60	7.3	-12.8	1127	1943	6.5	-6.6	-21	20	85.3	-135.6	8.6	5.6	1.5
37TH	462.68	7.5	-12.9	1127	1943	6.6	-6.6	-21	21	78.1	-122.8	7.0	4.6	1.3
38TH	474.76	7.6	-12.9	1127	1943	6.7	-6.6	-22	22	70.6	-109.9	5.6	3.7	1.2
39TH	486.84	7.7	-12.9	1127	1943	6.9	-6.7	-23	23	63.0	-97.0	4.4	2.9	1.1
40TH	498.92	7.9	-13.0	1127	1943	7.0	-6.7	-23	24	55.3	-84.1	3.3	2.2	.9
41ST	511.00	8.0	-13.0	1127	1943	7.1	-6.7	-24	25	47.4	-71.1	2.4	1.6	.7
42ND	523.08	8.9	-13.6	1174	2023	7.6	-6.7	-25	28	39.4	-58.1	1.6	1.0	.6
43RD	535.66	10.2	-14.1	1206	2078	8.4	-6.8	-26	32	30.5	-44.5	.9	.6	.4
44TH	548.58	15.3	-20.0	1680	2895	9.1	-6.9	-27	35	20.3	-30.5	.4	.3	.3
MR	566.58	5.0	-10.5	1085	2065	4.6	-5.1	-18	14	5.0	-10.5	.1	.0	.1
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 230 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									194.2	-836.2	295.9	88.2	6.9
2ND	23.00	-1.9	-13.9	2147	3699	-.9	-3.8	27	6	196.1	-822.3	276.8	83.7	7.2
3RD	35.92	-1.9	-8.9	1206	2078	-1.5	-4.3	21	7	197.9	-813.4	266.2	81.1	7.3
4TH	48.84	-1.4	-8.9	1206	2078	-1.2	-4.3	18	5	199.4	-804.6	255.8	78.6	7.4
5TH	61.76	-.9	-9.0	1206	2078	-.8	-4.3	18	3	200.3	-795.5	245.4	76.0	7.6
6TH	74.68	-.8	-9.4	1206	2078	-.6	-4.5	16	2	201.0	-786.2	235.2	73.4	7.7
7TH	87.60	-.6	-9.7	1206	2078	-.5	-4.7	14	1	201.6	-776.5	225.1	70.8	7.8
8TH	100.52	-.4	-10.0	1206	2078	-.3	-4.8	12	1	202.0	-766.5	215.2	68.2	7.9
9TH	113.44	-.2	-10.4	1206	2078	-.2	-5.0	10	0	202.2	-756.1	205.3	65.6	8.0
10TH	126.27	-.0	-10.6	1197	2063	-.0	-5.1	9	0	202.3	-745.5	195.7	63.0	8.0
11TH	139.10	.1	-10.9	1197	2063	.1	-5.3	7	-0	202.1	-734.5	186.2	60.4	8.1
12TH	151.93	.3	-11.5	1197	2063	.2	-5.6	4	-0	201.8	-723.1	176.9	57.8	8.1
13TH	164.76	.4	-12.0	1197	2063	.3	-5.8	1	-0	201.4	-711.1	167.7	55.2	8.1
14TH	177.59	.5	-12.5	1197	2063	.4	-6.0	-2	0	200.9	-698.7	158.6	52.6	8.1
15TH	190.42	.7	-13.0	1197	2063	.6	-6.3	-4	0	200.2	-685.7	149.7	50.1	8.1
16TH	203.25	.8	-13.5	1197	2063	.7	-6.5	-6	1	199.4	-672.2	141.0	47.5	8.0
17TH	216.08	1.2	-14.0	1197	2063	1.0	-6.8	-7	1	198.2	-658.2	132.5	44.9	7.9
18TH	228.66	1.7	-14.3	1174	2023	1.4	-7.1	-8	2	196.5	-643.9	124.3	42.5	7.8
19TH	241.24	2.1	-14.9	1174	2023	1.8	-7.3	-10	2	194.5	-629.1	116.3	40.0	7.7
20TH	253.82	2.5	-15.4	1174	2023	2.2	-7.6	-12	3	191.9	-613.7	108.5	37.6	7.6
21ST	266.40	3.0	-16.0	1174	2023	2.5	-7.9	-13	4	188.9	-597.6	100.8	35.2	7.4
22ND	278.98	3.4	-16.6	1174	2023	2.9	-8.2	-14	5	185.5	-581.0	93.4	32.8	7.2
23RD	291.56	3.9	-17.2	1174	2023	3.3	-8.5	-16	6	181.7	-563.9	86.2	30.5	7.0
24TH	304.14	4.2	-17.8	1174	2023	3.6	-8.8	-17	7	177.5	-546.0	79.2	28.3	6.8
25TH	316.72	4.4	-18.7	1174	2023	3.7	-9.2	-17	7	173.1	-527.3	72.5	26.1	6.6
		4.5	-19.2	1151	1983	3.9	-9.7	-17	7					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 230 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									168.7	-508.2	66.1	23.9	6.3
27TH	341.38	4.6	-20.0	1151	1983	4.0	-10.1	-18	7	164.0	-488.2	60.0	21.9	6.0
28TH	353.71	4.8	-20.8	1151	1983	4.2	-10.5	-18	7	159.2	-467.4	54.1	19.9	5.8
29TH	366.04	5.0	-21.6	1151	1983	4.3	-10.9	-18	7	154.3	-445.7	48.5	18.0	5.5
30TH	378.12	5.3	-22.0	1127	1943	4.7	-11.3	-17	7	149.0	-423.7	43.2	16.1	5.2
31ST	390.20	5.8	-22.7	1127	1943	5.2	-11.7	-17	7	143.2	-401.0	38.2	14.4	4.9
32ND	402.28	6.3	-23.3	1127	1943	5.6	-12.0	-17	8	136.8	-377.7	33.5	12.7	4.6
33RD	414.36	6.9	-24.0	1127	1943	6.1	-12.3	-18	9	130.0	-353.7	29.1	11.1	4.3
34TH	426.44	7.4	-24.6	1127	1943	6.6	-12.6	-18	9	122.5	-329.1	25.0	9.5	4.0
35TH	438.52	7.9	-25.2	1127	1943	7.1	-13.0	-19	10	114.6	-303.9	21.1	8.1	3.6
36TH	450.60	8.5	-25.8	1127	1943	7.5	-13.3	-19	11	106.1	-278.1	17.6	6.8	3.3
37TH	462.68	9.1	-26.4	1127	1943	8.0	-13.6	-19	11	97.1	-251.7	14.4	5.6	2.9
38TH	474.76	9.4	-26.6	1127	1943	8.4	-13.7	-19	12	87.6	-225.2	11.6	4.4	2.5
39TH	486.84	9.8	-26.6	1127	1943	8.7	-13.7	-19	12	77.9	-198.6	9.0	3.4	2.2
40TH	498.92	10.1	-26.6	1127	1943	9.0	-13.7	-19	13	67.8	-172.0	6.8	2.6	1.8
41ST	511.00	10.4	-26.7	1127	1943	9.3	-13.7	-19	13	57.3	-145.3	4.8	1.8	1.5
42ND	523.08	10.8	-26.7	1127	1943	9.6	-13.7	-19	13	46.5	-118.6	3.2	1.2	1.1
43RD	535.66	11.8	-27.8	1174	2023	10.1	-13.7	-18	13	34.7	-90.8	1.9	.7	.8
44TH	548.58	12.6	-28.5	1206	2078	10.5	-13.7	-14	11	22.1	-62.3	.9	.3	.5
MR	566.58	16.2	-39.5	1680	2895	9.6	-13.6	-9	7	5.9	-22.8	.2	.0	.3
TOP	581.67	5.9	-22.8	1085	2065	5.5	-11.0	-17	8	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 240 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									131.2	-1509.5	516.7	83.1	5.1
2ND	23.00	-5.6	-30.5	2147	3699	-2.6	-8.3	18	6	136.7	-1478.9	482.4	80.0	5.5
3RD	35.92	-4.3	-18.2	1206	2078	-3.6	-8.8	16	7	141.1	-1460.7	463.4	78.2	5.7
4TH	48.84	-4.3	-17.4	1206	2078	-3.5	-8.4	15	6	145.3	-1443.3	444.6	76.3	5.9
5TH	61.76	-4.0	-17.3	1206	2078	-3.3	-8.3	15	6	149.4	-1426.0	426.1	74.4	6.1
6TH	74.68	-3.8	-17.9	1206	2078	-3.2	-8.6	13	5	153.2	-1408.1	407.8	72.5	6.3
7TH	87.60	-3.6	-18.5	1206	2078	-3.0	-8.9	11	4	156.8	-1389.6	389.7	70.5	6.5
8TH	100.52	-3.4	-19.1	1206	2078	-2.8	-9.2	10	3	160.3	-1370.5	371.9	68.4	6.6
9TH	113.44	-3.2	-19.7	1206	2078	-2.7	-9.5	8	2	163.5	-1350.8	354.3	66.3	6.7
10TH	126.27	-3.0	-20.2	1197	2063	-2.5	-9.8	7	2	166.5	-1330.6	337.1	64.2	6.8
11TH	139.10	-2.8	-20.9	1197	2063	-2.4	-10.1	5	1	169.3	-1309.7	320.2	62.1	6.9
12TH	151.93	-2.8	-22.0	1197	2063	-2.3	-10.7	3	1	172.1	-1287.7	303.5	59.9	7.0
13TH	164.76	-2.7	-23.1	1197	2063	-2.2	-11.2	1	0	174.8	-1264.6	287.1	57.6	7.0
14TH	177.59	-2.6	-24.3	1197	2063	-2.2	-11.8	-0	-0	177.4	-1240.3	271.1	55.4	7.0
15TH	190.42	-2.5	-25.4	1197	2063	-2.1	-12.3	-2	-0	179.9	-1214.9	255.3	53.1	7.0
16TH	203.25	-2.5	-26.6	1197	2063	-2.1	-12.9	-3	-1	182.4	-1188.3	239.9	50.8	6.9
17TH	216.08	-2.4	-27.7	1197	2063	-2.0	-13.4	-4	-1	184.8	-1160.6	224.8	48.4	6.8
18TH	228.66	-2.0	-28.4	1174	2023	-1.7	-14.0	-4	-1	186.8	-1132.2	210.4	46.1	6.7
19TH	241.24	-1.6	-29.7	1174	2023	-1.3	-14.7	-5	-0	188.3	-1102.4	196.3	43.7	6.6
20TH	253.82	-1.1	-31.0	1174	2023	-1.0	-15.3	-6	-0	189.5	-1071.4	182.7	41.3	6.5
21ST	266.40	-.7	-32.3	1174	2023	-.6	-16.0	-6	-0	190.2	-1039.1	169.4	38.9	6.3
22ND	278.98	-.3	-33.6	1174	2023	-.3	-16.6	-7	-0	190.5	-1005.5	156.5	36.6	6.1
23RD	291.56	.1	-34.9	1174	2023	.1	-17.3	-7	0	190.4	-970.6	144.1	34.2	5.9
24TH	304.14	.7	-36.2	1174	2023	.6	-17.9	-8	0	189.8	-934.4	132.1	31.8	5.7
25TH	316.72	1.5	-37.1	1174	2023	1.3	-18.3	-8	1	188.2	-897.3	120.6	29.4	5.4
		2.3	-37.2	1151	1983	2.0	-18.7	-8	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 240 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									186.0	-860.2	109.8	27.1	5.2
		3.1	-38.0	1151	1983	2.7	-19.2	-9	1					
27TH	341.38									182.9	-822.1	99.4	24.8	4.9
		3.8	-38.9	1151	1983	3.3	-19.6	-9	2					
28TH	353.71									179.1	-783.2	89.5	22.6	4.6
		4.6	-39.7	1151	1983	4.0	-20.0	-9	2					
29TH	366.04									174.4	-743.5	80.1	20.4	4.4
		5.1	-39.8	1127	1943	4.6	-20.5	-8	2					
30TH	378.12									169.3	-703.7	71.3	18.3	4.1
		5.9	-40.3	1127	1943	5.2	-20.8	-8	2					
31ST	390.20									163.4	-663.4	63.1	16.3	3.9
		6.7	-40.6	1127	1943	6.0	-20.9	-8	2					
32ND	402.28									156.6	-622.8	55.3	14.4	3.6
		7.6	-41.0	1127	1943	6.7	-21.1	-8	2					
33RD	414.36									149.0	-581.8	48.0	12.5	3.4
		8.4	-41.3	1127	1943	7.5	-21.3	-8	3					
34TH	426.44									140.6	-540.5	41.3	10.8	3.1
		9.3	-41.6	1127	1943	8.2	-21.4	-8	3					
35TH	438.52									131.3	-498.9	35.0	9.1	2.9
		10.1	-41.9	1127	1943	9.0	-21.6	-8	3					
36TH	450.60									121.2	-457.0	29.2	7.6	2.6
		10.9	-42.2	1127	1943	9.7	-21.7	-8	3					
37TH	462.68									110.3	-414.7	23.9	6.2	2.4
		11.2	-42.6	1127	1943	10.0	-21.9	-8	4					
38TH	474.76									99.0	-372.1	19.2	5.0	2.1
		11.5	-43.0	1127	1943	10.2	-22.1	-8	4					
39TH	486.84									87.5	-329.1	15.0	3.8	1.9
		11.8	-43.4	1127	1943	10.5	-22.3	-8	4					
40TH	498.92									75.7	-285.7	11.2	2.8	1.6
		12.1	-43.8	1127	1943	10.7	-22.5	-9	4					
41ST	511.00									63.6	-241.9	8.1	2.0	1.3
		12.4	-44.2	1127	1943	11.0	-22.7	-9	4					
42ND	523.08									51.2	-197.7	5.4	1.3	1.0
		13.3	-46.4	1174	2023	11.3	-22.9	-8	4					
43RD	535.66									37.9	-151.3	3.2	.7	.7
		13.5	-47.7	1206	2078	11.2	-23.0	-6	3					
44TH	548.58									24.4	-103.6	1.6	.3	.5
		16.8	-65.3	1680	2895	10.0	-22.5	-3	1					
MR	566.58									7.5	-38.3	.3	.1	.4
		7.5	-38.3	1085	2065	6.9	-18.5	-13	4					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 25° CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									486.5	-1779.0	576.8	197.7	.8
2ND	23.00	.7	-39.2	2147	3699	.3	-10.6	27	-1	485.8	-1739.7	536.3	186.6	1.6
3RD	35.92	-1.7	-23.8	1206	2078	-1.4	-11.5	21	2	487.4	-1715.9	514.0	180.3	2.0
4TH	48.84	-.8	-23.0	1206	2078	-.6	-11.0	17	1	488.2	-1692.9	492.0	174.0	2.3
5TH	61.76	.6	-23.0	1206	2078	.5	-11.1	16	-1	487.6	-1669.9	470.3	167.7	2.6
6TH	74.68	1.3	-24.2	1206	2078	1.0	-11.6	14	-1	486.4	-1645.8	448.8	161.4	2.9
7TH	87.60	1.9	-25.4	1206	2078	1.6	-12.2	12	-1	484.5	-1620.4	427.7	155.1	3.1
8TH	100.52	2.5	-26.6	1206	2078	2.1	-12.8	9	-2	481.9	-1593.7	407.0	148.9	3.3
9TH	113.44	3.2	-27.8	1206	2078	2.6	-13.4	8	-1	478.7	-1565.9	386.6	142.7	3.5
10TH	126.27	3.8	-28.8	1197	2063	3.2	-14.0	6	-1	474.9	-1537.1	366.7	136.5	3.6
11TH	139.10	4.3	-30.0	1197	2063	3.6	-14.5	4	-1	470.6	-1507.1	347.1	130.5	3.7
12TH	151.93	4.5	-31.4	1197	2063	3.8	-15.2	2	-1	466.1	-1475.7	328.0	124.5	3.8
13TH	164.76	4.7	-32.8	1197	2063	3.9	-15.9	1	-0	461.4	-1442.9	309.3	118.5	3.8
14TH	177.59	4.9	-34.2	1197	2063	4.1	-16.6	-1	0	456.4	-1408.7	291.0	112.6	3.8
15TH	190.42	5.1	-35.6	1197	2063	4.3	-17.3	-2	1	451.3	-1373.1	273.1	106.8	3.7
16TH	203.25	5.3	-37.1	1197	2063	4.4	-18.0	-4	1	446.0	-1336.0	255.8	101.0	3.6
17TH	216.08	6.5	-38.5	1197	2063	5.4	-18.6	-3	1	439.5	-1297.5	238.9	95.4	3.5
18TH	228.66	6.9	-38.8	1174	2023	5.9	-19.2	-3	1	432.7	-1258.7	222.8	89.9	3.4
19TH	241.24	7.2	-39.8	1174	2023	6.1	-19.7	-4	1	425.5	-1218.9	207.2	84.5	3.3
20TH	253.82	7.5	-40.8	1174	2023	6.4	-20.2	-4	1	417.9	-1178.1	192.1	79.2	3.2
21ST	266.40	7.9	-41.8	1174	2023	6.7	-20.7	-4	1	410.0	-1136.3	177.6	74.0	3.0
22ND	278.98	8.2	-42.8	1174	2023	7.0	-21.1	-5	2	401.8	-1093.5	163.5	68.9	2.9
23RD	291.56	8.6	-43.8	1174	2023	7.3	-21.6	-5	2	393.2	-1049.8	150.1	63.9	2.7
24TH	304.14	9.1	-44.6	1174	2023	7.7	-22.1	-5	2	384.2	-1005.1	137.1	59.0	2.5
25TH	316.72	9.8	-45.0	1174	2023	8.4	-22.2	-5	2	374.3	-960.1	124.8	54.2	2.3
		10.4	-44.4	1151	1983	9.0	-22.4	-5	2					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 250 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									364.0	-915.7	113.2	49.7	2.2
27TH	341.38	11.1	-44.7	1151	1983	9.7	-22.6	-5	2	352.9	-871.0	102.2	45.2	2.0
28TH	353.71	11.8	-45.1	1151	1983	10.3	-22.7	-5	2	341.0	-825.9	91.7	41.0	1.8
29TH	366.04	12.6	-45.4	1151	1983	10.9	-22.9	-5	2	328.4	-780.5	81.8	36.8	1.7
30TH	378.12	13.6	-44.8	1127	1943	12.0	-23.1	-4	2	314.9	-735.7	72.7	32.9	1.5
31ST	390.20	14.6	-45.0	1127	1943	13.0	-23.1	-3	2	300.2	-690.8	64.0	29.2	1.4
32ND	402.28	15.4	-45.0	1127	1943	13.7	-23.2	-3	2	284.8	-645.8	56.0	25.7	1.3
33RD	414.36	16.2	-45.0	1127	1943	14.4	-23.2	-3	2	268.6	-600.8	48.4	22.4	1.2
34TH	426.44	17.0	-45.0	1127	1943	15.1	-23.2	-3	2	251.5	-555.8	41.5	19.2	1.1
35TH	438.52	17.8	-45.0	1127	1943	15.8	-23.2	-3	2	233.7	-510.7	35.0	16.3	1.0
36TH	450.60	18.6	-45.0	1127	1943	16.5	-23.2	-3	2	215.1	-465.7	29.1	13.6	.9
37TH	462.68	19.4	-45.1	1127	1943	17.2	-23.2	-3	2	195.7	-420.6	23.8	11.1	.8
38TH	474.76	19.9	-45.1	1127	1943	17.6	-23.2	-3	3	175.8	-375.5	19.0	8.8	.7
39TH	486.84	20.3	-45.2	1127	1943	18.0	-23.3	-4	3	155.5	-330.3	14.7	6.8	.6
40TH	498.92	20.8	-45.2	1127	1943	18.4	-23.3	-4	3	134.7	-285.0	11.0	5.1	.5
41ST	511.00	21.2	-45.3	1127	1943	18.8	-23.3	-4	3	113.5	-239.8	7.8	3.6	.4
42ND	523.08	21.7	-45.3	1127	1943	19.2	-23.3	-4	3	91.8	-194.4	5.2	2.4	.3
43RD	535.66	23.5	-47.3	1174	2023	20.0	-23.4	-3	3	68.3	-147.2	3.0	1.3	.2
44TH	548.58	24.7	-48.2	1206	2078	20.4	-23.2	-1	0	43.6	-99.0	1.5	.6	.2
MR	566.58	29.8	-65.2	1680	2895	17.7	-22.5	2	-2	13.9	-33.8	.3	.1	.3
TOP	581.67	13.9	-33.8	1085	2065	12.8	-16.4	-11	8	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 260 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									308.2	-2101.2	665.7	118.1	2.3
2ND	23.00	3.7	-53.8	2147	3699	1.7	-14.5	23	-3	304.5	-2047.5	618.0	111.1	3.3
3RD	35.92	-1.2	-31.7	1206	2078	-1.0	-15.3	18	1	305.8	-2015.8	591.7	107.2	3.7
4TH	48.84	-.9	-31.0	1206	2078	-.7	-14.9	15	1	306.6	-1984.8	565.9	103.2	4.1
5TH	61.76	.3	-31.2	1206	2078	.3	-15.0	15	-0	306.3	-1953.6	540.4	99.2	4.5
6TH	74.68	1.1	-32.6	1206	2078	.9	-15.7	12	-1	305.2	-1921.0	515.4	95.3	4.8
7TH	87.60	1.9	-34.0	1206	2078	1.6	-16.4	10	-1	303.3	-1887.0	490.8	91.4	5.0
8TH	100.52	2.7	-35.4	1206	2078	2.2	-17.0	8	-1	300.6	-1851.6	466.7	87.5	5.3
9TH	113.44	3.4	-36.8	1206	2078	2.8	-17.7	6	-1	297.2	-1814.8	443.0	83.6	5.4
10TH	126.27	4.2	-37.9	1197	2063	3.5	-18.4	4	-1	293.1	-1777.0	419.9	79.8	5.6
11TH	139.10	4.8	-39.2	1197	2063	4.0	-19.0	3	-1	288.3	-1737.8	397.4	76.1	5.7
12TH	151.93	4.7	-40.1	1197	2063	4.0	-19.4	2	-0	283.6	-1697.7	375.3	72.4	5.7
13TH	164.76	4.7	-41.1	1197	2063	3.9	-19.9	1	-0	278.8	-1656.6	353.8	68.8	5.8
14TH	177.59	4.7	-42.1	1197	2063	3.9	-20.4	-0	0	274.1	-1614.5	332.8	65.3	5.7
15TH	190.42	4.7	-43.0	1197	2063	3.9	-20.9	-1	0	269.4	-1571.5	312.4	61.8	5.7
16TH	203.25	4.7	-44.0	1197	2063	3.9	-21.3	-2	0	264.7	-1527.5	292.5	58.3	5.6
17TH	216.08	5.9	-45.0	1197	2063	4.9	-21.8	-2	0	258.8	-1482.5	273.2	55.0	5.6
18TH	228.66	6.0	-44.8	1174	2023	5.1	-22.2	-2	0	252.8	-1437.6	254.8	51.8	5.5
19TH	241.24	6.1	-45.5	1174	2023	5.2	-22.5	-2	1	246.7	-1392.1	237.0	48.6	5.4
20TH	253.82	6.2	-46.2	1174	2023	5.2	-22.8	-3	1	240.5	-1346.0	219.8	45.6	5.3
21ST	266.40	6.2	-46.8	1174	2023	5.3	-23.1	-3	1	234.3	-1299.1	203.2	42.6	5.2
22ND	278.98	6.3	-47.5	1174	2023	5.3	-23.5	-3	1	228.1	-1251.7	187.1	39.7	5.1
23RD	291.56	6.3	-48.2	1174	2023	5.4	-23.8	-3	1	221.7	-1203.5	171.7	36.8	5.0
24TH	304.14	6.4	-48.9	1174	2023	5.4	-24.1	-4	1	215.4	-1154.6	156.9	34.1	4.9
25TH	316.72	6.4	-49.7	1174	2023	5.4	-24.5	-4	1	209.0	-1105.0	142.6	31.4	4.7
		6.2	-49.4	1151	1983	5.4	-24.9	-4	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 260 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									202.8	-1055.6	129.3	28.9	4.6
		6.2	-50.2	1151	1983	5.4	-25.3	-5	1					
27TH	341.38									196.5	-1005.3	116.6	26.4	4.4
		6.2	-51.0	1151	1983	5.4	-25.7	-5	1					
28TH	353.71									190.3	-954.4	104.5	24.0	4.2
		6.2	-51.7	1151	1983	5.4	-26.1	-5	1					
29TH	366.04									184.1	-902.6	93.1	21.7	4.0
		6.7	-51.4	1127	1943	6.0	-26.5	-5	1					
30TH	378.12									177.3	-851.2	82.5	19.5	3.8
		7.4	-51.9	1127	1943	6.5	-26.7	-5	1					
31ST	390.20									170.0	-799.3	72.5	17.4	3.5
		7.8	-52.3	1127	1943	6.9	-26.9	-5	1					
32ND	402.28									162.2	-747.0	63.2	15.4	3.3
		8.2	-52.6	1127	1943	7.3	-27.1	-5	1					
33RD	414.36									154.0	-694.4	54.5	13.5	3.1
		8.6	-52.9	1127	1943	7.6	-27.3	-5	1					
34TH	426.44									145.4	-641.4	46.4	11.7	2.9
		9.0	-53.3	1127	1943	8.0	-27.4	-5	1					
35TH	438.52									136.4	-588.1	39.0	10.0	2.7
		9.4	-53.6	1127	1943	8.3	-27.6	-5	2					
36TH	450.60									127.0	-534.5	32.2	8.4	2.5
		9.7	-54.0	1127	1943	8.6	-27.8	-5	2					
37TH	462.68									117.3	-480.5	26.1	7.0	2.3
		10.3	-54.0	1127	1943	9.1	-27.8	-6	2					
38TH	474.76									107.0	-426.5	20.6	5.6	2.0
		10.9	-54.0	1127	1943	9.7	-27.8	-6	2					
39TH	486.84									96.0	-372.5	15.8	4.4	1.8
		11.5	-54.1	1127	1943	10.2	-27.8	-6	2					
40TH	498.92									84.5	-318.4	11.6	3.3	1.5
		12.2	-54.1	1127	1943	10.8	-27.8	-7	3					
41ST	511.00									72.3	-264.4	8.1	2.3	1.3
		12.8	-54.1	1127	1943	11.3	-27.8	-7	3					
42ND	523.08									59.6	-210.3	5.2	1.5	1.0
		14.5	-56.4	1174	2023	12.3	-27.9	-7	3					
43RD	535.66									45.1	-153.9	2.9	.9	.7
		16.0	-56.5	1206	2078	13.3	-27.2	-6	3					
44TH	548.58									29.0	-97.4	1.3	.4	.5
		20.4	-71.8	1680	2895	12.1	-24.8	-3	1					
MR	566.58									8.7	-25.6	.2	.1	.3
		8.7	-25.6	1085	2065	8.0	-12.4	-18	10					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 270 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									247.8	-2449.2	765.0	88.5	2.1
2ND	23.00	4.0	-66.2	2147	3699	1.9	-17.9	20	-2	243.8	-2383.0	709.5	82.8	3.2
3RD	35.92	-1.4	-39.3	1206	2078	-1.2	-18.9	17	1	245.3	-2343.7	678.9	79.7	3.7
4TH	48.84	-1.4	-37.1	1206	2078	-1.1	-17.8	14	1	246.6	-2306.6	648 9	76.5	4.1
5TH	61.76	-.2	-36.6	1206	2078	-.1	-17.6	14	0	246.8	-2270.0	619.3	73.3	4.5
6TH	74.68	.7	-38.4	1206	2078	.6	-18.5	12	-0	246.1	-2231.6	590.2	70.1	4.9
7TH	87.60	1.6	-40.2	1206	2078	1.3	-19.3	10	-1	244.5	-2191.4	561.7	66.9	5.2
8TH	100.52	2.5	-42.0	1206	2078	2.1	-20.2	9	-1	242.0	-2149.4	533.6	63.8	5.5
9TH	113.44	3.4	-43.8	1206	2078	2.8	-21.1	7	-1	238.6	-2105.6	506.1	60.7	5.7
10TH	126.27	4.3	-45.3	1197	2063	3.6	-21.9	6	-1	234.3	-2060.3	479.4	57.7	5.9
11TH	139.10	4.9	-47.0	1197	2063	4.1	-22.8	5	-1	229.4	-2013.4	453.3	54.7	6.1
12TH	151.93	4.9	-48.2	1197	2063	4.1	-23.4	4	-1	224.4	-1965.2	427.8	51.8	6.2
13TH	164.76	4.9	-49.5	1197	2063	4.1	-24.0	2	-0	219.5	-1915.7	402.9	48.9	6.3
14TH	177.59	4.9	-50.8	1197	2063	4.1	-24.6	1	-0	214.6	-1864.9	378.6	46.1	6.4
15TH	190.42	4.9	-52.0	1197	2063	4.1	-25.2	0	-0	209.6	-1812.9	355.0	43.4	6.4
16TH	203.25	4.9	-53.3	1197	2063	4.1	-25.8	-1	0	204.7	-1759.6	332.1	40.8	6.4
17TH	216.08	6.2	-54.6	1197	2063	5.2	-26.4	-0	0	198.5	-1705.0	309.9	38.2	6.4
18TH	228.66	6.3	-54.0	1174	2023	5.4	-26.7	-1	0	192.2	-1651.0	288 8	35.7	6.3
19TH	241.24	6.3	-54.4	1174	2023	5.4	-26.9	-1	0	185.8	-1596.6	268.3	33.3	6.3
20TH	253.82	6.4	-54.7	1174	2023	5.4	-27.0	-2	0	179.5	-1541.9	248.6	31.0	6.2
21ST	266.40	6.4	-55.0	1174	2023	5.4	-27.2	-2	0	173.1	-1486.9	229.5	28.8	6.1
22ND	278.98	6.4	-55.4	1174	2023	5.4	-27.4	-2	0	166.7	-1431.5	211.2	26.7	6.0
23RD	291.56	6.4	-55.7	1174	2023	5.4	-27.5	-3	1	160.4	-1375.8	193.5	24.6	5.9
24TH	304.14	6.3	-56.3	1174	2023	5.4	-27.8	-3	1	154.1	-1319.4	176.6	22.7	5.8
25TH	316.72	6.0	-57.4	1174	2023	5.1	-28.4	-4	1	148.0	-1262.0	160.3	20.8	5.6
		5.7	-57.3	1151	1983	4.9	-28.9	-4	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 270 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									142.4	-1204.7	145.1	19.0	5.4
27TH	341.38	5.4	-58.3	1151	1983	4.7	-29.4	-5	1	136.9	-1146.3	130.6	17.2	5.2
28TH	353.71	5.2	-59.4	1151	1983	4.5	-29.9	-5	1	131.8	-1087.0	116.9	15.6	5.0
29TH	366.04	4.9	-60.4	1151	1983	4.3	-30.5	-5	1	126.9	-1026.5	103.8	14.0	4.7
30TH	378.12	5.5	-60.2	1127	1943	4.9	-31.0	-5	1	121.4	-966.4	91.8	12.5	4.5
31ST	390.20	6.1	-60.7	1127	1943	5.4	-31.2	-5	1	115.3	-905.7	80.5	11.1	4.2
32ND	402.28	6.3	-61.0	1127	1943	5.6	-31.4	-5	1	109.0	-844.7	69.9	9.7	3.9
33RD	414.36	6.5	-61.3	1127	1943	5.8	-31.5	-5	1	102.5	-783.5	60.1	8.4	3.7
34TH	426.44	6.7	-61.5	1127	1943	5.9	-31.7	-5	1	95.8	-721.9	51.0	7.2	3.4
35TH	438.52	6.9	-61.8	1127	1943	6.1	-31.8	-5	1	88.9	-660.1	42.7	6.1	3.2
36TH	450.60	7.1	-62.1	1127	1943	6.3	-32.0	-5	1	81.8	-598.0	35.1	5.1	2.9
37TH	462.68	7.2	-62.4	1127	1943	6.4	-32.1	-6	1	74.5	-535.6	28.2	4.1	2.6
38TH	474.76	7.4	-62.3	1127	1943	6.6	-32.1	-6	1	67.1	-473.3	22.1	3.3	2.3
39TH	486.84	7.7	-62.2	1127	1943	6.8	-32.0	-6	1	59.4	-411.1	16.8	2.5	2.0
40TH	498.92	7.9	-62.1	1127	1943	7.0	-32.0	-6	1	51.5	-349.0	12.2	1.9	1.7
41ST	511.00	8.2	-62.0	1127	1943	7.2	-31.9	-6	1	43.3	-287.0	8.3	1.3	1.4
42ND	523.08	8.4	-61.9	1127	1943	7.5	-31.8	-7	2	34.9	-225.1	5 2	.8	1.1
43RD	535.66	9.4	-64.3	1174	2023	8.0	-31.8	-7	2	25.5	-160.8	2.8	.4	.8
44TH	548.58	10.5	-63.9	1206	2078	8.7	-30.8	-6	2	15.0	-96.9	1.2	.2	.5
MR	566.58	13.1	-79.7	1680	2895	7.8	-27.5	-4	1	1.9	-17.2	.1	.0	.2
TOP	581.67	1.9	-17.2	1085	2065	1.8	-8.3	-17	3	0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 280 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIPECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									134.7	-2376.7	763.6	62.7	-.4
2ND	23.00	-4.2	-57.6	2147	3699	-2.0	-15.6	22	3	139.0	-2319.1	709.6	59.5	.6
3RD	35.92	-6.3	-34.3	1206	2078	-5.2	-16.5	19	6	145.2	-2284.8	679.8	57.7	1.1
4TH	48.84	-6.4	-32.8	1206	2078	-5.3	-15.8	17	6	151.6	-2252.0	650.5	55.8	1.6
5TH	61.76	-5.4	-32.6	1206	2078	-4.5	-15.7	16	5	157.1	-2219.3	621.6	53.8	2.0
6TH	74.68	-4.3	-34.1	1206	2078	-3.6	-16.4	15	3	161.4	-2185.2	593.2	51.7	2.4
7TH	87.60	-3.2	-35.6	1206	2078	-2.7	-17.1	13	2	164.6	-2149.6	565.2	49.6	2.8
8TH	100.52	-2.1	-37.1	1206	2078	-1.7	-17.9	12	1	166.7	-2112.5	537.6	47.5	3.1
9TH	113.44	-1.0	-38.6	1206	2078	-.8	-18.6	11	0	167.7	-2073.9	510.6	45.3	3.4
10TH	126.27	.1	-39.8	1197	2063	.1	-19.3	10	-0	167.6	-2034.1	484.2	43.2	3.7
11TH	139.10	1.0	-41.2	1197	2063	.9	-20.0	8	-0	166.6	-1992.9	458.4	41.0	4.0
12TH	151.93	1.2	-42.8	1197	2063	1.0	-20.7	7	-0	165.3	-1950.2	433.1	38.9	4.2
13TH	164.76	1.5	-44.3	1197	2063	1.2	-21.5	6	-0	163.9	-1905.9	408.4	36.8	4.4
14TH	177.59	1.7	-45.8	1197	2063	1.4	-22.2	4	-0	162.2	-1860.1	384.2	34.7	4.6
15TH	190.42	1.9	-47.4	1197	2063	1.6	-23.0	3	-0	160.2	-1812.7	360.6	32.6	4.7
16TH	203.25	2.1	-48.9	1197	2063	1.8	-23.7	2	-0	158.1	-1763.8	337.7	30.6	4.8
17TH	216.08	3.7	-50.4	1197	2063	3.1	-24.4	3	-0	154.4	-1713.4	315.4	28.6	4.9
18TH	228.66	4.2	-50.5	1174	2023	3.6	-25.0	2	-0	150.2	-1662.9	294.2	26.7	5.0
19TH	241.24	4.4	-51.4	1174	2023	3.8	-25.4	1	-0	145.8	-1611.5	273.6	24.8	5.0
20TH	253.82	4.7	-52.3	1174	2023	4.0	-25.8	-0	0	141.1	-1559.2	253.6	23.0	5.0
21ST	266.40	5.0	-53.2	1174	2023	4.3	-26.3	-1	0	136.1	-1506.0	234.3	21.2	4.9
22ND	278.98	5.3	-54.1	1174	2023	4.5	-26.7	-2	0	130.8	-1452.0	215.7	19.6	4.9
23RD	291.56	5.5	-55.0	1174	2023	4.7	-27.2	-3	1	125.3	-1397.0	197.8	18.0	4.7
24TH	304.14	5.6	-56.0	1174	2023	4.8	-27.7	-4	1	119.6	-1341.0	180.6	16.4	4.6
25TH	316.72	5.4	-57.1	1174	2023	4.6	-28.2	-4	1	114.3	-1283.9	164.1	14.9	4.4
		5.0	-57.1	1151	1983	4.4	-28.8	-4	1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 280 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05	4.8	-58.1	1151	1983	4.2	-29.3	-4	1	109.2	-1226.8	148.6	13.6	4.2
27TH	341.38	4.6	-59.2	1151	1983	4.0	-29.9	-4	1	104.4	-1168.7	133.8	12.2	4.0
28TH	353.71	4.4	-60.3	1151	1983	3.8	-30.4	-4	1	99.8	-1109.5	119.8	11.0	3.8
29TH	366.04	5.1	-60.1	1127	1943	4.5	-30.9	-4	1	95.4	-1049.2	106.5	9.8	3.6
30TH	378.12	5.6	-60.8	1127	1943	5.0	-31.3	-4	1	90.3	-989.1	94.2	8.7	3.4
31ST	390.20	5.7	-61.3	1127	1943	5.0	-31.6	-4	1	84.7	-928.3	82.6	7.6	3.2
32ND	402.28	5.7	-61.9	1127	1943	5.0	-31.9	-4	1	79.0	-867.0	71.7	6.6	3.0
33RD	414.36	5.7	-62.5	1127	1943	5.1	-32.1	-4	1	73.3	-805.1	61.6	5.7	2.8
34TH	426.44	5.7	-63.0	1127	1943	5.1	-32.4	-4	1	67.6	-742.6	52.3	4.8	2.6
35TH	438.52	5.7	-63.6	1127	1943	5.1	-32.7	-4	1	61.9	-679.6	43.7	4.1	2.4
36TH	450.60	5.7	-64.1	1127	1943	5.0	-33.0	-5	1	56.2	-616.0	35.9	3.3	2.1
37TH	462.68	5.6	-64.2	1127	1943	5.0	-33.1	-4	1	50.5	-551.9	28.8	2.7	1.9
38TH	474.76	5.6	-64.3	1127	1943	5.0	-33.1	-4	1	44.8	-487.7	22.6	2.1	1.7
39TH	486.84	5.6	-64.4	1127	1943	4.9	-33.1	-4	1	39.2	-423.4	17.0	1.6	1.5
40TH	498.92	5.5	-64.5	1127	1943	4.9	-33.2	-4	1	33.7	-359.0	12.3	1.2	1.3
41ST	511.00	5.5	-64.6	1127	1943	4.9	-33.2	-4	1	28.2	-294.5	8.4	.8	1.0
42ND	523.08	6.3	-67.3	1174	2023	5.4	-33.3	-3	1	22.7	-229.9	5.2	.5	.9
43RD	535.66	7.5	-67.0	1206	2078	6.2	-32.2	-3	1	16.3	-162.6	2.7	.3	.7
44TH	548.58	8.2	-82.9	1680	2895	4.9	-28.6	-5	1	8.9	-95.7	1.1	.1	.5
MR	566.58	.7	-12.8	1085	2065	.6	-6.2	-19	2	.7	-12.8	.1	.0	.2
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 290 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 86 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									136.6	-2112.1	693.0	58.6	-5.4
2ND	23.00	-2.3	-49.8	2147	3699	-1.1	-13.5	26	2	138.9	-2062.3	645.0	55.5	-4.3
3RD	35.92	-4.9	-29.9	1206	2078	-4.0	-14.4	21	6	143.8	-2032.5	618.6	53.6	-3.8
4TH	48.84	-5.0	-28.5	1206	2078	-4.2	-13.7	19	6	148.8	-2004.0	592.5	51.7	-3.4
5TH	61.76	-4.2	-28.2	1206	2078	-3.5	-13.6	19	5	153.0	-1975.8	566.8	49.8	-3.0
6TH	74.68	-3.3	-29.4	1206	2078	-2.7	-14.1	18	3	156.3	-1946.4	541.4	47.8	-2.6
7TH	87.60	-2.4	-30.5	1206	2078	-2.0	-14.7	17	2	158.7	-1915.9	516.5	45.8	-2.2
8TH	100.52	-1.5	-31.6	1206	2078	-1.3	-15.2	16	1	160.3	-1884.2	491.9	43.7	-1.7
9TH	113.44	-.7	-32.8	1206	2078	-.6	-15.8	15	1	160.9	-1851.5	467.8	41.6	-1.4
10TH	126.27	.2	-33.7	1197	2063	.2	-16.3	14	-0	160.7	-1817.8	444.3	39.6	-1.0
11TH	139.10	1.0	-34.8	1197	2063	.8	-16.9	13	-1	159.7	-1783.0	421.2	37.5	-.6
12TH	151.93	1.4	-36.1	1197	2063	1.2	-17.5	11	-1	158.4	-1746.9	398.5	35.5	-.3
13TH	164.76	1.8	-37.4	1197	2063	1.5	-18.1	9	-1	156.5	-1709.5	376.4	33.4	-.0
14TH	177.59	2.2	-38.7	1197	2063	1.9	-18.8	8	-1	154.3	-1670.8	354.7	31.5	.2
15TH	190.42	2.7	-40.0	1197	2063	2.2	-19.4	6	-1	151.6	-1630.7	333.5	29.5	.4
16TH	203.25	3.1	-41.3	1197	2063	2.6	-20.0	4	-1	148.5	-1589.4	312.8	27.6	.6
17TH	216.08	4.7	-42.6	1197	2063	3.9	-20.7	5	-1	143.8	-1546.8	292.7	25.7	.7
18TH	228.66	4.9	-42.8	1174	2023	4.2	-21.1	5	-1	139.0	-1504.0	273.5	23.9	.9
19TH	241.24	4.9	-43.7	1174	2023	4.2	-21.6	4	-1	134.1	-1460.3	254.9	22.2	1.0
20TH	253.82	4.9	-44.5	1174	2023	4.2	-22.0	3	-1	129.2	-1415.8	236.8	20.5	1.1
21ST	266.40	4.9	-45.4	1174	2023	4.2	-22.4	3	-0	124.3	-1370.4	219.3	18.9	1.2
22ND	278.98	4.9	-46.3	1174	2023	4.2	-22.9	2	-0	119.4	-1324.1	202.3	17.4	1.3
23RD	291.56	4.9	-47.2	1174	2023	4.2	-23.3	1	-0	114.5	-1276.9	186.0	15.9	1.4
24TH	304.14	4.9	-48.1	1174	2023	4.1	-23.8	1	-0	109.7	-1228.8	170.2	14.5	1.4
25TH	316.72	4.8	-49.1	1174	2023	4.1	-24.3	1	-0	104.9	-1179.7	155.0	13.2	1.4
		4.6	-49.0	1151	1983	4.0	-24.7	0	-0					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 290 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									100.3	-1130.7	140.8	11.9	1.4
		4.5	-49.9	1151	1983	3.9	-25.2	-0	0					
27TH	341.38									95.8	-1080.8	127.2	10.7	1.4
		4.4	-50.9	1151	1983	3.9	-25.6	-1	0					
28TH	353.71									91.3	-1029.9	114.2	9.6	1.4
		4.3	-51.8	1151	1983	3.8	-26.1	-1	0					
29TH	366.04									87.0	-978.2	101.8	8.5	1.4
		5.0	-51.6	1127	1943	4.4	-26.6	-1	0					
30TH	378.12									82.0	-926.5	90.3	7.4	1.3
		5.5	-52.7	1127	1943	4.9	-27.1	-1	0					
31ST	390.20									76.5	-873.8	79.4	6.5	1.3
		5.5	-54.0	1127	1943	4.9	-27.8	-1	0					
32ND	402.28									71.0	-819.8	69.2	5.6	1.2
		5.6	-55.2	1127	1943	5.0	-28.4	-1	0					
33RD	414.36									65.4	-764.6	59.6	4.8	1.2
		5.6	-56.4	1127	1943	5.0	-29.1	-1	0					
34TH	426.44									59.8	-708.2	50.7	4.0	1.1
		5.7	-57.7	1127	1943	5.1	-29.7	-2	0					
35TH	438.52									54.1	-650.5	42.5	3.3	1.0
		5.8	-58.9	1127	1943	5.1	-30.3	-2	0					
36TH	450.60									48.3	-591.6	35.0	2.7	1.0
		5.8	-60.1	1127	1943	5.1	-31.0	-2	0					
37TH	462.68									42.5	-531.4	28.2	2.1	.9
		5.6	-60.5	1127	1943	4.9	-31.1	-2	0					
38TH	474.76									36.9	-471.0	22.2	1.7	.8
		5.3	-60.7	1127	1943	4.7	-31.3	-2	0					
39TH	486.84									31.6	-410.3	16.8	1.3	.7
		5.1	-61.0	1127	1943	4.5	-31.4	-2	0					
40TH	498.92									26.5	-349.3	12.2	.9	.6
		4.8	-61.2	1127	1943	4.3	-31.5	-2	0					
41ST	511.00									21.7	-288.1	8.4	.6	.5
		4.6	-61.5	1127	1943	4.1	-31.7	-2	0					
42ND	523.08									17.1	-226.6	5.3	.4	.4
		5.0	-64.3	1174	2023	4.2	-31.8	-1	0					
43RD	535.66									12.1	-162.2	2.8	.2	.4
		5.5	-64.4	1206	2078	4.6	-31.0	-1	0					
44TH	548.58									6.6	-97.9	1.2	.1	.3
		5.8	-80.9	1680	2895	3.5	-27.9	-2	0					
MR	566.59									.8	-17.0	.1	.0	.1
		.8	-17.0	1085	2065	.7	-8.2	-11	1					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 360 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									201.5	-2016.0	665.4	84.1	-13.9
2ND	23.00	-5.6	-42.9	2147	3699	-2.6	-11.6	26	6	207.1	-1973.1	619.5	79.4	-13.0
3RD	35.92	-4.9	-28.4	1206	2078	-4.1	-13.6	23	7	212.0	-1944.8	594.2	76.7	-12.5
4TH	48.84	-4.2	-27.5	1206	2078	-3.4	-13.2	24	6	216.1	-1917.3	569.2	73.9	-12.0
5TH	61.76	-3.0	-27.5	1206	2078	-2.5	-13.2	25	5	219.1	-1889.8	544.6	71.1	-11.5
6TH	74.68	-2.2	-28.5	1206	2078	-1.9	-13.7	23	3	221.4	-1861.3	520.4	68.3	-10.9
7TH	87.60	-1.5	-29.6	1206	2078	-1.2	-14.2	22	2	222.8	-1831.7	496.5	65.4	-10.4
8TH	100.52	-.7	-30.6	1206	2078	-.6	-14.7	21	1	223.5	-1801.1	473.1	62.5	-9.9
9TH	113.44	.1	-31.7	1206	2078	.1	-15.2	20	-0	223.4	-1769.5	450.0	59.6	-9.4
10TH	126.27	.9	-32.5	1197	2063	.7	-15.7	19	-1	222.6	-1737.0	427.5	56.8	-9.0
11TH	139.10	1.5	-33.5	1197	2063	1.3	-16.2	18	-1	221.0	-1703.5	405.4	53.9	-8.5
12TH	151.93	2.0	-34.5	1197	2063	1.6	-16.7	16	-2	219.1	-1668.9	383.8	51.1	-8.0
13TH	164.76	2.4	-35.6	1197	2063	2.0	-17.2	15	-2	216.7	-1633.4	362.6	48.3	-7.6
14TH	177.59	2.8	-36.6	1197	2063	2.3	-17.7	13	-2	213.9	-1596.8	341.9	45.6	-7.2
15TH	190.42	3.2	-37.6	1197	2063	2.7	-18.2	12	-2	210.6	-1559.2	321.7	42.8	-6.9
16TH	203.25	3.6	-38.6	1197	2063	3.0	-18.7	11	-2	207.0	-1520.6	301.9	40.2	-6.5
17TH	216.08	5.2	-39.6	1197	2063	4.3	-19.2	12	-3	201.8	-1481.0	282.7	37.5	-6.1
18TH	228.66	5.6	-39.7	1174	2023	4.8	-19.6	12	-3	196.2	-1441.3	264.3	35.0	-5.8
19TH	241.24	5.9	-40.5	1174	2023	5.0	-20.0	11	-3	190.4	-1400.7	246.4	32.6	-5.4
20TH	253.82	6.2	-41.4	1174	2023	5.3	-20.4	10	-3	184.2	-1359.4	229.0	30.2	-5.1
21ST	266.40	6.5	-42.2	1174	2023	5.5	-20.9	9	-2	177.8	-1317.2	212.2	28.0	-4.8
22ND	278.98	6.8	-43.0	1174	2023	5.7	-21.3	9	-2	171.0	-1274.2	195.9	25.8	-4.5
23RD	291.56	7.0	-43.9	1174	2023	6.0	-21.7	8	-2	164.0	-1230.3	180.1	23.7	-4.2
24TH	304.14	7.1	-44.9	1174	2023	6.1	-22.2	7	-2	156.8	-1185.4	164.9	21.6	-4.0
25TH	316.72	6.9	-46.1	1174	2023	5.9	-22.8	7	-2	149.9	-1139.3	150.3	19.7	-3.7
		6.5	-46.4	1151	1983	5.7	-23.4	6	-1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 300 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									143.4	-1092.9	136.6	17.9	-3.5
		6.3	-47.6	1151	1983	5.4	-24.0	6	-1					
27TH	341.38									137.2	-1045.3	123.4	16.2	-3.3
		6.0	-48.7	1151	1983	5.2	-24.6	5	-1					
28TH	353.71									131.1	-996.6	110.8	14.5	-3.1
		5.8	-49.9	1151	1983	5.0	-25.2	5	-1					
29TH	366.04									125.4	-946.7	98.8	12.9	-2.9
		6.5	-50.0	1127	1943	5.7	-25.8	5	-1					
30TH	378.12									118.9	-896.6	87.7	11.5	-2.7
		7.1	-51.1	1127	1943	6.3	-26.3	5	-1					
31ST	390.20									111.7	-845.5	77.2	10.1	-2.5
		7.3	-52.1	1127	1943	6.5	-26.8	5	-1					
32ND	402.28									104.4	-793.4	67.3	8.8	-2.3
		7.5	-53.2	1127	1943	6.6	-27.4	5	-1					
33RD	414.36									97.0	-740.2	58.0	7.5	-2.1
		7.6	-54.2	1127	1943	6.8	-27.9	5	-1					
34TH	426.44									89.4	-686.0	49.4	6.4	-1.8
		7.8	-55.2	1127	1943	6.9	-28.4	5	-1					
35TH	438.52									81.6	-630.8	41.4	5.4	-1.6
		7.9	-56.2	1127	1943	7.0	-29.0	5	-1					
36TH	450.60									73.7	-574.6	34.2	4.5	-1.4
		8.1	-57.3	1127	1943	7.1	-29.5	5	-1					
37TH	462.68									65.6	-517.3	27.6	3.6	-1.2
		7.8	-57.9	1127	1943	6.9	-29.8	5	-1					
38TH	474.76									57.8	-459.4	21.7	2.9	-1.0
		7.5	-58.5	1127	1943	6.7	-30.1	4	-1					
39TH	486.84									50.3	-400.9	16.5	2.2	-.8
		7.2	-59.1	1127	1943	6.4	-30.4	4	-1					
40TH	498.92									43.1	-341.8	12.0	1.6	-.6
		6.9	-59.7	1127	1943	6.1	-30.7	3	-1					
41ST	511.00									36.2	-282.1	8.2	1.2	-.4
		6.6	-60.3	1127	1943	5.9	-31.0	3	-1					
42ND	523.08									29.5	-221.9	5.2	.8	-.3
		7.1	-63.4	1174	2023	6.1	-31.3	3	-1					
43RD	535.66									22.4	-158.5	2.8	.4	-.1
		8.0	-63.4	1206	2078	6.6	-30.5	3	-1					
44TH	548.58									14.4	-95.1	1.1	.2	.0
		9.7	-78.5	1680	2895	5.8	-27.1	1	-0					
MR	566.58									4.7	-16.6	.1	.0	.1
		4.7	-16.6	1085	2065	4.3	-8.0	-8	4					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS ; NO. 15 COLUMBUS CIRCLE NEW YORK CASE 3
WIND DIRECTION 310 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									186.6	-1871.2	624.9	84.1	-19.2
2ND	23.00	-6.8	-42.4	2147	3699	-3.2	-11.5	26	7	193.4	-1828.8	581.4	79.7	-18.4
3RD	35.92	-4.7	-25.9	1206	2078	-3.9	-12.5	23	7	198.1	-1802.9	558.0	77.2	-17.9
4TH	48.84	-3.9	-25.0	1206	2078	-3.2	-12.0	22	6	202.0	-1777.9	534.8	74.6	-17.5
5TH	61.76	-2.7	-24.9	1206	2078	-2.3	-12.0	23	4	204.7	-1753.0	512.0	72.0	-17.0
6TH	74.68	-2.0	-25.6	1206	2078	-1.7	-12.3	22	3	206.8	-1727.5	489.5	69.3	-16.6
7TH	87.60	-1.3	-26.3	1206	2078	-1.1	-12.6	22	2	208.1	-1701.2	467.4	66.7	-16.1
8TH	100.52	-.6	-27.0	1206	2078	-.5	-13.0	21	1	208.7	-1674.2	445.6	64.0	-15.7
9TH	113.44	.1	-27.7	1206	2078	.1	-13.3	21	-0	208.7	-1646.5	424.1	61.3	-15.2
10TH	126.27	.8	-28.2	1197	2063	.6	-13.7	20	-1	207.9	-1618.3	403.2	58.6	-14.8
11TH	139.10	1.3	-29.0	1197	2063	1.1	-14.1	20	-2	206.5	-1589.3	382.6	55.9	-14.3
12TH	151.93	1.4	-30.1	1197	2063	1.2	-14.6	18	-1	205.1	-1559.1	362.4	53.3	-13.9
13TH	164.76	1.5	-31.3	1197	2063	1.3	-15.2	17	-1	203.6	-1527.8	342.6	50.7	-13.4
14TH	177.59	1.6	-32.4	1197	2063	1.3	-15.7	15	-1	202.0	-1495.4	323.2	48.1	-13.0
15TH	190.42	1.7	-33.6	1197	2063	1.4	-16.3	14	-1	200.3	-1461.8	304.2	45.5	-12.7
16TH	203.25	1.8	-34.8	1197	2063	1.5	-16.8	13	-1	198.5	-1427.0	285.7	42.9	-12.3
17TH	216.08	2.8	-35.9	1197	2063	2.3	-17.4	14	-2	195.7	-1391.1	267.6	40.4	-11.9
18TH	228.66	3.2	-36.1	1174	2023	2.8	-17.8	13	-2	192.5	-1355.0	250.4	38.0	-11.5
19TH	241.24	3.6	-36.9	1174	2023	3.1	-18.3	13	-2	188.8	-1318.1	233.6	35.6	-11.2
20TH	253.82	4.0	-37.8	1174	2023	3.4	-18.7	13	-2	184.8	-1280.3	217.2	33.2	-10.8
21ST	266.40	4.4	-38.6	1174	2023	3.8	-19.1	12	-2	180.4	-1241.7	201.3	30.9	-10.4
22ND	278.98	4.8	-39.5	1174	2023	4.1	-19.5	12	-2	175.6	-1202.2	186.0	28.7	-10.0
23RD	291.56	5.2	-40.3	1174	2023	4.4	-19.9	11	-3	170.4	-1161.9	171.1	26.5	-9.7
24TH	304.14	5.4	-41.3	1174	2023	4.6	-20.4	11	-2	165.0	-1120.6	156.7	24.4	-9.3
25TH	316.72	5.4	-42.5	1174	2023	4.6	-21.0	11	-2	159.5	-1078.2	142.9	22.4	-8.9
		5.3	-42.8	1151	1983	4.6	-21.6	11	-2					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 310 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									154.2	-1035.4	129.9	20.4	-8.6
		5.3	-43.9	1151	1983	4.6	-22.1	11	-2					
27TH	341.38									148.8	-991.5	117.4	18.6	-8.2
		5.3	-45.0	1151	1983	4.6	-22.7	11	-2					
28TH	353.71									143.5	-946.6	105.4	16.8	-7.8
		5.3	-46.1	1151	1983	4.6	-23.2	11	-2					
29TH	366.04									138.2	-900.5	94.1	15.0	-7.4
		6.0	-46.2	1127	1943	5.3	-23.8	12	-3					
30TH	378.12									132.2	-854.2	83.5	13.4	-7.0
		6.7	-47.5	1127	1943	5.9	-24.5	12	-3					
31ST	390.20									125.5	-806.7	73.4	11.8	-6.5
		7.0	-48.8	1127	1943	6.2	-25.1	12	-3					
32ND	402.28									118.5	-757.9	64.0	10.4	-6.0
		7.4	-50.2	1127	1943	6.5	-25.8	12	-3					
33RD	414.36									111.1	-707.7	55.1	9.0	-5.5
		7.7	-51.5	1127	1943	6.8	-26.5	12	-3					
34TH	426.44									103.4	-656.2	46.9	7.7	-5.0
		8.1	-52.8	1127	1943	7.1	-27.2	12	-3					
35TH	438.52									95.3	-603.4	39.3	6.5	-4.5
		8.4	-54.2	1127	1943	7.5	-27.9	12	-3					
36TH	450.60									86.9	-549.2	32.3	5.4	-4.0
		8.7	-55.5	1127	1943	7.7	-28.5	12	-3					
37TH	462.68									78.2	-493.8	26.0	4.4	-3.5
		8.6	-56.0	1127	1943	7.7	-28.8	12	-3					
38TH	474.76									69.6	-437.8	20.4	3.5	-3.0
		8.5	-56.5	1127	1943	7.6	-29.1	11	-3					
39TH	486.84									61.0	-381.3	15.4	2.7	-2.5
		8.4	-57.0	1127	1943	7.5	-29.3	10	-3					
40TH	498.92									52.6	-324.3	11.2	2.0	-2.0
		8.3	-57.5	1127	1943	7.4	-29.6	10	-2					
41ST	511.00									44.3	-266.8	7.6	1.4	-1.6
		8.2	-57.9	1127	1943	7.3	-29.8	9	-2					
42ND	523.08									36.1	-208.9	4.7	.9	-1.2
		9.0	-60.9	1174	2023	7.7	-30.1	9	-2					
43RD	535.66									27.2	-148.0	2.5	.5	-.8
		9.9	-60.9	1206	2078	8.3	-29.3	9	-2					
44TH	548.58									17.2	-87.1	1.0	.3	-.3
		11.3	-75.9	1680	2895	6.7	-26.2	6	-1					
MR	566.58									5.9	-11.2	.1	.0	-.0
		5.9	-11.2	1085	2065	5.4	-5.4	1	-1					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 320 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									39.3	-1564.9	529.3	33.5	-23.9
2ND	23.00	-7.2	-34.7	2147	3699	-3.3	-9.4	28	10	46.4	-1530.2	493.7	32.5	-23.1
3RD	35.92	-4.8	-21.7	1206	2078	-3.9	-10.4	24	9	51.2	-1508.6	474.1	31.9	-22.7
4TH	48.84	-3.8	-21.0	1206	2078	-3.1	-10.1	24	7	55.0	-1487.6	454.8	31.2	-22.3
5TH	61.76	-3.1	-20.8	1206	2078	-2.6	-10.0	26	6	58.1	-1466.8	435.7	30.5	-21.9
6TH	74.68	-2.9	-21.3	1206	2078	-2.4	-10.2	25	6	60.9	-1445.5	416.9	29.7	-21.5
7TH	87.60	-2.7	-21.7	1206	2078	-2.2	-10.4	24	5	63.6	-1423.8	398.3	28.9	-21.1
8TH	100.52	-2.5	-22.2	1206	2078	-2.0	-10.7	24	5	66.1	-1401.7	380.1	28.1	-20.7
9TH	113.44	-2.3	-22.6	1206	2078	-1.9	-10.9	23	4	68.3	-1379.1	362.1	27.2	-20.2
10TH	126.27	-2.0	-22.9	1197	2063	-1.7	-11.1	23	3	70.4	-1356.1	344.6	26.3	-19.8
11TH	139.10	-1.9	-23.4	1197	2063	-1.6	-11.3	22	3	72.2	-1332.7	327.3	25.4	-19.4
12TH	151.93	-1.7	-24.1	1197	2063	-1.4	-11.7	20	2	74.0	-1308.7	310.4	24.4	-19.0
13TH	164.76	-1.6	-24.7	1197	2063	-1.3	-12.0	19	2	75.6	-1284.0	293.7	23.5	-18.7
14TH	177.59	-1.5	-25.4	1197	2063	-1.2	-12.3	17	2	77.0	-1258.6	277.4	22.5	-18.3
15TH	190.42	-1.3	-26.1	1197	2063	-1.1	-12.6	16	1	78.3	-1232.5	261.4	21.5	-18.0
16TH	203.25	-1.2	-26.7	1197	2063	-1.0	-12.9	15	1	79.5	-1205.8	245.8	20.5	-17.7
17TH	216.08	-.4	-27.4	1197	2063	-.3	-13.3	16	0	79.9	-1178.4	230.5	19.5	-17.3
18TH	228.66	-.2	-27.7	1174	2023	-.1	-13.7	16	0	80.1	-1150.7	215.8	18.5	-17.0
19TH	241.24	-.1	-28.6	1174	2023	-.1	-14.1	16	0	80.1	-1122.1	201.6	17.5	-16.6
20TH	253.82	.0	-29.5	1174	2023	.0	-14.6	16	-0	80.1	-1092.6	187.6	16.5	-16.2
21ST	266.40	.1	-30.4	1174	2023	.1	-15.0	16	-0	80.0	-1062.2	174.1	15.4	-15.8
22ND	278.98	.2	-31.3	1174	2023	.2	-15.5	16	-0	79.8	-1030.9	160.9	14.4	-15.4
23RD	291.56	.3	-32.2	1174	2023	.3	-15.9	17	-0	79.5	-998.7	148.1	13.4	-15.0
24TH	304.14	.4	-33.4	1174	2023	.4	-16.5	17	-0	79.0	-965.3	135.8	12.4	-14.6
25TH	316.72	.6	-34.9	1174	2023	.5	-17.2	16	-0	78.4	-930.5	123.9	11.5	-14.1
		.7	-35.6	1151	1983	.6	-17.9	16	-1					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 320 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									77.7	-894.9	112.6	10.5	-13.6
		.8	-37.0	1151	1983	.7	-18.7	16	-1					
27TH	341.38									76.9	-857.9	101.8	9.5	-13.1
		1.0	-38.4	1151	1983	.8	-19.4	16	-1					
28TH	353.71									75.9	-819.4	91.5	8.6	-12.6
		1.1	-39.8	1151	1983	1.0	-20.1	16	-1					
29TH	366.04									74.8	-779.6	81.6	7.7	-12.1
		2.2	-40.4	1127	1943	1.9	-20.8	18	-2					
30TH	378.12									72.6	-739.2	72.4	6.8	-11.6
		3.2	-41.5	1127	1943	2.8	-21.4	19	-2					
31ST	390.20									69.4	-697.7	63.7	5.9	-10.9
		3.7	-42.4	1127	1943	3.3	-21.8	19	-3					
32ND	402.28									65.7	-655.3	55.6	5.1	-10.3
		4.2	-43.3	1127	1943	3.8	-22.3	20	-3					
33RD	414.36									61.5	-612.0	47.9	4.3	-9.6
		4.8	-44.3	1127	1943	4.2	-22.8	20	-4					
34TH	426.44									56.7	-567.7	40.8	3.6	-8.9
		5.3	-45.2	1127	1943	4.7	-23.3	21	-4					
35TH	438.52									51.4	-522.6	34.2	3.0	-8.2
		5.8	-46.1	1127	1943	5.2	-23.7	21	-5					
36TH	450.60									45.6	-476.5	28.2	2.4	-7.4
		6.4	-47.0	1127	1943	5.7	-24.2	22	-5					
37TH	462.68									39.2	-429.4	22.7	1.9	-6.6
		6.0	-47.8	1127	1943	5.3	-24.6	21	-4					
38TH	474.76									33.2	-381.7	17.8	1.4	-5.8
		5.5	-48.5	1127	1943	4.9	-25.0	20	-4					
39TH	486.84									27.8	-333.1	13.5	1.1	-5.0
		5.0	-49.3	1127	1943	4.4	-25.4	20	-3					
40TH	498.92									22.8	-283.8	9.8	.8	-4.2
		4.5	-50.0	1127	1943	4.0	-25.8	19	-3					
41ST	511.00									18.3	-233.8	6.6	.5	-3.5
		4.0	-50.8	1127	1943	3.5	-26.2	19	-3					
42ND	523.08									14.3	-183.0	4.1	.3	-2.7
		4.4	-53.7	1174	2023	3.7	-26.5	19	-3					
43RD	535.66									10.0	-129.3	2.2	.2	-1.9
		5.0	-53.9	1206	2078	4.2	-25.9	20	-3					
44TH	548.58									4.9	-75.4	.8	.1	-1.1
		3.8	-66.2	1680	2895	2.2	-22.9	17	-2					
MR	566.58									1.2	-9.2	1	.0	-.2
		1.2	-9.2	1085	2065	1.1	-4.5	27	-6					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 330 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-215.8	-1250.9	421.5	-75.6	-27.6
2ND	23.00	-4.1	-29.9	2147	3699	-1.9	-8.1	29	7	-211.7	-1221.1	393.0	-70.7	-26.9
3RD	35.92	-3.1	-18.3	1206	2078	-2.6	-8.8	26	7	-208.6	-1202.8	377.4	-68.0	-26.5
4TH	48.84	-2.6	-17.5	1206	2078	-2.1	-8.4	27	7	-206.1	-1185.3	362.0	-65.3	-26.2
5TH	61.76	-2.2	-17.2	1206	2078	-1.8	-8.3	26	6	-203.9	-1168.1	346.8	-62.6	-25.8
6TH	74.68	-2.1	-17.5	1206	2078	-1.7	-8.4	28	6	-201.8	-1150.6	331.8	-60.0	-25.4
7TH	87.60	-2.0	-17.8	1206	2078	-1.6	-8.6	27	5	-199.8	-1132.8	317.0	-57.4	-25.0
8TH	100.52	-1.8	-18.1	1206	2078	-1.5	-8.7	27	5	-198.0	-1114.8	302.5	-54.9	-24.6
9TH	113.44	-1.7	-18.4	1206	2078	-1.4	-8.8	27	4	-196.3	-1096.4	288.2	-52.3	-24.2
10TH	126.27	-1.6	-18.6	1197	2063	-1.3	-9.0	26	4	-194.7	-1077.8	274.3	-49.8	-23.9
11TH	139.10	-1.6	-18.9	1197	2063	-1.3	-9.2	26	4	-193.1	-1058.9	260.6	-47.3	-23.5
12TH	151.93	-2.0	-19.5	1197	2063	-1.7	-9.4	25	4	-191.1	-1039.5	247.1	-44.8	-23.1
13TH	164.76	-2.5	-20.1	1197	2063	-2.1	-9.7	24	5	-188.6	-1019.4	233.9	-42.4	-22.7
14TH	177.59	-2.9	-20.7	1197	2063	-2.4	-10.0	23	6	-185.7	-998.8	221.0	-40.0	-22.3
15TH	190.42	-3.4	-21.2	1197	2063	-2.8	-10.3	22	6	-182.3	-977.5	208.3	-37.6	-22.0
16TH	203.25	-3.8	-21.8	1197	2063	-3.2	-10.6	21	6	-178.5	-955.7	195.9	-35.3	-21.6
17TH	216.08	-3.9	-22.4	1197	2063	-3.2	-10.9	23	7	-174.6	-933.2	183.8	-33.1	-21.2
18TH	228.66	-4.1	-22.5	1174	2023	-3.5	-11.1	24	7	-170.5	-910.8	172.2	-30.9	-20.8
19TH	241.24	-4.5	-23.0	1174	2023	-3.8	-11.3	24	8	-166.1	-887.8	160.8	-28.8	-20.4
20TH	253.82	-4.8	-23.4	1174	2023	-4.1	-11.6	25	9	-161.2	-864.4	149.8	-26.7	-19.9
21ST	266.40	-5.2	-23.9	1174	2023	-4.5	-11.8	26	10	-156.0	-840.5	139.1	-24.7	-19.5
22ND	278.98	-5.6	-24.4	1174	2023	-4.8	-12.0	26	10	-150.4	-816.1	128.7	-22.8	-19.0
23RD	291.56	-6.0	-24.8	1174	2023	-5.1	-12.3	27	11	-144.4	-791.3	118.6	-20.9	-18.5
24TH	304.14	-6.2	-25.6	1174	2023	-5.3	-12.6	27	11	-138.2	-765.7	108.8	-19.2	-17.9
25TH	316.72	-6.3	-26.7	1174	2023	-5.4	-13.2	28	11	-131.9	-739.0	99.3	-17.5	-17.4
		-6.3	-27.2	1151	1983	-5.5	-13.7	28	11					

TABLE 7 SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 330 . CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-125.6	-711.8	90 4	-15.9	-16.8
		-6.4	-28.2	1151	1983	-5.6	-14.2	29	11					
27TH	341.38									-119.2	-683.6	81 8	-14.4	-16.2
		-6.5	-29.3	1151	1983	-5.7	-14.8	29	11					
28TH	353.71									-112.6	-654.3	73.5	-12.9	-15.5
		-6.6	-30.3	1151	1983	-5.7	-15.3	29	11					
29TH	366.04									-106 0	-623.9	65.6	-11.6	-14.9
		-5.9	-30.7	1127	1943	-5.2	-15.8	31	10					
30TH	378.12									-100.1	-593.2	58.3	-10.3	-14.1
		-5.5	-31.8	1127	1943	-4.8	-16.4	32	9					
31ST	390.20									-94.7	-561.4	51 3	-9.2	-13.3
		-5.5	-33.0	1127	1943	-4.9	-17.0	32	9					
32ND	402.28									-89 2	-528.4	44.7	-8.1	-12.5
		-5.5	-34.1	1127	1943	-4.9	-17.6	32	9					
33RD	414.36									-83.6	-494.3	38.6	-7.0	-11.7
		-5.6	-35.3	1127	1943	-4.9	-18.1	32	9					
34TH	426.44									-78.1	-459.1	32.8	-6.0	-10.8
		-5.6	-36.4	1127	1943	-5.0	-18.7	32	8					
35TH	438.52									-72.5	-422.7	27.5	-5.1	-9.9
		-5.6	-37.5	1127	1943	-5.0	-19.3	32	8					
36TH	450.60									-66.8	-385.1	22.6	-4.3	-8.9
		-5.6	-38.7	1127	1943	-5.0	-19.9	32	8					
37TH	462.68									-61 2	-346.5	18.2	-3.5	-8.0
		-5.9	-39.2	1127	1943	-5.2	-20.2	31	8					
38TH	474.76									-55.4	-307.3	14.2	-2.8	-7.0
		-6.2	-39.6	1127	1943	-5.5	-20.4	30	8					
39TH	486.84									-49.2	-267.7	10.8	-2.2	-6.1
		-6.5	-40.0	1127	1943	-5.8	-20.6	30	8					
40TH	498.92									-42.7	-227.7	7.8	-1.6	-5.2
		-6.8	-40.4	1127	1943	-6.1	-20.8	29	8					
41ST	511.00									-35.8	-187.3	5.3	-1.1	-4.2
		-7.1	-40.8	1127	1943	-6.3	-21.0	29	9					
42ND	523.08									-28.7	-146.5	3.2	-.8	-3.3
		-7.3	-43.0	1174	2023	-6.2	-21.2	29	8					
43RD	535.66									-21.4	-103.5	1.7	-.4	-2.4
		-6.7	-43.5	1206	2078	-5.6	-20.9	29	8					
44TH	548.58									-14.7	-60.0	.6	-.2	-1.4
		-10.0	-56.1	1680	2895	-6.0	-19.4	25	8					
MR	566.58									-4.7	-4.0	.0	-.0	-.3
		-4.7	-4.0	1085	2065	-4.3	-1.9	-245	-492					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 340 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-344.3	-1054.1	351.1	-137.2	-26.3
2ND	23.00	-2.6	-24.1	2147	3699	-1.2	-6.5	26	5	-341.7	-1030.0	327.1	-129.3	-25.8
3RD	35.92	-1.6	-14.7	1206	2078	-1.4	-7.1	23	4	-340.1	-1015.3	313.9	-124.9	-25.5
4TH	48.84	-1.5	-14.0	1206	2078	-1.3	-6.7	25	5	-338.5	-1001.3	300.9	-120.5	-25.2
5TH	61.76	-1.4	-13.8	1206	2078	-1.2	-6.6	27	5	-337.1	-987.6	288.0	-116.2	-24.9
6TH	74.68	-1.2	-14.2	1206	2078	-1.0	-6.8	28	4	-335.9	-973.3	275.3	-111.8	-24.6
7TH	87.60	-.9	-14.7	1206	2078	-.8	-7.1	29	3	-335.0	-958.6	262.9	-107.5	-24.2
8TH	100.52	-.7	-15.2	1206	2078	-.6	-7.3	30	2	-334.3	-943.5	250.6	-103.2	-23.9
9TH	113.44	-.5	-15.6	1206	2078	-.4	-7.5	30	2	-333.8	-927.8	238.5	-98.8	-23.5
10TH	126.27	-.2	-16.0	1197	2063	-.2	-7.7	31	1	-333.6	-911.9	226.7	-94.6	-23.1
11TH	139.10	-.2	-16.5	1197	2063	-.2	-8.0	31	1	-333.4	-895.4	215.1	-90.3	-22.7
12TH	151.93	-.8	-17.3	1197	2063	-.6	-8.4	30	2	-332.6	-878.1	203.7	-86.0	-22.3
13TH	164.76	-1.4	-18.1	1197	2063	-1.1	-8.8	29	4	-331.2	-860.0	192.6	-81.8	-21.9
14TH	177.59	-1.9	-18.9	1197	2063	-1.6	-9.2	28	5	-329.3	-841.1	181.7	-77.5	-21.4
15TH	190.42	-2.5	-19.7	1197	2063	-2.1	-9.6	28	6	-326.8	-821.3	171.0	-73.3	-21.0
16TH	203.25	-3.1	-20.6	1197	2063	-2.6	-10.0	27	7	-323.7	-800.8	160.6	-69.1	-20.6
17TH	216.08	-3.2	-21.4	1197	2063	-2.6	-10.4	29	7	-320.5	-779.4	150.4	-65.0	-20.1
18TH	228.66	-4.0	-21.3	1174	2023	-3.4	-10.5	29	9	-316.5	-758.1	140.8	-61.0	-19.6
19TH	241.24	-5.0	-21.4	1174	2023	-4.3	-10.6	30	12	-311.5	-736.7	131.4	-57.0	-19.1
20TH	253.82	-6.1	-21.6	1174	2023	-5.2	-10.7	30	14	-305.4	-715.1	122.2	-53.2	-18.6
21ST	266.40	-7.1	-21.8	1174	2023	-6.0	-10.8	31	17	-298.3	-693.3	113.4	-49.4	-18.2
22ND	278.98	-8.1	-21.9	1174	2023	-6.9	-10.8	32	20	-290.2	-671.4	104.8	-45.7	-17.7
23RD	291.56	-9.2	-22.1	1174	2023	-7.8	-10.9	33	23	-281.1	-649.3	96.5	-42.1	-17.2
24TH	304.14	-9.9	-22.6	1174	2023	-8.4	-11.1	34	25	-271.1	-626.7	88.5	-38.6	-16.7
25TH	316.72	-10.3	-23.2	1174	2023	-8.8	-11.5	35	26	-260.8	-603.5	80.7	-35.3	-16.2
		-10.5	-23.4	1151	1983	-9.1	-11.8	36	27					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 340 CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-250.3	-580.2	73.4	-32.1	-15.7
		-10.9	-24.0	1151	1983	-9.5	-12.1	37	29					
27TH	341.38									-239.4	-556.2	66.4	-29.1	-15.1
		-11.3	-24.6	1151	1983	-9.8	-12.4	38	30					
28TH	353.71									-228.1	-531.6	59.7	-26.2	-14.5
		-11.7	-25.2	1151	1983	-10.2	-12.7	39	31					
29TH	366.04									-216.4	-506.4	53.3	-23.5	-13.9
		-11.5	-25.3	1127	1943	-10.2	-13.0	41	32					
30TH	378.12									-204.9	-481.2	47.4	-20.9	-13.2
		-11.4	-26.0	1127	1943	-10.1	-13.4	42	31					
31ST	390.20									-193.6	-455.1	41.7	-18.5	-12.5
		-11.5	-26.9	1127	1943	-10.2	-13.9	42	30					
32ND	402.28									-182.1	-428.2	36.4	-16.2	-11.8
		-11.6	-27.8	1127	1943	-10.3	-14.3	42	30					
33RD	414.36									-170.5	-400.4	31.4	-14.1	-11.0
		-11.7	-28.7	1127	1943	-10.4	-14.8	42	29					
34TH	426.44									-158.8	-371.7	26.7	-12.1	-10.2
		-11.8	-29.5	1127	1943	-10.5	-15.2	42	28					
35TH	438.52									-146.9	-342.2	22.4	-10.3	-9.4
		-11.9	-30.4	1127	1943	-10.6	-15.7	42	28					
36TH	450.60									-135.0	-311.8	18.4	-8.6	-8.6
		-11.9	-31.3	1127	1943	-10.5	-16.1	42	27					
37TH	462.68									-123.1	-280.5	14.9	-7.0	-7.7
		-12.2	-31.6	1127	1943	-10.9	-16.2	42	27					
38TH	474.76									-110.9	-249.0	11.7	-5.6	-6.8
		-12.7	-31.8	1127	1943	-11.2	-16.4	41	28					
39TH	486.84									-98.2	-217.2	8.8	-4.3	-5.9
		-13.1	-32.1	1127	1943	-11.6	-16.5	41	29					
40TH	498.92									-85.1	-185.1	6.4	-3.2	-5.0
		-13.5	-32.3	1127	1943	-12.0	-16.6	41	29					
41ST	511.00									-71.6	-152.8	4.4	-2.3	-4.1
		-13.9	-32.6	1127	1943	-12.4	-16.8	41	30					
42ND	523.08									-57.7	-120.2	2.7	-1.5	-3.2
		-14.6	-34.2	1174	2023	-12.4	-16.9	42	30					
43RD	535.66									-43.1	-86.1	1.4	-.9	-2.3
		-14.5	-34.8	1206	2078	-12.0	-16.8	41	29					
44TH	548.58									-28.6	-51.2	.5	-.4	-1.4
		-19.4	-46.6	1680	2895	-11.6	-16.1	34	24					
MR	566.58									-9.2	-4.7	0	-.1	-.3
		-9.2	-4.7	1085	2065	-8.4	-2.3	-30	-101					
TOP	581.67									0.0	0.0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 25° CONFIGURATION A REFERENCE PRESSURE 34.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 90 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
GRND	0.00									-352.6	-859.0	285.8	-144.0	-22.7
2ND	23.00	-.0	-19.7	2147	3699	-.0	-5.3	28	0	-352.5	-839.2	266.3	-135.9	-22.3
3RD	35.92	-.4	-11.4	1206	2078	-.4	-5.5	25	2	-352.1	-827.9	255.5	-131.3	-22.1
4TH	48.84	-.6	-11.0	1206	2078	-.5	-5.3	25	2	-351.5	-816.8	244.9	-126.8	-21.8
5TH	61.76	-.5	-11.0	1206	2078	-.4	-5.3	27	2	-351.0	-805.8	234.4	-122.2	-21.6
6TH	74.68	-.3	-11.5	1206	2078	-.3	-5.5	28	1	-350.6	-794.3	224.1	-117.7	-21.3
7TH	87.60	-.1	-11.9	1206	2078	-.1	-5.7	30	1	-350.5	-782.5	213.9	-113.2	-21.1
8TH	100.52	.1	-12.3	1206	2078	.0	-5.9	31	-0	-350.5	-770.1	203.8	-108.6	-20.8
9TH	113.44	.3	-12.7	1206	2078	.2	-6.1	32	-1	-350.8	-757.4	194.0	-104.1	-20.4
10TH	126.27	.5	-13.1	1197	2063	.4	-6.3	34	-2	-351.3	-744.3	184.3	-99.6	-20.1
11TH	139.10	.5	-13.5	1197	2063	.4	-6.6	34	-2	-351.7	-730.8	174.9	-95.1	-19.7
12TH	151.93	-.2	-14.2	1197	2063	-.2	-6.9	33	1	-351.5	-716.5	165.6	-90.6	-19.3
13TH	164.76	-.9	-14.9	1197	2063	-.8	-7.2	31	3	-350.5	-701.6	156.5	-86.1	-18.9
14TH	177.59	-1.7	-15.7	1197	2063	-1.4	-7.6	30	5	-348.9	-685.9	147.6	-81.6	-18.6
15TH	190.42	-2.4	-16.4	1197	2063	-2.0	-7.9	29	7	-346.5	-669.6	138.9	-77.1	-18.2
16TH	203.25	-3.1	-17.1	1197	2063	-2.6	-8.3	29	9	-343.4	-652.5	130.4	-72.7	-17.8
17TH	216.08	-3.4	-17.8	1197	2063	-2.8	-8.6	30	10	-340.1	-634.7	122.2	-68.3	-17.4
18TH	228.66	-4.4	-17.6	1174	2023	-3.7	-8.7	31	13	-335.7	-617.1	114.3	-64.1	-17.0
19TH	241.24	-5.6	-17.7	1174	2023	-4.8	-8.8	33	17	-330.1	-599.4	106.6	-59.9	-16.6
20TH	253.82	-6.8	-17.8	1174	2023	-5.8	-8.8	34	22	-323.3	-581.6	99.2	-55.8	-16.2
21ST	266.40	-8.0	-17.9	1174	2023	-6.8	-8.8	37	28	-315.3	-563.7	92.0	-51.8	-15.7
22ND	278.98	-9.2	-18.0	1174	2023	-7.8	-8.9	40	35	-306.2	-545.7	85.0	-47.9	-15.3
23RD	291.56	-10.4	-18.0	1174	2023	-8.8	-8.9	44	43	-295.8	-527.7	78.3	-44.1	-14.9
24TH	304.14	-11.2	-18.5	1174	2023	-9.5	-9.1	47	48	-284.6	-509.3	71.8	-40.4	-14.5
25TH	316.72	-11.4	-19.1	1174	2023	-9.7	-9.4	47	48	-273.2	-490.2	65.5	-36.9	-14.0
		-11.4	-19.3	1151	1983	-9.9	-9.7	48	49					

TABLE 7. SHEAR AND MOMENT DIAGRAMS : NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
WIND DIRECTION 350 CONFIGURATION A REFERENCE PRESSURE 34 0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 80 FT IN THE X DIRECTION AND 47 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) X	MOMENT (1000-FT-KIPS) Y	MOMENT (1000-FT-KIPS) Z
26TH	329.05									-261.8	-470.9	59.5	-33.6	-13.5
27TH	341.38	-11.7	-19.9	1151	1983	-10.2	-10.0	49	49	-250.1	-451.1	53.9	-30.5	-13.0
28TH	353.71	-11.9	-20.4	1151	1983	-10.4	-10.3	49	49	-238.1	-430.6	48.4	-27.4	-12.5
29TH	366.04	-12.2	-21.0	1151	1983	-10.6	-10.6	50	49	-226.0	-409.6	43.2	-24.6	-11.9
30TH	378.12	-11.9	-21.2	1127	1943	-10.6	-10.9	52	50	-214.0	-388.4	38.4	-21.9	-11.3
31ST	390.20	-11.9	-21.7	1127	1943	-10.5	-11.1	52	49	-202.1	-366.8	33.9	-19.4	-10.7
32ND	402.28	-12.0	-22.1	1127	1943	-10.6	-11.4	52	48	-190.2	-344.6	29.6	-17 0	-10.0
33RD	414.36	-12.1	-22.6	1127	1943	-10.7	-11.6	52	47	-178.1	-322.0	25.5	-14.8	-9.4
34TH	426.44	-12.2	-23.1	1127	1943	-10.8	-11.9	51	46	-165.9	-298.9	21.8	-12.7	-8.7
35TH	438.52	-12.3	-23.6	1127	1943	-10.9	-12.1	51	45	-153.7	-275.3	18.3	-10.8	-8.0
36TH	450.60	-12.4	-24.1	1127	1943	-11.0	-12.4	51	45	-141.3	-251.2	15.1	-9.0	-7.2
37TH	462.68	-12.3	-24.6	1127	1943	-10.9	-12.6	51	43	-129.0	-226.6	12.3	-7.4	-6.5
38TH	474.76	-12.7	-24.9	1127	1943	-11.2	-12.8	51	44	-116.4	-201.8	9.7	-5.9	-5.7
39TH	486.84	-13.1	-25.1	1127	1943	-11.6	-12.9	51	45	-103.2	-176.7	7.4	-4.6	-5.0
40TH	498.92	-13.6	-25.4	1127	1943	-12.0	-13.1	51	47	-89.7	-151.2	5.4	-3.4	-4.2
41ST	511.00	-14.0	-25.7	1127	1943	-12.4	-13.2	52	48	-75.7	-125.6	3.7	-2.4	-3.5
42ND	523.08	-14.4	-26.0	1127	1943	-12.8	-13.4	52	49	-61.3	-99.6	2 4	-1.6	-2.8
43RD	535.66	-15.4	-27.3	1174	2023	-13.1	-13.5	53	50	-45.9	-72.3	1.3	-.9	-2.0
44TH	548.58	-15.6	-27.8	1206	2078	-13.0	-13.4	52	49	-30.3	-44.5	.5	-.4	-1.2
MR	566.58	-20.6	-36.5	1680	2895	-12.3	-12.6	43	41	-9.6	-8.0	.1	-.1	-.3
TOP	581.67	-9.6	-8.0	1085	2065	-8.9	-3.9	-112	-230	0.0	0.0	0.0	0.0	0.0

TABLE 7. NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 1
PROJECT 7950 CONFIGURATION A
SCALE = 500 REF. PRESSURE = 34.0
GUST FACTOR = 1.32 STANDARD FLOOR HEIGHT = 12.08
NUMBER OF SIDES = 4 NO. OF FLOORS = 45

SIDE	ANGLE	Z-AXIS
1	0.0	1.128
2	90.0	1.884
3	180.0	1.128
4	270.0	1.966

FLOOR #	LABEL	HEIGHT-FT
1	GRND	23.00
2	2ND	12.92
3	3RD	12.92
4	4TH	12.92
5	5TH	12.92
6	6TH	12.92
7	7TH	12.92
8	8TH	12.92
9	9TH	12.83
10	10TH	12.83
11	11TH	12.83
12	12TH	12.83
13	13TH	12.83
14	14TH	12.83
15	15TH	12.83
16	16TH	12.83
17	17TH	12.58
18	18TH	12.58
19	19TH	12.58
20	20TH	12.58
21	21ST	12.58
22	22ND	12.58
23	23RD	12.58
24	24TH	12.58
25	25TH	12.33
26	26TH	12.33
27	27TH	12.33
28	28TH	12.33
29	29TH	12.08
30	30TH	12.08
31	31ST	12.08
32	32ND	12.08
33	33RD	12.08
34	34TH	12.08
35	35TH	12.08
36	36TH	12.08
37	37TH	12.08
38	38TH	12.08
39	39TH	12.08
40	40TH	12.08
41	41ST	12.08
42	42ND	12.58
43	43RD	12.92
44	44TH	18.00
45	MR	15.08

TABLE 7. NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 2
PROJECT 7950 CONFIGURATION A
SCALE = 500 REF. PRESSURE = 34.0
GUST FACTOR = 1.32 STANDARD FLOOR HEIGHT = 12.08
NUMBER OF SIDES = 4 NO. OF FLOORS = 45

SIDE	ANGLE	Z-AXIS
1	0.0	1.020
2	90.0	1.920
3	180.0	1.236
4	270.0	1.920

FLOOR #	LABEL	HEIGHT-FT
1	GRND	23.00
2	2ND	12.92
3	3RD	12.92
4	4TH	12.92
5	5TH	12.92
6	6TH	12.92
7	7TH	12.92
8	8TH	12.92
9	9TH	12.83
10	10TH	12.83
11	11TH	12.83
12	12TH	12.83
13	13TH	12.83
14	14TH	12.83
15	15TH	12.83
16	16TH	12.83
17	17TH	12.58
18	18TH	12.58
19	19TH	12.58
20	20TH	12.58
21	21ST	12.58
22	22ND	12.58
23	23RD	12.58
24	24TH	12.58
25	25TH	12.33
26	26TH	12.33
27	27TH	12.33
28	28TH	12.33
29	29TH	12.08
30	30TH	12.08
31	31ST	12.08
32	32ND	12.08
33	33RD	12.08
34	34TH	12.08
35	35TH	12.08
36	36TH	12.08
37	37TH	12.08
38	38TH	12.08
39	39TH	12.08
40	40TH	12.08
41	41ST	12.08
42	42ND	12.58
43	43RD	12.92
44	44TH	18.00
45	MR	15.08

TABLE 7. NO. 15 COLUMBUS CIRCLE, NEW YORK CASE 3
PROJECT 7950 CONFIGURATION A
SCALE = 500 REF. PRESSURE = 34.0
GUST FACTOR = 1.32 STANDARD FLOOR HEIGHT = 12.08
NUMBER OF SIDES = 4 NO. OF FLOORS = 45

SIDE	ANGLE	Z-AXIS
1	0.0	1.128
2	90.0	1.920
3	180.0	1.128
4	270.0	1.920

FLOOR #	LABEL	HEIGHT-FT
1	GRND	23.00
2	2ND	12.92
3	3RD	12.92
4	4TH	12.92
5	5TH	12.92
6	6TH	12.92
7	7TH	12.92
8	8TH	12.92
9	9TH	12.83
10	10TH	12.83
11	11TH	12.83
12	12TH	12.83
13	13TH	12.83
14	14TH	12.83
15	15TH	12.83
16	16TH	12.83
17	17TH	12.58
18	18TH	12.58
19	19TH	12.58
20	20TH	12.58
21	21ST	12.58
22	22ND	12.58
23	23RD	12.58
24	24TH	12.58
25	25TH	12.33
26	26TH	12.33
27	27TH	12.33
28	28TH	12.33
29	29TH	12.08
30	30TH	12.08
31	31ST	12.08
32	32ND	12.08
33	33RD	12.08
34	34TH	12.08
35	35TH	12.08
36	36TH	12.08
37	37TH	12.08
38	38TH	12.08
39	39TH	12.08
40	40TH	12.08
41	41ST	12.08
42	42ND	12.58
43	43RD	12.92
44	44TH	18.00
45	MR	15.08

APPENDIX A

PRESSURE DATA

Note: Pressure coefficients are defined in Section 4.3.

Pressure tap designation is explained in Figure 3.

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
0	101	-.167	.108	.377	-.662
0	102	-.020	.150	.702	-.669
0	103	.116	.223	.966	-.662
0	104	.075	.152	.676	-.420
0	105	.094	.170	.799	-.406
0	106	.094	.177	.750	-.700
0	107	.082	.187	.867	-.412
0	108	.104	.231	.939	-.955
0	109	-.016	.092	.436	-.350
0	110	.037	.130	.669	-.433
0	111	.076	.151	.867	-.359
0	112	.102	.169	.977	-.333
0	113	.111	.148	.965	-.513
0	114	.088	.199	1.061	-.838
0	115	-.137	.081	.123	-.595
0	116	.152	.171	.848	-.612
0	117	-.060	.065	.312	-.376
0	118	-.019	.078	.381	-.388
0	119	.015	.083	.471	-.353
0	120	.042	.082	.678	-.254
0	121	.043	.120	.844	-.674
0	122	.006	.156	.740	-1.617
0	123	-.072	.051	.147	-.333
0	124	-.043	.056	.237	-.288
0	125	-.019	.060	.315	-.224
0	126	.003	.070	.451	-.243
0	127	.008	.089	.399	-.674
0	128	-.031	.143	.487	-.760
0	129	-.128	.076	.106	-.722
0	130	.133	.137	.989	-.322
0	131	-.084	.047	.092	-.340
0	132	-.060	.053	.197	-.263
0	133	-.038	.059	.291	-.275
0	134	-.019	.070	.346	-.526
0	135	-.018	.080	.344	-.578
0	136	-.049	.123	.500	-.871
0	137	-.089	.047	.094	-.407
0	138	-.072	.045	.116	-.298
0	139	-.064	.042	.100	-.306
0	140	-.060	.055	.167	-.389
0	141	-.066	.099	.370	-.966
0	142	-.128	.135	.366	-1.041
0	143	-.137	.058	.093	-.541
0	144	-.074	.070	.463	-.129
0	145	-.093	.044	.040	-.343
0	146	-.080	.040	.040	-.312
0	147	-.078	.043	.054	-.425
0	148	-.093	.047	.080	-.362
0	149	-.111	.054	.040	-.432
0	150	-.114	.062	.058	-.485
0	151	-.072	.032	.067	-.186
0	152	-.069	.033	.085	-.179
0	153	-.071	.033	.055	-.189
0	154	-.077	.040	.056	-.268
0	155	-.082	.047	.084	-.416
0	156	-.081	.048	.142	-.438
0	157	-.076	.035	.023	-.241
0	158	-.064	.049	.308	-.187
0	159	-.067	.035	.126	-.232
0	160	-.069	.037	.128	-.229
0	161	-.075	.038	.043	-.244
0	162	-.075	.050	.311	-.260
0	163	-.069	.038	.048	-.232
0	164	-.066	.038	.056	-.224
0	165	-.073	.035	.053	-.202
0	166	-.073	.043	.207	-.263
0	201	-.122	.062	.064	-.610
0	202	-.132	.075	.087	-.798
0	203	-.126	.076	.150	-.658
0	204	-.159	.105	.117	-.929
0	205	-.197	.092	.037	-.703
0	206	-.161	.059	.142	-.394
0	207	-.165	.063	.075	-.503
0	208	-.116	.064	.072	-.433
0	209	-.118	.078	.121	-.610
0	210	-.126	.069	.066	-.539
0	211	-.121	.069	.082	-.540
0	212	-.118	.056	.085	-.417
0	213	-.108	.054	.062	-.353
0	214	-.119	.059	.042	-.502
0	215	-.117	.064	.082	-.555
0	216	-.119	.066	.090	-.497
0	217	-.122	.069	.093	-.447
0	218	-.129	.064	.071	-.419
0	219	-.126	.068	.064	-.520
0	220	-.117	.049	.018	-.321
0	221	-.114	.045	.015	-.296
0	222	-.131	.057	.007	-.639
0	223	-.131	.064	.027	-.715
0	224	-.131	.074	.080	-.648
0	225	-.131	.077	.057	-.595
0	226	-.129	.084	.075	-.703
0	227	-.125	.084	.073	-.715
0	228	-.114	.056	.033	-.457
0	229	-.114	.046	.035	-.350
0	230	-.121	.054	.034	-.462
0	231	-.115	.055	.059	-.451
0	232	-.115	.062	.086	-.712
0	233	-.125	.074	.118	-.595
0	234	-.125	.084	.162	-.876
0	235	-.120	.083	.160	-.891
0	236	-.108	.058	.067	-.528
0	237	-.105	.047	.022	-.367
0	238	-.114	.048	.042	-.349
0	239	-.109	.045	.061	-.324
0	240	-.111	.048	.084	-.353
0	241	-.124	.056	.040	-.507
0	242	-.120	.061	.032	-.668
0	243	-.117	.062	.042	-.903
0	244	-.087	.043	.069	-.322
0	245	-.085	.038	.027	-.328
0	246	-.101	.043	.044	-.279
0	247	-.109	.043	.020	-.299
0	248	-.124	.050	.020	-.431
0	249	-.136	.055	.005	-.514
0	250	-.125	.057	.012	-.497
0	251	-.125	.065	.065	-.547
0	252	-.067	.037	.072	-.249
0	253	-.087	.038	.025	-.235
0	254	-.077	.038	.032	-.251
0	255	-.080	.040	.047	-.292
0	256	-.094	.045	.041	-.320
0	257	-.122	.059	.020	-.426
0	258	-.132	.078	.014	-.921
0	259	-.130	.082	.051	-.823
0	260	-.051	.035	.093	-.223
0	261	-.052	.032	.030	-.274
0	262	-.064	.035	.069	-.265
0	263	-.064	.035	.047	-.305
0	264	-.065	.037	.034	-.240
0	265	-.074	.034	.025	-.252
0	266	-.073	.038	.032	-.369
0	267	-.070	.040	.035	-.372
0	268	-.051	.032	.034	-.214
0	269	-.069	.032	.040	-.223
0	270	-.065	.034	.052	-.234
0	271	-.059	.034	.073	-.208
0	272	-.063	.034	.046	-.256
0	273	-.048	.031	.039	-.174
0	274	-.055	.032	.034	-.194
0	275	-.058	.032	.082	-.212
0	276	-.052	.029	.038	-.163
0	277	-.062	.035	.046	-.274
0	300	-.092	.050	.054	-.271
0	301	-.145	.069	.043	-.545
0	302	-.158	.075	.063	-.515
0	303	-.152	.096	.045	-.715
0	304	-.207	.074	.163	-.515
0	305	-.127	.062	.057	-.517
0	306	-.133	.071	.072	-.485
0	307	-.131	.074	.163	-.515

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
0	308	-.120	.068	.082	-.481	0	358	-.075	.055	.054	-.571	0	428	.098	.134	.627	-.655
0	309	-.191	.089	.032	-.642	0	359	-.076	.053	.043	-.434	0	429	.106	.131	.609	-.481
0	310	-.179	.069	-.009	-.627	0	360	-.082	.049	.023	-.692	0	430	.078	.102	.618	-.189
0	311	-.128	.070	.122	-.446	0	361	-.071	.035	.075	-.212	0	431	.055	.089	.584	-.214
0	312	-.123	.068	.044	-.536	0	362	-.071	.035	.059	-.206	0	432	-.023	.064	.315	-.271
0	313	-.126	.065	.025	-.443	0	363	-.080	.050	.048	-.531	0	433	-.078	.061	.155	-.342
0	314	-.138	.058	.013	-.525	0	364	-.091	.041	.030	-.318	0	434	-.199	.094	.068	-.924
0	315	-.117	.056	.057	-.441	0	365	-.065	.041	.062	-.271	0	435	-.162	.100	.146	-.629
0	316	-.121	.058	.051	-.451	0	366	-.058	.040	.059	-.283	0	436	.082	.129	.723	-.456
0	317	-.077	.068	.240	-.397	0	367	-.059	.041	.057	-.283	0	437	.065	.122	.713	-.373
0	318	-.121	.047	.037	-.362	0	368	-.067	.041	.035	-.413	0	438	.065	.090	.741	-.344
0	319	-.211	.080	-.026	-.656	0	369	-.059	.037	.067	-.290	0	439	.046	.074	.627	-.166
0	320	-.202	.092	.028	-.578	0	370	-.060	.037	.082	-.328	0	440	-.021	.055	.269	-.266
0	321	-.150	.088	.087	-.649	0	371	-.020	.034	.096	-.126	0	441	-.068	.053	.131	-.290
0	322	-.141	.070	.035	-.824	0	372	-.058	.033	.093	-.187	0	442	-.179	.091	.023	-.667
0	323	-.154	.082	.106	-.737	0	373	-.061	.035	.055	-.289	0	443	-.129	.100	.227	-.679
0	324	-.152	.089	.042	-.984	0	374	-.060	.040	.069	-.359	0	444	.038	.088	.512	-.297
0	325	-.117	.053	.032	-.406	0	375	-.061	.040	.074	-.319	0	445	.057	.087	.590	-.300
0	326	-.127	.051	.050	-.342	0	376	-.064	.040	.062	-.345	0	446	.059	.071	.574	-.175
0	327	-.207	.094	.003	-.957	0	377	-.060	.033	.033	-.239	0	447	.045	.063	.484	-.159
0	328	-.212	.080	-.033	-.610	0	378	-.060	.039	.051	-.266	0	448	-.009	.044	.265	-.223
0	329	-.175	.106	.085	-1.016	0	379	-.062	.040	.045	-.312	0	449	-.052	.044	.098	-.269
0	330	-.168	.106	.059	-.866	0	380	-.064	.043	.041	-.428	0	450	-.151	.076	.068	-.696
0	331	-.166	.098	.036	-.765	0	401	-.013	.239	.903	-.895	0	451	-.102	.074	.166	-.429
0	332	-.179	.090	.059	-.892	0	402	-.090	.173	.654	-.954	0	452	-.017	.052	.255	-.194
0	333	-.127	.056	.025	-.453	0	403	-.086	.117	.391	-.823	0	453	.024	.064	.402	-.151
0	334	-.132	.059	.018	-.479	0	404	-.111	.095	.264	-.639	0	454	.054	.062	.398	-.089
0	335	-.073	.058	.157	-.336	0	405	-.137	.085	.269	-.756	0	455	.071	.064	.432	-.091
0	336	-.116	.043	-.002	-.303	0	406	.078	.185	.788	-1.081	0	456	.012	.040	.207	-.122
0	337	-.191	.097	.006	-.786	0	407	.053	.120	.559	-.424	0	457	-.037	.037	.096	-.198
0	338	-.185	.099	.054	-.779	0	408	.047	.120	.477	-.454	0	458	-.122	.065	.021	-.642
0	339	-.171	.121	.094	-1.149	0	409	.027	.107	.450	-.386	0	459	-.091	.064	.126	-.424
0	340	-.169	.094	.003	-.918	0	410	.026	.109	.447	-.396	0	460	-.017	.047	.262	-.175
0	341	-.162	.098	.040	-.776	0	411	-.148	.077	.205	-.476	0	461	.016	.060	.345	-.184
0	342	-.160	.104	.047	-.802	0	412	.089	.197	.777	-.624	0	462	.053	.065	.442	-.114
0	343	-.109	.053	.045	-.364	0	413	.097	.190	.771	-.725	0	463	.079	.059	.402	-.100
0	344	-.112	.044	-.002	-.366	0	414	.061	.140	.687	-.471	0	464	.032	.043	.224	-.122
0	345	-.149	.071	.020	-.530	0	415	.072	.105	.542	-.292	0	465	-.017	.037	.165	-.148
0	346	-.143	.072	.051	-.538	0	416	-.011	.084	.387	-.312	0	466	-.102	.062	.044	-.551
0	347	-.115	.076	.064	-.619	0	417	-.058	.069	.322	-.331	0	467	-.088	.053	.146	-.405
0	348	-.107	.071	.094	-.740	0	418	-.203	.097	.105	-.683	0	468	.013	.053	.320	-.115
0	349	-.110	.066	.048	-.633	0	419	-.162	.081	.109	-.483	0	469	.048	.056	.314	-.095
0	350	-.109	.073	.046	-.779	0	420	.098	.163	.792	-.617	0	470	.056	.061	.398	-.129
0	351	-.085	.042	.036	-.394	0	421	.113	.163	.755	-.650	0	471	.048	.054	.341	-.133
0	352	-.086	.035	.015	-.289	0	422	.092	.137	.666	-.422	0	472	.026	.047	.270	-.120
0	353	-.040	.040	.109	-.249	0	423	.071	.097	.582	-.177	0	473	-.009	.037	.184	-.119
0	354	-.093	.039	.028	-.243	0	424	-.016	.077	.401	-.235	0	474	.059	.068	.461	-.109
0	355	-.111	.061	.064	-.556	0	425	-.072	.062	.204	-.379	0	475	.060	.066	.406	-.121
0	356	-.113	.052	.005	-.534	0	426	-.207	.089	-.006	-.650	0	476	.050	.057	.350	-.134
0	357	-.079	.057	.055	-.626	0	427	-.179	.097	.146	-.692	0	477	-.005	.030	.137	-.122

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
0	801	-.091	.037	.023	-.326	10	123	-.058	.066	.439	-.351	10	207	-.089	.069	.105	-.464
0	802	-.079	.041	.041	-.291	10	124	-.029	.071	.563	-.270	10	208	-.099	.073	.153	-.523
0	803	-.066	.037	.045	-.213	10	125	-.011	.070	.540	-.265	10	209	-.132	.102	.262	-.701
0	804	.056	.064	.467	-.099	10	126	.002	.071	.374	-.417	10	210	-.157	.104	.133	-.745
0	805	.074	.050	.290	-.108	10	127	-.001	.068	.318	-.547	10	211	-.164	.112	.130	-.969
0	806	.006	.040	.180	-.122	10	128	-.016	.094	.428	-.633	10	212	-.085	.060	.101	-.596
0	807	-.064	.041	.062	-.276	10	129	-.116	.087	.218	-.736	10	213	-.083	.057	.088	-.546
0	808	-.063	.041	.069	-.303	10	130	.037	.104	.585	-.814	10	214	-.101	.068	.123	-.582
0	809	-.062	.033	.047	-.259	10	131	-.069	.047	.163	-.301	10	215	-.111	.078	.173	-.617
0	810	-.065	.038	.074	-.286	10	132	-.047	.049	.169	-.242	10	216	-.131	.089	.215	-.856
0	901	-.119	.093	.313	-.603	10	133	-.032	.049	.220	-.246	10	217	-.159	.105	.298	-.986
0	902	-.137	.086	.136	-.562	10	134	-.020	.055	.208	-.371	10	218	-.156	.090	.098	-.708
0	903	-.121	.068	.107	-.497	10	135	-.023	.065	.353	-.531	10	219	-.155	.095	.097	-.847
0	904	-.008	.100	.395	-.349	10	136	-.040	.100	.453	-.680	10	220	-.088	.050	.064	-.413
0	905	-.170	.092	.152	-.608	10	137	-.066	.044	.067	-.265	10	221	-.086	.046	.050	-.348
0	906	-.140	.081	.148	-.504	10	138	-.052	.041	.088	-.222	10	222	-.098	.057	.063	-.606
0	907	-.127	.070	.074	-.501	10	139	-.041	.036	.083	-.226	10	223	-.106	.068	.127	-.630
0	908	-.249	.101	.039	-.700	10	140	-.041	.046	.100	-.378	10	224	-.122	.088	.174	-.700
0	909	-.059	.124	.583	-.603	10	141	-.045	.073	.260	-.692	10	225	-.156	.106	.125	-.792
0	910	-.175	.102	.122	-.644	10	142	-.077	.090	.215	-.805	10	226	-.169	.126	.138	-.971
0	911	-.124	.108	.587	-.560	10	143	-.088	.062	.052	-.506	10	227	-.172	.124	.130	-.880
0	912	-.159	.088	.139	-.535	10	144	-.038	.058	.363	-.268	10	228	-.079	.046	.090	-.300
0	913	-.127	.095	.245	-.612	10	145	-.043	.039	.090	-.245	10	229	-.076	.039	.068	-.283
0	914	-.130	.078	.199	-.547	10	146	-.041	.036	.080	-.191	10	230	-.085	.051	.072	-.678
0	915	-.209	.094	.118	-.620	10	147	-.042	.037	.071	-.186	10	231	-.092	.054	.120	-.644
0	916	-.124	.156	.625	-.717	10	148	-.050	.041	.092	-.416	10	232	-.102	.065	.128	-.434
0	917	-.107	.129	.425	-.722	10	149	-.054	.038	.083	-.313	10	233	-.116	.081	.189	-.685
0	918	-.149	.094	.159	-.665	10	150	-.052	.043	.098	-.309	10	234	-.128	.102	.219	-.895
10	101	-.149	.138	.584	-.760	10	151	-.024	.036	.158	-.204	10	235	-.130	.099	.230	-.802
10	102	.044	.168	.832	-.472	10	152	-.027	.034	.097	-.162	10	236	-.058	.041	.095	-.257
10	103	.135	.248	.989	-.603	10	153	-.033	.030	.050	-.158	10	237	-.061	.035	.051	-.243
10	104	.103	.166	.749	-.360	10	154	-.034	.034	.072	-.173	10	238	-.066	.042	.069	-.316
10	105	.127	.185	.821	-.360	10	155	-.035	.035	.065	-.251	10	239	-.073	.047	.079	-.389
10	106	.082	.186	.934	-.488	10	156	-.033	.036	.085	-.256	10	240	-.086	.057	.124	-.505
10	107	.124	.195	1.008	-.332	10	157	-.016	.037	.143	-.332	10	241	-.104	.068	.048	-.574
10	108	.133	.207	.977	-.734	10	158	-.015	.039	.192	-.332	10	242	-.108	.073	.077	-.759
10	109	.014	.117	.584	-.376	10	159	-.023	.035	.112	-.157	10	243	-.107	.071	.064	-.749
10	110	.074	.154	.855	-.431	10	160	-.031	.032	.076	-.145	10	244	-.090	.033	.050	-.169
10	111	.105	.169	1.033	-.354	10	161	-.035	.029	.068	-.158	10	245	-.050	.031	.053	-.184
10	112	.119	.173	.934	-.465	10	162	-.031	.033	.090	-.163	10	246	-.050	.034	.064	-.232
10	113	.123	.157	.830	-.564	10	163	-.030	.035	.119	-.243	10	247	-.055	.036	.052	-.225
10	114	.105	.181	.972	-.677	10	164	-.029	.033	.083	-.174	10	248	-.068	.046	.050	-.281
10	115	.164	.116	.299	-.881	10	165	-.029	.029	.055	-.153	10	249	-.098	.058	.051	-.453
10	116	.019	.182	.749	-1.275	10	166	-.028	.033	.131	-.194	10	250	-.107	.065	.079	-.592
10	117	.035	.080	.481	-.733	10	201	-.106	.073	.095	-.584	10	251	-.100	.069	.082	-.631
10	118	.010	.093	.530	-.299	10	202	-.121	.091	.127	-.850	10	252	-.040	.034	.071	-.157
10	119	.033	.098	.572	-.347	10	203	-.131	.093	.183	-.654	10	253	-.042	.030	.048	-.171
10	120	.053	.090	.506	-.196	10	204	-.184	.120	.097	-.767	10	254	-.039	.031	.051	-.164
10	121	.054	.108	.678	-.334	10	205	-.213	.107	.165	-.639	10	255	-.040	.032	.057	-.162
10	122	.032	.122	.730	-.563	10	206	-.060	.064	.165	-.404	10	256	-.043	.034	.069	-.179

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
10	257	-.056	.039	.039	-.310	10	330	-.088	.072	.699	-.801	10	380	-.030	.036	.091	-.226
10	258	-.070	.057	.051	-.500	10	331	-.086	.063	.078	-.433	10	401	-.081	.107	.801	-.687
10	259	-.075	.066	.076	-.593	10	332	-.100	.063	.030	-.682	10	402	-.073	.110	.409	-.579
10	260	-.032	.030	.076	-.138	10	333	-.077	.045	.075	-.353	10	403	-.053	.099	.292	-.780
10	261	-.033	.030	.068	-.147	10	334	-.080	.047	.075	-.427	10	404	-.076	.079	.224	-.610
10	262	-.022	.033	.104	-.166	10	335	-.054	.049	.148	-.287	10	405	-.095	.076	.253	-.547
10	263	-.020	.033	.095	-.143	10	336	-.083	.043	.047	-.334	10	406	-.045	.193	.735	-1.224
10	264	-.027	.030	.088	-.129	10	337	-.106	.072	.055	-.576	10	407	-.024	.099	.397	-.531
10	265	-.033	.028	.056	-.181	10	338	-.105	.074	.085	-.600	10	408	-.004	.098	.344	-.492
10	266	-.032	.034	.082	-.199	10	339	-.081	.076	.110	-.823	10	409	-.002	.089	.373	-.376
10	267	-.033	.036	.130	-.250	10	340	-.078	.055	.054	-.595	10	410	-.001	.087	.402	-.358
10	268	-.028	.029	.078	-.126	10	341	-.074	.060	.080	-.551	10	411	-.005	.080	.122	-.381
10	269	-.035	.027	.053	-.125	10	342	-.075	.064	.076	-.612	10	412	-.048	.178	.849	-.610
10	270	-.033	.030	.074	-.138	10	343	-.059	.038	.087	-.223	10	413	-.031	.186	.792	-1.093
10	271	-.028	.031	.081	-.123	10	344	-.072	.034	.047	-.252	10	414	-.031	.127	.476	-.980
10	272	-.029	.034	.088	-.184	10	345	-.094	.063	.050	-.666	10	415	-.022	.073	.352	-.304
10	273	-.021	.028	.081	-.118	10	346	-.092	.065	.061	-.703	10	416	-.040	.069	.275	-.347
10	274	-.026	.029	.072	-.165	10	347	-.061	.058	.106	-.609	10	417	-.050	.059	.192	-.329
10	275	-.028	.030	.083	-.150	10	348	-.053	.052	.093	-.498	10	418	-.115	.074	.092	-.569
10	276	-.014	.028	.102	-.117	10	349	-.057	.052	.120	-.401	10	419	-.107	.065	.125	-.578
10	277	-.011	.034	.204	-.125	10	350	-.056	.053	.087	-.542	10	420	-.037	.166	.594	-.956
10	301	-.134	.075	.092	-.504	10	351	-.049	.038	.087	-.233	10	421	-.021	.164	.682	-.971
10	302	-.115	.069	.065	-.584	10	352	-.054	.029	.040	-.193	10	422	-.019	.122	.558	-.920
10	303	-.118	.074	.144	-.664	10	353	-.026	.038	.163	-.195	10	423	-.009	.071	.290	-.444
10	304	-.129	.076	.052	-.494	10	354	-.055	.037	.054	-.226	10	424	-.039	.060	.192	-.525
10	305	-.079	.062	.100	-.407	10	355	-.068	.047	.061	-.409	10	425	-.056	.052	.186	-.567
10	306	-.079	.051	.089	-.299	10	356	-.067	.041	.052	-.316	10	426	-.122	.078	.049	-.514
10	307	-.080	.060	.098	-.291	10	357	-.042	.045	.088	-.305	10	427	-.124	.078	.117	-.505
10	308	-.083	.061	.087	-.420	10	358	-.038	.044	.102	-.380	10	428	-.114	.123	.522	-.617
10	309	-.113	.071	.059	-.477	10	359	-.038	.041	.092	-.325	10	429	-.026	.119	.546	-.790
10	310	-.106	.057	.032	-.455	10	360	-.042	.034	.059	-.247	10	430	-.017	.085	.487	-.671
10	311	-.080	.061	.075	-.428	10	361	-.040	.034	.072	-.178	10	431	-.014	.071	.456	-.628
10	312	-.078	.059	.078	-.528	10	362	-.040	.034	.068	-.171	10	432	-.030	.054	.268	-.329
10	313	-.078	.057	.080	-.569	10	363	-.044	.042	.080	-.288	10	433	-.052	.049	.191	-.354
10	314	-.084	.047	.064	-.385	10	364	-.053	.036	.077	-.230	10	434	-.024	.081	.045	-.968
10	315	-.077	.054	.095	-.486	10	365	-.034	.040	.085	-.295	10	435	-.098	.083	.765	-.954
10	316	-.082	.057	.099	-.504	10	366	-.030	.039	.082	-.305	10	436	-.039	.109	.708	-.736
10	317	-.077	.059	.164	-.341	10	367	-.031	.038	.096	-.289	10	437	-.047	.105	.711	-.620
10	318	-.102	.052	.086	-.450	10	368	-.035	.028	.052	-.153	10	438	-.033	.074	.434	-.431
10	319	-.123	.062	.025	-.492	10	369	-.035	.031	.072	-.145	10	439	-.034	.064	.354	-.455
10	320	-.126	.079	.037	-.535	10	370	-.035	.031	.078	-.150	10	440	-.017	.048	.307	-.344
10	321	-.102	.081	.134	-.839	10	371	-.003	.036	.129	-.119	10	441	-.041	.044	.140	-.258
10	322	-.104	.065	.032	-.576	10	372	-.028	.032	.068	-.147	10	442	-.107	.063	.060	-.531
10	323	-.097	.066	.129	-.656	10	373	-.032	.027	.063	-.135	10	443	-.107	.066	.155	-.620
10	324	-.108	.075	.046	-.837	10	374	-.031	.030	.088	-.153	10	444	-.119	.066	.496	-.667
10	325	-.088	.052	.056	-.341	10	375	-.032	.030	.074	-.171	10	445	-.035	.068	.479	-.667
10	326	-.090	.050	.052	-.305	10	376	-.033	.031	.077	-.178	10	446	-.038	.057	.329	-.127
10	327	-.127	.082	.055	-.646	10	377	-.029	.030	.068	-.176	10	447	-.035	.055	.438	-.128
10	328	-.118	.062	.025	-.679	10	378	-.030	.035	.086	-.217	10	448	-.002	.040	.236	-.134
10	329	-.091	.080	.145	-1.076	10	379	-.031	.035	.091	-.216	10	449	-.028	.038	.090	-.186

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
10	450	-.084	.052	.075	-.489	10	913	-.039	.098	.399	-.441	20	145	-.017	.041	.147	-.186
10	451	-.056	.051	.122	-.380	10	914	-.078	.069	.202	-.362	20	146	-.026	.036	.148	-.201
10	452	-.017	.041	.204	-.161	10	915	-.194	.102	.088	-.645	20	147	-.026	.034	.145	-.150
10	453	-.001	.049	.244	-.152	10	916	-.129	.116	.434	-.629	20	148	-.026	.031	.117	-.183
10	454	.024	.052	.207	-.110	10	917	-.054	.103	.272	-.546	20	149	-.030	.029	.063	-.144
10	455	.046	.061	.369	-.100	10	918	-.083	.078	.139	-.503	20	150	-.031	.033	.084	-.216
10	456	.016	.044	.236	-.104	20	101	-.148	.191	.831	-.913	20	151	-.005	.040	.182	-.155
10	457	-.017	.036	.109	-.167	20	102	.087	.212	.885	-.578	20	152	-.013	.034	.131	-.136
10	458	-.067	.046	.043	-.406	20	103	.110	.276	1.119	-1.014	20	153	-.025	.030	.093	-.159
10	459	-.044	.049	.173	-.362	20	104	.170	.180	.842	-.375	20	154	-.027	.032	.087	-.178
10	460	-.017	.036	.283	-.136	20	105	.194	.199	1.100	-.502	20	155	-.025	.031	.080	-.131
10	461	-.008	.045	.339	-.140	20	106	.170	.212	.995	-.481	20	156	-.024	.030	.079	-.124
10	462	.006	.050	.290	-.124	20	107	.189	.205	.901	-.440	20	157	-.009	.038	.209	-.131
10	463	.033	.052	.307	-.106	20	108	.165	.195	.890	-.434	20	158	-.027	.032	.119	-.138
10	464	.019	.045	.204	-.116	20	109	.101	.140	.732	-.469	20	159	-.007	.036	.192	-.133
10	465	.002	.037	.143	-.120	20	110	.169	.188	1.068	-.501	20	160	-.018	.033	.133	-.122
10	466	-.055	.049	.102	-.433	20	111	.224	.204	1.206	-.411	20	161	-.020	.028	.108	-.127
10	467	-.039	.050	.186	-.429	20	112	.216	.195	1.051	-.472	20	162	-.018	.029	.089	-.123
10	468	.002	.038	.232	-.106	20	113	.180	.168	.918	-.361	20	163	-.017	.038	.143	-.164
10	469	.023	.051	.267	-.096	20	114	.107	.161	.921	-.536	20	164	-.015	.033	.124	-.129
10	470	.035	.062	.355	-.147	20	115	-.293	.192	.192	-1.395	20	165	-.017	.032	.103	-.119
10	471	.036	.058	.367	-.126	20	116	-.212	.234	.760	-1.141	20	166	-.021	.034	.117	-.133
10	472	.029	.051	.289	-.143	20	117	.038	.112	.554	-.321	20	201	-.103	.071	.143	-.594
10	473	-.006	.029	.109	-.092	20	118	.103	.145	.742	-.317	20	202	-.118	.087	.183	-1.012
10	474	.020	.049	.223	-.142	20	119	.129	.155	.923	-.220	20	203	-.158	.103	.132	-.695
10	475	.026	.053	.302	-.140	20	120	.124	.137	.764	-.181	20	204	-.264	.140	.114	-1.076
10	476	.033	.047	.245	-.111	20	121	.083	.127	.687	-.453	20	205	-.324	.153	.146	-.959
10	477	.015	.032	.175	-.070	20	122	.027	.108	.610	-.806	20	206	-.083	.064	.221	-.397
10	601	-.035	.031	.085	-.142	20	123	-.068	.083	.399	-.363	20	207	-.078	.067	.168	-.452
10	602	-.033	.032	.081	-.173	20	124	.027	.095	.508	-.251	20	208	-.096	.070	.135	-.436
10	603	-.028	.030	.089	-.124	20	125	.039	.095	.485	-.256	20	209	-.164	.121	.199	-.902
10	604	.036	.055	.279	-.099	20	126	.032	.088	.547	-.254	20	210	-.243	.133	.113	-1.019
10	605	.048	.046	.242	-.063	20	127	.015	.073	.461	-.220	20	211	-.297	.151	.041	-1.025
10	606	.011	.037	.155	-.111	20	128	-.018	.075	.407	-.360	20	212	-.084	.061	.122	-.390
10	607	-.034	.034	.081	-.226	20	129	-.115	.135	.257	-.794	20	213	-.085	.059	.087	-.332
10	608	-.031	.034	.082	-.226	20	130	-.105	.150	.301	-1.063	20	214	-.087	.061	.118	-.597
10	609	-.031	.028	.053	-.147	20	131	-.017	.058	.248	-.445	20	215	-.113	.078	.113	-.703
10	610	-.033	.033	.071	-.170	20	132	-.007	.061	.273	-.357	20	216	-.164	.114	.184	-.898
10	901	-.139	.097	.231	-.595	20	133	-.004	.058	.337	-.249	20	217	-.264	.158	.257	-1.086
10	902	-.123	.091	.181	-.650	20	134	-.007	.056	.306	-.202	20	218	-.297	.150	.068	-.999
10	903	-.107	.086	.219	-.544	20	135	-.019	.048	.187	-.307	20	219	-.295	.152	.077	-1.002
10	904	-.029	.098	.491	-.322	20	136	-.035	.058	.278	-.441	20	220	-.082	.059	.090	-.440
10	905	-.164	.098	.161	-.627	20	137	-.018	.054	.218	-.319	20	221	-.084	.057	.066	-.558
10	906	-.102	.075	.149	-.527	20	138	-.016	.049	.268	-.264	20	222	-.080	.055	.093	-.438
10	907	-.083	.065	.156	-.394	20	139	-.019	.041	.206	-.279	20	223	-.105	.076	.152	-.636
10	908	-.245	.101	.004	-.785	20	140	-.027	.042	.157	-.259	20	224	-.141	.122	.177	-1.026
10	909	-.040	.121	.465	-.582	20	141	-.025	.048	.125	-.339	20	225	-.234	.166	.153	-1.135
10	910	-.106	.080	.179	-.487	20	142	-.038	.044	.104	-.339	20	226	-.301	.202	.159	-1.918
10	911	-.004	.111	.415	-.412	20	143	-.015	.054	.235	-.474	20	227	-.311	.191	.154	-1.776
10	912	-.104	.070	.124	-.439	20	144	-.013	.049	.247	-.368	20	228	-.271	.057	.109	-.422

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
20	229	-.074	.051	.063	-.413	20	302	-.112	.071	.093	-.588	20	352	-.043	.032	.082	-.224
20	230	-.059	.050	.098	-.412	20	303	-.125	.078	.076	-.776	20	353	-.025	.034	.098	-.191
20	231	-.071	.058	.112	-.601	20	304	-.101	.065	.112	-.445	20	354	-.037	.033	.084	-.222
20	232	-.077	.079	.170	-.689	20	305	-.069	.057	.110	-.363	20	355	-.042	.036	.082	-.260
20	233	-.129	.113	.116	-1.019	20	306	-.069	.052	.095	-.465	20	356	-.046	.033	.059	-.189
20	234	-.189	.174	.201	-1.478	20	307	-.065	.058	.098	-.591	20	357	-.031	.036	.082	-.196
20	235	-.214	.171	.125	-1.643	20	308	-.085	.064	.119	-.495	20	358	-.029	.035	.087	-.190
20	236	-.051	.046	.085	-.453	20	309	-.091	.061	.089	-.449	20	359	-.031	.035	.082	-.192
20	237	-.058	.043	.058	-.335	20	310	-.083	.056	.074	-.442	20	360	-.025	.030	.072	-.260
20	238	-.046	.039	.085	-.258	20	311	-.071	.060	.087	-.431	20	361	-.031	.033	.080	-.158
20	239	-.048	.040	.125	-.400	20	312	-.069	.057	.084	-.416	20	362	-.029	.033	.079	-.163
20	240	-.043	.046	.138	-.524	20	313	-.068	.056	.079	-.379	20	363	-.027	.035	.082	-.241
20	241	-.072	.071	.136	-.750	20	314	-.073	.049	.062	-.457	20	364	-.032	.029	.054	-.161
20	242	-.101	.119	.165	-1.159	20	315	-.076	.056	.108	-.385	20	365	-.023	.033	.090	-.183
20	243	-.121	.119	.162	-.999	20	316	-.079	.058	.104	-.391	20	366	-.019	.032	.087	-.188
20	244	-.040	.038	.100	-.405	20	317	-.092	.071	.147	-.456	20	367	-.021	.031	.077	-.146
20	245	-.044	.033	.078	-.222	20	318	-.107	.063	.143	-.518	20	368	-.023	.029	.087	-.158
20	246	-.035	.032	.087	-.179	20	319	-.090	.054	.051	-.487	20	369	-.028	.032	.098	-.155
20	247	-.035	.030	.112	-.148	20	320	-.085	.058	.082	-.448	20	370	-.024	.032	.097	-.151
20	248	-.028	.035	.102	-.165	20	321	-.078	.060	.111	-.427	20	371	-.012	.034	.125	-.121
20	249	-.040	.043	.091	-.410	20	322	-.069	.047	.064	-.485	20	372	-.020	.034	.101	-.137
20	250	-.039	.061	.131	-.474	20	323	-.068	.050	.074	-.439	20	373	-.021	.030	.100	-.134
20	251	-.031	.060	.148	-.634	20	324	-.068	.054	.092	-.450	20	374	-.019	.033	.112	-.160
20	252	-.035	.034	.075	-.153	20	325	-.073	.054	.072	-.386	20	375	-.021	.033	.098	-.162
20	253	-.038	.031	.050	-.194	20	326	-.081	.056	.087	-.467	20	376	-.023	.034	.101	-.173
20	254	-.030	.030	.064	-.165	20	327	-.069	.054	.077	-.508	20	377	-.024	.029	.093	-.124
20	255	-.029	.030	.063	-.153	20	328	-.072	.042	.046	-.381	20	378	-.024	.034	.104	-.129
20	256	-.021	.031	.083	-.153	20	329	-.059	.051	.100	-.627	20	379	-.025	.034	.103	-.130
20	257	-.019	.033	.123	-.136	20	330	-.055	.046	.072	-.571	20	380	-.024	.034	.101	-.149
20	258	-.007	.039	.175	-.209	20	331	-.055	.045	.070	-.364	20	401	-.230	.181	.453	-.935
20	259	-.006	.047	.221	-.266	20	332	-.059	.040	.100	-.272	20	402	-.147	.144	.400	-.930
20	260	-.027	.035	.114	-.189	20	333	-.066	.048	.108	-.312	20	403	-.101	.101	.200	-.686
20	261	-.032	.029	.070	-.146	20	334	-.067	.050	.117	-.349	20	404	-.088	.084	.307	-.588
20	262	-.009	.030	.089	-.108	20	335	-.053	.045	.106	-.519	20	405	-.087	.081	.252	-.587
20	263	-.008	.030	.105	-.119	20	336	-.074	.047	.057	-.358	20	406	-.259	.243	.384	-1.848
20	264	-.013	.031	.114	-.157	20	337	-.060	.042	.067	-.462	20	407	-.157	.152	.318	-.997
20	265	-.013	.030	.128	-.111	20	338	-.059	.041	.077	-.485	20	408	-.088	.131	.352	-.878
20	266	-.003	.037	.139	-.121	20	339	-.046	.043	.106	-.609	20	409	-.057	.101	.322	-.602
20	267	-.001	.040	.159	-.140	20	340	-.044	.035	.064	-.305	20	410	-.042	.088	.372	-.603
20	268	-.012	.031	.117	-.121	20	341	-.042	.039	.082	-.245	20	411	-.083	.061	.163	-.351
20	269	-.023	.029	.075	-.139	20	342	-.045	.042	.087	-.326	20	412	-.226	.195	.460	-1.250
20	270	-.014	.032	.103	-.126	20	343	-.056	.045	.077	-.313	20	413	-.228	.218	.527	-1.481
20	271	-.006	.033	.140	-.140	20	344	-.055	.043	.092	-.386	20	414	-.191	.191	.272	-1.102
20	272	-.004	.037	.194	-.172	20	345	-.046	.039	.103	-.194	20	415	-.096	.111	.355	-.768
20	273	-.009	.020	.098	-.118	20	346	-.047	.040	.107	-.203	20	416	-.080	.081	.249	-.483
20	274	-.028	.035	.078	-.174	20	347	-.036	.041	.108	-.396	20	417	-.068	.064	.179	-.413
20	275	-.014	.035	.114	-.137	20	348	-.029	.036	.096	-.193	20	418	-.093	.065	.128	-.475
20	276	.006	.032	.158	-.085	20	349	-.030	.036	.116	-.186	20	419	-.089	.060	.107	-.398
20	277	.013	.043	.254	-.201	20	350	-.031	.038	.117	-.218	20	420	-.189	.163	.488	-1.137
20	301	-.127	.084	.114	-.616	20	351	-.041	.040	.116	-.229	20	421	-.188	.174	.421	-1.102

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
20	422	-.163	.167	.263	-1.162
20	423	-.096	.101	.176	-.652
20	424	-.075	.078	.124	-.604
20	425	-.068	.061	.145	-.497
20	426	-.089	.057	.065	-.541
20	427	-.076	.063	.158	-.591
20	428	-.147	.152	.179	-1.070
20	429	-.140	.160	.178	-1.209
20	430	-.114	.126	.185	-.945
20	431	-.064	.095	.166	-.802
20	432	-.057	.066	.124	-.565
20	433	-.054	.053	.090	-.452
20	434	-.069	.049	.094	-.425
20	435	-.054	.050	.141	-.352
20	436	-.070	.104	.240	-1.032
20	437	-.060	.101	.199	-.941
20	438	-.046	.068	.171	-.659
20	439	-.022	.053	.163	-.415
20	440	-.029	.039	.109	-.275
20	441	-.032	.035	.081	-.309
20	442	-.054	.035	.082	-.226
20	443	-.039	.040	.111	-.262
20	444	-.037	.062	.153	-.693
20	445	-.030	.063	.230	-.679
20	446	-.019	.048	.180	-.342
20	447	-.002	.046	.239	-.163
20	448	-.012	.038	.216	-.140
20	449	-.020	.035	.128	-.161
20	450	-.047	.035	.080	-.206
20	451	-.031	.036	.118	-.191
20	452	-.025	.038	.145	-.372
20	453	-.021	.041	.175	-.329
20	454	-.017	.043	.417	-.231
20	455	.001	.047	.329	-.143
20	456	-.006	.038	.179	-.133
20	457	-.015	.032	.088	-.125
20	458	-.038	.031	.062	-.196
20	459	-.023	.034	.093	-.156
20	460	-.019	.033	.162	-.174
20	461	-.017	.036	.213	-.146
20	462	-.017	.032	.208	-.122
20	463	.002	.037	.175	-.108
20	464	-.003	.036	.124	-.113
20	465	-.005	.033	.138	-.118
20	466	-.029	.034	.128	-.177
20	467	-.019	.034	.115	-.211
20	468	-.012	.033	.169	-.187
20	469	-.001	.040	.257	-.105
20	470	.007	.047	.306	-.137
20	471	.013	.044	.217	-.120
20	472	.011	.041	.203	-.119
20	473	-.013	.028	.082	-.115
20	474	-.002	.039	.199	-.135
20	475	.005	.042	.198	-.199
20	476	.011	.040	.162	-.124
20	477	-.003	.028	.108	-.088
20	801	-.001	.037	.137	-.121
20	802	-.011	.033	.107	-.150
20	803	-.009	.031	.093	-.128
20	804	-.009	.042	.232	-.201
20	805	.013	.040	.212	-.111
20	806	-.001	.036	.137	-.119
20	807	-.026	.033	.091	-.159
20	808	-.025	.033	.087	-.161
20	809	-.022	.027	.070	-.119
20	810	-.023	.031	.089	-.165
20	901	-.260	.140	.155	-1.009
20	902	-.154	.109	.149	-.777
20	903	-.105	.078	.320	-.556
20	904	-.050	.103	.399	-.491
20	905	-.262	.146	.090	-.976
20	906	-.161	.106	.161	-.728
20	907	-.074	.070	.148	-.473
20	908	-.336	.135	.044	-1.000
20	909	-.113	.149	.634	-.811
20	910	-.147	.102	.219	-.661
20	911	.006	.110	.520	-.365
20	912	-.169	.094	.075	-.782
20	913	-.010	.110	.608	-.592
20	914	-.056	.070	.226	-.443
20	915	-.217	.112	.087	-.694
20	916	-.238	.135	.159	-.926
20	917	-.098	.108	.242	-.697
20	918	-.076	.069	.170	-.478
30	101	-.230	.199	.651	-1.008
30	102	-.007	.240	.769	-.800
30	103	.092	.294	1.082	-.960
30	104	.231	.151	.857	-.168
30	105	.255	.168	.938	-.183
30	106	.245	.183	.934	-.336
30	107	.264	.179	.945	-.379
30	108	.234	.172	.891	-.363
30	109	.203	.131	.731	-.201
30	110	.312	.177	1.036	-.161
30	111	.356	.199	1.168	-.183
30	112	.346	.202	1.161	-.151
30	113	.265	.174	.917	-.223
30	114	.160	.159	.767	-.441
30	115	-.336	.231	.330	-1.691
30	116	-.329	.202	.314	-1.379
30	117	.119	.111	.537	-.266
30	118	.207	.140	.728	-.179
30	119	.239	.153	.787	-.169
30	120	.251	.150	.917	-.124
30	121	.179	.153	.919	-.212
30	122	.072	.132	.662	-.335
30	123	.086	.111	.599	-.285
30	124	.143	.127	.728	-.166
30	125	.155	.126	.857	-.171
30	126	.127	.117	.817	-.170
30	127	.064	.094	.716	-.201
30	128	-.010	.093	.528	-.369
30	129	-.103	.195	.388	-1.412
30	130	-.249	.188	.247	-1.586
30	131	.075	.102	.654	-.362
30	132	.099	.106	.772	-.258
30	133	.089	.093	.669	-.161
30	134	.057	.078	.436	-.184
30	135	.014	.061	.418	-.189
30	136	-.039	.066	.327	-.286
30	137	.092	.098	.674	-.193
30	138	.090	.093	.691	-.158
30	139	.042	.065	.385	-.146
30	140	.010	.057	.329	-.192
30	141	-.007	.056	.276	-.313
30	142	-.058	.049	.234	-.305
30	143	.043	.073	.426	-.461
30	144	-.121	.078	.067	-.762
30	145	.044	.064	.368	-.184
30	146	.015	.047	.212	-.142
30	147	-.011	.040	.164	-.165
30	148	-.018	.034	.115	-.165
30	149	-.045	.034	.087	-.181
30	150	-.062	.040	.083	-.245
30	151	.019	.057	.303	-.164
30	152	.002	.042	.185	-.139
30	153	-.028	.032	.102	-.154
30	154	-.040	.037	.144	-.209
30	155	-.045	.029	.063	-.164
30	156	-.051	.040	.114	-.285
30	157	.045	.051	.378	-.082
30	158	-.082	.052	.075	-.446
30	159	.011	.047	.230	-.127
30	160	-.019	.036	.130	-.208
30	161	-.031	.033	.077	-.151
30	162	-.030	.035	.096	-.209
30	163	-.006	.051	.256	-.174
30	164	-.013	.040	.173	-.146
30	165	-.021	.033	.144	-.151
30	166	-.046	.040	.154	-.260

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
30	201	-.115	.069	.196	-.521	30	251	-.026	.106	.316	-.655	30	324	-.092	.056	.068	-.387
30	202	-.131	.080	.239	-.572	30	252	-.061	.045	.085	-.326	30	325	-.102	.056	.058	-.444
30	203	-.180	.117	.145	-.802	30	253	-.061	.039	.047	-.332	30	326	-.109	.061	.062	-.451
30	204	-.333	.157	.068	-.961	30	254	-.033	.034	.092	-.199	30	327	-.107	.061	.049	-.512
30	205	-.390	.162	-.023	-1.112	30	255	-.034	.033	.093	-.192	30	328	-.104	.051	.048	-.430
30	206	-.101	.069	.156	-.492	30	256	-.006	.034	.153	-.162	30	329	-.096	.053	.046	-.443
30	207	-.061	.063	.160	-.389	30	257	-.011	.035	.123	-.219	30	330	-.088	.047	.049	-.353
30	208	-.100	.077	.088	-.587	30	258	.034	.044	.215	-.232	30	331	-.086	.049	.097	-.378
30	209	-.152	.134	.199	-.900	30	259	.041	.055	.266	-.355	30	332	-.094	.049	.070	-.340
30	210	-.298	.165	.086	-1.036	30	260	-.048	.039	.068	-.353	30	333	-.105	.056	.072	-.398
30	211	-.397	.174	.022	-1.115	30	261	-.056	.036	.060	-.274	30	334	-.103	.057	.080	-.379
30	212	-.111	.067	.093	-.402	30	262	-.023	.033	.089	-.185	30	335	-.133	.082	.082	-.545
30	213	-.112	.066	.102	-.389	30	263	-.013	.032	.109	-.169	30	336	-.114	.048	.030	-.450
30	214	-.093	.058	.135	-.382	30	264	.000	.033	.116	-.106	30	337	-.098	.053	.046	-.327
30	215	-.132	.079	.226	-.680	30	265	-.003	.033	.158	-.131	30	338	-.090	.051	.049	-.302
30	216	-.179	.139	.142	-.909	30	266	.030	.044	.197	-.119	30	339	-.083	.046	.039	-.332
30	217	-.329	.199	.099	-1.471	30	267	.036	.049	.226	-.132	30	340	-.082	.044	.050	-.450
30	218	-.423	.170	.198	-1.250	30	268	-.014	.033	.136	-.121	30	341	-.079	.052	.069	-.588
30	219	-.412	.166	.105	-1.171	30	269	-.028	.031	.093	-.146	30	342	-.079	.056	.068	-.564
30	220	-.116	.067	.105	-.436	30	270	.005	.034	.143	-.116	30	343	-.090	.055	.068	-.473
30	221	-.114	.062	.095	-.428	30	271	.014	.033	.179	-.095	30	344	-.088	.045	.045	-.280
30	222	-.089	.057	.126	-.463	30	272	.022	.037	.182	-.104	30	345	-.081	.047	.057	-.438
30	223	-.122	.078	.136	-.829	30	273	-.007	.032	.100	-.124	30	346	-.073	.045	.076	-.379
30	224	-.147	.138	.174	-.894	30	274	-.043	.041	.078	-.183	30	347	-.069	.044	.068	-.287
30	225	-.300	.204	.128	-1.252	30	275	.008	.040	.133	-.153	30	348	-.060	.040	.055	-.258
30	226	-.401	.222	.151	-1.711	30	276	.025	.033	.180	-.086	30	349	-.060	.050	.059	-.687
30	227	-.408	.202	.120	-1.576	30	277	.048	.054	.331	-.116	30	350	-.059	.055	.085	-.920
30	228	-.110	.067	.087	-.460	30	301	-.169	.101	.126	-.792	30	351	-.070	.050	.085	-.523
30	229	-.112	.061	.057	-.468	30	302	-.146	.093	.060	-.750	30	352	-.076	.042	.030	-.348
30	230	-.076	.052	.102	-.384	30	303	-.156	.067	.009	-.453	30	353	-.087	.055	.062	-.405
30	231	-.102	.060	.149	-.681	30	304	-.128	.056	.019	-.415	30	354	-.066	.042	.066	-.270
30	232	-.084	.092	.150	-.796	30	305	-.091	.066	.114	-.456	30	355	-.062	.039	.082	-.306
30	233	-.176	.169	.218	-1.315	30	306	-.096	.057	.085	-.372	30	356	-.056	.032	.073	-.231
30	234	-.293	.257	.249	-1.439	30	307	-.090	.065	.102	-.395	30	357	-.053	.041	.087	-.474
30	235	-.339	.232	.192	-1.557	30	308	-.120	.071	.090	-.435	30	358	-.049	.040	.080	-.392
30	236	-.095	.063	.085	-.595	30	309	-.129	.073	.189	-.454	30	359	-.051	.047	.068	-.714
30	237	-.091	.052	.057	-.516	30	310	-.113	.059	.090	-.455	30	360	-.053	.042	.055	-.407
30	238	-.059	.041	.079	-.307	30	311	-.103	.062	.079	-.451	30	361	-.065	.047	.062	-.352
30	239	-.073	.042	.058	-.288	30	312	-.095	.058	.085	-.379	30	362	-.062	.045	.063	-.289
30	240	-.042	.047	.133	-.380	30	313	-.092	.058	.075	-.373	30	363	-.044	.034	.077	-.173
30	241	-.078	.083	.118	-.860	30	314	-.100	.055	.080	-.445	30	364	-.044	.030	.055	-.174
30	242	-.097	.162	.249	-1.446	30	315	-.110	.066	.135	-.428	30	365	-.041	.037	.072	-.375
30	243	-.155	.162	.273	-1.378	30	316	-.112	.068	.136	-.579	30	366	-.035	.036	.088	-.195
30	244	-.072	.048	.075	-.307	30	317	-.158	.105	.158	-.924	30	367	-.037	.037	.089	-.235
30	245	-.071	.043	.042	-.332	30	318	-.138	.060	.075	-.450	30	368	-.040	.034	.073	-.226
30	246	-.044	.036	.074	-.199	30	319	-.125	.063	.050	-.494	30	369	-.053	.041	.072	-.309
30	247	-.052	.035	.053	-.236	30	320	-.111	.066	.090	-.423	30	370	-.044	.038	.080	-.246
30	248	-.022	.038	.131	-.184	30	321	-.104	.059	.063	-.440	30	371	-.035	.037	.192	-.202
30	249	-.034	.045	.158	-.636	30	322	-.093	.043	.058	-.293	30	372	-.023	.035	.095	-.226
30	250	.006	.079	.254	-.940	30	323	-.097	.058	.058	-.583	30	373	-.038	.030	.056	-.158

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
30	374	-.034	.033	.073	-.160
30	375	-.032	.033	.084	-.161
30	376	-.032	.034	.083	-.193
30	377	-.036	.028	.058	-.148
30	378	-.035	.032	.070	-.145
30	379	-.033	.033	.084	-.163
30	380	-.032	.033	.085	-.188
30	401	-.332	.163	.148	-.971
30	402	-.281	.157	.190	-.939
30	403	-.239	.142	.136	-.906
30	404	-.169	.131	.188	-.894
30	405	-.141	.115	.254	-.957
30	406	-.343	.196	.180	-1.445
30	407	-.311	.162	.202	-1.107
30	408	-.234	.167	.226	-1.055
30	409	-.162	.140	.259	-.923
30	410	-.118	.117	.311	-.929
30	411	-.117	.076	.172	-.541
30	412	-.342	.191	.289	-1.510
30	413	-.357	.203	.276	-1.578
30	414	-.343	.216	.303	-1.759
30	415	-.239	.152	.202	-1.006
30	416	-.163	.121	.256	-.733
30	417	-.125	.101	.206	-.795
30	418	-.111	.074	.154	-.501
30	419	-.121	.072	.108	-.512
30	420	-.312	.183	.185	-1.175
30	421	-.323	.195	.247	-1.244
30	422	-.311	.201	.206	-1.291
30	423	-.241	.147	.195	-.979
30	424	-.187	.137	.210	-.935
30	425	-.159	.124	.152	-.960
30	426	-.114	.060	.069	-.421
30	427	-.115	.072	.095	-.569
30	428	-.265	.174	.114	-1.442
30	429	-.269	.184	.107	-1.409
30	430	-.244	.153	.108	-1.009
30	431	-.181	.137	.178	-.967
30	432	-.144	.106	.121	-.746
30	433	-.126	.094	.126	-.711
30	434	-.107	.058	.062	-.413
30	435	-.105	.069	.082	-.532
30	436	-.205	.143	.070	-1.225
30	437	-.206	.150	.119	-1.414
30	438	-.173	.110	.143	-.750
30	439	-.135	.102	.148	-.735
30	440	-.113	.082	.085	-.490
30	441	-.102	.075	.093	-.593
30	442	-.086	.049	.076	-.315
30	443	-.079	.055	.115	-.320
30	444	-.140	.094	.051	-.962
30	445	-.141	.097	.100	-1.000
30	446	-.129	.079	.084	-.755
30	447	-.107	.082	.135	-.584
30	448	-.086	.072	.099	-.715
30	449	-.071	.059	.083	-.624
30	450	-.065	.039	.086	-.231
30	451	-.057	.042	.110	-.267
30	452	-.106	.076	.063	-.647
30	453	-.108	.077	.131	-.692
30	454	-.100	.062	.059	-.645
30	455	-.076	.060	.105	-.408
30	456	-.055	.049	.092	-.395
30	457	-.048	.041	.081	-.361
30	458	-.051	.032	.047	-.315
30	459	-.045	.038	.085	-.413
30	460	-.083	.055	.068	-.548
30	461	-.088	.058	.067	-.655
30	462	-.083	.052	.057	-.359
30	463	-.057	.038	.106	-.269
30	464	-.038	.039	.097	-.251
30	465	-.040	.032	.060	-.178
30	466	-.041	.034	.076	-.177
30	467	-.046	.033	.094	-.217
30	468	-.083	.053	.045	-.586
30	469	-.067	.042	.088	-.279
30	470	-.049	.042	.098	-.244
30	471	-.039	.039	.128	-.246
30	472	-.033	.036	.128	-.158
30	473	-.062	.034	.051	-.217
30	474	-.055	.040	.073	-.216
30	475	-.053	.044	.136	-.270
30	476	-.034	.036	.109	-.246
30	477	-.029	.028	.066	-.138
30	801	.026	.040	.181	-.099
30	802	-.005	.038	.135	-.128
30	803	-.009	.034	.137	-.118
30	804	-.070	.058	.118	-.372
30	805	-.045	.045	.113	-.259
30	806	-.025	.038	.130	-.278
30	807	-.035	.036	.089	-.286
30	808	-.034	.036	.088	-.329
30	809	-.041	.028	.049	-.192
30	810	-.042	.033	.079	-.183
30	901	-.361	.133	-.031	-1.122
30	902	-.195	.107	.092	-.759
30	903	-.116	.076	.182	-.516
30	904	-.181	.099	.461	-.649
30	905	-.383	.136	.010	-.850
30	906	-.288	.120	.014	-.888
30	907	-.099	.075	.197	-.662
30	908	-.452	.146	.113	-1.188
30	909	-.251	.137	.273	-.919
30	910	-.272	.124	.097	-.917
30	911	-.060	.109	.666	-.527
30	912	-.316	.117	.006	-.751
30	913	-.087	.123	.438	-.556
30	914	-.106	.083	.180	-.574
30	915	-.324	.121	.099	-.820
30	916	-.360	.144	.019	-.863
30	917	-.260	.157	.288	-.993
30	918	-.145	.101	.175	-.676
40	101	-.256	.163	.636	-.813
40	102	-.184	.227	.816	-.824
40	103	-.142	.216	.901	-.736
40	104	.267	.145	.816	-.171
40	105	.264	.150	.887	-.172
40	106	.208	.149	.809	-.340
40	107	.222	.145	.789	-.205
40	108	.202	.140	.667	-.213
40	109	.277	.131	.776	-.131
40	110	.374	.167	1.080	-.060
40	111	.395	.180	1.225	-.066
40	112	.365	.174	1.188	-.065
40	113	.292	.146	.800	-.131
40	114	.184	.131	.674	-.222
40	115	-.314	.282	.609	-1.300
40	116	-.237	.115	.062	-.980
40	117	.248	.127	.754	-.199
40	118	.350	.163	.920	-.097
40	119	.372	.176	1.012	-.070
40	120	.310	.143	.788	-.018
40	121	.221	.135	.772	-.109
40	122	.107	.111	.569	-.272
40	123	.233	.122	.718	-.148
40	124	.309	.149	.937	-.087
40	125	.302	.151	.929	-.030
40	126	.250	.134	.847	-.058
40	127	.155	.096	.527	-.078
40	128	.052	.086	.435	-.284
40	129	-.113	.221	.456	-1.117
40	130	-.233	.139	.090	-1.195
40	131	.214	.113	.723	-.141
40	132	.255	.132	.843	-.136
40	133	.234	.124	.794	-.068
40	134	.170	.099	.618	-.095
40	135	.082	.070	.361	-.148
40	136	-.011	.064	.334	-.296
40	137	.218	.126	.903	-.260
40	138	.226	.130	.861	-.160

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
40	139	.168	.103	.689	-.080
40	140	.100	.089	.578	-.134
40	141	.049	.079	.392	-.164
40	142	-.063	.061	.178	-.331
40	143	.111	.092	.528	-.345
40	144	-.221	.099	.059	-1.083
40	145	.129	.090	.619	-.153
40	146	.070	.061	.363	-.153
40	147	.009	.049	.243	-.165
40	148	.004	.044	.223	-.122
40	149	-.069	.040	.079	-.252
40	150	-.114	.050	.048	-.340
40	151	.060	.071	.328	-.170
40	152	.021	.046	.213	-.132
40	153	-.038	.031	.074	-.172
40	154	-.061	.038	.125	-.254
40	155	-.081	.029	.022	-.175
40	156	-.109	.050	.095	-.461
40	157	.099	.064	.375	-.056
40	158	-.214	.079	.031	-.668
40	159	.049	.054	.283	-.160
40	160	-.017	.040	.173	-.165
40	161	-.043	.034	.086	-.170
40	162	-.048	.040	.112	-.220
40	163	.022	.064	.235	-.201
40	164	-.005	.045	.213	-.183
40	165	-.026	.035	.122	-.150
40	166	-.092	.044	.112	-.281
40	201	-.153	.068	.086	-.476
40	202	-.161	.070	.084	-.460
40	203	-.142	.097	.140	-.723
40	204	-.280	.155	.140	-1.138
40	205	-.417	.146	-.040	-1.195
40	206	-.167	.079	.064	-.499
40	207	-.066	.057	.248	-.389
40	208	-.069	.052	.088	-.406
40	209	-.092	.090	.184	-.686
40	210	-.238	.162	.071	-.982
40	211	-.416	.190	.056	-1.213
40	212	-.169	.078	.105	-.570
40	213	-.168	.076	.080	-.563
40	214	-.108	.051	.073	-.395
40	215	-.139	.059	.066	-.563
40	216	-.111	.099	.125	-.745
40	217	-.243	.201	.167	-1.162
40	218	-.401	.179	.254	-1.222
40	219	-.392	.171	.141	-1.110
40	220	-.176	.072	.066	-.592
40	221	-.172	.067	.039	-.635
40	222	-.124	.049	.038	-.345
40	223	-.157	.056	.041	-.501
40	224	-.119	.105	.191	-.891
40	225	-.231	.200	.151	-1.077
40	226	-.386	.227	.333	-1.588
40	227	-.386	.199	.310	-1.423
40	228	-.192	.080	.046	-.614
40	229	-.194	.071	-.007	-.689
40	230	-.126	.054	.079	-.404
40	231	-.159	.059	.066	-.472
40	232	-.084	.066	.162	-.826
40	233	-.151	.148	.161	-1.002
40	234	-.336	.260	.357	-1.349
40	235	-.361	.233	.381	-1.324
40	236	-.202	.090	.072	-.718
40	237	-.207	.080	.018	-.636
40	238	-.129	.059	.033	-.368
40	239	-.148	.056	.034	-.375
40	240	-.064	.054	.138	-.432
40	241	-.078	.072	.166	-.857
40	242	-.159	.197	.477	-1.560
40	243	-.221	.184	.467	-1.282
40	244	-.213	.099	.002	-.727
40	245	-.209	.094	-.002	-.608
40	246	-.119	.062	.059	-.363
40	247	-.116	.053	.019	-.321
40	248	-.032	.046	.130	-.201
40	249	-.055	.055	.199	-.553
40	250	-.001	.131	.357	-1.059
40	251	-.079	.164	.367	-.820
40	252	-.170	.108	.283	-.966
40	253	-.226	.133	-.012	-.839
40	254	-.104	.059	.043	-.355
40	255	-.087	.043	.031	-.304
40	256	-.011	.036	.128	-.138
40	257	-.022	.054	.239	-.298
40	258	.107	.063	.444	-.093
40	259	.127	.082	.583	-.255
40	260	-.118	.073	.089	-.486
40	261	-.129	.068	.016	-.573
40	262	-.050	.040	.112	-.244
40	263	-.030	.036	.118	-.153
40	264	.012	.034	.140	-.130
40	265	-.003	.041	.136	-.217
40	266	.090	.053	.341	-.065
40	267	.106	.064	.440	-.072
40	268	-.011	.036	.128	-.159
40	269	-.020	.042	.123	-.187
40	270	.031	.038	.187	-.106
40	271	.039	.041	.226	-.102
40	272	.069	.051	.326	-.097
40	273	-.022	.035	.093	-.155
40	274	-.092	.049	.102	-.274
40	275	.015	.033	.134	-.099
40	276	.045	.036	.175	-.122
40	277	.094	.064	.334	-.135
40	301	-.199	.112	.127	-.894
40	302	-.209	.112	.014	-1.026
40	303	-.209	.070	-.023	-.515
40	304	-.167	.057	.005	-.397
40	305	-.145	.074	.081	-.487
40	306	-.152	.070	.061	-.566
40	307	-.140	.078	.134	-.483
40	308	-.175	.077	.059	-.522
40	309	-.178	.080	.068	-.662
40	310	-.176	.066	.021	-.518
40	311	-.165	.073	.025	-.633
40	312	-.161	.072	.027	-.525
40	313	-.156	.073	.078	-.521
40	314	-.150	.062	.061	-.495
40	315	-.160	.070	.067	-.519
40	316	-.162	.070	.057	-.522
40	317	-.196	.091	.182	-.676
40	318	-.191	.057	.016	-.422
40	319	-.179	.063	.026	-.520
40	320	-.171	.069	.042	-.540
40	321	-.178	.069	.027	-.730
40	322	-.172	.057	.026	-.442
40	323	-.162	.063	.034	-.531
40	324	-.168	.070	.128	-.606
40	325	-.189	.070	.095	-.521
40	326	-.173	.065	.018	-.555
40	327	-.187	.079	.059	-.633
40	328	-.174	.065	-.005	-.523
40	329	-.191	.082	.036	-.656
40	330	-.182	.075	.022	-.686
40	331	-.177	.072	.022	-.691
40	332	-.176	.061	.016	-.495
40	333	-.185	.070	.062	-.573
40	334	-.185	.070	.005	-.554
40	335	-.203	.096	.102	-.928
40	336	-.176	.054	-.025	-.384
40	337	-.176	.074	.043	-.609
40	338	-.167	.071	.057	-.552
40	339	-.207	.098	.020	-.914
40	340	-.215	.086	-.007	-.814
40	341	-.206	.096	-.046	-.775
40	342	-.206	.099	-.000	-.945
40	343	-.214	.091	-.004	-.781
40	344	-.204	.076	.013	-.576
40	345	-.177	.076	.051	-.568

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
40	346	-.169	.075	.116	-.530	40	416	-.230	.124	.161	-.877	40	466	-.096	.055	.047	-.370
40	347	-.220	.118	.005	-1.047	40	417	-.228	.125	.157	-.929	40	467	-.112	.068	.078	-.470
40	348	-.233	.123	.040	-.943	40	418	-.181	.089	.141	-.585	40	468	-.263	.103	-.036	-.905
40	349	-.220	.128	.025	-.981	40	419	-.170	.073	.052	-.507	40	469	-.194	.077	-.045	-.498
40	350	-.217	.127	.029	-1.215	40	420	-.208	.103	.053	-.912	40	470	-.112	.079	.119	-.529
40	351	-.210	.098	-.004	-.873	40	421	-.214	.108	.049	-.939	40	471	-.075	.061	.115	-.346
40	352	-.238	.103	-.005	-.882	40	422	-.221	.117	.104	-1.105	40	472	-.061	.051	.101	-.352
40	353	-.226	.090	.072	-.640	40	423	-.227	.113	.067	-.948	40	473	-.176	.056	.008	-.438
40	354	-.158	.073	.029	-.569	40	424	-.224	.124	.073	-.977	40	474	-.152	.071	.172	-.455
40	355	-.146	.072	.098	-.555	40	425	-.225	.127	.073	-1.042	40	475	-.138	.089	.141	-.513
40	356	-.130	.054	.089	-.412	40	426	-.174	.069	.008	-.490	40	476	-.069	.053	.153	-.307
40	357	-.134	.086	.085	-.893	40	427	-.180	.083	.016	-.759	40	477	-.065	.037	.053	-.312
40	358	-.154	.108	.086	-.841	40	428	-.223	.134	.037	-1.220	40	801	.082	.045	.250	-.073
40	359	-.194	.132	.119	-.975	40	429	-.229	.141	.035	-1.348	40	802	-.011	.041	.165	-.186
40	360	-.227	.145	.023	-1.529	40	430	-.255	.133	.082	-1.348	40	803	-.021	.038	.100	-.222
40	361	-.239	.137	.010	-1.087	40	431	-.251	.143	.121	-1.077	40	804	-.231	.095	.013	-.853
40	362	-.231	.128	.007	-.997	40	432	-.246	.131	.114	-1.042	40	805	-.163	.077	.075	-.491
40	363	-.104	.060	.115	-.363	40	433	-.247	.132	.078	-.973	40	806	-.070	.062	.120	-.584
40	364	-.109	.060	.064	-.457	40	434	-.183	.072	.028	-.558	40	807	-.083	.062	.091	-.456
40	365	-.082	.060	.160	-.617	40	435	-.190	.085	.053	-.724	40	808	-.081	.065	.086	-.474
40	366	-.071	.057	.126	-.416	40	436	-.235	.133	.092	-1.343	40	809	-.087	.050	.043	-.321
40	367	-.091	.075	.219	-.436	40	437	-.241	.140	.151	-1.461	40	810	-.094	.059	.087	-.383
40	368	-.094	.063	.043	-.483	40	438	-.244	.130	.074	-1.456	40	901	-.384	.127	-.043	-.880
40	369	-.128	.077	.049	-.558	40	439	-.237	.126	.078	-1.258	40	902	-.181	.093	.127	-.593
40	370	-.102	.062	.059	-.423	40	440	-.242	.121	.128	-1.044	40	903	-.157	.071	.137	-.459
40	371	-.105	.071	.117	-.533	40	441	-.246	.123	.132	-1.006	40	904	-.223	.092	.068	-.622
40	372	-.056	.048	.100	-.254	40	442	-.176	.065	.045	-.639	40	905	-.314	.106	-.058	-.750
40	373	-.088	.049	.073	-.312	40	443	-.185	.078	.091	-.812	40	906	-.287	.105	.003	-.739
40	374	-.073	.051	.087	-.325	40	444	-.236	.114	.000	-1.160	40	907	-.158	.083	.153	-.590
40	375	-.068	.051	.095	-.407	40	445	-.242	.119	.005	-1.195	40	908	-.400	.120	-.113	-.987
40	376	-.070	.054	.086	-.405	40	446	-.259	.110	.015	-.938	40	909	-.316	.121	.175	-.749
40	377	-.079	.046	.043	-.363	40	447	-.257	.117	.141	-.977	40	910	-.267	.105	.035	-.736
40	378	-.072	.051	.057	-.370	40	448	-.252	.114	.164	-.895	40	911	-.110	.097	.334	-.487
40	379	-.069	.051	.088	-.439	40	449	-.241	.115	.113	-.813	40	912	-.318	.093	-.069	-.709
40	380	-.063	.050	.079	-.419	40	450	-.169	.070	.077	-.558	40	913	-.169	.115	.329	-.610
40	401	-.236	.117	.049	-.869	40	451	-.174	.077	.086	-.639	40	914	-.184	.099	.215	-.566
40	402	-.259	.112	.129	-.721	40	452	-.266	.133	-.031	-1.475	40	915	-.307	.092	-.079	-.634
40	403	-.246	.105	.086	-.732	40	453	-.273	.142	.023	-1.777	40	916	-.299	.090	-.056	-.719
40	404	-.232	.136	.196	-1.280	40	454	-.264	.100	-.034	-1.083	40	917	-.259	.108	.114	-.782
40	405	-.207	.125	.220	-.784	40	455	-.252	.099	.101	-.849	40	918	-.214	.113	.219	-.884
40	406	-.224	.096	.068	-.794	40	456	-.203	.084	.080	-.582	50	101	-.265	.152	.311	-.750
40	407	-.240	.099	.062	-.688	40	457	-.167	.079	.066	-.526	50	102	-.230	.183	.610	-.795
40	408	-.243	.122	.196	-.824	40	458	-.127	.058	.072	-.431	50	103	-.278	.163	.515	-.915
40	409	-.231	.126	.229	-.931	40	459	-.126	.070	.144	-.553	50	104	.241	.148	.940	-.151
40	410	-.212	.123	.153	-.856	40	460	-.231	.107	.032	-.895	50	105	.209	.148	.937	-.216
40	411	-.162	.077	.121	-.485	40	461	-.245	.115	.005	-1.025	50	106	.153	.154	.682	-.367
40	412	-.210	.089	.011	-.771	40	462	-.234	.080	.067	-.720	50	107	.185	.147	.705	-.187
40	413	-.218	.094	.022	-.801	40	463	-.165	.079	.048	-.637	50	108	.164	.136	.656	-.209
40	414	-.225	.103	.080	-.811	40	464	-.098	.059	.121	-.469	50	109	.353	.156	.945	-.052
40	415	-.244	.118	.177	-.919	40	465	-.110	.057	.068	-.387	50	110	.404	.182	1.043	-.042

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
50	111	.383	.181	1.018	-.099	50	161	-.052	.046	.115	-.211	50	245	-.308	.103	-.104	-.793
50	112	.327	.167	.906	-.073	50	162	-.066	.056	.131	-.405	50	246	-.176	.068	.027	-.495
50	113	.212	.127	.816	-.114	50	163	.069	.080	.375	-.189	50	247	-.159	.062	.073	-.406
50	114	.110	.111	.664	-.197	50	164	.006	.057	.235	-.171	50	248	-.028	.056	.238	-.245
50	115	-.048	.289	.681	-1.108	50	165	-.036	.041	.130	-.193	50	249	-.023	.066	.363	-.278
50	116	-.223	.069	-.027	-.601	50	166	-.131	.060	.181	-.416	50	250	.065	.129	.510	-.761
50	117	.295	.137	.940	-.027	50	201	-.214	.069	-.014	-.558	50	251	.010	.186	.545	-.864
50	118	.349	.157	1.083	-.024	50	202	-.214	.073	.022	-.567	50	252	-.318	.154	.255	-1.851
50	119	.340	.158	1.123	-.040	50	203	-.153	.101	.097	-.666	50	253	-.384	.171	-.089	-1.454
50	120	.302	.139	.848	-.094	50	204	-.222	.144	.250	-.916	50	254	-.180	.073	.035	-.615
50	121	.192	.125	.707	-.162	50	205	-.347	.112	.123	-.808	50	255	-.128	.056	.061	-.391
50	122	.068	.097	.505	-.255	50	206	-.222	.068	.032	-.490	50	256	-.009	.045	.224	-.163
50	123	.294	.128	.816	-.099	50	207	-.077	.059	.189	-.285	50	257	-.017	.072	.321	-.301
50	124	.344	.153	.883	-.022	50	208	-.053	.051	.134	-.374	50	258	.140	.069	.516	-.096
50	125	.328	.153	.987	-.035	50	209	-.044	.076	.219	-.642	50	259	.172	.087	.660	-.190
50	126	.256	.133	.883	-.078	50	210	-.133	.089	.258	-.678	50	260	-.205	.122	.115	-1.000
50	127	.140	.098	.488	-.111	50	211	-.283	.179	.290	-.917	50	261	-.239	.109	-.026	-.830
50	128	.027	.083	.382	-.220	50	212	-.228	.069	-.013	-.580	50	262	-.089	.052	.056	-.323
50	129	.022	.212	.529	-1.103	50	213	-.221	.065	-.026	-.541	50	263	-.054	.042	.081	-.204
50	130	-.240	.090	.104	-.816	50	214	-.120	.045	.036	-.376	50	264	.006	.033	.123	-.106
50	131	.260	.113	.694	-.206	50	215	-.143	.051	.052	-.390	50	265	-.014	.048	.151	-.204
50	132	.284	.136	.873	-.083	50	216	-.054	.071	.255	-.632	50	266	.111	.060	.383	-.104
50	133	.254	.135	.857	-.038	50	217	-.118	.146	.231	-1.072	50	267	.137	.072	.495	-.102
50	134	.180	.113	.699	-.080	50	218	-.229	.230	.391	-.905	50	268	-.020	.041	.127	-.175
50	135	.086	.075	.483	-.139	50	219	-.255	.205	.533	-1.073	50	269	-.021	.040	.114	-.216
50	136	-.014	.064	.364	-.332	50	220	-.239	.066	-.038	-.558	50	270	.026	.038	.183	-.155
50	137	.234	.119	.825	-.338	50	221	-.232	.061	-.062	-.514	50	271	.043	.043	.259	-.131
50	138	.234	.125	.811	-.197	50	222	-.141	.043	.011	-.388	50	272	.092	.054	.317	-.084
50	139	.186	.107	.726	-.052	50	223	-.167	.054	-.001	-.459	50	273	-.051	.046	.088	-.262
50	140	.109	.100	.654	-.108	50	224	-.055	.068	.188	-.504	50	274	-.127	.058	.062	-.330
50	141	.035	.081	.446	-.166	50	225	-.097	.149	.226	-.828	50	275	.004	.038	.142	-.175
50	142	-.074	.068	.226	-.292	50	226	-.201	.267	.472	-1.130	50	276	.048	.036	.197	-.061
50	143	-.146	.099	.531	-.586	50	227	-.219	.240	.562	-1.049	50	277	.140	.077	.535	-.078
50	144	-.243	.081	.000	-.892	50	228	-.258	.075	-.014	-.639	50	301	-.247	.102	.049	-.792
50	145	.153	.115	.634	-.238	50	229	-.255	.068	-.076	-.581	50	302	-.247	.096	-.044	-.914
50	146	.081	.072	.378	-.172	50	230	-.152	.049	.019	-.398	50	303	-.263	.071	-.050	-.507
50	147	.001	.054	.214	-.164	50	231	-.157	.056	.056	-.372	50	304	-.210	.050	-.074	-.390
50	148	-.010	.049	.190	-.143	50	232	-.039	.059	.175	-.320	50	305	-.200	.073	.020	-.651
50	149	-.100	.047	.097	-.318	50	233	-.073	.110	.263	-.933	50	306	-.190	.061	-.016	-.560
50	150	-.155	.057	.047	-.421	50	234	-.177	.249	.470	-1.288	50	307	-.186	.067	.014	-.534
50	151	.105	.094	.649	-.314	50	235	-.204	.227	.515	-1.116	50	308	-.215	.070	-.018	-.589
50	152	.043	.057	.343	-.283	50	236	-.292	.093	-.048	-.863	50	309	-.195	.063	.004	-.618
50	153	-.055	.035	.090	-.203	50	237	-.291	.086	-.064	-.725	50	310	-.196	.053	-.034	-.475
50	154	-.090	.048	.123	-.324	50	238	-.176	.059	.011	-.418	50	311	-.201	.065	-.009	-.570
50	155	-.122	.035	-.003	-.228	50	239	-.165	.058	.038	-.359	50	312	-.195	.064	-.018	-.568
50	156	-.168	.063	.073	-.524	50	240	-.043	.056	.178	-.269	50	313	-.189	.065	-.005	-.519
50	157	.160	.080	.627	-.042	50	241	-.045	.071	.258	-.531	50	314	-.197	.055	-.047	-.503
50	158	-.300	.094	-.057	-.840	50	242	-.080	.197	.480	-.963	50	315	-.215	.063	-.033	-.547
50	159	.090	.071	.505	-.113	50	243	-.124	.195	.552	-.951	50	316	-.211	.063	-.033	-.541
50	160	-.025	.051	.221	-.230	50	244	-.314	.100	-.053	-.767	50	317	-.217	.070	-.003	-.526

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
50	318	-.208	.055	-.049	-.423
50	319	-.212	.056	-.042	-.459
50	320	-.205	.061	-.026	-.505
50	321	-.219	.065	-.050	-.544
50	322	-.213	.054	-.070	-.604
50	323	-.205	.063	-.018	-.694
50	324	-.208	.061	-.038	-.548
50	325	-.224	.062	-.060	-.534
50	326	-.224	.060	-.054	-.439
50	327	-.231	.070	-.033	-.750
50	328	-.218	.061	-.003	-.635
50	329	-.261	.094	-.044	-.871
50	330	-.246	.085	-.028	-.952
50	331	-.232	.078	-.023	-.613
50	332	-.240	.068	-.098	-.774
50	333	-.264	.082	-.091	-.966
50	334	-.259	.081	-.086	-.965
50	335	-.230	.070	-.037	-.667
50	336	-.203	.062	-.026	-.439
50	337	-.262	.086	-.041	-.702
50	338	-.248	.083	-.010	-.649
50	339	-.312	.119	-.025	-.907
50	340	-.303	.099	-.078	-.846
50	341	-.294	.109	-.059	-1.153
50	342	-.291	.112	-.049	-1.124
50	343	-.309	.110	-.037	-.768
50	344	-.301	.096	-.101	-.717
50	345	-.271	.105	.030	-.892
50	346	-.262	.104	.047	-.861
50	347	-.346	.159	-.033	-1.045
50	348	-.341	.128	-.033	-.989
50	349	-.350	.155	-.038	-1.495
50	350	-.342	.156	-.016	-1.672
50	351	-.328	.119	-.010	-1.242
50	352	-.326	.105	-.080	-.813
50	353	-.275	.093	.009	-.702
50	354	-.178	.075	.045	-.526
50	355	-.212	.092	.101	-.788
50	356	-.195	.071	.082	-.550
50	357	-.240	.133	.083	-1.071
50	358	-.264	.158	.068	-1.028
50	359	-.331	.195	.103	-1.694
50	360	-.364	.183	.031	-1.891
50	361	-.360	.159	.001	-1.356
50	362	-.346	.151	.013	-1.283
50	363	-.144	.083	.133	-.596
50	364	-.141	.085	.095	-.511
50	365	-.133	.089	.133	-.618
50	366	-.118	.087	.191	-.586
50	367	-.141	.108	.091	-.707
50	368	-.154	.095	.054	-.671
50	369	-.211	.112	.072	-.792
50	370	-.169	.096	.090	-.697
50	371	-.182	.087	.108	-.545
50	372	-.094	.056	.074	-.340
50	373	-.157	.066	.015	-.435
50	374	-.131	.072	.054	-.427
50	375	-.118	.069	.070	-.399
50	376	-.121	.074	.065	-.430
50	377	-.139	.061	.079	-.438
50	378	-.118	.067	.054	-.650
50	379	-.113	.066	.060	-.684
50	380	-.103	.064	.065	-.571
50	401	-.231	.080	.033	-.745
50	402	-.257	.081	.012	-.764
50	403	-.246	.081	.034	-.905
50	404	-.251	.111	.070	-1.131
50	405	-.241	.107	.048	-.917
50	406	-.221	.068	-.039	-.706
50	407	-.221	.059	-.051	-.558
50	408	-.224	.071	-.004	-.704
50	409	-.233	.083	.018	-.760
50	410	-.231	.093	.014	-.918
50	411	-.204	.070	-.003	-.620
50	412	-.214	.063	-.058	-.467
50	413	-.221	.066	-.053	-.473
50	414	-.235	.070	-.058	-.512
50	415	-.229	.068	-.008	-.880
50	416	-.232	.080	.057	-.896
50	417	-.244	.090	-.006	-.947
50	418	-.205	.067	-.017	-.560
50	419	-.203	.061	-.048	-.560
50	420	-.213	.074	.021	-.758
50	421	-.219	.078	.031	-.898
50	422	-.222	.083	.050	-.992
50	423	-.234	.073	.004	-.785
50	424	-.244	.085	-.011	-.974
50	425	-.251	.095	-.060	-1.035
50	426	-.206	.057	-.043	-.435
50	427	-.212	.066	-.043	-.574
50	428	-.222	.084	-.009	-.905
50	429	-.225	.087	-.017	-.949
50	430	-.230	.083	-.046	-.795
50	431	-.236	.094	.008	-.868
50	432	-.248	.097	-.048	-.964
50	433	-.251	.101	-.041	-1.124
50	434	-.222	.055	-.043	-.525
50	435	-.228	.064	.008	-.561
50	436	-.223	.078	.016	-.667
50	437	-.228	.079	.029	-.774
50	438	-.242	.082	.002	-1.227
50	439	-.255	.095	.123	-1.021
50	440	-.273	.100	.006	-1.123
50	441	-.281	.104	-.019	-.980
50	442	-.244	.068	-.021	-.518
50	443	-.263	.084	.011	-.707
50	444	-.253	.085	-.041	-.765
50	445	-.259	.087	-.036	-.810
50	446	-.258	.080	-.068	-.832
50	447	-.276	.090	.006	-.939
50	448	-.293	.095	-.053	-.792
50	449	-.300	.106	-.058	-.894
50	450	-.259	.083	-.016	-.827
50	451	-.274	.096	.001	-.929
50	452	-.316	.108	-.063	-.846
50	453	-.318	.108	-.070	-.946
50	454	-.331	.116	-.101	-1.040
50	455	-.337	.121	-.083	-1.118
50	456	-.321	.115	-.048	-.986
50	457	-.293	.113	.007	-.898
50	458	-.226	.075	.009	-.683
50	459	-.238	.091	.060	-.878
50	460	-.329	.124	-.075	-1.285
50	461	-.336	.133	-.072	-1.530
50	462	-.302	.091	-.073	-.795
50	463	-.314	.088	-.011	-.788
50	464	-.235	.100	.092	-.959
50	465	-.193	.082	.075	-.667
50	466	-.166	.088	.175	-.610
50	467	-.182	.094	.066	-.683
50	468	-.342	.113	-.113	-.961
50	469	-.312	.088	.157	-.825
50	470	-.261	.101	.132	-.775
50	471	-.197	.090	.161	-.604
50	472	-.139	.076	.112	-.611
50	473	-.298	.071	-.069	-.670
50	474	-.271	.079	-.001	-.637
50	475	-.281	.108	.088	-.790
50	476	-.188	.084	.052	-.522
50	477	-.159	.069	.094	-.477
50	801	.105	.047	.330	-.027
50	802	-.021	.045	.115	-.181
50	803	-.044	.045	.104	-.216
50	804	-.291	.091	-.046	-.749
50	805	-.279	.078	.071	-.713
50	806	-.166	.085	.137	-.558
50	807	-.136	.089	.101	-.629
50	808	-.138	.096	.100	-.677
50	809	-.156	.077	.057	-.763
50	810	-.153	.084	.150	-.525

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
50	901	-.349	.112	-.029	-.821
50	902	-.214	.089	.088	-.585
50	903	-.207	.071	.029	-.480
50	904	-.244	.074	.052	-.612
50	905	-.317	.089	-.067	-.727
50	906	-.269	.085	.024	-.705
50	907	-.211	.077	.131	-.568
50	908	-.386	.104	-.119	-.916
50	909	-.332	.108	.075	-.744
50	910	-.280	.089	-.007	-.722
50	911	-.137	.096	.239	-.439
50	912	-.293	.075	-.026	-.658
50	913	-.117	.130	.464	-.491
50	914	-.228	.085	.105	-.611
50	915	-.283	.073	-.044	-.619
50	916	-.307	.074	-.094	-.625
50	917	-.272	.084	.065	-.997
50	918	-.263	.103	.071	-.768
60	101	-.141	.173	.566	-.658
60	102	-.239	.175	.606	-.765
60	103	-.318	.128	.260	-.782
60	104	.264	.160	.911	-.212
60	105	.198	.151	.771	-.239
60	106	.030	.138	.634	-.411
60	107	.117	.130	.630	-.250
60	108	.100	.117	.572	-.216
60	109	.343	.163	.934	-.104
60	110	.343	.175	.939	-.113
60	111	.287	.163	.856	-.109
60	112	.217	.143	.714	-.131
60	113	.114	.110	.608	-.213
60	114	.021	.092	.505	-.318
60	115	.173	.190	.831	-1.000
60	116	-.244	.055	-.069	-.555
60	117	.360	.144	.939	-.102
60	118	.373	.165	.985	-.007
60	119	.330	.163	.928	-.026
60	120	.241	.126	.687	-.082
60	121	.124	.110	.553	-.189
60	122	.001	.083	.358	-.262
60	123	.308	.137	.786	-.122
60	124	.314	.150	.874	-.186
60	125	.270	.144	.843	-.036
60	126	.187	.123	.655	-.085
60	127	.085	.085	.449	-.161
60	128	-.024	.070	.301	-.270
60	129	.174	.161	.639	-.626
60	130	-.254	.058	-.083	-.551
60	131	.295	.135	.798	-.189
60	132	.297	.145	.874	-.131
60	133	.248	.139	.839	-.041
60	134	.162	.120	.738	-.102
60	135	.030	.073	.477	-.144
60	136	-.057	.062	.316	-.227
60	137	.191	.129	.724	-.352
60	138	.177	.114	.691	-.242
60	139	.162	.115	.632	-.099
60	140	.081	.107	.591	-.156
60	141	-.012	.081	.315	-.234
60	142	-.107	.072	.265	-.306
60	143	.178	.091	.589	-.484
60	144	-.260	.066	-.040	-.690
60	145	.114	.146	.614	-.580
60	146	.057	.084	.367	-.505
60	147	-.030	.054	.244	-.275
60	148	-.048	.049	.181	-.200
60	149	-.136	.053	.088	-.381
60	150	-.186	.063	.056	-.431
60	151	.114	.106	.605	-.318
60	152	.052	.065	.411	-.199
60	153	-.073	.038	.106	-.233
60	154	-.124	.049	.048	-.345
60	155	-.161	.038	-.053	-.330
60	156	-.204	.066	.040	-.520
60	157	.174	.091	.684	-.048
60	158	-.346	.093	-.020	-.797
60	159	.102	.087	.591	-.349
60	160	-.034	.059	.223	-.304
60	161	-.073	.049	.121	-.231
60	162	-.089	.060	.132	-.313
60	163	.087	.101	.491	-.252
60	164	.011	.068	.278	-.242
60	165	-.055	.049	.165	-.226
60	166	-.178	.065	.099	-.439
60	201	-.275	.066	-.058	-.574
60	202	-.276	.083	-.003	-.720
60	203	-.243	.126	.137	-.746
60	204	-.258	.171	.268	-.973
60	205	-.246	.146	.337	-.747
60	206	-.277	.070	-.052	-.589
60	207	-.050	.074	.217	-.280
60	208	-.043	.057	.158	-.248
60	209	-.008	.083	.338	-.364
60	210	-.137	.092	.277	-.489
60	211	-.083	.200	.595	-.821
60	212	-.289	.069	-.085	-.593
60	213	-.280	.065	-.077	-.565
60	214	-.124	.043	.047	-.304
60	215	-.129	.055	.125	-.330
60	216	-.006	.071	.327	-.199
60	217	-.049	.092	.377	-.531
60	218	.049	.218	.693	-.908
60	219	-.002	.226	.834	-.903
60	220	-.302	.070	-.107	-.628
60	221	-.294	.068	-.111	-.669
60	222	-.150	.046	.022	-.314
60	223	-.141	.062	.092	-.366
60	224	.003	.076	.300	-.196
60	225	.005	.094	.372	-.845
60	226	.046	.220	.673	-.885
60	227	.011	.223	.781	-.830
60	228	-.305	.079	-.094	-.688
60	229	-.304	.073	-.113	-.707
60	230	-.158	.051	.020	-.371
60	231	-.134	.059	.078	-.354
60	232	.011	.072	.295	-.198
60	233	.007	.085	.473	-.512
60	234	.056	.218	.639	-.893
60	235	.019	.221	.657	-.749
60	236	-.353	.103	-.118	-.804
60	237	-.347	.098	-.131	-.893
60	238	-.185	.060	-.014	-.471
60	239	-.143	.067	.085	-.386
60	240	.005	.071	.321	-.176
60	241	.021	.084	.405	-.432
60	242	.112	.174	.770	-.803
60	243	.077	.196	.850	-.877
60	244	-.375	.115	.070	-1.009
60	245	-.380	.109	-.134	-1.068
60	246	-.198	.069	.017	-.502
60	247	-.144	.063	.100	-.403
60	248	.005	.063	.343	-.164
60	249	.012	.078	.302	-.326
60	250	.135	.123	.529	-.918
60	251	.125	.161	.633	-.751
60	252	-.391	.159	.046	-1.234
60	253	-.428	.153	-.131	-1.268
60	254	-.200	.071	.002	-.615
60	255	-.129	.059	.075	-.458
60	256	.004	.052	.210	-.183
60	257	.014	.079	.335	-.361
60	258	.164	.073	.452	-.086
60	259	.192	.091	.598	-.174
60	260	-.251	.147	.210	-1.154
60	261	-.287	.119	.007	-1.281
60	262	-.119	.058	.077	-.423
60	263	-.063	.047	.153	-.285
60	264	.009	.040	.234	-.121
60	265	-.003	.057	.235	-.246
60	266	.129	.062	.428	-.029

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
60	267	.152	.075	.536	-.041
60	268	-.029	.048	.184	-.258
60	269	-.014	.038	.155	-.154
60	270	.039	.037	.223	-.093
60	271	.056	.043	.302	-.070
60	272	.117	.057	.379	-.089
60	273	-.083	.056	.080	-.332
60	274	-.145	.062	.109	-.376
60	275	-.006	.040	.236	-.143
60	276	.061	.037	.313	-.057
60	277	.181	.089	.550	-.056
60	301	-.291	.092	-.066	-1.004
60	302	-.273	.069	-.062	-.569
60	303	-.298	.061	-.106	-.520
60	304	-.247	.045	-.121	-.415
60	305	-.248	.067	-.026	-.593
60	306	-.193	.057	.024	-.442
60	307	-.186	.063	.055	-.478
60	308	-.214	.065	-.021	-.558
60	309	-.198	.058	.027	-.420
60	310	-.193	.054	-.039	-.482
60	311	-.194	.064	-.011	-.516
60	312	-.191	.064	-.009	-.492
60	313	-.187	.064	-.007	-.485
60	314	-.195	.055	-.046	-.452
60	315	-.209	.063	-.028	-.501
60	316	-.207	.063	-.021	-.514
60	317	-.215	.067	-.019	-.554
60	318	-.210	.051	-.069	-.407
60	319	-.213	.053	-.061	-.562
60	320	-.206	.057	-.045	-.463
60	321	-.219	.063	-.052	-.604
60	322	-.210	.052	-.073	-.422
60	323	-.205	.057	-.033	-.506
60	324	-.206	.061	-.040	-.533
60	325	-.221	.063	-.036	-.511
60	326	-.220	.059	-.041	-.460
60	327	-.225	.070	.101	-.577
60	328	-.219	.058	-.051	-.530
60	329	-.252	.088	-.054	-.831
60	330	-.242	.079	-.050	-.985
60	331	-.231	.073	-.040	-.745
60	332	-.245	.059	-.083	-.497
60	333	-.262	.070	-.056	-.554
60	334	-.259	.070	-.058	-.543
60	335	-.253	.081	-.028	-.762
60	336	-.206	.057	-.039	-.455
60	337	-.254	.080	-.026	-.779
60	338	-.242	.077	.003	-.677
60	339	-.302	.111	-.059	-1.223
60	340	-.286	.088	-.054	-.707
60	341	-.275	.095	-.044	-.862
60	342	-.275	.098	-.031	-.794
60	343	-.292	.099	-.036	-.707
60	344	-.298	.091	-.091	-.652
60	345	-.255	.094	.017	-.801
60	346	-.251	.094	.040	-.733
60	347	-.336	.150	-.016	-1.423
60	348	-.386	.143	-.113	-1.377
60	349	-.355	.146	-.036	-1.352
60	350	-.347	.144	-.053	-1.329
60	351	-.329	.109	-.064	-.826
60	352	-.325	.101	-.078	-.913
60	353	-.268	.086	.012	-.696
60	354	-.186	.067	.033	-.477
60	355	-.210	.080	.031	-.606
60	356	-.211	.072	.001	-.562
60	357	-.233	.126	.030	-1.122
60	358	-.267	.162	.096	-1.519
60	359	-.340	.199	.151	-1.495
60	360	-.370	.182	-.001	-1.756
60	361	-.363	.152	-.013	-1.077
60	362	-.347	.142	-.014	-1.043
60	363	-.148	.069	.048	-.432
60	364	-.158	.080	.116	-.480
60	365	-.125	.080	.134	-.590
60	366	-.110	.078	.157	-.643
60	367	-.147	.104	.144	-.833
60	368	-.167	.087	.044	-.515
60	369	-.214	.105	.035	-.740
60	370	-.168	.083	.060	-.580
60	371	-.207	.115	.262	-.649
60	372	-.113	.060	.059	-.408
60	373	-.193	.077	.053	-.566
60	374	-.159	.082	.063	-.575
60	375	-.151	.082	.087	-.627
60	376	-.154	.088	.101	-.636
60	377	-.176	.073	.048	-.632
60	378	-.147	.074	.075	-.516
60	379	-.140	.074	.052	-.573
60	380	-.133	.073	.059	-.478
60	401	-.051	.069	-.028	-.627
60	402	-.267	.068	-.022	-.547
60	403	-.265	.071	-.005	-.640
60	404	-.273	.095	-.015	-.872
60	405	-.265	.082	-.038	-.775
60	406	-.243	.059	-.062	-.475
60	407	-.255	.053	-.111	-.500
60	408	-.259	.063	-.071	-.696
60	409	-.269	.078	-.062	-.726
60	410	-.265	.082	-.069	-.792
60	411	-.242	.060	-.069	-.615
60	412	-.245	.054	-.081	-.463
60	413	-.248	.055	-.084	-.463
60	414	-.251	.056	-.086	-.497
60	415	-.247	.051	-.081	-.492
60	416	-.253	.062	-.053	-.734
60	417	-.256	.072	-.057	-.956
60	418	-.232	.057	-.053	-.540
60	419	-.254	.058	-.074	-.586
60	420	-.255	.057	-.051	-.488
60	421	-.257	.058	-.072	-.495
60	422	-.260	.060	-.079	-.514
60	423	-.260	.053	-.108	-.482
60	424	-.266	.062	-.091	-.613
60	425	-.270	.068	-.083	-.866
60	426	-.240	.046	-.103	-.423
60	427	-.245	.053	-.068	-.440
60	428	-.242	.060	-.045	-.519
60	429	-.245	.061	-.055	-.521
60	430	-.256	.059	-.096	-.664
60	431	-.264	.067	-.076	-.742
60	432	-.272	.072	-.062	-.782
60	433	-.277	.074	-.076	-.736
60	434	-.260	.052	-.093	-.554
60	435	-.266	.059	-.010	-.591
60	436	-.251	.062	-.045	-.690
60	437	-.255	.063	-.036	-.707
60	438	-.261	.063	-.108	-.568
60	439	-.276	.071	-.111	-.707
60	440	-.291	.078	.008	-.695
60	441	-.301	.085	-.105	-.714
60	442	-.274	.066	-.059	-.669
60	443	-.291	.080	-.083	-.654
60	444	-.255	.072	-.057	-.610
60	445	-.264	.073	-.062	-.601
60	446	-.299	.081	-.101	-.943
60	447	-.321	.091	-.043	-1.001
60	448	-.347	.099	-.057	-1.004
60	449	-.359	.114	-.091	-1.253
60	450	-.298	.093	-.081	-.849
60	451	-.314	.108	-.061	-.925
60	452	-.308	.096	-.031	-.854
60	453	-.315	.096	-.053	-.908
60	454	-.327	.099	-.076	-.898
60	455	-.349	.108	-.071	-1.023
60	456	-.352	.118	-.026	-.881
60	457	-.342	.135	-.017	-1.180
60	458	-.267	.087	-.029	-.820
60	459	-.282	.104	-.013	-.797

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
60	460	-.327	.109	-.031	-1.243
60	461	-.333	.110	-.046	-1.074
60	462	-.350	.093	-.096	-.788
60	463	-.367	.100	.016	-.880
60	464	-.325	.137	.126	-1.019
60	465	-.274	.122	.112	-.901
60	466	-.210	.121	.162	-1.175
60	467	-.221	.126	.144	-.923
60	468	-.358	.108	-.067	-1.257
60	469	-.381	.090	-.126	-.963
60	470	-.357	.102	.097	-.973
60	471	-.303	.108	.161	-.784
60	472	-.223	.110	.246	-.652
60	473	-.361	.082	-.082	-.770
60	474	-.321	.083	-.080	-.654
60	475	-.336	.107	.056	-.846
60	476	-.270	.095	.185	-.612
60	477	-.246	.098	.082	-.733
60	801	.124	.054	.380	-.035
60	802	-.029	.055	.211	-.237
60	803	-.064	.050	.182	-.263
60	804	-.346	.093	-.059	-.854
60	805	-.331	.096	.014	-.726
60	806	-.210	.115	.209	-.961
60	807	-.177	.093	.125	-.656
60	808	-.178	.103	.119	-.775
60	809	-.196	.095	.009	-.806
60	810	-.191	.105	.092	-.764
60	901	-.351	.110	.124	-.828
60	902	-.279	.099	.111	-.689
60	903	-.271	.073	-.024	-.564
60	904	-.273	.062	-.080	-.559
60	905	-.372	.105	-.099	-.813
60	906	-.296	.080	-.055	-.653
60	907	-.265	.070	-.060	-.584
60	908	-.415	.106	-.131	-.995
60	909	-.341	.104	.057	-.734
60	910	-.317	.090	-.052	-.784
60	911	-.216	.105	.260	-.724
60	912	-.296	.070	-.092	-.576
60	913	-.073	.134	.558	-.502
60	914	-.265	.077	-.013	-.621
60	915	-.303	.078	-.095	-.681
60	916	-.307	.067	-.102	-.598
60	917	-.276	.074	-.050	-.671
60	918	-.278	.086	-.038	-.717
70	101	-.159	.205	.682	-.679
70	102	-.199	.191	.454	-.888
70	103	-.356	.128	.148	-.846
70	104	.183	.182	.853	-.550
70	105	.085	.152	.759	-.329
70	106	-.098	.118	.392	-.502
70	107	.062	.123	.505	-.370
70	108	.045	.109	.423	-.362
70	109	.304	.182	.926	-.403
70	110	.285	.172	.953	-.546
70	111	.211	.151	.821	-.133
70	112	.135	.129	.642	-.167
70	113	.042	.096	.424	-.208
70	114	-.047	.078	.296	-.269
70	115	.304	.153	.909	-.345
70	116	-.288	.053	-.115	-.491
70	117	.327	.198	.979	-.436
70	118	.318	.186	.997	-.344
70	119	.253	.162	.909	-.136
70	120	.145	.112	.584	-.144
70	121	.029	.092	.472	-.235
70	122	-.086	.067	.246	-.288
70	123	.275	.173	.792	-.616
70	124	.272	.158	.878	-.507
70	125	.213	.134	.799	-.161
70	126	.121	.111	.591	-.172
70	127	.016	.086	.406	-.215
70	128	-.088	.067	.252	-.276
70	129	.271	.136	.819	-.171
70	130	-.288	.058	-.108	-.530
70	131	.259	.177	.812	-.367
70	132	.251	.162	.907	-.380
70	133	.192	.140	.836	-.148
70	134	.100	.118	.684	-.235
70	135	-.023	.077	.378	-.261
70	136	-.115	.065	.285	-.331
70	137	.139	.198	.794	-.864
70	138	.141	.151	.718	-.825
70	139	.094	.114	.642	-.159
70	140	.009	.099	.500	-.253
70	141	-.089	.076	.409	-.280
70	142	-.174	.069	.183	-.430
70	143	.218	.101	.699	-.059
70	144	-.293	.061	-.083	-.664
70	145	.066	.187	.648	-.709
70	146	.029	.105	.438	-.814
70	147	-.067	.053	.148	-.374
70	148	-.094	.044	.083	-.246
70	149	-.186	.053	.036	-.410
70	150	-.232	.063	.042	-.543
70	151	.103	.141	.590	-.642
70	152	.044	.082	.338	-.505
70	153	-.087	.042	.064	-.365
70	154	-.154	.052	.058	-.439
70	155	-.195	.039	-.081	-.358
70	156	-.235	.066	-.020	-.657
70	157	.195	.095	.776	-.015
70	158	-.382	.107	-.111	-.944
70	159	.104	.115	.647	-.383
70	160	-.043	.070	.267	-.313
70	161	-.097	.053	.137	-.380
70	162	-.116	.064	.130	-.383
70	163	.090	.138	.552	-.358
70	164	.008	.087	.399	-.303
70	165	-.071	.059	.203	-.251
70	166	-.217	.068	.071	-.530
70	201	-.337	.071	-.088	-.666
70	202	-.336	.093	.054	-.740
70	203	-.330	.145	.213	-.819
70	204	-.418	.158	.290	-.998
70	205	-.124	.182	.598	-.616
70	206	-.349	.076	-.100	-.771
70	207	-.003	.085	.342	-.265
70	208	-.033	.077	.329	-.302
70	209	.015	.101	.393	-.279
70	210	-.110	.131	.372	-.566
70	211	.091	.181	.750	-.597
70	212	-.362	.081	.146	-.676
70	213	-.362	.081	-.127	-.735
70	214	-.125	.054	.040	-.323
70	215	-.089	.071	.215	-.328
70	216	.066	.102	.536	-.203
70	217	.046	.137	.606	-.386
70	218	.250	.178	.858	-.533
70	219	.234	.233	1.012	-.535
70	220	-.375	.087	.045	-.794
70	221	-.373	.091	-.164	-.897
70	222	-.161	.052	.030	-.398
70	223	-.095	.071	.220	-.294
70	224	.080	.095	.494	-.174
70	225	.116	.127	.675	-.268
70	226	.265	.172	.838	-.507
70	227	.251	.207	.959	-.501
70	228	-.384	.090	-.060	-.865
70	229	-.393	.096	-.188	-.849
70	230	-.180	.059	.036	-.425
70	231	-.105	.068	.238	-.317
70	232	.069	.089	.459	-.142
70	233	.100	.108	.555	-.216
70	234	.224	.133	.686	-.461
70	235	.210	.158	.747	-.464
70	236	-.381	.099	.174	-.875
70	237	-.405	.097	-.196	-1.161
70	238	-.194	.060	.013	-.430

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
70	239	-.115	.063	.151	-.331
70	240	.051	.076	.459	-.176
70	241	.098	.108	.555	-.276
70	242	.219	.133	.733	-.615
70	243	.208	.156	.742	-.627
70	244	-.393	.119	.131	-.964
70	245	-.433	.105	-.181	-.944
70	246	-.202	.066	.072	-.469
70	247	-.105	.069	.151	-.309
70	248	.058	.077	.340	-.140
70	249	.065	.093	.495	-.256
70	250	.180	.099	.679	-.453
70	251	.212	.127	.810	-.397
70	252	-.362	.137	.179	-1.287
70	253	-.430	.130	-.143	-1.276
70	254	-.199	.066	.031	-.489
70	255	-.110	.062	.203	-.358
70	256	.033	.061	.360	-.161
70	257	.047	.079	.357	-.278
70	258	.181	.096	.499	-.005
70	259	.205	.097	.651	-.043
70	260	-.280	.133	.249	-1.099
70	261	-.343	.112	.055	-1.006
70	262	-.144	.060	.081	-.481
70	263	-.067	.053	.167	-.256
70	264	.008	.041	.164	-.142
70	265	.011	.061	.250	-.223
70	266	.142	.070	.402	-.033
70	267	.165	.084	.474	-.100
70	268	-.045	.055	.172	-.236
70	269	-.011	.043	.212	-.153
70	270	.045	.044	.272	-.079
70	271	.067	.049	.321	-.112
70	272	.136	.066	.512	-.118
70	273	-.116	.060	.077	-.418
70	274	-.157	.067	.115	-.398
70	275	-.017	.043	.176	-.184
70	276	.069	.043	.332	-.055
70	277	.182	.091	.805	-.176
70	301	-.327	.085	-.111	-.803
70	302	-.310	.064	-.111	-.575
70	303	-.363	.064	-.194	-.618
70	304	-.292	.047	-.171	-.480
70	305	-.300	.067	-.108	-.698
70	306	-.300	.059	-.132	-.654
70	307	-.294	.066	-.099	-.596
70	308	-.349	.073	-.117	-.677
70	309	-.285	.058	-.128	-.618
70	310	-.291	.047	-.134	-.477
70	311	-.306	.063	-.135	-.634
70	312	-.301	.060	-.117	-.539
70	313	-.297	.063	-.104	-.599
70	314	-.295	.055	-.102	-.567
70	315	-.352	.077	-.099	-.726
70	316	-.350	.078	-.095	-.733
70	317	-.284	.053	-.123	-.513
70	318	-.171	.059	.038	-.404
70	319	-.291	.050	-.139	-.482
70	320	-.275	.050	-.132	-.468
70	321	-.304	.069	-.109	-.890
70	322	-.296	.053	-.129	-.609
70	323	-.298	.067	-.087	-.621
70	324	-.295	.065	-.061	-.650
70	325	-.356	.085	-.150	-.923
70	326	-.353	.084	-.152	-.752
70	327	-.291	.055	-.135	-.540
70	328	-.294	.045	-.164	-.479
70	329	-.322	.076	-.137	-.867
70	330	-.313	.068	-.139	-.694
70	331	-.308	.067	-.121	-.661
70	332	-.316	.062	-.094	-.627
70	333	-.381	.093	-.152	-.907
70	334	-.377	.094	-.152	-.895
70	335	-.295	.054	-.143	-.513
70	336	-.170	.058	.068	-.412
70	337	-.316	.066	-.137	-.708
70	338	-.302	.064	-.120	-.630
70	339	-.349	.103	-.104	-1.226
70	340	-.341	.083	-.087	-.895
70	341	-.330	.086	-.063	-.879
70	342	-.330	.089	-.032	-.868
70	343	-.401	.100	-.131	-1.077
70	344	-.389	.080	-.204	-.777
70	345	-.328	.078	-.096	-.910
70	346	-.308	.075	-.098	-.684
70	347	-.363	.116	-.099	-1.365
70	348	-.355	.107	-.116	-1.030
70	349	-.350	.110	-.114	-1.423
70	350	-.348	.110	-.098	-1.368
70	351	-.416	.103	-.157	-1.185
70	352	-.395	.079	-.192	-.827
70	353	-.307	.080	-.073	-.754
70	354	-.159	.068	.098	-.404
70	355	-.325	.090	.002	-.719
70	356	-.309	.086	.003	-.754
70	357	-.355	.122	-.073	-1.065
70	358	-.350	.123	.000	-1.145
70	359	-.355	.150	-.092	-2.158
70	360	-.361	.134	-.099	-1.477
70	361	-.410	.117	-.091	-.971
70	362	-.405	.115	-.090	-.907
70	363	-.307	.123	.131	-1.031
70	364	-.286	.105	.056	-.837
70	365	-.322	.123	.304	-1.037
70	366	-.308	.116	.071	-1.047
70	367	-.300	.116	.057	-1.077
70	368	-.326	.100	-.034	-.867
70	369	-.381	.103	-.058	-.877
70	370	-.355	.102	-.027	-.838
70	371	-.215	.116	.316	-.646
70	372	-.148	.060	.054	-.394
70	373	-.323	.102	-.004	-.716
70	374	-.300	.116	.045	-.766
70	375	-.289	.115	.045	-.764
70	376	-.291	.118	.042	-.749
70	377	-.299	.101	.004	-.829
70	378	-.276	.110	.057	-.742
70	379	-.269	.107	.040	-.728
70	380	-.259	.108	.091	-.638
70	401	-.277	.066	-.066	-.584
70	402	-.290	.066	-.085	-.601
70	403	-.311	.071	-.119	-.765
70	404	-.322	.089	-.100	-1.018
70	405	-.299	.073	-.081	-.826
70	406	-.279	.057	-.111	-.594
70	407	-.284	.052	-.122	-.499
70	408	-.290	.063	-.087	-.562
70	409	-.296	.074	-.052	-.613
70	410	-.284	.072	.069	-.661
70	411	-.278	.055	-.112	-.565
70	412	-.276	.052	-.133	-.498
70	413	-.279	.053	-.129	-.507
70	414	-.281	.053	-.132	-.521
70	415	-.284	.049	-.127	-.496
70	416	-.289	.060	-.105	-.703
70	417	-.287	.066	-.098	-.746
70	418	-.272	.058	-.071	-.523
70	419	-.276	.056	-.085	-.533
70	420	-.273	.054	-.110	-.483
70	421	-.276	.054	-.110	-.490
70	422	-.278	.055	-.111	-.490
70	423	-.281	.046	-.144	-.516
70	424	-.287	.053	-.134	-.545
70	425	-.288	.057	-.120	-.613
70	426	-.276	.047	-.141	-.504
70	427	-.281	.054	-.120	-.582
70	428	-.276	.052	-.132	-.475
70	429	-.278	.052	-.130	-.485
70	430	-.288	.047	-.131	-.449
70	431	-.294	.052	-.133	-.481

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
70	432	-.299	.054	-.129	-.521	70	805	-.328	.110	.023	-.793	80	127	-.063	.069	.302	-.280
70	433	-.301	.057	-.135	-.672	70	806	-.223	.116	.200	-.749	80	128	-.150	.055	.153	-.340
70	434	-.284	.054	-.141	-.518	70	807	-.269	.108	.002	-.735	80	129	.316	.143	.937	-.057
70	435	-.290	.061	-.123	-.551	70	808	-.268	.112	.012	-.805	80	130	-.295	.052	-.108	-.480
70	436	-.283	.063	-.083	-.574	70	809	-.299	.097	-.030	-.706	80	131	.052	.243	.803	-.777
70	437	-.286	.064	-.104	-.592	70	810	-.305	.119	.129	-.949	80	132	.084	.218	.760	-.935
70	438	-.295	.059	-.134	-.669	70	901	-.439	.132	-.053	-.976	80	133	.076	.131	.595	-.636
70	439	-.306	.066	-.113	-.683	70	902	-.364	.109	-.015	-.894	80	134	.000	.097	.417	-.403
70	440	-.317	.069	-.148	-.637	70	903	-.345	.076	-.080	-.627	80	135	-.086	.068	.289	-.302
70	441	-.319	.078	-.123	-.964	70	904	-.334	.059	-.141	-.647	80	136	-.188	.061	.117	-.368
70	442	-.285	.055	-.151	-.694	70	905	-.462	.118	-.166	-.954	80	137	.000	.230	.718	-1.058
70	443	-.297	.064	-.118	-.667	70	906	-.396	.091	-.071	-.857	80	138	.039	.180	.702	-1.033
70	444	-.283	.062	-.066	-.507	70	907	-.336	.075	-.107	-.650	80	139	.015	.093	.526	-.602
70	445	-.288	.062	-.092	-.509	70	908	-.517	.133	-.214	-1.117	80	140	-.063	.077	.329	-.325
70	446	-.321	.063	-.139	-.634	70	909	-.370	.109	.057	-.737	80	141	-.134	.069	.170	-.459
70	447	-.342	.073	-.138	-.746	70	910	-.390	.089	-.076	-.725	80	142	-.224	.061	.112	-.445
70	448	-.359	.085	-.127	-.870	70	911	-.341	.067	.028	-.794	80	143	.244	.108	.767	.007
70	449	-.351	.094	-.078	-.938	70	912	-.357	.065	-.096	-.622	80	144	-.298	.055	-.143	-.582
70	450	-.311	.080	-.109	-.718	70	913	-.161	.112	.385	-.553	80	145	-.057	.225	.620	-.919
70	451	-.321	.093	-.128	-.801	70	914	-.331	.075	-.076	-.744	80	146	-.047	.152	.365	-.916
70	452	-.329	.087	-.098	-.727	70	915	-.379	.084	-.138	-.720	80	147	-.107	.058	.050	-.511
70	453	-.335	.086	-.106	-.722	70	916	-.350	.068	-.124	-.617	80	148	-.137	.047	.098	-.465
70	454	-.358	.081	-.129	-.866	70	917	-.329	.060	-.079	-.771	80	149	-.218	.047	-.048	-.492
70	455	-.390	.100	-.120	-.902	70	918	-.328	.081	-.076	-.707	80	150	-.256	.057	-.059	-.598
70	456	-.385	.126	-.030	-.966	80	101	-.314	.164	.611	-.792	80	151	.046	.171	.583	-.577
70	457	-.356	.139	.008	-1.620	80	102	-.118	.207	.441	-.677	80	152	.018	.104	.345	-.518
70	458	-.275	.086	.014	-.883	80	103	-.350	.119	.144	-.887	80	153	-.098	.049	.090	-.297
70	459	-.280	.101	.006	-1.074	80	104	.009	.221	.785	-1.001	80	154	-.172	.057	.033	-.406
70	460	-.336	.088	-.093	-.848	80	105	-.035	.114	.420	-.693	80	155	-.210	.037	-.096	-.359
70	461	-.343	.089	-.127	-.902	80	106	-.210	.095	.298	-.541	80	156	-.249	.070	.026	-.518
70	462	-.359	.085	-.075	-.844	80	107	.010	.106	.485	-.317	80	157	.185	.084	.753	-.025
70	463	-.405	.110	.017	-1.017	80	108	-.002	.093	.467	-.329	80	158	-.349	.088	-.062	-.858
70	464	-.319	.153	.234	-1.078	80	109	.106	.224	.778	-.609	80	159	.082	.132	.554	-.533
70	465	-.290	.137	.121	-1.373	80	110	.134	.197	.719	-.774	80	160	-.053	.071	.256	-.398
70	466	-.237	.115	.337	-.888	80	111	.097	.129	.576	-.420	80	161	-.110	.057	.110	-.317
70	467	-.265	.122	.164	-.936	80	112	.036	.103	.462	-.237	80	162	-.130	.066	.140	-.391
70	468	-.392	.106	-.119	-.905	80	113	-.038	.072	.254	-.242	80	163	.080	.169	.598	-.357
70	469	-.417	.104	-.013	-.941	80	114	-.112	.060	.155	-.299	80	164	.009	.106	.398	-.317
70	470	-.387	.131	.090	-1.142	80	115	.335	.174	1.000	-.121	80	165	-.080	.064	.209	-.262
70	471	-.327	.149	.159	-.997	80	116	-.297	.053	-.125	-.506	80	166	-.236	.062	.018	-.498
70	472	-.242	.135	.182	-.869	80	117	.159	.242	.808	-.687	80	201	-.399	.090	-.074	-.873
70	473	-.418	.109	-.141	-.883	80	118	.177	.216	.768	-.776	80	202	-.407	.114	-.006	-.834
70	474	-.376	.103	-.051	-.855	80	119	.146	.143	.669	-.653	80	203	-.427	.148	.205	-.957
70	475	-.396	.126	.096	-1.012	80	120	.054	.097	.429	-.287	80	204	-.518	.155	.482	-1.118
70	476	-.318	.142	.191	-1.018	80	121	-.049	.076	.278	-.289	80	205	-.106	.229	.625	-.717
70	477	-.240	.125	.239	-.888	80	122	-.143	.055	.068	-.339	80	206	-.421	.104	.201	-.949
70	801	.131	.059	.364	-.040	80	123	.142	.214	.796	-.704	80	207	.024	.099	.367	-.344
70	802	-.019	.062	.338	-.286	80	124	.158	.190	.671	-.817	80	208	-.038	.084	.281	-.301
70	803	-.089	.053	.134	-.267	80	125	.125	.124	.544	-.543	80	209	.037	.118	.519	-.329
70	804	-.334	.105	.003	-.851	80	126	.044	.095	.410	-.247	80	210	.024	.143	.595	-.615

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
80	211	.206	.166	.773	-.408
80	212	-.421	.115	.343	-.877
80	213	-.464	.103	-.194	-.897
80	214	-.141	.057	.084	-.342
80	215	-.033	.089	.308	-.267
80	216	.132	.127	.647	-.196
80	217	.176	.163	.806	-.307
80	218	.323	.171	.842	-.342
80	219	.340	.195	1.026	-.421
80	220	-.433	.123	.291	-.990
80	221	-.481	.120	-.214	-1.302
80	222	-.188	.063	.028	-.398
80	223	-.042	.088	.316	-.309
80	224	.168	.128	.680	-.164
80	225	.240	.159	.850	-.212
80	226	.362	.172	1.060	-.123
80	227	.362	.189	1.044	-.217
80	228	-.430	.136	.202	-.936
80	229	-.494	.119	-.222	-1.011
80	230	-.193	.068	.031	-.594
80	231	-.051	.083	.291	-.370
80	232	.153	.112	.595	-.137
80	233	.246	.142	.794	-.309
80	234	.353	.163	.948	-.487
80	235	.350	.178	.953	-.372
80	236	-.428	.138	.379	-1.010
80	237	-.487	.118	-.140	-1.126
80	238	-.202	.065	.031	-.487
80	239	-.060	.076	.230	-.357
80	240	.119	.096	.519	-.133
80	241	.189	.134	.763	-.197
80	242	.292	.145	.906	-.194
80	243	.286	.157	.948	-.340
80	244	-.399	.145	.231	-1.307
80	245	-.479	.109	-.230	-1.026
80	246	-.202	.063	.049	-.489
80	247	-.071	.070	.198	-.327
80	248	.100	.084	.423	-.167
80	249	.144	.105	.580	-.235
80	250	.242	.114	.715	-.136
80	251	.235	.118	.783	-.161
80	252	-.362	.143	.194	-1.096
80	253	-.446	.117	-.010	-1.113
80	254	-.197	.064	.127	-.468
80	255	-.093	.071	.358	-.382
80	256	.055	.073	.420	-.167
80	257	.116	.097	.694	-.225
80	258	.214	.102	.697	-.014
80	259	.220	.122	.733	-.091
80	260	-.303	.140	.344	-1.002
80	261	-.403	.125	-.054	-1.202
80	262	-.157	.055	.078	-.346
80	263	-.058	.058	.271	-.249
80	264	.022	.047	.349	-.174
80	265	.037	.078	.401	-.301
80	266	.148	.075	.488	-.071
80	267	.164	.093	.587	-.146
80	268	-.061	.058	.339	-.278
80	269	-.003	.054	.342	-.132
80	270	.055	.057	.397	-.087
80	271	.081	.062	.481	-.066
80	272	.140	.075	.524	-.137
80	273	-.150	.066	.070	-.418
80	274	-.138	.089	.315	-.397
80	275	-.004	.058	.314	-.185
80	276	.084	.045	.432	-.045
80	277	.207	.099	.690	-.064
80	301	-.347	.084	-.120	-.774
80	302	-.345	.074	-.128	-.869
80	303	-.440	.076	-.230	-.748
80	304	-.319	.047	-.182	-.474
80	305	-.332	.075	-.115	-.678
80	306	-.328	.064	-.153	-.723
80	307	-.323	.071	-.079	-.655
80	308	-.425	.092	-.195	-.820
80	309	-.304	.058	-.117	-.626
80	310	-.310	.051	-.143	-.535
80	311	-.340	.080	-.129	-.938
80	312	-.333	.072	-.128	-.733
80	313	-.326	.076	-.102	-.690
80	314	-.335	.066	-.135	-.708
80	315	-.443	.091	-.214	-1.000
80	316	-.445	.093	-.212	-.974
80	317	-.304	.058	-.136	-.621
80	318	-.137	.075	.143	-.356
80	319	-.324	.049	-.178	-.560
80	320	-.313	.056	-.135	-.534
80	321	-.352	.088	-.112	-.977
80	322	-.340	.067	-.130	-.731
80	323	-.335	.078	-.095	-.790
80	324	-.337	.082	-.068	-.832
80	325	-.466	.116	-.165	-.936
80	326	-.463	.106	-.214	-.891
80	327	-.322	.061	-.149	-.629
80	328	-.307	.050	-.168	-.494
80	329	-.342	.094	-.139	-1.906
80	330	-.333	.081	-.118	-1.423
80	331	-.324	.079	-.075	-1.038
80	332	-.343	.073	-.132	-.782
80	333	-.480	.119	-.147	-1.021
80	334	-.479	.120	-.188	-1.044
80	335	-.310	.055	-.153	-.565
80	336	-.126	.067	.260	-.311
80	337	-.331	.065	-.160	-.741
80	338	-.320	.062	-.150	-.626
80	339	-.358	.106	-.090	-1.375
80	340	-.348	.077	-.148	-.866
80	341	-.339	.085	-.079	-.907
80	342	-.344	.089	-.078	-.977
80	343	-.473	.118	-.141	-1.065
80	344	-.461	.095	-.214	-.929
80	345	-.342	.077	-.118	-.733
80	346	-.324	.073	-.103	-.698
80	347	-.367	.114	-.112	-1.704
80	348	-.353	.083	-.170	-1.033
80	349	-.347	.090	-.072	-1.167
80	350	-.348	.091	-.041	-1.231
80	351	-.469	.102	-.124	-1.075
80	352	-.473	.097	-.132	-.934
80	353	-.322	.070	-.095	-.655
80	354	-.135	.080	.323	-.454
80	355	-.369	.097	-.095	-.814
80	356	-.372	.088	-.120	-.830
80	357	-.391	.116	-.123	-1.263
80	358	-.377	.109	-.143	-1.203
80	359	-.370	.106	-.129	-1.109
80	360	-.382	.097	-.148	-.960
80	361	-.471	.115	-.095	-1.068
80	362	-.469	.114	-.120	-1.059
80	363	-.396	.121	.000	-1.087
80	364	-.375	.101	.030	-.764
80	365	-.391	.113	-.074	-1.530
80	366	-.379	.108	.007	-1.674
80	367	-.373	.105	-.017	-.931
80	368	-.386	.092	-.112	-1.090
80	369	-.446	.104	-.027	-.987
80	370	-.423	.101	-.140	-.872
80	371	-.275	.102	.251	-.709
80	372	-.158	.072	.144	-.403
80	373	-.362	.079	-.073	-.791
80	374	-.348	.088	-.048	-.879
80	375	-.341	.085	-.051	-.881
80	376	-.341	.085	-.017	-.769
80	377	-.357	.087	-.031	-.757
80	378	-.343	.099	-.011	-.797
80	379	-.328	.098	-.015	-.740
80	380	-.331	.099	.016	-.723
80	401	-.295	.068	-.106	-.617
80	402	-.306	.068	-.079	-.634
80	403	-.328	.073	-.128	-.702

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
80	404	-.329	.081	-.109	-.801	80	454	-.347	.071	-.152	-.693	80	917	-.348	.079	-.115	-.683
80	405	-.321	.072	-.106	-.760	80	455	-.374	.091	-.059	-.893	80	918	-.348	.079	-.090	-.701
80	406	-.288	.060	-.089	-.598	80	456	-.345	.107	-.027	-.971	90	101	-.457	.127	.234	-1.029
80	407	-.295	.050	-.113	-.495	80	457	-.309	.097	-.023	-.942	90	102	-.105	.206	.430	-.784
80	408	-.302	.061	-.087	-.637	80	458	-.293	.073	-.001	-.724	90	103	-.327	.123	.041	-.931
80	409	-.302	.066	-.098	-.641	80	459	-.286	.079	-.007	-.853	90	104	-.240	.233	.635	-1.070
80	410	-.300	.065	-.026	-.793	80	460	-.319	.091	.012	-.746	90	105	-.116	.128	.248	-1.000
80	411	-.300	.053	-.101	-.722	80	461	-.339	.088	-.044	-.753	90	106	-.278	.088	.120	-.919
80	412	-.293	.051	-.129	-.510	80	462	-.357	.084	-.118	-.829	90	107	-.028	.106	.381	-.619
80	413	-.287	.052	-.122	-.517	80	463	-.391	.107	-.009	-.968	90	108	-.039	.089	.353	-.420
80	414	-.288	.051	-.121	-.514	80	464	-.306	.141	.286	-1.155	90	109	-.154	.249	.585	-1.011
80	415	-.306	.049	-.167	-.495	80	465	-.290	.106	.119	-.927	90	110	-.085	.279	.592	-.995
80	416	-.310	.056	-.129	-.545	80	466	-.269	.114	.157	-.956	90	111	-.001	.148	.430	-.991
80	417	-.311	.059	-.103	-.555	80	467	-.294	.097	.181	-.769	90	112	-.035	.091	.302	-.878
80	418	-.307	.059	-.131	-.549	80	468	-.378	.105	-.070	-.908	90	113	-.113	.061	.148	-.455
80	419	-.306	.055	-.157	-.539	80	469	-.403	.093	-.073	-.883	90	114	-.167	.053	.055	-.479
80	420	-.287	.052	-.149	-.500	80	470	-.368	.114	.071	-.950	90	115	.367	.185	1.035	-.123
80	421	-.290	.053	-.151	-.495	80	471	-.308	.127	.173	-.828	90	116	-.308	.056	-.163	-.531
80	422	-.293	.053	-.147	-.507	80	472	-.243	.113	.323	-.705	90	117	-.114	.264	.676	-1.251
80	423	-.296	.045	-.147	-.459	80	473	-.383	.096	-.101	-.743	90	118	-.063	.290	.628	-1.128
80	424	-.301	.052	-.132	-.488	80	474	-.359	.095	-.041	-.767	90	119	.008	.182	.532	-1.137
80	425	-.300	.055	-.093	-.519	80	475	-.392	.128	.032	-.972	90	120	-.029	.089	.340	-.938
80	426	-.300	.052	-.154	-.542	80	476	-.279	.130	.164	-.824	90	121	-.116	.067	.202	-.667
80	427	-.305	.059	-.129	-.555	80	477	-.237	.110	.091	-.878	90	122	-.195	.052	.016	-.534
80	428	-.294	.054	-.118	-.512	80	801	.151	.059	.400	.000	90	123	-.096	.256	.860	-.945
80	429	-.296	.054	-.131	-.524	80	802	-.021	.075	.289	-.473	90	124	-.048	.273	.845	-1.121
80	430	-.299	.047	-.184	-.464	80	803	-.113	.060	.130	-.343	90	125	.003	.175	.646	-1.043
80	431	-.301	.051	-.169	-.510	80	804	-.323	.113	.039	-.820	90	126	-.040	.101	.402	-.740
80	432	-.308	.052	-.170	-.576	80	805	-.307	.104	.059	-.662	90	127	-.125	.057	.130	-.400
80	433	-.309	.055	-.047	-.648	80	806	-.256	.104	.167	-.956	90	128	-.192	.049	.027	-.438
80	434	-.297	.052	-.133	-.539	80	807	-.371	.096	-.046	-.921	90	129	.309	.139	.792	-.053
80	435	-.301	.060	-.082	-.644	80	808	-.365	.101	-.045	-1.077	90	130	-.300	.045	-.182	-.466
80	436	-.299	.059	-.149	-.541	80	809	-.275	.087	-.080	-.823	90	131	-.115	.238	.524	-.877
80	437	-.301	.059	-.138	-.552	80	810	-.379	.102	.031	-.864	90	132	-.056	.253	.530	-.935
80	438	-.309	.054	-.147	-.522	80	901	-.517	.133	-.064	-1.166	90	133	-.015	.161	.495	-.886
80	439	-.315	.060	-.139	-.570	80	902	-.439	.123	.064	-.947	90	134	-.064	.096	.387	-.735
80	440	-.325	.064	-.146	-.605	80	903	-.422	.086	-.134	-.872	90	135	-.135	.064	.135	-.493
80	441	-.324	.067	-.133	-.652	80	904	-.379	.063	-.183	-.708	90	136	-.202	.054	.004	-.515
80	442	-.315	.054	-.125	-.620	80	905	-.498	.111	-.155	-1.036	90	137	-.127	.272	.606	-1.020
80	443	-.323	.065	-.146	-.659	80	906	-.457	.099	-.185	-.891	90	138	-.076	.251	.511	-1.072
80	444	-.318	.066	-.089	-.596	80	907	-.374	.077	-.096	-.850	90	139	-.066	.125	.408	-.769
80	445	-.323	.066	-.100	-.652	80	908	-.593	.152	-.236	-1.405	90	140	-.117	.078	.300	-.592
80	446	-.332	.059	-.167	-.693	80	909	-.347	.118	.007	-.843	90	141	-.188	.063	.061	-.495
80	447	-.348	.070	-.174	-.682	80	910	-.444	.098	-.168	-.903	90	142	-.252	.061	-.018	-.502
80	448	-.356	.081	-.153	-.868	80	911	-.401	.092	-.118	-.898	90	143	.246	.116	.848	-.030
80	449	-.341	.081	-.114	-.713	80	912	-.392	.068	-.166	-.740	90	144	-.307	.056	-.160	-.622
80	450	-.303	.059	-.111	-.668	80	913	-.277	.101	.221	-.665	90	145	-.165	.236	.669	-1.080
80	451	-.304	.064	-.134	-.724	80	914	-.353	.077	-.089	-.755	90	146	-.116	.180	.356	-1.023
80	452	-.318	.080	-.079	-.746	80	915	-.411	.089	-.109	-.740	90	147	-.140	.067	.057	-.733
80	453	-.326	.079	-.084	-.746	80	916	-.348	.071	-.136	-.620	90	148	-.173	.054	.023	-.631

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
90	149	-.240	.048	-.072	-.408
90	150	-.274	.058	-.056	-.512
90	151	.002	.218	.755	-.936
90	152	-.007	.137	.436	-.861
90	153	-.109	.053	.105	-.400
90	154	-.188	.060	.009	-.461
90	155	-.225	.038	-.098	-.341
90	156	-.253	.066	-.003	-.519
90	157	.193	.097	.729	-.021
90	158	-.374	.089	-.066	-.783
90	159	.065	.166	.678	-.747
90	160	-.055	.091	.336	-.599
90	161	-.122	.062	.120	-.392
90	162	-.134	.069	.182	-.396
90	163	.059	.199	.587	-.631
90	164	-.001	.126	.382	-.614
90	165	-.079	.072	.201	-.324
90	166	-.246	.067	-.012	-.512
90	201	-.446	.101	.011	-.844
90	202	-.443	.134	.087	-.929
90	203	-.489	.146	.183	-1.014
90	204	-.479	.246	.836	-1.215
90	205	-.316	.201	.559	-.868
90	206	-.367	.162	.292	-.902
90	207	.026	.100	.475	-.337
90	208	-.008	.090	.320	-.269
90	209	.031	.118	.523	-.314
90	210	.094	.136	.581	-.318
90	211	.194	.160	.738	-.266
90	212	-.352	.215	.573	-.977
90	213	-.508	.135	.306	-1.086
90	214	-.120	.070	.194	-.388
90	215	.042	.112	.485	-.271
90	216	.215	.147	.733	-.190
90	217	.294	.179	.859	-.381
90	218	.300	.161	.824	-.155
90	219	.291	.173	1.002	-.233
90	220	-.368	.183	.356	-.931
90	221	-.512	.133	.108	-1.010
90	222	-.172	.065	.128	-.385
90	223	.031	.099	.503	-.233
90	224	.228	.131	.736	-.102
90	225	.297	.148	.863	-.076
90	226	.345	.162	.888	-.030
90	227	.311	.170	.906	-.076
90	228	-.349	.191	.349	-.879
90	229	-.510	.128	.130	-1.039
90	230	-.173	.078	.213	-.418
90	231	.005	.094	.502	-.239
90	232	.182	.109	.716	-.075
90	233	.288	.143	.851	-.145
90	234	.324	.145	.868	-.098
90	235	.281	.150	.865	-.268
90	236	-.320	.190	.383	-1.177
90	237	-.527	.133	-.006	-1.240
90	238	-.184	.074	.117	-.486
90	239	-.002	.088	.309	-.256
90	240	.178	.106	.640	-.078
90	241	.265	.128	.891	-.041
90	242	.293	.136	.868	-.058
90	243	.247	.140	.789	-.105
90	244	-.304	.190	.495	-1.082
90	245	-.473	.130	.016	-1.138
90	246	-.178	.074	.203	-.517
90	247	-.030	.075	.378	-.285
90	248	.124	.085	.588	-.102
90	249	.196	.106	.710	-.160
90	250	.238	.112	.718	-.035
90	251	.236	.136	.886	-.184
90	252	-.302	.159	.356	-.850
90	253	-.417	.116	.028	-1.094
90	254	-.164	.068	.165	-.436
90	255	-.037	.077	.365	-.349
90	256	.092	.078	.585	-.142
90	257	.144	.098	.598	-.269
90	258	.210	.095	.718	-.017
90	259	.195	.114	.846	-.102
90	260	-.289	.132	.268	-.826
90	261	-.391	.099	-.046	-.896
90	262	-.164	.061	.256	-.366
90	263	-.049	.066	.395	-.234
90	264	.031	.049	.259	-.130
90	265	.056	.067	.323	-.306
90	266	.142	.067	.472	-.073
90	267	.148	.087	.512	-.117
90	268	-.067	.051	.180	-.228
90	269	.005	.050	.207	-.145
90	270	.061	.059	.287	-.088
90	271	.086	.053	.322	-.078
90	272	.134	.070	.509	-.121
90	273	-.148	.069	.118	-.375
90	274	-.112	.109	.426	-.386
90	275	.012	.075	.508	-.227
90	276	.096	.056	.404	-.049
90	277	.195	.103	.689	-.096
90	301	-.362	.085	-.081	-.856
90	302	-.363	.073	-.132	-.746
90	303	-.475	.086	-.249	-.897
90	304	-.333	.044	-.212	-.517
90	305	-.343	.072	-.083	-.793
90	306	-.343	.070	-.159	-.871
90	307	-.338	.075	-.111	-.823
90	308	-.468	.113	-.186	-1.184
90	309	-.321	.060	-.148	-.593
90	310	-.312	.050	-.164	-.540
90	311	-.340	.082	-.133	-1.058
90	312	-.332	.071	-.128	-.766
90	313	-.329	.074	-.106	-.703
90	314	-.330	.060	-.123	-.606
90	315	-.458	.116	-.016	-.870
90	316	-.466	.114	-.078	-.894
90	317	-.298	.049	-.115	-.518
90	318	-.049	.092	.353	-.299
90	319	-.315	.048	-.179	-.576
90	320	-.301	.048	-.171	-.503
90	321	-.341	.081	-.125	-.995
90	322	-.334	.065	-.135	-.699
90	323	-.325	.075	-.064	-.758
90	324	-.331	.078	-.097	-.704
90	325	-.489	.126	-.075	-1.059
90	326	-.492	.123	-.135	-.998
90	327	-.309	.058	-.150	-.695
90	328	-.308	.047	-.150	-.692
90	329	-.342	.091	-.118	-1.140
90	330	-.331	.078	-.109	-.954
90	331	-.325	.077	-.097	-.847
90	332	-.328	.062	-.110	-.638
90	333	-.486	.138	.027	-1.165
90	334	-.486	.135	-.039	-1.167
90	335	-.299	.059	-.165	-.529
90	336	-.057	.087	.503	-.309
90	337	-.317	.058	-.126	-.623
90	338	-.308	.058	-.131	-.618
90	339	-.339	.089	-.115	-1.190
90	340	-.329	.066	-.157	-.819
90	341	-.323	.073	-.108	-.855
90	342	-.327	.077	-.083	-.829
90	343	-.476	.137	.153	-1.042
90	344	-.480	.108	-.123	-.942
90	345	-.340	.070	-.163	-.733
90	346	-.326	.067	-.155	-.702
90	347	-.354	.098	-.064	-1.419
90	348	-.357	.077	-.156	-.894
90	349	-.337	.079	-.093	-.843
90	350	-.342	.081	-.083	-.958
90	351	-.468	.138	.002	-1.082
90	352	-.493	.112	-.096	-.993
90	353	-.327	.074	-.066	-.730
90	354	-.102	.080	.277	-.397
90	355	-.377	.093	-.153	-.934

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
90	356	-.358	.082	-.154	-.809
90	357	-.363	.099	-.096	-.943
90	358	-.352	.092	-.131	-.817
90	359	-.349	.092	-.111	-1.068
90	360	-.361	.081	-.172	-.851
90	361	-.451	.123	.044	-.985
90	362	-.451	.120	-.035	-.980
90	363	-.376	.101	-.080	-1.235
90	364	-.372	.085	-.047	-1.006
90	365	-.372	.098	-.086	-1.038
90	366	-.364	.092	-.068	-.927
90	367	-.366	.092	-.097	-1.035
90	368	-.372	.085	-.157	-.957
90	369	-.418	.106	-.126	-.930
90	370	-.399	.100	-.150	-.906
90	371	-.316	.091	.032	-.730
90	372	-.151	.075	.223	-.428
90	373	-.382	.081	-.193	-.937
90	374	-.369	.086	-.171	-.817
90	375	-.362	.084	-.153	-.796
90	376	-.364	.085	-.140	-.854
90	377	-.376	.078	-.178	-.760
90	378	-.368	.086	-.133	-.857
90	379	-.361	.083	-.146	-.846
90	380	-.358	.083	-.135	-.842
90	401	-.320	.076	-.102	-.709
90	402	-.319	.065	-.120	-.633
90	403	-.340	.070	-.167	-.868
90	404	-.340	.077	-.106	-.735
90	405	-.340	.074	-.075	-.652
90	406	-.301	.058	-.139	-.534
90	407	-.313	.049	-.160	-.507
90	408	-.318	.057	-.136	-.566
90	409	-.319	.057	-.123	-.591
90	410	-.323	.058	-.149	-.586
90	411	-.326	.059	-.098	-.701
90	412	-.302	.055	-.126	-.549
90	413	-.302	.055	-.119	-.565
90	414	-.304	.055	-.125	-.555
90	415	-.318	.050	-.167	-.526
90	416	-.325	.058	-.126	-.559
90	417	-.326	.061	-.087	-.664
90	418	-.327	.064	-.090	-.574
90	419	-.333	.054	-.189	-.679
90	420	-.307	.049	-.169	-.591
90	421	-.307	.049	-.167	-.545
90	422	-.311	.050	-.170	-.548
90	423	-.311	.044	-.197	-.472
90	424	-.311	.050	-.162	-.492
90	425	-.313	.054	-.149	-.512
90	426	-.312	.051	-.157	-.548
90	427	-.317	.059	-.144	-.589
90	428	-.298	.052	-.114	-.507
90	429	-.301	.052	-.125	-.522
90	430	-.312	.050	-.177	-.484
90	431	-.316	.054	-.159	-.511
90	432	-.317	.056	-.162	-.572
90	433	-.318	.059	-.149	-.545
90	434	-.316	.052	-.169	-.519
90	435	-.321	.059	-.161	-.554
90	436	-.314	.058	-.155	-.556
90	437	-.315	.059	-.153	-.659
90	438	-.312	.043	-.179	-.509
90	439	-.317	.047	-.169	-.574
90	440	-.319	.050	-.179	-.577
90	441	-.319	.054	-.146	-.583
90	442	-.322	.056	-.162	-.620
90	443	-.330	.067	-.149	-.745
90	444	-.331	.063	-.148	-.582
90	445	-.335	.064	-.153	-.590
90	446	-.342	.068	-.201	-.748
90	447	-.355	.078	-.197	-.825
90	448	-.354	.094	-.152	-.953
90	449	-.342	.082	-.123	-.812
90	450	-.334	.069	-.140	-.841
90	451	-.337	.075	-.124	-.810
90	452	-.352	.084	-.092	-.743
90	453	-.359	.083	-.109	-.812
90	454	-.358	.071	-.182	-.721
90	455	-.375	.091	-.078	-.815
90	456	-.346	.103	.004	-.934
90	457	-.320	.086	-.009	-.869
90	458	-.308	.068	-.049	-.711
90	459	-.301	.072	-.023	-.765
90	460	-.339	.085	-.039	-.668
90	461	-.348	.082	-.035	-.694
90	462	-.364	.080	-.113	-.777
90	463	-.394	.092	-.081	-.893
90	464	-.320	.125	.147	-.999
90	465	-.309	.099	.055	-.883
90	466	-.295	.101	.137	-.836
90	467	-.312	.094	.034	-.865
90	468	-.383	.095	-.089	-.849
90	469	-.405	.094	-.108	-.871
90	470	-.374	.112	.012	-.952
90	471	-.322	.116	.327	-.839
90	472	-.277	.103	.212	-.937
90	473	-.397	.096	-.136	-.789
90	474	-.360	.096	-.034	-.784
90	475	-.381	.121	-.000	-.958
90	476	-.296	.122	.185	-.946
90	477	-.267	.082	.049	-.736
90	801	.155	.058	.393	-.006
90	802	-.003	.095	.563	-.416
90	803	-.101	.077	.430	-.343
90	804	-.346	.105	-.002	-.914
90	805	-.341	.095	.021	-.755
90	806	-.300	.086	.164	-.641
90	807	-.374	.086	-.182	-.810
90	808	-.369	.088	-.144	-.788
90	809	-.359	.075	-.159	-.750
90	810	-.366	.089	-.116	-.815
90	901	-.559	.126	-.128	-1.117
90	902	-.495	.114	-.002	-1.009
90	903	-.443	.099	-.141	-.807
90	904	-.422	.068	-.203	-.731
90	905	-.501	.101	-.209	-.924
90	906	-.516	.110	-.180	-1.092
90	907	-.411	.086	-.139	-.732
90	908	-.557	.122	-.245	-1.055
90	909	-.346	.108	-.011	-.791
90	910	-.467	.099	-.134	-.856
90	911	-.414	.090	-.079	-.775
90	912	-.443	.078	-.201	-.761
90	913	-.367	.096	.012	-.756
90	914	-.374	.079	-.053	-.739
90	915	-.446	.097	-.171	-.826
90	916	-.342	.073	-.116	-.649
90	917	-.354	.071	-.136	-.705
90	918	-.362	.073	-.119	-.800
100	101	-.527	.123	-.192	-1.109
100	102	-.302	.203	.335	-1.021
100	103	-.264	.117	.060	-.824
100	104	-.465	.197	.337	-1.292
100	105	-.259	.214	.210	-1.308
100	106	-.285	.111	.122	-1.057
100	107	-.094	.116	.243	-1.191
100	108	-.088	.089	.190	-.820
100	109	-.394	.191	.272	-1.290
100	110	-.357	.256	.330	-1.325
100	111	-.172	.236	.287	-1.475
100	112	-.120	.123	.166	-1.277
100	113	-.158	.062	.068	-.604
100	114	-.194	.054	-.023	-.551
100	115	.342	.171	1.181	-.101
100	116	-.290	.046	-.140	-.481
100	117	-.363	.208	.377	-1.148
100	118	-.334	.267	.446	-1.346
100	119	-.194	.252	.284	-1.232
100	120	-.169	.161	.164	-1.170

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
100	121	-.186	.106	.067	-1.012
100	122	-.227	.080	-.017	-.940
100	123	-.378	.221	.416	-1.258
100	124	-.348	.279	.488	-1.343
100	125	-.224	.275	.325	-1.492
100	126	-.164	.171	.183	-1.322
100	127	-.178	.081	.026	-.842
100	128	-.221	.066	-.008	-.950
100	129	.340	.160	1.260	-.000
100	130	-.295	.055	-.142	-.611
100	131	-.349	.224	.407	-1.553
100	132	-.303	.280	.481	-1.844
100	133	-.172	.229	.453	-1.492
100	134	-.145	.130	.173	-.969
100	135	-.178	.064	.044	-.758
100	136	-.220	.055	-.028	-.677
100	137	-.325	.237	.682	-1.263
100	138	-.266	.264	.519	-1.402
100	139	-.200	.191	.181	-1.180
100	140	-.181	.111	.080	-1.072
100	141	-.222	.076	.074	-.720
100	142	-.261	.061	-.089	-.752
100	143	.247	.122	.854	-.090
100	144	-.292	.052	-.145	-.525
100	145	-.305	.255	.613	-1.533
100	146	-.236	.236	.342	-1.169
100	147	-.191	.120	.034	-1.206
100	148	-.219	.069	-.050	-.730
100	149	-.252	.047	-.094	-.555
100	150	-.278	.053	-.096	-.511
100	151	-.183	.233	.487	-1.118
100	152	-.120	.171	.291	-1.202
100	153	-.131	.071	.107	-.574
100	154	-.186	.061	.035	-.521
100	155	-.221	.039	-.087	-.412
100	156	-.248	.066	.053	-.571
100	157	.176	.090	.718	-.028
100	158	-.349	.079	-.030	-.824
100	159	.019	.192	.682	-.824
100	160	-.062	.101	.300	-.681
100	161	-.129	.060	.205	-.344
100	162	-.128	.065	.195	-.366
100	163	-.033	.215	.766	-.574
100	164	-.046	.144	.498	-.604
100	165	-.081	.086	.279	-.437
100	166	-.242	.068	.065	-.556
100	201	-.421	.100	-.001	-.864
100	202	-.411	.165	.317	-.972
100	203	-.474	.136	.180	-1.044
100	204	-.302	.280	1.055	-1.108
100	205	-.487	.145	.249	-.961
100	206	-.150	.234	.752	-.761
100	207	.036	.106	.481	-.250
100	208	.029	.102	.398	-.248
100	209	.081	.138	.606	-.290
100	210	.138	.139	.748	-.222
100	211	.183	.155	.858	-.278
100	212	-.162	.269	.874	-.887
100	213	-.464	.193	.393	-1.017
100	214	-.045	.098	.403	-.346
100	215	.107	.135	.614	-.227
100	216	.237	.160	.878	-.123
100	217	.297	.178	.948	-.116
100	218	.309	.160	.889	-.086
100	219	.244	.161	.904	-.176
100	220	-.182	.218	.656	-.890
100	221	-.445	.170	.271	-1.115
100	222	-.087	.098	.403	-.344
100	223	.114	.122	.678	-.161
100	224	.274	.151	.976	-.057
100	225	.344	.155	.837	-.063
100	226	.327	.162	.922	-.102
100	227	.232	.162	.842	-.257
100	228	-.178	.213	.659	-.835
100	229	-.454	.177	.264	-1.080
100	230	-.104	.101	.347	-.400
100	231	.096	.114	.556	-.216
100	232	.253	.131	.891	-.039
100	233	.319	.149	1.068	-.073
100	234	.306	.161	1.095	-.067
100	235	.221	.165	1.044	-.225
100	236	-.206	.216	.656	-.955
100	237	-.475	.174	.205	-1.053
100	238	-.121	.095	.251	-.451
100	239	.084	.109	.610	-.211
100	240	.245	.132	.905	-.034
100	241	.276	.125	.817	-.033
100	242	.267	.133	.815	-.080
100	243	.187	.142	.798	-.196
100	244	-.205	.188	.558	-.904
100	245	-.397	.153	.242	-1.065
100	246	-.115	.089	.251	-.435
100	247	.042	.093	.471	-.225
100	248	.169	.104	.735	-.106
100	249	.247	.112	.763	-.014
100	250	.252	.124	.772	-.069
100	251	.190	.135	.761	-.207
100	252	-.243	.171	.458	-.840
100	253	-.391	.133	.202	-.914
100	254	-.139	.079	.210	-.392
100	255	-.006	.090	.502	-.264
100	256	.121	.089	.620	-.089
100	257	.184	.100	.790	-.247
100	258	.209	.115	.782	-.064
100	259	.165	.140	.891	-.206
100	260	-.251	.138	.338	-1.208
100	261	-.364	.120	.150	-.907
100	262	-.142	.061	.176	-.392
100	263	-.021	.071	.311	-.266
100	264	.067	.066	.465	-.092
100	265	.082	.076	.542	-.262
100	266	.148	.075	.520	-.151
100	267	.141	.098	.515	-.213
100	268	-.052	.063	.288	-.266
100	269	.029	.062	.296	-.170
100	270	.079	.061	.370	-.100
100	271	.101	.062	.451	-.103
100	272	.133	.068	.424	-.147
100	273	-.128	.065	.309	-.392
100	274	-.087	.104	.308	-.378
100	275	.029	.067	.336	-.182
100	276	.117	.058	.422	-.087
100	277	.171	.100	.743	-.102
100	301	-.344	.079	-.097	-.695
100	302	-.343	.070	-.143	-.677
100	303	-.428	.097	-.191	-.752
100	304	-.317	.042	-.203	-.456
100	305	-.325	.070	-.097	-.674
100	306	-.338	.067	-.116	-.724
100	307	-.328	.068	-.106	-.655
100	308	-.424	.119	-.088	-.966
100	309	-.314	.056	-.120	-.681
100	310	-.313	.046	-.143	-.488
100	311	-.336	.069	-.116	-.793
100	312	-.328	.063	-.112	-.716
100	313	-.326	.066	-.089	-.766
100	314	-.341	.059	-.148	-.685
100	315	-.427	.161	.224	-.981
100	316	-.445	.150	.008	-1.002
100	317	-.319	.053	-.157	-.520
100	318	.050	.109	.585	-.271
100	319	-.308	.046	-.178	-.507
100	320	-.294	.052	-.110	-.523
100	321	-.327	.074	-.091	-1.211
100	322	-.320	.053	-.180	-.591
100	323	-.313	.060	-.101	-.674
100	324	-.318	.064	-.095	-.629
100	325	-.422	.170	.274	-1.207
100	326	-.420	.152	.159	-.981
100	327	-.304	.052	-.154	-.640

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
100	328	-.305	.051	-.173	-.495	100	378	-.339	.076	-.132	-.813	100	448	-.337	.072	-.099	-.716
100	329	-.329	.069	-.169	-.843	100	379	-.336	.074	-.100	-.810	100	449	-.325	.068	-.098	-.717
100	330	-.319	.064	-.151	-.629	100	380	-.334	.074	-.105	-.824	100	450	-.310	.058	-.131	-.621
100	331	-.317	.065	-.150	-.695	100	401	-.335	.096	-.042	-.902	100	451	-.309	.061	-.142	-.648
100	332	-.316	.053	-.136	-.623	100	402	-.311	.071	-.098	-.643	100	452	-.331	.073	-.156	-.716
100	333	-.408	.166	.232	-.983	100	403	-.315	.057	-.094	-.664	100	453	-.334	.073	-.156	-.720
100	334	-.412	.161	.100	-.980	100	404	-.317	.061	-.100	-.675	100	454	-.340	.071	-.148	-.657
100	335	-.287	.047	-.131	-.476	100	405	-.323	.064	-.118	-.640	100	455	-.351	.087	-.068	-.729
100	336	.026	.102	.477	-.224	100	406	-.285	.055	-.060	-.699	100	456	-.334	.093	.011	-.778
100	337	-.308	.053	-.172	-.638	100	407	-.297	.049	-.140	-.516	100	457	-.312	.081	-.056	-.936
100	338	-.299	.051	-.158	-.538	100	408	-.303	.054	-.117	-.558	100	458	-.301	.071	-.031	-.812
100	339	-.324	.067	-.145	-.780	100	409	-.312	.056	-.132	-.571	100	459	-.296	.076	-.092	-.908
100	340	-.319	.055	-.173	-.827	100	410	-.315	.058	-.135	-.599	100	460	-.323	.083	-.035	-.709
100	341	-.315	.061	-.142	-.916	100	411	-.312	.053	-.128	-.584	100	461	-.328	.082	-.023	-.717
100	342	-.318	.066	-.090	-1.023	100	412	-.290	.050	-.135	-.747	100	462	-.343	.074	-.085	-.706
100	343	-.404	.173	.161	-1.049	100	413	-.293	.050	-.144	-.540	100	463	-.373	.089	-.046	-.842
100	344	-.419	.137	-.032	-.923	100	414	-.295	.048	-.144	-.494	100	464	-.315	.104	.037	-.883
100	345	-.330	.069	-.149	-.893	100	415	-.302	.045	-.111	-.485	100	465	-.316	.087	.040	-.647
100	346	-.318	.064	-.153	-.672	100	416	-.307	.051	-.075	-.526	100	466	-.301	.087	-.021	-.815
100	347	-.339	.078	-.120	-.794	100	417	-.312	.054	-.109	-.554	100	467	-.326	.087	.101	-.779
100	348	-.344	.069	-.162	-.888	100	418	-.313	.057	-.102	-.606	100	468	-.369	.092	.024	-.768
100	349	-.314	.066	-.111	-.703	100	419	-.315	.053	-.145	-.516	100	469	-.395	.086	-.149	-.997
100	350	-.315	.068	-.119	-.651	100	420	-.290	.053	-.100	-.603	100	470	-.372	.096	-.061	-.815
100	351	-.369	.145	.178	-.909	100	421	-.293	.052	-.125	-.523	100	471	-.330	.096	.060	-.770
100	352	-.407	.129	-.008	-.805	100	422	-.295	.051	-.144	-.482	100	472	-.294	.088	.189	-.727
100	353	-.314	.061	-.124	-.575	100	423	-.284	.044	-.160	-.487	100	473	-.404	.090	-.167	-.882
100	354	-.015	.093	.386	-.312	100	424	-.285	.050	-.109	-.518	100	474	-.353	.084	-.136	-.760
100	355	-.350	.078	-.138	-.770	100	425	-.286	.053	-.105	-.540	100	475	-.351	.097	-.007	-.984
100	356	-.346	.068	-.163	-.692	100	426	-.302	.050	-.150	-.529	100	476	-.308	.098	.031	-.784
100	357	-.352	.083	-.137	-.825	100	427	-.305	.056	-.154	-.571	100	477	-.277	.074	.018	-.736
100	358	-.340	.078	-.093	-.814	100	428	-.295	.057	-.142	-.671	100	801	.153	.062	.522	-.015
100	359	-.338	.077	-.138	-.754	100	429	-.295	.055	-.137	-.636	100	802	.064	.104	.643	-.388
100	360	-.354	.070	-.158	-.844	100	430	-.288	.048	-.145	-.475	100	803	-.039	.086	.479	-.307
100	361	-.392	.132	.054	-1.006	100	431	-.288	.052	-.145	-.484	100	804	-.373	.082	.006	-.751
100	362	-.395	.125	-.028	-.997	100	432	-.291	.053	-.144	-.483	100	805	-.360	.076	-.017	-.678
100	363	-.361	.090	-.138	-1.067	100	433	-.292	.054	-.149	-.505	100	806	-.300	.076	.141	-.639
100	364	-.354	.074	-.136	-.734	100	434	-.305	.049	-.153	-.504	100	807	-.356	.081	-.129	-.892
100	365	-.357	.086	-.129	-1.036	100	435	-.305	.055	-.125	-.548	100	808	-.351	.081	-.121	-.824
100	366	-.351	.085	-.102	-.942	100	436	-.306	.058	-.130	-.723	100	809	-.355	.069	-.126	-.769
100	367	-.358	.087	-.089	-.858	100	437	-.307	.057	-.154	-.680	100	810	-.358	.081	-.090	-.782
100	368	-.373	.078	-.195	-.805	100	438	-.300	.047	-.150	-.478	100	901	-.540	.124	-.182	-1.097
100	369	-.393	.111	-.064	-.973	100	439	-.302	.051	-.152	-.496	100	902	-.496	.122	-.057	-.996
100	370	-.381	.100	-.148	-.913	100	440	-.305	.052	-.149	-.523	100	903	-.435	.101	-.155	-.809
100	371	-.306	.084	.015	-1.022	100	441	-.303	.053	-.154	-.508	100	904	-.409	.074	-.189	-.697
100	372	-.087	.083	.192	-.350	100	442	-.314	.051	-.160	-.577	100	905	-.487	.110	-.125	-.899
100	373	-.362	.074	-.136	-.895	100	443	-.316	.059	-.142	-.603	100	906	-.483	.118	-.127	-.994
100	374	-.349	.074	-.107	-.755	100	444	-.324	.063	-.151	-.592	100	907	-.392	.094	-.066	-.810
100	375	-.344	.072	-.117	-.762	100	445	-.327	.063	-.151	-.601	100	908	-.496	.110	-.201	-1.057
100	376	-.338	.075	-.046	-.699	100	446	-.328	.058	-.191	-.597	100	909	-.354	.105	.050	-.815
100	377	-.349	.071	-.156	-.801	100	447	-.336	.067	-.127	-.881	100	910	-.445	.098	-.127	-.883

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
100	911	-.402	.091	-.066	-.921	110	143	.231	.122	.777	-.048	110	227	.135	.142	.735	-.232
100	912	-.439	.087	-.120	-.891	110	144	-.273	.059	-.143	-.628	110	228	-.032	.181	.678	-.715
100	913	-.386	.087	-.056	-.848	110	145	-.429	.219	.427	-1.311	110	229	-.323	.187	.402	-1.049
100	914	-.354	.081	-.030	-.749	110	146	-.361	.242	.250	-1.485	110	230	.001	.111	.501	-.313
100	915	-.415	.095	-.089	-.917	110	147	-.262	.155	-.008	-1.313	110	231	.195	.127	.715	-.115
100	916	-.318	.069	-.110	-.711	110	148	-.278	.108	-.038	-1.026	110	232	.316	.145	.886	-.007
100	917	-.350	.071	-.066	-.720	110	149	-.257	.057	-.084	-.756	110	233	.328	.154	.875	-.030
100	918	-.355	.076	-.053	-.683	110	150	-.271	.062	-.040	-.740	110	234	.274	.151	.824	-.076
110	101	-.605	.150	-.202	-1.246	110	151	-.217	.261	.520	-1.105	110	235	.130	.138	.800	-.272
110	102	-.504	.159	.116	-1.082	110	152	-.147	.197	.403	-1.273	110	236	-.057	.182	.644	-.624
110	103	-.284	.124	.070	-.996	110	153	-.168	.078	.087	-.972	110	237	-.289	.182	.519	-.843
110	104	-.579	.177	-.117	-1.452	110	154	-.199	.058	.015	-.526	110	238	-.007	.108	.553	-.357
110	105	-.474	.220	.117	-1.355	110	155	-.227	.036	-.120	-.385	110	239	.164	.120	.760	-.145
110	106	-.364	.174	.023	-1.430	110	156	-.252	.059	-.046	-.572	110	240	.269	.133	.859	-.003
110	107	-.228	.164	.204	-1.149	110	157	-.145	.079	.589	-.071	110	241	.269	.137	.832	-.058
110	108	-.179	.125	.177	-1.009	110	158	-.348	.089	-.126	-1.140	110	242	.225	.137	.814	-.129
110	109	-.513	.147	-.091	-1.296	110	159	-.106	.228	.800	-.918	110	243	.099	.135	.680	-.272
110	110	-.515	.176	.177	-1.380	110	160	-.118	.128	.394	-.819	110	244	-.082	.177	.512	-.654
110	111	-.422	.232	.153	-1.599	110	161	-.150	.066	.119	-.457	110	245	-.307	.168	.349	-.881
110	112	-.280	.183	.132	-1.023	110	162	-.137	.070	.149	-.414	110	246	-.046	.090	.390	-.412
110	113	-.262	.120	.023	-.821	110	163	-.110	.241	.617	-.684	110	247	.107	.092	.520	-.155
110	114	-.260	.106	.003	-.854	110	164	-.098	.176	.430	-.655	110	248	.211	.106	.786	-.049
110	115	.331	.175	1.084	-.127	110	165	-.115	.093	.255	-.440	110	249	.232	.117	.852	-.068
110	116	-.299	.066	-.077	-.683	110	166	-.238	.062	.066	-.526	110	250	.199	.121	.863	-.139
110	117	-.529	.163	.008	-1.211	110	201	-.429	.107	.013	-.942	110	251	.088	.118	.620	-.286
110	118	-.533	.200	.268	-1.637	110	202	-.330	.237	.957	-1.101	110	252	-.112	.163	.438	-.762
110	119	-.431	.266	.223	-1.387	110	203	-.494	.144	.158	-.999	110	253	-.273	.152	.405	-.767
110	120	-.314	.190	.077	-1.266	110	204	-.294	.267	.747	-1.178	110	254	-.054	.095	.566	-.329
110	121	-.266	.149	.126	-1.162	110	205	-.550	.142	.290	-1.044	110	255	.077	.102	.660	-.242
110	122	-.275	.138	.072	-1.368	110	206	.071	.235	.845	-.753	110	256	.166	.099	.556	-.083
110	123	-.534	.170	.000	-1.399	110	207	.092	.116	.528	-.294	110	257	.183	.100	.669	-.055
110	124	-.534	.215	.291	-1.688	110	208	.085	.105	.471	-.192	110	258	.171	.105	.681	-.071
110	125	-.435	.272	.211	-1.808	110	209	.117	.147	.808	-.255	110	259	.094	.121	.692	-.249
110	126	-.294	.212	.120	-1.356	110	210	.136	.140	.720	-.233	110	260	-.160	.137	.406	-.676
110	127	-.264	.142	.025	-1.130	110	211	.144	.146	.697	-.274	110	261	-.284	.112	.130	-.769
110	128	-.270	.138	.030	-1.218	110	212	.106	.240	.970	-.764	110	262	-.091	.064	.212	-.286
110	129	.275	.132	.839	-.052	110	213	-.235	.227	.798	-1.019	110	263	.034	.073	.455	-.174
110	130	-.285	.074	-.096	-.826	110	214	.078	.119	.562	-.248	110	264	.078	.070	.507	-.103
110	131	-.505	.181	.119	-1.713	110	215	.233	.159	.842	-.167	110	265	.106	.073	.440	-.205
110	132	-.497	.231	.258	-1.925	110	216	.326	.181	.977	-.075	110	266	.132	.075	.462	-.136
110	133	-.378	.266	.201	-1.441	110	217	.351	.189	1.062	-.184	110	267	.104	.093	.455	-.182
110	134	-.274	.193	.066	-1.121	110	218	.279	.155	.872	-.065	110	268	-.031	.068	.242	-.289
110	135	-.239	.105	-.012	-.917	110	219	.172	.146	.762	-.214	110	269	.061	.070	.458	-.119
110	136	-.258	.097	-.028	-1.170	110	220	.000	.213	.922	-.687	110	270	.103	.068	.470	-.094
110	137	-.499	.204	.208	-1.531	110	221	-.283	.205	.541	-.975	110	271	.118	.067	.448	-.097
110	138	-.462	.248	.229	-1.544	110	222	.028	.117	.537	-.276	110	272	.117	.083	.453	-.169
110	139	-.324	.210	.084	-1.251	110	223	.220	.146	.876	-.188	110	273	-.093	.075	.285	-.382
110	140	-.252	.145	-.005	-1.185	110	224	.333	.169	1.000	-.087	110	274	-.017	.134	.512	-.364
110	141	-.272	.112	.007	-.990	110	225	.327	.162	.910	-.027	110	275	.078	.098	.627	-.230
110	142	-.276	.082	-.042	-.986	110	226	.275	.158	.886	-.100	110	276	.135	.074	.570	-.095

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
110	277	.172	.112	.628	-.121	110	350	-.324	.072	-.152	-.745	110	420	-.293	.075	-.068	-.800
110	301	-.335	.078	-.084	-.664	110	351	-.267	.155	.256	-.885	110	421	-.289	.067	-.080	-.689
110	302	-.345	.079	-.136	-.803	110	352	-.292	.141	.156	-.759	110	422	-.290	.063	-.112	-.649
110	303	-.376	.087	-.152	-.685	110	353	-.314	.064	-.113	-.611	110	423	-.284	.052	-.097	-.485
110	304	-.326	.054	-.154	-.609	110	354	.072	.099	.720	-.251	110	424	-.284	.056	-.080	-.502
110	305	-.331	.079	-.113	-.821	110	355	-.351	.083	-.115	-.784	110	425	-.284	.057	-.082	-.503
110	306	-.335	.067	-.146	-.729	110	356	-.344	.073	-.173	-.817	110	426	-.291	.055	-.161	-.598
110	307	-.322	.068	-.134	-.813	110	357	-.363	.091	-.149	-1.085	110	427	-.293	.061	-.121	-.620
110	308	-.340	.095	-.032	-.821	110	358	-.349	.086	-.125	-.833	110	428	-.292	.078	-.059	-.783
110	309	-.316	.064	-.125	-.685	110	359	-.351	.083	-.118	-.868	110	429	-.287	.071	-.070	-.722
110	310	-.307	.054	-.151	-.523	110	360	-.350	.071	-.173	-.729	110	430	-.294	.059	-.139	-.644
110	311	-.333	.080	-.113	-.703	110	361	-.304	.148	.213	-.913	110	431	-.291	.058	-.121	-.600
110	312	-.323	.071	-.125	-.745	110	362	-.308	.139	.137	-.907	110	432	-.291	.058	-.090	-.595
110	313	-.323	.071	-.115	-.625	110	363	-.346	.088	-.103	-.856	110	433	-.290	.059	-.093	-.586
110	314	-.324	.057	-.151	-.676	110	364	-.349	.086	-.156	-1.048	110	434	-.287	.055	-.134	-.531
110	315	-.238	.164	.310	-.852	110	365	-.354	.096	-.087	-1.075	110	435	-.287	.060	-.101	-.554
110	316	-.281	.135	.201	-.868	110	366	-.354	.096	-.140	-1.138	110	436	-.295	.077	-.119	-.839
110	317	-.302	.055	-.130	-.550	110	367	-.374	.104	-.144	-1.189	110	437	-.291	.073	-.129	-.767
110	318	.175	.128	.651	-.179	110	368	-.375	.096	-.163	-1.166	110	438	-.295	.062	-.159	-.647
110	319	-.304	.052	-.171	-.513	110	369	-.314	.109	.095	-.934	110	439	-.296	.064	-.141	-.657
110	320	-.300	.057	-.135	-.637	110	370	-.322	.098	-.035	-.897	110	440	-.295	.062	-.126	-.680
110	321	-.337	.078	-.140	-.875	110	371	-.308	.077	-.005	-.726	110	441	-.291	.060	-.124	-.656
110	322	-.308	.051	-.176	-.686	110	372	-.026	.086	.369	-.308	110	442	-.293	.062	-.124	-.610
110	323	-.313	.065	-.154	-.608	110	373	-.343	.082	-.047	-.938	110	443	-.294	.068	-.116	-.695
110	324	-.307	.061	-.123	-.646	110	374	-.343	.079	-.097	-.840	110	444	-.301	.085	-.097	-.793
110	325	-.258	.160	.285	-.827	110	375	-.349	.082	-.095	-.981	110	445	-.302	.083	-.115	-.762
110	326	-.266	.156	.282	-.903	110	376	-.312	.084	.014	-.717	110	446	-.310	.067	-.156	-.715
110	327	-.292	.051	-.149	-.539	110	377	-.345	.083	-.150	-.943	110	447	-.314	.073	-.141	-.732
110	328	-.287	.047	-.143	-.560	110	378	-.339	.083	-.112	-.808	110	448	-.307	.069	-.114	-.682
110	329	-.314	.066	-.116	-.918	110	379	-.340	.084	-.117	-.843	110	449	-.300	.066	-.110	-.612
110	330	-.302	.059	-.148	-.703	110	380	-.349	.087	-.110	-.897	110	450	-.310	.070	-.156	-.755
110	331	-.301	.061	-.135	-.731	110	401	-.342	.099	-.044	-.750	110	451	-.306	.070	-.141	-.690
110	332	-.320	.060	-.168	-.684	110	402	-.309	.077	-.016	-.687	110	452	-.310	.086	-.061	-.704
110	333	-.264	.174	.302	-.890	110	403	-.323	.065	-.105	-.625	110	453	-.315	.088	-.070	-.776
110	334	-.274	.166	.226	-.932	110	404	-.324	.071	-.098	-.732	110	454	-.324	.075	-.149	-.904
110	335	-.293	.055	-.152	-.516	110	405	-.325	.072	-.128	-.675	110	455	-.339	.085	-.066	-.772
110	336	.126	.107	.643	-.138	110	406	-.293	.072	-.068	-.725	110	456	-.319	.087	-.051	-1.216
110	337	-.307	.062	-.121	-.695	110	407	-.292	.058	-.117	-.607	110	457	-.309	.079	-.011	-1.059
110	338	-.298	.060	-.116	-.597	110	408	-.301	.062	-.078	-.687	110	458	-.310	.074	-.097	-.759
110	339	-.323	.076	-.118	-.914	110	409	-.307	.064	-.097	-.689	110	459	-.308	.079	-.096	-.722
110	340	-.318	.055	-.136	-.726	110	410	-.305	.065	-.091	-.710	110	460	-.311	.087	-.063	-.800
110	341	-.322	.062	-.123	-.721	110	411	-.302	.058	-.154	-.546	110	461	-.317	.089	-.075	-.859
110	342	-.319	.066	-.123	-.745	110	412	-.292	.063	-.093	-.650	110	462	-.325	.084	-.088	-1.039
110	343	-.278	.163	.338	-.885	110	413	-.292	.062	-.107	-.665	110	463	-.336	.084	-.050	-.745
110	344	-.279	.140	.259	-.885	110	414	-.293	.059	-.117	-.623	110	464	-.295	.091	-.018	-.879
110	345	-.329	.069	-.146	-.708	110	415	-.298	.051	-.127	-.519	110	465	-.313	.077	.038	-.747
110	346	-.315	.067	-.150	-.646	110	416	-.303	.057	-.106	-.522	110	466	-.311	.097	-.027	-1.139
110	347	-.336	.081	-.142	-.912	110	417	-.303	.060	-.080	-.540	110	467	-.331	.084	-.076	-.854
110	348	-.341	.074	-.145	-.890	110	418	-.302	.062	-.101	-.576	110	468	-.341	.090	-.078	-.939
110	349	-.329	.070	-.172	-.736	110	419	-.304	.057	-.146	-.580	110	469	-.347	.086	-.077	-.828

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
110	470	-.326	.095	-.074	-.901	120	115	.286	.150	.809	-.098	120	165	-.140	.098	.242	-.546
110	471	-.300	.088	.026	-.758	120	116	-.313	.083	-.025	-.794	120	166	-.230	.061	.010	-.462
110	472	-.289	.080	.081	-.690	120	117	-.484	.142	-.166	-1.240	120	201	-.359	.129	.322	-.969
110	473	-.366	.084	-.094	-.723	120	118	-.494	.164	-.128	-1.345	120	202	-.280	.273	.786	-1.248
110	474	-.329	.086	-.045	-.806	120	119	-.500	.186	-.003	-1.643	120	203	-.447	.138	.744	-1.160
110	475	-.340	.101	-.050	-.906	120	120	-.422	.170	.071	-1.230	120	204	-.313	.213	.802	-1.117
110	476	-.290	.084	.053	-.659	120	121	-.361	.173	.079	-1.153	120	205	-.492	.133	.255	-1.000
110	477	-.293	.067	-.060	-.636	120	122	-.360	.191	.026	-1.424	120	206	.216	.185	.942	-.452
110	801	.148	.071	.443	-.038	120	123	-.505	.170	-.017	-1.400	120	207	.146	.126	.697	-.205
110	802	.128	.103	.569	-.279	120	124	-.516	.197	.051	-1.658	120	208	.143	.121	.601	-.261
110	803	.023	.092	.424	-.236	120	125	-.506	.216	.070	-2.049	120	209	.136	.141	.653	-.259
110	804	-.394	.108	-.147	-1.102	120	126	-.425	.210	.108	-1.506	120	210	.159	.124	.599	-.309
110	805	-.328	.077	-.052	-.686	120	127	-.364	.167	.074	-1.381	120	211	.144	.126	.693	-.261
110	806	-.288	.066	.002	-.552	120	128	-.365	.197	.106	-1.655	120	212	.282	.200	.944	-.399
110	807	-.353	.095	-.090	-.986	120	129	.263	.136	.869	-.051	120	213	.004	.246	.868	-.812
110	808	-.357	.097	-.101	-.950	120	130	-.306	.099	-.051	-.780	120	214	.164	.134	.675	-.201
110	809	-.336	.071	-.123	-.708	120	131	-.512	.173	-.126	-1.556	120	215	.283	.169	.917	-.131
110	810	-.328	.080	-.115	-.699	120	132	-.523	.204	.106	-1.799	120	216	.330	.183	.971	-.119
110	901	-.537	.128	-.194	-1.140	120	133	-.483	.235	.094	-2.049	120	217	.314	.183	.968	-.165
110	902	-.491	.130	.121	-.990	120	134	-.367	.198	.180	-1.395	120	218	.260	.145	.883	-.144
110	903	-.455	.105	-.152	-1.099	120	135	-.314	.146	-.040	-1.010	120	219	.126	.129	.743	-.276
110	904	-.383	.072	-.160	-.714	120	136	-.313	.154	.063	-1.305	120	220	.136	.176	.792	-.705
110	905	-.459	.104	-.152	-1.008	120	137	-.556	.202	.116	-1.976	120	221	-.100	.191	.604	-.890
110	906	-.436	.106	-.100	-.889	120	138	-.543	.232	.096	-1.976	120	222	.143	.119	.704	-.201
110	907	-.372	.083	-.129	-.851	120	139	-.427	.212	-.000	-1.662	120	223	.298	.147	.962	-.018
110	908	-.456	.093	-.192	-.860	120	140	-.321	.180	.023	-1.373	120	224	.363	.157	1.031	-.010
110	909	-.423	.120	-.012	-1.055	120	141	-.337	.155	.018	-1.285	120	225	.309	.140	.979	-.032
110	910	-.393	.084	-.150	-.799	120	142	-.296	.127	-.010	-1.380	120	226	.239	.133	.897	-.080
110	911	-.390	.091	-.134	-.841	120	143	.215	.132	.811	-.072	120	227	.081	.114	.609	-.271
110	912	-.420	.091	-.141	-.867	120	144	-.289	.082	-.094	-.741	120	228	.073	.164	.738	-.564
110	913	-.392	.093	-.147	-.936	120	145	-.551	.198	.258	-1.777	120	229	-.116	.155	.518	-.880
110	914	-.352	.082	-.103	-.725	120	146	-.505	.221	.099	-1.516	120	230	.101	.109	.560	-.314
110	915	-.395	.098	-.072	-.827	120	147	-.371	.184	-.027	-1.369	120	231	.245	.129	.771	-.095
110	916	-.312	.072	-.089	-.692	120	148	-.344	.135	-.091	-1.176	120	232	.305	.140	.904	-.004
110	917	-.330	.072	-.087	-.632	120	149	-.279	.089	-.064	-.869	120	233	.276	.125	.837	.008
110	918	-.335	.076	-.091	-.706	120	150	-.282	.086	-.035	-.931	120	234	.211	.123	.691	-.085
120	101	-.544	.142	-.168	-1.067	120	151	-.397	.212	.427	-1.325	120	235	.063	.113	.585	-.249
120	102	-.542	.132	-.191	-1.124	120	152	-.313	.218	.303	-1.369	120	236	.027	.149	.608	-.597
120	103	-.360	.136	-.000	-1.031	120	153	-.198	.086	.039	-.652	120	237	-.166	.148	.520	-.660
120	104	-.549	.162	-.176	-1.382	120	154	-.217	.063	.013	-.547	120	238	.053	.102	.560	-.226
120	105	-.542	.174	-.082	-1.335	120	155	-.237	.042	-.098	-.450	120	239	.196	.118	.780	-.126
120	106	-.475	.165	.015	-1.300	120	156	-.260	.070	-.027	-.725	120	240	.266	.125	.819	-.006
120	107	-.381	.154	.041	-.999	120	157	.138	.076	.536	-.045	120	241	.275	.129	.756	.003
120	108	-.294	.142	.089	-.884	120	158	-.325	.106	-.075	-1.035	120	242	.209	.126	.713	-.108
120	109	-.492	.144	-.153	-1.072	120	159	-.193	.208	.473	-.994	120	243	.058	.117	.568	-.367
120	110	-.502	.163	-.118	-1.161	120	160	-.141	.125	.244	-.908	120	244	.007	.165	.663	-.663
120	111	-.505	.180	.019	-1.269	120	161	-.157	.072	.089	-.625	120	245	-.176	.152	.412	-.866
120	112	-.427	.175	.203	-1.259	120	162	-.138	.070	.081	-.537	120	246	.034	.099	.409	-.239
120	113	-.357	.129	-.000	-.901	120	163	-.177	.231	.675	-.720	120	247	.171	.112	.600	-.145
120	114	-.349	.143	.205	-1.161	120	164	-.145	.182	.559	-.761	120	248	.240	.117	.660	-.139

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
120	249	.223	.111	.780	-.098	120	322	-.332	.083	-.104	-.961	120	372	.020	.097	.547	-.366
120	250	.170	.112	.688	-.219	120	323	-.325	.095	-.048	-.911	120	373	-.311	.082	-.100	-.852
120	251	.056	.114	.589	-.414	120	324	-.332	.097	-.057	-1.034	120	374	-.320	.086	-.056	-.869
120	252	-.019	.157	.469	-.533	120	325	-.115	.168	.524	-.776	120	375	-.337	.093	-.089	-.840
120	253	-.213	.153	.501	-.785	120	326	-.145	.136	.336	-.764	120	376	-.277	.083	-.053	-.735
120	254	-.019	.091	.439	-.397	120	327	-.313	.085	-.052	-1.088	120	377	-.327	.082	-.122	-.854
120	255	.105	.096	.612	-.182	120	328	-.299	.067	-.144	-.623	120	378	-.326	.080	-.109	-.861
120	256	.179	.102	.641	-.070	120	329	-.324	.100	-.029	-.991	120	379	-.335	.087	-.094	-.730
120	257	.175	.098	.680	-.041	120	330	-.317	.089	-.083	-.819	120	380	-.354	.092	-.135	-.765
120	258	.146	.097	.625	-.090	120	331	-.317	.090	-.070	-.942	120	401	-.322	.099	-.019	-.786
120	259	.048	.107	.486	-.305	120	332	-.317	.080	-.101	-.939	120	402	-.301	.089	-.049	-.682
120	260	-.096	.122	.292	-.529	120	333	-.131	.149	.499	-.746	120	403	-.332	.073	-.130	-.673
120	261	-.200	.137	.238	-.772	120	334	-.144	.142	.481	-.763	120	404	-.326	.079	-.099	-.747
120	262	-.063	.073	.261	-.290	120	335	-.280	.070	-.079	-.717	120	405	-.327	.083	-.098	-.798
120	263	.074	.090	.459	-.159	120	336	.213	.106	.676	-.049	120	406	-.310	.089	-.068	-.757
120	264	.106	.077	.462	-.108	120	337	-.313	.088	-.105	-.978	120	407	-.307	.072	-.113	-.622
120	265	.133	.076	.506	-.201	120	338	-.302	.086	-.096	-.870	120	408	-.310	.076	-.109	-.642
120	266	.123	.080	.550	-.106	120	339	-.331	.105	-.075	-1.047	120	409	-.312	.077	-.046	-.666
120	267	.064	.096	.583	-.239	120	340	-.328	.078	-.091	-1.019	120	410	-.304	.078	-.066	-.633
120	268	.021	.076	.386	-.179	120	341	-.329	.091	-.141	-1.047	120	411	-.297	.071	-.113	-.644
120	269	.104	.087	.493	-.120	120	342	-.328	.094	-.123	-1.105	120	412	-.304	.088	-.064	-.695
120	270	.131	.084	.502	-.158	120	343	-.157	.142	.342	-.697	120	413	-.299	.083	-.058	-.735
120	271	.136	.078	.481	-.066	120	344	-.160	.109	.287	-.565	120	414	-.298	.078	-.068	-.710
120	272	.090	.076	.469	-.139	120	345	-.321	.093	-.116	-.850	120	415	-.307	.064	-.139	-.593
120	273	-.051	.084	.313	-.288	120	346	-.311	.090	-.108	-.851	120	416	-.307	.072	-.096	-.772
120	274	.051	.143	.611	-.323	120	347	-.331	.103	-.067	-1.100	120	417	-.308	.077	-.086	-.817
120	275	.124	.107	.632	-.129	120	348	-.343	.097	-.121	-.949	120	418	-.308	.083	-.085	-.846
120	276	.163	.089	.580	-.027	120	349	-.332	.098	-.141	-1.277	120	419	-.294	.068	-.061	-.644
120	277	.118	.107	.637	-.164	120	350	-.329	.099	-.125	-1.134	120	420	-.306	.099	-.026	-.762
120	301	-.331	.097	-.006	-.884	120	351	-.168	.152	.352	-.858	120	421	-.294	.087	-.010	-.656
120	302	-.348	.093	-.079	-.822	120	352	-.182	.112	.162	-.638	120	422	-.290	.080	-.040	-.698
120	303	-.344	.080	-.045	-.704	120	353	-.314	.090	-.105	-.884	120	423	-.288	.060	-.110	-.590
120	304	-.317	.052	-.158	-.520	120	354	-.158	.109	.662	-.120	120	424	-.284	.064	-.105	-.534
120	305	-.325	.094	-.032	-.820	120	355	-.350	.111	-.106	-1.572	120	425	-.285	.070	-.096	-.686
120	306	-.354	.091	-.074	-.818	120	356	-.334	.078	-.156	-.763	120	426	-.298	.071	-.108	-.717
120	307	-.341	.100	-.072	-.988	120	357	-.352	.104	-.098	-1.106	120	427	-.295	.077	-.071	-.720
120	308	-.277	.105	.149	-.714	120	358	-.350	.104	-.110	-.905	120	428	-.312	.114	-.034	-.882
120	309	-.317	.089	-.058	-.764	120	359	-.351	.104	-.149	-1.028	120	429	-.296	.098	-.042	-.801
120	310	-.306	.069	-.096	-.638	120	360	-.364	.094	-.177	-.871	120	430	-.288	.074	-.095	-.607
120	311	-.336	.104	-.034	-.914	120	361	-.208	.141	.384	-.983	120	431	-.276	.069	-.054	-.637
120	312	-.329	.098	-.025	-.951	120	362	-.221	.131	.210	-.980	120	432	-.272	.066	-.103	-.628
120	313	-.336	.100	-.048	-.927	120	363	-.331	.096	-.084	-1.047	120	433	-.272	.070	-.080	-.626
120	314	-.334	.085	-.141	-1.034	120	364	-.357	.099	-.136	-1.011	120	434	-.293	.067	-.113	-.666
120	315	-.087	.167	.675	-.853	120	365	-.354	.109	-.080	-.993	120	435	-.292	.073	-.101	-.710
120	316	-.155	.142	.515	-.841	120	366	-.362	.115	-.098	-.997	120	436	-.315	.107	-.017	-.803
120	317	-.300	.074	-.098	-.793	120	367	-.394	.136	-.103	-1.200	120	437	-.305	.098	-.045	-.747
120	318	.246	.132	.941	-.139	120	368	-.377	.103	-.174	-1.350	120	438	-.293	.083	-.117	-.685
120	319	-.314	.071	-.124	-.836	120	369	-.266	.104	.091	-.907	120	439	-.285	.078	-.059	-.647
120	320	-.293	.073	-.091	-.677	120	370	-.291	.086	-.010	-.927	120	440	-.281	.074	-.074	-.589
120	321	-.327	.097	-.077	-.889	120	371	-.313	.087	-.096	-.773	120	441	-.279	.075	-.096	-.612

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
120	442	-.290	.068	-.137	-.866	120	905	-.442	.107	-.136	-.948	130	137	-.517	.197	-.053	-1.613
120	443	-.289	.075	-.041	-.869	120	906	-.452	.116	-.110	-.931	130	138	-.523	.213	-.028	-1.684
120	444	-.301	.094	-.072	-.819	120	907	-.391	.099	-.111	-.921	130	139	-.454	.204	-.032	-1.698
120	445	-.298	.090	-.066	-.787	120	908	-.459	.103	-.134	-.950	130	140	-.322	.177	.124	-1.309
120	446	-.307	.083	-.120	-.729	120	909	-.457	.134	.020	-1.067	130	141	-.276	.137	.079	-1.466
120	447	-.302	.082	-.051	-.790	120	910	-.410	.107	-.122	-.819	130	142	-.265	.127	.107	-1.235
120	448	-.293	.076	-.077	-.714	120	911	-.412	.115	-.106	-.855	130	143	.198	.125	.775	-.100
120	449	-.291	.074	-.049	-.787	120	912	-.437	.103	-.117	-.955	130	144	-.251	.076	-.060	-.709
120	450	-.305	.077	-.100	-.819	120	913	-.422	.111	-.046	-1.054	130	145	-.556	.201	.053	-1.807
120	451	-.300	.078	-.106	-.705	120	914	-.366	.098	-.047	-.850	130	146	-.527	.221	.025	-1.975
120	452	-.303	.093	-.050	-.860	120	915	-.403	.110	-.049	-.926	130	147	-.397	.201	.043	-1.880
120	453	-.305	.094	-.052	-.822	120	916	-.362	.093	-.022	-.733	130	148	-.309	.124	-.050	-1.346
120	454	-.326	.107	-.093	-1.349	120	917	-.354	.087	-.069	-.724	130	149	-.236	.077	-.039	-.725
120	455	-.313	.108	-.029	-1.161	120	918	-.356	.090	-.093	-.819	130	150	-.229	.079	.014	-.808
120	456	-.302	.092	-.012	-.841	130	101	-.469	.126	-.119	-1.195	130	151	-.388	.219	.352	-1.490
120	457	-.307	.092	-.045	-.848	130	102	-.440	.126	-.124	-1.107	130	152	-.299	.213	.205	-1.617
120	458	-.333	.093	-.078	-.810	130	103	-.356	.135	.025	-.998	130	153	-.208	.091	.063	-.730
120	459	-.328	.101	-.051	-.932	130	104	-.423	.138	-.062	-1.234	130	154	-.197	.067	.014	-.576
120	460	-.310	.114	.065	-1.035	130	105	-.432	.150	-.070	-1.385	130	155	-.209	.064	-.013	-.545
120	461	-.317	.117	.016	-1.017	130	106	-.425	.156	-.046	-1.327	130	156	-.228	.069	-.046	-.559
120	462	-.317	.106	-.047	-1.019	130	107	-.368	.141	.017	-1.220	130	157	.110	.068	.495	-.073
120	463	-.317	.102	-.049	-1.177	130	108	-.314	.132	.080	-.888	130	158	-.276	.102	-.033	-.763
120	464	-.289	.094	-.007	-.848	130	109	-.405	.120	-.134	-1.131	130	159	-.246	.203	.400	-1.005
120	465	-.319	.088	-.049	-1.088	130	110	-.409	.140	-.072	-1.163	130	160	-.187	.131	.222	-.925
120	466	-.328	.109	-.096	-1.504	130	111	-.420	.151	.002	-1.363	130	161	-.152	.065	.063	-.584
120	467	-.346	.105	-.107	-1.170	130	112	-.389	.145	.065	-1.099	130	162	-.127	.069	.119	-.388
120	468	-.318	.112	-.066	-.979	130	113	-.363	.124	-.042	-1.049	130	163	-.205	.222	.635	-1.090
120	469	-.347	.105	-.097	-.840	130	114	-.358	.156	.038	-1.372	130	164	-.171	.169	.387	-.873
120	470	-.317	.100	-.036	-.907	130	115	-.232	.170	.977	-.320	130	165	-.127	.089	.313	-.517
120	471	-.310	.087	.022	-.855	130	116	-.299	.095	-.090	-.876	130	166	-.205	.064	.048	-.573
120	472	-.318	.090	-.070	-.783	130	117	-.408	.133	-.142	-1.307	130	201	-.193	.231	.619	-.889
120	473	-.338	.091	-.082	-1.039	130	118	-.414	.157	-.098	-1.463	130	202	-.075	.322	1.025	-1.027
120	474	-.306	.091	.033	-1.164	130	119	-.424	.172	-.005	-1.535	130	203	-.338	.193	.788	-.906
120	475	-.321	.105	-.002	-1.353	130	120	-.422	.143	-.024	-1.031	130	204	-.228	.206	.733	-.916
120	476	-.293	.081	.058	-.716	130	121	-.393	.167	.051	-1.275	130	205	-.383	.159	.364	-1.033
120	477	-.303	.073	-.082	-.847	130	122	-.401	.201	.042	-1.655	130	206	.230	.192	.934	-.479
120	801	.132	.065	.415	-.049	130	123	-.443	.147	-.103	-1.256	130	207	.165	.148	.713	-.243
120	802	.161	.111	.659	-.301	130	124	-.450	.174	-.035	-1.476	130	208	.167	.143	.698	-.248
120	803	.064	.106	.561	-.226	130	125	-.453	.190	-.005	-1.598	130	209	.147	.160	.780	-.322
120	804	-.373	.125	-.032	-1.370	130	126	-.407	.189	.092	-1.610	130	210	.137	.144	.875	-.277
120	805	-.299	.076	-.046	-.682	130	127	-.353	.146	.027	-1.072	130	211	.116	.144	.815	-.292
120	806	-.278	.065	-.048	-.634	130	128	-.349	.189	.082	-1.513	130	212	.247	.200	1.048	-.508
120	807	-.379	.112	-.120	-1.023	130	129	-.206	.131	.772	-.108	130	213	.139	.253	1.070	-.935
120	808	-.380	.112	-.151	-.998	130	130	-.272	.092	-.051	-.817	130	214	.208	.154	.843	-.147
120	809	-.343	.077	-.100	-.748	130	131	-.477	.165	-.088	-1.571	130	215	.282	.177	.964	-.211
120	810	-.321	.078	-.096	-.729	130	132	-.486	.197	-.017	-1.578	130	216	.299	.178	.943	-.159
120	901	-.515	.125	-.122	-1.136	130	133	-.459	.206	.070	-1.545	130	217	.245	.171	.809	-.306
120	902	-.496	.131	.232	-1.116	130	134	-.373	.192	.045	-1.716	130	218	.218	.156	.799	-.198
120	903	-.448	.115	-.150	-1.062	130	135	-.310	.136	.007	-1.034	130	219	.087	.136	.620	-.330
120	904	-.430	.093	-.172	-.760	130	136	-.300	.158	.090	-1.439	130	220	.126	.162	.948	-.605

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
130	221	-.008	.194	.985	-.793	130	271	.135	.082	.477	-.093	130	344	-.144	.095	.259	-.569
130	222	.151	.124	.656	-.164	130	272	.069	.072	.383	-.270	130	345	-.270	.077	-.004	-.968
130	223	.272	.151	.903	-.176	130	273	-.021	.065	.267	-.252	130	346	-.261	.074	-.021	-.673
130	224	.315	.169	1.031	-.171	130	274	.059	.116	.600	-.309	130	347	-.284	.092	-.048	-.997
130	225	.252	.144	.865	-.090	130	275	.121	.095	.816	-.187	130	348	-.277	.079	-.079	-.735
130	226	.192	.141	.797	-.193	130	276	.148	.074	.626	-.013	130	349	-.283	.107	-.056	-1.003
130	227	.042	.123	.555	-.418	130	277	.089	.095	.514	-.169	130	350	-.284	.112	-.078	-1.053
130	228	.058	.139	.609	-.429	130	301	-.313	.107	-.014	-.854	130	351	-.152	.105	.292	-.739
130	229	-.067	.165	.619	-.581	130	302	-.380	.116	-.080	-1.067	130	352	-.167	.080	.127	-.523
130	230	.106	.114	.663	-.198	130	303	-.345	.136	.309	-.954	130	353	-.247	.067	-.064	-.666
130	231	.224	.129	.934	-.069	130	304	-.296	.099	.037	-.898	130	354	.116	.089	.587	-.123
130	232	.274	.143	1.011	-.039	130	305	-.307	.127	.104	-.940	130	355	-.272	.079	-.066	-.934
130	233	.234	.135	.772	-.097	130	306	-.373	.126	.027	-.996	130	356	-.271	.066	-.125	-.699
130	234	.174	.132	.721	-.214	130	307	-.419	.178	-.014	-1.430	130	357	-.291	.086	-.076	-.855
130	235	.029	.117	.538	-.343	130	308	-.184	.152	.536	-.683	130	358	-.285	.085	-.073	-.893
130	236	.031	.134	.680	-.427	130	309	-.284	.096	-.001	-.868	130	359	-.287	.086	-.097	-.901
130	237	-.115	.139	.653	-.677	130	310	-.283	.080	-.057	-.645	130	360	-.284	.076	-.113	-.932
130	238	.072	.094	.639	-.188	130	311	-.313	.131	.071	-1.075	130	361	-.184	.100	.213	-.583
130	239	.199	.112	.693	-.054	130	312	-.345	.152	.195	-1.178	130	362	-.194	.093	.106	-.515
130	240	.260	.133	.892	-.025	130	313	-.411	.180	.290	-1.278	130	363	-.263	.081	-.076	-.659
130	241	.224	.125	.796	-.184	130	314	-.420	.146	-.108	-1.136	130	364	-.268	.064	-.103	-.756
130	242	.166	.124	.762	-.229	130	315	.045	.204	.880	-.691	130	365	-.274	.076	-.014	-.633
130	243	.023	.114	.506	-.467	130	316	-.036	.187	.831	-.769	130	366	-.279	.079	-.095	-.723
130	244	.007	.136	.590	-.446	130	317	-.278	.079	-.055	-.650	130	367	-.293	.086	-.111	-.838
130	245	-.130	.114	.374	-.588	130	318	.269	.150	.907	-.076	130	368	-.294	.082	-.123	-.765
130	246	.039	.081	.398	-.252	130	319	-.278	.086	-.054	-.763	130	369	-.207	.083	.068	-.658
130	247	.154	.100	.681	-.110	130	320	-.276	.101	.159	-.869	130	370	-.228	.074	-.028	-.635
130	248	.213	.118	.771	-.056	130	321	-.313	.141	.175	-1.109	130	371	-.260	.071	-.044	-.728
130	249	.199	.115	.779	-.077	130	322	-.330	.123	.009	-1.180	130	372	.021	.083	.428	-.216
130	250	.150	.112	.640	-.163	130	323	-.353	.165	.039	-1.377	130	373	-.258	.072	-.026	-.818
130	251	.029	.114	.646	-.350	130	324	-.375	.168	.015	-1.450	130	374	-.262	.074	-.072	-.674
130	252	-.006	.136	.761	-.493	130	325	-.038	.180	.714	-.716	130	375	-.273	.079	-.060	-.642
130	253	-.165	.108	.401	-.672	130	326	-.047	.160	.545	-.663	130	376	-.227	.072	-.014	-.612
130	254	.004	.077	.411	-.294	130	327	-.276	.105	.004	-1.005	130	377	-.268	.067	-.107	-.830
130	255	.110	.093	.596	-.137	130	328	-.265	.077	-.069	-.817	130	378	-.266	.067	-.096	-.671
130	256	.172	.101	.669	-.082	130	329	-.294	.117	.064	-1.182	130	379	-.271	.072	-.098	-.724
130	257	.175	.093	.648	-.068	130	330	-.302	.128	.058	-1.125	130	380	-.280	.075	-.108	-.685
130	258	.143	.090	.585	-.077	130	331	-.328	.152	.023	-1.747	130	401	-.296	.096	-.026	-.895
130	259	.043	.098	.492	-.292	130	332	-.341	.138	-.079	-1.508	130	402	-.287	.089	-.047	-.871
130	260	-.065	.119	.431	-.612	130	333	-.077	.139	.478	-.571	130	403	-.275	.070	-.040	-.694
130	261	-.161	.111	.310	-.529	130	334	-.094	.133	.455	-.551	130	404	-.270	.079	-.056	-.732
130	262	-.043	.066	.370	-.259	130	335	-.244	.071	-.069	-.945	130	405	-.292	.090	-.050	-.735
130	263	.073	.083	.434	-.168	130	336	.174	.098	.664	-.040	130	406	-.271	.084	-.045	-.677
130	264	.112	.079	.495	-.082	130	337	-.263	.091	-.014	-.940	130	407	-.277	.074	-.049	-.639
130	265	.126	.074	.599	-.109	130	338	-.255	.086	-.006	-.771	130	408	-.271	.078	.012	-.680
130	266	.113	.074	.484	-.095	130	339	-.284	.114	-.008	-1.426	130	409	-.271	.078	.007	-.745
130	267	.049	.084	.492	-.232	130	340	-.279	.082	-.040	-.998	130	410	-.263	.080	-.026	-.689
130	268	.028	.074	.559	-.215	130	341	-.290	.113	-.014	-1.742	130	411	-.268	.073	-.061	-.658
130	269	.112	.082	.436	-.100	130	342	-.295	.124	-.044	-2.600	130	412	-.283	.083	-.051	-.724
130	270	.135	.084	.459	-.072	130	343	-.133	.117	.456	-.749	130	413	-.277	.079	-.078	-.697

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
130	414	-.273	.076	-.091	-.730	130	464	-.245	.068	-.043	-.617	140	109	-.302	.095	-.088	-.939
130	415	-.269	.063	-.109	-.559	130	465	-.268	.077	-.067	-.798	140	110	-.305	.110	-.036	-1.007
130	416	-.270	.076	-.046	-.658	130	466	-.261	.074	-.058	-.659	140	111	-.318	.119	-.020	-1.012
130	417	-.272	.081	-.036	-.664	130	467	-.287	.088	-.050	-.885	140	112	-.314	.120	.021	-.867
130	418	-.274	.086	.001	-.698	130	468	-.265	.099	-.025	-1.005	140	113	-.319	.113	.027	-.954
130	419	-.275	.074	-.066	-.715	130	469	-.262	.070	-.081	-.646	140	114	-.320	.144	.053	-1.058
130	420	-.290	.103	-.051	-.795	130	470	-.249	.071	-.037	-.610	140	115	.167	.157	.745	-.289
130	421	-.275	.090	-.036	-.702	130	471	-.248	.069	.065	-.787	140	116	-.244	.079	-.061	-.689
130	422	-.268	.081	-.047	-.703	130	472	-.251	.069	-.069	-.699	140	117	-.330	.111	-.073	-1.223
130	423	-.251	.055	-.104	-.574	130	473	-.266	.075	-.073	-.796	140	118	-.332	.130	-.033	-1.400
130	424	-.256	.067	-.092	-.679	130	474	-.247	.077	-.042	-.836	140	119	-.343	.142	.024	-1.442
130	425	-.259	.078	-.065	-.730	130	475	-.255	.086	.027	-1.279	140	120	-.326	.120	-.073	-1.153
130	426	-.271	.080	-.071	-.722	130	476	-.232	.067	.095	-.591	140	121	-.323	.147	.094	-1.222
130	427	-.270	.092	-.037	-.817	130	477	-.248	.061	-.012	-.602	140	122	-.333	.174	.090	-1.378
130	428	-.272	.105	-.005	-.928	130	801	.121	.064	.474	-.098	140	123	-.357	.123	-.060	-1.121
130	429	-.253	.091	-.022	-.760	130	802	.148	.102	.711	-.147	140	124	-.361	.146	-.000	-1.397
130	430	-.248	.066	-.073	-.663	130	803	.061	.092	.666	-.189	140	125	-.364	.160	-.000	-1.376
130	431	-.233	.057	-.068	-.497	130	804	-.294	.090	.075	-.901	140	126	-.336	.166	.057	-1.430
130	432	-.238	.065	-.071	-.723	130	805	-.264	.066	-.036	-.562	140	127	-.291	.129	.107	-1.029
130	433	-.244	.078	-.033	-.914	130	806	-.247	.061	-.067	-.527	140	128	-.289	.165	.097	-1.318
130	434	-.285	.086	-.090	-.928	130	807	-.308	.098	-.079	-.847	140	129	.074	.089	.493	-.210
130	435	-.280	.097	-.046	-1.118	130	808	-.309	.098	-.085	-.807	140	130	-.217	.075	-.018	-.708
130	436	-.277	.110	-.019	-.992	130	809	-.271	.067	-.088	-.574	140	131	-.418	.156	-.083	-1.777
130	437	-.264	.099	-.015	-.908	130	810	-.258	.071	-.040	-.618	140	132	-.429	.193	-.003	-1.974
130	438	-.237	.065	-.068	-.617	130	901	-.436	.120	-.120	-1.174	140	133	-.384	.200	.034	-1.816
130	439	-.226	.056	-.041	-.489	130	902	-.397	.146	.358	-.996	140	134	-.307	.183	.150	-1.569
130	440	-.228	.056	-.064	-.535	130	903	-.411	.133	-.084	-1.062	140	135	-.251	.130	.139	-.984
130	441	-.232	.064	-.045	-.601	130	904	-.435	.101	-.159	-.862	140	136	-.242	.148	.186	-1.257
130	442	-.248	.071	-.054	-.634	130	905	-.436	.126	-.005	-1.110	140	137	-.420	.196	.141	-1.872
130	443	-.245	.079	-.044	-.795	130	906	-.461	.133	-.108	-.962	140	138	-.397	.217	.109	-1.903
130	444	-.240	.084	-.033	-.735	130	907	-.420	.134	-.032	-1.207	140	139	-.302	.169	.067	-1.500
130	445	-.236	.078	-.038	-.710	130	908	-.441	.107	-.145	-.931	140	140	-.215	.136	.204	-1.326
130	446	-.240	.069	-.080	-.718	130	909	-.428	.138	-.075	-1.156	140	141	-.205	.102	.067	-1.014
130	447	-.231	.065	-.024	-.671	130	910	-.436	.121	-.124	-1.087	140	142	-.196	.099	.112	-.939
130	448	-.233	.066	-.047	-.695	130	911	-.442	.130	-.128	-1.223	140	143	.101	.085	.546	-.325
130	449	-.240	.069	-.072	-.850	130	912	-.424	.105	-.142	-.879	140	144	-.176	.061	-.035	-.619
130	450	-.248	.063	-.064	-.617	130	913	-.414	.118	-.097	-.891	140	145	-.371	.167	.558	-1.395
130	451	-.242	.064	-.061	-.585	130	914	-.339	.106	.046	-.840	140	146	-.307	.181	.286	-1.535
130	452	-.227	.072	-.038	-.815	130	915	-.364	.106	-.036	-.801	140	147	-.197	.115	.220	-1.001
130	453	-.228	.074	-.008	-.850	130	916	-.333	.090	-.061	-.796	140	148	-.192	.064	.006	-.706
130	454	-.241	.075	-.085	-.672	130	917	-.313	.088	-.030	-.801	140	149	-.157	.046	.075	-.507
130	455	-.233	.074	.101	-.722	130	918	-.314	.092	-.043	-.739	140	150	-.152	.051	.076	-.480
130	456	-.233	.067	.016	-.905	140	101	-.388	.111	-.083	-1.116	140	151	-.188	.142	.315	-.797
130	457	-.241	.069	-.068	-.790	140	102	-.366	.101	-.077	-.949	140	152	-.134	.116	.198	-.809
130	458	-.258	.069	-.080	-.912	140	103	-.319	.137	.024	-1.195	140	153	-.119	.050	.085	-.427
130	459	-.254	.073	-.066	-.940	140	104	-.333	.099	-.051	-.762	140	154	-.131	.051	.109	-.327
130	460	-.237	.079	.021	-.806	140	105	-.351	.111	-.085	-.893	140	155	-.142	.048	.019	-.340
130	461	-.239	.081	.011	-.779	140	106	-.327	.126	-.005	-1.076	140	156	-.152	.052	.018	-.377
130	462	-.249	.071	-.008	-.974	140	107	-.305	.122	.034	-.958	140	157	.098	.062	.456	-.098
130	463	-.255	.075	-.076	-.720	140	108	-.286	.127	.253	-.972	140	158	-.189	.078	-.013	-.821

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
140	159	-.077	.125	.545	-.640	140	243	-.026	.091	.510	-.396	140	316	.071	.195	.901	-.512
140	160	-.076	.068	.294	-.490	140	244	-.043	.100	.523	-.434	140	317	-.236	.077	-.006	-.598
140	161	-.101	.045	.077	-.292	140	245	-.135	.088	.269	-.592	140	318	.269	.162	.877	-.070
140	162	-.079	.052	.145	-.263	140	246	-.005	.064	.318	-.237	140	319	-.259	.095	-.023	-.854
140	163	-.089	.162	.821	-.687	140	247	.088	.074	.483	-.146	140	320	-.247	.099	.017	-.769
140	164	-.067	.105	.416	-.449	140	248	.143	.081	.549	-.100	140	321	-.263	.147	.074	-1.397
140	165	-.072	.055	.202	-.225	140	249	.131	.077	.520	-.090	140	322	-.273	.138	.051	-1.101
140	166	-.141	.051	.109	-.403	140	250	.094	.082	.537	-.222	140	323	-.365	.214	.234	-1.772
140	201	.003	.251	.919	-.619	140	251	-.017	.098	.441	-.446	140	324	-.378	.185	.183	-1.632
140	202	.090	.285	1.200	-.794	140	252	-.069	.101	.350	-.453	140	325	.034	.155	.783	-.572
140	203	-.190	.200	.616	-.727	140	253	-.178	.082	.227	-.486	140	326	-.001	.155	.616	-.574
140	204	-.122	.187	.642	-.765	140	254	-.036	.065	.285	-.330	140	327	-.239	.111	.034	-1.141
140	205	-.274	.154	.400	-.752	140	255	.055	.076	.427	-.209	140	328	-.245	.091	-.033	-.881
140	206	.253	.192	.948	-.444	140	256	.123	.082	.544	-.109	140	329	-.268	.142	.044	-1.178
140	207	.214	.159	.902	-.215	140	257	.147	.082	.594	-.085	140	330	-.288	.154	.089	-1.171
140	208	.246	.161	.976	-.266	140	258	.126	.082	.517	-.119	140	331	-.328	.175	.121	-1.310
140	209	.187	.172	.812	-.308	140	259	.046	.092	.483	-.413	140	332	-.355	.147	.019	-1.377
140	210	.176	.151	.754	-.272	140	260	-.131	.091	.222	-.583	140	333	-.048	.129	.564	-.674
140	211	.149	.152	.663	-.350	140	261	-.192	.062	.117	-.469	140	334	-.068	.125	.509	-.712
140	212	.269	.198	1.025	-.393	140	262	-.056	.057	.209	-.250	140	335	-.227	.079	-.044	-.765
140	213	.252	.245	1.144	-.699	140	263	.026	.067	.355	-.209	140	336	.121	.092	.650	-.136
140	214	.244	.176	.916	-.193	140	264	.075	.060	.360	-.074	140	337	-.227	.102	.009	-1.246
140	215	.278	.188	1.092	-.139	140	265	.102	.063	.378	-.102	140	338	-.221	.095	.002	-.971
140	216	.270	.185	.967	-.151	140	266	.104	.072	.555	-.101	140	339	-.243	.116	.104	-1.095
140	217	.200	.168	.871	-.213	140	267	.066	.082	.573	-.209	140	340	-.252	.098	-.060	-.906
140	218	.174	.148	.717	-.176	140	268	-.001	.053	.256	-.171	140	341	-.273	.126	-.049	-1.194
140	219	.048	.121	.552	-.308	140	269	.065	.058	.314	-.127	140	342	-.282	.132	-.051	-1.168
140	220	.104	.154	.899	-.420	140	270	.093	.060	.391	-.106	140	343	-.117	.096	.357	-.558
140	221	.067	.186	1.023	-.692	140	271	.101	.060	.408	-.076	140	344	-.126	.081	.288	-.467
140	222	.167	.140	.715	-.230	140	272	.079	.072	.388	-.258	140	345	-.222	.075	-.036	-.764
140	223	.251	.162	.905	-.081	140	273	-.040	.050	.298	-.207	140	346	-.217	.072	-.015	-.608
140	224	.267	.164	.912	-.081	140	274	.003	.091	.510	-.287	140	347	-.237	.093	.034	-.907
140	225	.183	.136	.811	-.097	140	275	.075	.065	.508	-.096	140	348	-.254	.103	.051	-1.081
140	226	.137	.133	.799	-.192	140	276	.115	.060	.459	-.037	140	349	-.253	.105	.001	-1.211
140	227	.004	.110	.502	-.376	140	277	.112	.082	.455	-.090	140	350	-.258	.108	.017	-1.200
140	228	.036	.124	.651	-.576	140	301	-.256	.100	.093	-.696	140	351	-.156	.088	.229	-.570
140	229	-.026	.127	.621	-.476	140	302	-.353	.145	.104	-1.044	140	352	-.166	.067	.128	-.447
140	230	.074	.100	.640	-.174	140	303	-.259	.172	.596	-.961	140	353	-.192	.065	-.041	-.661
140	231	.157	.113	.744	-.192	140	304	-.250	.098	.029	-.880	140	354	.050	.073	.401	-.224
140	232	.185	.116	.803	-.104	140	305	-.152	.142	.236	-1.008	140	355	-.216	.070	-.056	-.855
140	233	.162	.108	.643	-.105	140	306	-.310	.150	.026	-1.044	140	356	-.207	.050	-.060	-.489
140	234	.114	.109	.618	-.182	140	307	-.445	.246	.222	-1.417	140	357	-.214	.067	-.024	-.651
140	235	-.015	.101	.461	-.369	140	308	-.075	.178	.666	-.688	140	358	-.212	.068	-.000	-.680
140	236	-.010	.109	.483	-.443	140	309	-.258	.093	.020	-.872	140	359	-.214	.070	-.023	-.626
140	237	-.088	.108	.498	-.599	140	310	-.235	.066	-.003	-.605	140	360	-.226	.066	-.082	-.765
140	238	.023	.080	.504	-.212	140	311	-.217	.112	.046	-.835	140	361	-.185	.080	.205	-.558
140	239	.112	.090	.679	-.161	140	312	-.242	.176	.219	-1.351	140	362	-.194	.076	.072	-.570
140	240	.154	.095	.743	-.130	140	313	-.378	.242	.361	-1.480	140	363	-.208	.062	-.068	-.584
140	241	.137	.085	.693	-.092	140	314	-.440	.177	.152	-1.345	140	364	-.205	.051	-.070	-.529
140	242	.089	.088	.696	-.189	140	315	.138	.201	.958	-.483	140	365	-.206	.062	-.034	-.656

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
140	366	-.207	.063	-.048	-.630
140	367	-.214	.066	-.020	-.706
140	368	-.224	.060	-.080	-.501
140	369	-.195	.059	.019	-.440
140	370	-.197	.057	-.051	-.440
140	371	-.200	.054	-.033	-.700
140	372	-.030	.058	.306	-.203
140	373	-.211	.061	.009	-.694
140	374	-.213	.061	.031	-.592
140	375	-.219	.065	-.006	-.676
140	376	-.178	.065	.118	-.510
140	377	-.209	.054	-.062	-.596
140	378	-.208	.054	-.014	-.477
140	379	-.209	.056	-.018	-.513
140	380	-.222	.061	-.043	-.564
140	401	-.261	.088	-.014	-.718
140	402	-.250	.081	-.027	-.654
140	403	-.244	.072	-.030	-.684
140	404	-.243	.085	-.033	-.860
140	405	-.303	.113	.001	-1.072
140	406	-.250	.089	-.006	-.702
140	407	-.238	.066	-.030	-.586
140	408	-.228	.070	.001	-.614
140	409	-.227	.072	-.011	-.619
140	410	-.223	.076	-.018	-.631
140	411	-.230	.071	-.052	-.560
140	412	-.251	.086	-.051	-.708
140	413	-.240	.080	-.063	-.652
140	414	-.234	.074	-.050	-.562
140	415	-.224	.059	-.083	-.529
140	416	-.225	.068	-.055	-.634
140	417	-.226	.072	-.032	-.617
140	418	-.229	.075	-.025	-.619
140	419	-.229	.072	-.030	-.694
140	420	-.248	.087	-.014	-.727
140	421	-.230	.075	-.042	-.633
140	422	-.223	.067	-.029	-.635
140	423	-.213	.047	-.059	-.445
140	424	-.224	.063	-.035	-.525
140	425	-.227	.074	-.015	-.663
140	426	-.242	.087	-.042	-.914
140	427	-.247	.100	-.021	-1.079
140	428	-.241	.100	-.006	-.744
140	429	-.223	.085	-.022	-.672
140	430	-.233	.079	-.066	-.639
140	431	-.225	.066	-.055	-.629
140	432	-.239	.088	-.049	-.824
140	433	-.248	.108	-.002	-1.106
140	434	-.244	.090	-.037	-1.003
140	435	-.247	.103	.033	-1.142
140	436	-.220	.094	.104	-.845
140	437	-.211	.082	.035	-.751
140	438	-.208	.065	-.073	-.612
140	439	-.197	.052	-.023	-.455
140	440	-.201	.062	-.049	-.732
140	441	-.211	.077	-.025	-.859
140	442	-.229	.087	-.033	-.869
140	443	-.232	.100	-.016	-.999
140	444	-.187	.076	.064	-.640
140	445	-.165	.071	.038	-.578
140	446	-.179	.052	-.030	-.529
140	447	-.174	.049	-.026	-.499
140	448	-.174	.050	-.025	-.525
140	449	-.181	.058	.001	-.670
140	450	-.204	.062	-.016	-.574
140	451	-.199	.064	-.011	-.644
140	452	-.160	.055	-.006	-.471
140	453	-.161	.055	-.005	-.481
140	454	-.172	.052	-.028	-.596
140	455	-.169	.049	-.002	-.416
140	456	-.174	.048	.015	-.431
140	457	-.186	.050	-.034	-.587
140	458	-.192	.051	-.073	-.485
140	459	-.189	.054	-.053	-.529
140	460	-.156	.051	.001	-.475
140	461	-.158	.054	-.006	-.481
140	462	-.173	.056	-.028	-.716
140	463	-.183	.065	.019	-.619
140	464	-.174	.053	.093	-.454
140	465	-.209	.068	.027	-.678
140	466	-.196	.058	-.050	-.582
140	467	-.222	.087	-.008	-.777
140	468	-.189	.092	.085	-.694
140	469	-.188	.075	.014	-.702
140	470	-.176	.064	.068	-.552
140	471	-.179	.067	.108	-.566
140	472	-.189	.068	.131	-.617
140	473	-.196	.075	.014	-.725
140	474	-.180	.076	.076	-.562
140	475	-.196	.087	.044	-.691
140	476	-.174	.066	.109	-.532
140	477	-.194	.054	-.034	-.526
140	801	.109	.057	.378	-.060
140	802	.077	.078	.458	-.196
140	803	.009	.070	.378	-.183
140	804	-.229	.083	.055	-.845
140	805	-.191	.052	.011	-.471
140	806	-.190	.048	.004	-.435
140	807	-.215	.053	-.049	-.449
140	808	-.220	.056	-.051	-.482
140	809	-.213	.049	-.031	-.459
140	810	-.207	.054	-.044	-.577
140	901	-.369	.097	-.107	-.732
140	902	-.315	.132	.204	-.819
140	903	-.344	.137	.280	-.948
140	904	-.417	.102	-.155	-.909
140	905	-.409	.129	-.052	-.965
140	906	-.450	.136	-.057	-1.118
140	907	-.439	.159	-.050	-1.121
140	908	-.387	.096	-.077	-.745
140	909	-.354	.110	-.022	-.948
140	910	-.421	.119	-.057	-1.002
140	911	-.432	.127	-.064	-.961
140	912	-.425	.108	-.077	-.836
140	913	-.425	.126	-.043	-1.015
140	914	-.299	.114	.061	-.797
140	915	-.344	.105	-.020	-.895
140	916	-.319	.093	-.064	-.819
140	917	-.281	.090	-.022	-.840
140	918	-.295	.099	-.028	-.802
150	101	-.288	.100	-.030	-.730
150	102	-.249	.082	-.032	-.684
150	103	-.240	.110	.038	-.792
150	104	-.215	.070	-.040	-.642
150	105	-.228	.078	-.039	-.694
150	106	-.224	.092	.003	-.925
150	107	-.225	.092	.021	-.864
150	108	-.223	.101	.062	-.835
150	109	-.203	.062	-.048	-.581
150	110	-.203	.072	-.027	-.672
150	111	-.213	.077	.029	-.697
150	112	-.219	.081	.069	-.747
150	113	-.232	.076	-.030	-.774
150	114	-.225	.096	.011	-.895
150	115	.075	.117	.486	-.225
150	116	-.180	.059	-.002	-.441
150	117	-.215	.065	-.023	-.515
150	118	-.216	.076	.016	-.599
150	119	-.224	.083	.002	-.695
150	120	-.233	.078	-.005	-.678
150	121	-.241	.095	.033	-.733
150	122	-.248	.110	.021	-.860
150	123	-.252	.094	-.025	-.927
150	124	-.256	.110	.011	-1.128
150	125	-.260	.115	.043	-1.194
150	126	-.257	.115	.031	-1.008
150	127	-.253	.099	-.005	-.811
150	128	-.259	.125	.016	-.996
150	129	.010	.072	.394	-.247
150	130	-.190	.066	-.012	-.505

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
150	131	-.301	.122	-.008	-1.414
150	132	-.303	.146	.028	-1.768
150	133	-.288	.143	.031	-1.150
150	134	-.255	.135	.090	-1.022
150	135	-.221	.102	.037	-.932
150	136	-.218	.124	.054	-1.229
150	137	-.286	.147	.101	-1.380
150	138	-.265	.160	.164	-1.542
150	139	-.222	.120	.029	-1.110
150	140	-.176	.106	.345	-.954
150	141	-.163	.099	.100	-.990
150	142	-.159	.090	.050	-1.027
150	143	.007	.052	.256	-.284
150	144	-.139	.056	.083	-.431
150	145	-.236	.135	.168	-1.257
150	146	-.195	.141	.116	-1.138
150	147	-.143	.102	.171	-1.098
150	148	-.123	.053	.150	-.521
150	149	-.115	.040	.116	-.418
150	150	-.114	.043	.109	-.429
150	151	-.097	.088	.244	-.736
150	152	-.076	.071	.152	-.704
150	153	-.081	.041	.056	-.431
150	154	-.093	.040	.094	-.245
150	155	-.098	.039	.046	-.250
150	156	-.102	.040	.043	-.313
150	157	.032	.041	.269	-.080
150	158	-.125	.047	.051	-.546
150	159	-.056	.079	.261	-.426
150	160	-.058	.051	.133	-.460
150	161	-.073	.036	.074	-.233
150	162	-.064	.039	.114	-.225
150	163	-.053	.089	.438	-.436
150	164	-.047	.059	.266	-.242
150	165	-.048	.040	.239	-.181
150	166	-.096	.045	.231	-.250
150	201	-.007	.232	1.071	-.629
150	202	.119	.248	.843	-.696
150	203	-.108	.172	.609	-.741
150	204	-.095	.154	.511	-.744
150	205	-.176	.119	.405	-.569
150	206	.214	.185	.952	-.356
150	207	.168	.156	.857	-.238
150	208	.150	.138	.714	-.169
150	209	.145	.162	.940	-.304
150	210	.096	.126	.658	-.208
150	211	.086	.132	.652	-.270
150	212	.199	.169	.843	-.371
150	213	.222	.197	1.013	-.477
150	214	.216	.180	1.034	-.279
150	215	.185	.169	.989	-.212
150	216	.167	.152	.889	-.194
150	217	.089	.125	.703	-.256
150	218	.114	.120	.665	-.205
150	219	.006	.089	.380	-.298
150	220	.112	.131	.759	-.327
150	221	.146	.159	.852	-.652
150	222	.146	.122	.705	-.156
150	223	.151	.125	.749	-.157
150	224	.143	.119	.701	-.129
150	225	.070	.095	.579	-.235
150	226	.049	.099	.476	-.260
150	227	-.038	.078	.285	-.306
150	228	.011	.097	.539	-.313
150	229	.037	.114	.523	-.348
150	230	.070	.100	.607	-.210
150	231	.097	.093	.582	-.168
150	232	.099	.088	.615	-.214
150	233	.045	.080	.550	-.168
150	234	.023	.085	.455	-.245
150	235	-.062	.082	.338	-.359
150	236	-.037	.083	.312	-.365
150	237	-.031	.093	.424	-.407
150	238	.011	.075	.372	-.217
150	239	.057	.073	.495	-.175
150	240	.074	.074	.566	-.138
150	241	.046	.073	.503	-.203
150	242	.018	.077	.387	-.363
150	243	-.064	.083	.321	-.460
150	244	-.067	.078	.251	-.443
150	245	-.097	.085	.220	-.478
150	246	-.037	.060	.284	-.270
150	247	.019	.058	.256	-.199
150	248	.053	.059	.350	-.119
150	249	.038	.057	.343	-.159
150	250	.020	.064	.382	-.207
150	251	-.046	.085	.259	-.458
150	252	-.091	.068	.322	-.439
150	253	-.142	.067	.176	-.417
150	254	-.065	.051	.221	-.338
150	255	-.009	.054	.268	-.182
150	256	.040	.056	.334	-.173
150	257	.056	.061	.358	-.277
150	258	.053	.067	.342	-.142
150	259	.017	.083	.447	-.284
150	260	-.113	.057	.137	-.379
150	261	-.136	.045	.073	-.373
150	262	-.056	.048	.134	-.230
150	263	.002	.049	.184	-.150
150	264	.016	.048	.246	-.135
150	265	.028	.051	.255	-.186
150	266	.049	.062	.445	-.162
150	267	.044	.074	.464	-.252
150	268	-.030	.045	.151	-.188
150	269	.001	.048	.203	-.141
150	270	.028	.044	.239	-.104
150	271	.038	.046	.260	-.143
150	272	.042	.056	.308	-.230
150	273	-.050	.040	.175	-.189
150	274	-.078	.075	.204	-.335
150	275	.012	.044	.188	-.138
150	276	.046	.043	.316	-.068
150	277	.077	.069	.407	-.164
150	301	-.191	.085	.140	-.581
150	302	-.229	.133	.252	-.856
150	303	-.136	.169	.706	-.844
150	304	-.200	.075	.017	-.608
150	305	-.056	.099	.394	-.621
150	306	-.172	.078	.092	-.661
150	307	-.249	.210	.288	-1.268
150	308	.049	.162	.824	-.578
150	309	-.195	.062	-.030	-.551
150	310	-.185	.052	-.052	-.434
150	311	-.123	.065	.204	-.517
150	312	-.093	.109	.381	-.998
150	313	-.169	.214	.537	-1.088
150	314	-.302	.193	.404	-1.046
150	315	.221	.184	.843	-.433
150	316	.184	.181	.869	-.402
150	317	-.193	.061	-.007	-.493
150	318	.228	.145	.908	-.186
150	319	-.205	.059	-.049	-.556
150	320	-.199	.063	-.001	-.599
150	321	-.157	.075	.088	-.861
150	322	-.140	.102	.236	-.873
150	323	-.216	.206	.319	-1.226
150	324	-.307	.205	.559	-1.425
150	325	.120	.142	.826	-.421
150	326	.103	.136	.677	-.297
150	327	-.211	.086	.083	-1.050
150	328	-.201	.061	-.032	-.615
150	329	-.177	.072	.058	-.708
150	330	-.181	.102	.082	-.877
150	331	-.250	.156	.230	-1.205
150	332	-.343	.141	.177	-1.150
150	333	.020	.108	.586	-.411
150	334	.004	.106	.568	-.433
150	335	-.200	.079	-.030	-.795
150	336	.071	.075	.572	-.152
150	337	-.209	.096	-.007	-.874

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
150	338	-.199	.087	-.004	-.727	150	408	-.174	.061	-.006	-.494	150	458	-.143	.043	-.007	-.361
150	339	-.190	.075	.030	-.663	150	409	-.177	.063	.020	-.529	150	459	-.140	.050	-.001	-.446
150	340	-.210	.078	.080	-.834	150	410	-.177	.064	.028	-.481	150	460	-.103	.039	.061	-.280
150	341	-.266	.124	.154	-.886	150	411	-.189	.057	-.016	-.506	150	461	-.105	.040	.047	-.289
150	342	-.303	.133	.132	-.993	150	412	-.199	.065	-.008	-.489	150	462	-.106	.034	.091	-.245
150	343	-.057	.084	.354	-.414	150	413	-.190	.063	.006	-.512	150	463	-.123	.039	-.002	-.434
150	344	-.070	.068	.245	-.337	150	414	-.187	.063	-.020	-.561	150	464	-.114	.036	.013	-.246
150	345	-.179	.076	.073	-.825	150	415	-.186	.057	-.036	-.543	150	465	-.144	.044	.013	-.455
150	346	-.171	.068	.029	-.616	150	416	-.189	.064	-.021	-.547	150	466	-.136	.042	.016	-.351
150	347	-.180	.066	.009	-.542	150	417	-.190	.065	-.026	-.478	150	467	-.163	.054	-.017	-.574
150	348	-.215	.089	.055	-.696	150	418	-.194	.065	-.027	-.514	150	468	-.125	.053	.019	-.505
150	349	-.214	.087	.028	-.720	150	419	-.188	.056	-.039	-.486	150	469	-.131	.058	.028	-.567
150	350	-.226	.096	-.023	-.969	150	420	-.204	.066	.050	-.567	150	470	-.122	.052	.031	-.455
150	351	-.115	.073	.198	-.409	150	421	-.192	.058	.020	-.567	150	471	-.124	.048	.079	-.346
150	352	-.128	.058	.165	-.386	150	422	-.191	.058	-.036	-.614	150	472	-.131	.048	.052	-.347
150	353	-.152	.049	.096	-.552	150	423	-.183	.050	-.061	-.484	150	473	-.131	.052	.055	-.398
150	354	-.012	.057	.309	-.222	150	424	-.190	.062	-.035	-.572	150	474	-.121	.055	.049	-.435
150	355	-.155	.044	-.014	-.412	150	425	-.188	.064	-.015	-.538	150	475	-.128	.058	.031	-.444
150	356	-.156	.035	-.003	-.325	150	426	-.194	.055	-.048	-.555	150	476	-.116	.047	.047	-.305
150	357	-.163	.048	-.002	-.458	150	427	-.192	.062	-.033	-.574	150	477	-.133	.041	-.004	-.356
150	358	-.166	.048	-.027	-.414	150	428	-.210	.072	.018	-.628	150	801	.052	.042	.244	-.092
150	359	-.172	.053	-.021	-.505	150	429	-.195	.062	-.013	-.526	150	802	.027	.056	.251	-.159
150	360	-.178	.049	-.069	-.500	150	430	-.191	.054	-.046	-.442	150	803	-.010	.055	.233	-.167
150	361	-.156	.057	.107	-.440	150	431	-.191	.061	-.038	-.594	150	804	-.131	.053	.026	-.407
150	362	-.162	.055	.079	-.376	150	432	-.206	.079	-.033	-.792	150	805	-.115	.037	.083	-.279
150	363	-.147	.042	.081	-.391	150	433	-.211	.086	.002	-.822	150	806	-.120	.040	.012	-.347
150	364	-.146	.033	-.045	-.281	150	434	-.200	.069	-.046	-.764	150	807	-.151	.045	-.018	-.383
150	365	-.148	.043	-.021	-.281	150	435	-.201	.076	.017	-.690	150	808	-.154	.047	-.022	-.414
150	366	-.147	.043	-.018	-.367	150	436	-.188	.075	.011	-.570	150	809	-.148	.038	-.032	-.317
150	367	-.148	.044	.009	-.347	150	437	-.180	.067	.006	-.535	150	810	-.137	.043	.041	-.327
150	368	-.157	.037	-.049	-.466	150	438	-.176	.055	.011	-.644	150	901	-.263	.084	-.029	-.686
150	369	-.146	.042	.003	-.344	150	439	-.173	.056	-.041	-.544	150	902	-.227	.122	.278	-.847
150	370	-.144	.041	-.020	-.322	150	440	-.189	.077	-.045	-.928	150	903	-.265	.143	.248	-.925
150	371	-.129	.042	-.006	-.334	150	441	-.199	.094	-.015	-.807	150	904	-.329	.086	-.107	-.685
150	372	-.041	.053	.175	-.228	150	442	-.215	.088	-.041	-.715	150	905	-.301	.125	.038	-.872
150	373	-.138	.040	.014	-.343	150	443	-.221	.102	.004	-1.004	150	906	-.358	.121	.036	-.890
150	374	-.140	.043	.017	-.340	150	444	-.153	.057	.028	-.480	150	907	-.310	.137	.160	-.967
150	375	-.148	.045	-.001	-.465	150	445	-.151	.054	.002	-.424	150	908	-.277	.080	.038	-.602
150	376	-.115	.048	.045	-.297	150	446	-.146	.041	.023	-.346	150	909	-.242	.081	-.017	-.701
150	377	-.129	.045	.100	-.353	150	447	-.143	.041	.022	-.376	150	910	-.331	.108	-.031	-.816
150	378	-.131	.046	.065	-.362	150	448	-.152	.051	-.014	-.669	150	911	-.349	.113	-.028	-.801
150	379	-.133	.049	.069	-.383	150	449	-.158	.063	.004	-.642	150	912	-.290	.091	.065	-.771
150	380	-.149	.052	.100	-.384	150	450	-.179	.070	-.014	-1.010	150	913	-.315	.107	-.034	-.764
150	401	-.200	.072	.013	-.608	150	451	-.182	.081	-.011	-.964	150	914	-.222	.095	.094	-.747
150	402	-.192	.070	.013	-.559	150	452	-.118	.043	.059	-.415	150	915	-.229	.084	.108	-.648
150	403	-.197	.062	-.011	-.486	150	453	-.119	.043	.101	-.308	150	916	-.231	.071	.006	-.626
150	404	-.206	.080	.004	-.655	150	454	-.115	.035	.016	-.302	150	917	-.210	.069	-.027	-.503
150	405	-.279	.103	-.009	-.795	150	455	-.114	.036	.027	-.252	150	918	-.224	.078	-.002	-.581
150	406	-.193	.073	.028	-.583	150	456	-.121	.036	.008	-.299	160	101	-.206	.077	-.007	-.586
150	407	-.176	.056	-.041	-.538	150	457	-.130	.040	.006	-.375	160	102	-.176	.065	.003	-.639

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
160	103	-.173	.080	.069	-.583	160	153	-.080	.032	.025	-.393	160	237	-.045	.057	.228	-.225
160	104	-.158	.058	.009	-.431	160	154	-.081	.032	.025	-.210	160	238	-.047	.060	.198	-.310
160	105	-.163	.062	.008	-.426	160	155	-.083	.032	.021	-.219	160	239	-.033	.055	.251	-.310
160	106	-.160	.067	.032	-.752	160	156	-.088	.033	.024	-.225	160	240	-.026	.052	.244	-.209
160	107	-.160	.070	.052	-.863	160	157	-.020	.032	.108	-.114	160	241	-.042	.053	.243	-.273
160	108	-.161	.077	.139	-.879	160	158	-.099	.032	.005	-.332	160	242	-.047	.056	.270	-.333
160	109	-.149	.047	-.029	-.374	160	159	-.064	.049	.104	-.425	160	243	-.097	.056	.133	-.449
160	110	-.150	.055	-.013	-.415	160	160	-.064	.036	.074	-.347	160	244	-.086	.051	.099	-.297
160	111	-.153	.057	-.013	-.434	160	161	-.073	.030	.035	-.205	160	245	-.083	.049	.130	-.315
160	112	-.158	.058	-.013	-.512	160	162	-.068	.033	.060	-.212	160	246	-.068	.046	.164	-.263
160	113	-.162	.054	-.017	-.430	160	163	-.071	.052	.160	-.269	160	247	-.047	.048	.192	-.258
160	114	-.162	.066	-.000	-.557	160	164	-.066	.042	.116	-.227	160	248	-.029	.049	.244	-.195
160	115	-.033	.085	.449	-.379	160	165	-.062	.030	.062	-.222	160	249	-.038	.042	.155	-.222
160	116	-.151	.050	-.006	-.470	160	166	-.077	.031	.057	-.200	160	250	-.044	.047	.143	-.266
160	117	-.156	.049	.003	-.510	160	201	-.082	.168	.620	-.579	160	251	-.063	.062	.183	-.376
160	118	-.153	.057	.012	-.562	160	202	.055	.188	.741	-.765	160	252	-.098	.042	.070	-.297
160	119	-.160	.060	.009	-.580	160	203	-.117	.135	.457	-.721	160	253	-.106	.041	.060	-.273
160	120	-.176	.055	-.031	-.444	160	204	-.109	.117	.404	-.808	160	254	-.086	.039	.107	-.209
160	121	-.180	.067	-.013	-.542	160	205	-.165	.086	.304	-.627	160	255	-.066	.040	.214	-.246
160	122	-.188	.074	-.022	-.707	160	206	.138	.153	.826	-.217	160	256	-.046	.041	.193	-.204
160	123	-.174	.059	-.021	-.528	160	207	.070	.130	.627	-.465	160	257	-.037	.040	.100	-.184
160	124	-.175	.068	-.005	-.587	160	208	.070	.109	.593	-.236	160	258	-.031	.042	.100	-.178
160	125	-.182	.071	-.006	-.662	160	209	.055	.129	.756	-.309	160	259	-.044	.055	.155	-.290
160	126	-.190	.075	-.011	-.653	160	210	.035	.099	.482	-.220	160	260	-.090	.035	.036	-.214
160	127	-.193	.060	-.034	-.501	160	211	.042	.108	.545	-.271	160	261	-.100	.033	.007	-.222
160	128	-.197	.075	.022	-.702	160	212	.179	.146	.835	-.221	160	262	-.060	.038	.129	-.180
160	129	-.057	.054	.191	-.291	160	213	.192	.151	.838	-.214	160	263	-.022	.045	.229	-.137
160	130	-.161	.049	-.018	-.376	160	214	.124	.147	.774	-.461	160	264	-.042	.037	.123	-.168
160	131	-.207	.070	-.017	-.694	160	215	.086	.134	.738	-.315	160	265	-.036	.036	.102	-.200
160	132	-.210	.083	-.005	-.899	160	216	.082	.122	.781	-.280	160	266	-.021	.037	.125	-.153
160	133	-.212	.087	.004	-.880	160	217	.011	.104	.535	-.454	160	267	-.024	.042	.157	-.201
160	134	-.206	.084	.003	-.662	160	218	.040	.094	.472	-.242	160	268	-.053	.037	.128	-.178
160	135	-.199	.080	.001	-.652	160	219	-.032	.071	.321	-.292	160	269	-.058	.049	.112	-.265
160	136	-.201	.104	.022	-1.159	160	220	.107	.130	.835	-.206	160	270	-.031	.042	.133	-.209
160	137	-.228	.111	-.006	-1.007	160	221	.131	.133	.749	-.260	160	271	-.027	.039	.143	-.174
160	138	-.227	.118	-.010	-1.170	160	222	.078	.119	.618	-.386	160	272	-.024	.041	.128	-.236
160	139	-.201	.093	-.002	-1.053	160	223	.056	.102	.604	-.307	160	273	-.057	.034	.111	-.171
160	140	-.163	.083	.105	-.582	160	224	.046	.091	.546	-.273	160	274	-.085	.060	.151	-.268
160	141	-.133	.075	.034	-.649	160	225	-.011	.073	.407	-.230	160	275	-.041	.039	.161	-.172
160	142	-.143	.074	.028	-.770	160	226	-.004	.079	.398	-.310	160	276	-.021	.034	.211	-.139
160	143	-.035	.051	.163	-.227	160	227	-.066	.059	.261	-.313	160	277	-.001	.045	.222	-.141
160	144	-.104	.036	.003	-.300	160	228	.010	.087	.372	-.260	160	301	-.170	.084	.184	-.542
160	145	-.178	.096	.050	-.949	160	229	.032	.091	.527	-.278	160	302	-.118	.108	.353	-.625
160	146	-.155	.097	.045	-.805	160	230	.013	.095	.615	-.408	160	303	-.057	.163	.589	-.707
160	147	-.125	.074	.064	-.627	160	231	.010	.078	.531	-.238	160	304	-.185	.067	.073	-.463
160	148	-.099	.036	.025	-.327	160	232	.010	.070	.438	-.195	160	305	-.012	.093	.452	-.514
160	149	-.100	.034	.018	-.310	160	233	-.040	.057	.188	-.323	160	306	-.134	.083	.292	-.662
160	150	-.099	.037	.030	-.300	160	234	-.035	.062	.257	-.400	160	307	-.066	.177	.713	-.930
160	151	-.098	.059	.095	-.446	160	235	-.089	.055	.115	-.441	160	308	.087	.159	.865	-.435
160	152	-.088	.052	.081	-.394	160	236	-.048	.065	.366	-.260	160	309	-.210	.075	-.005	-.603

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
160	310	-.197	.054	-.052	-.424	160	360	-.129	.040	.038	-.335	160	430	-.171	.053	-.041	-.450
160	311	-.098	.062	.341	-.383	160	361	-.107	.039	.067	-.246	160	431	-.190	.069	-.025	-.514
160	312	-.039	.093	.723	-.590	160	362	-.113	.040	.029	-.243	160	432	-.214	.086	-.009	-.929
160	313	-.026	.162	.974	-.972	160	363	-.101	.033	.021	-.209	160	433	-.216	.091	.017	-1.117
160	314	-.112	.177	.493	-.981	160	364	-.101	.029	.002	-.210	160	434	-.229	.083	-.043	-.765
160	315	.170	.146	.838	-.475	160	365	-.097	.034	.017	-.251	160	435	-.226	.089	-.017	-.786
160	316	.153	.147	.795	-.430	160	366	-.096	.034	.010	-.270	160	436	-.148	.057	.008	-.445
160	317	-.180	.066	.019	-.545	160	367	-.098	.035	.016	-.286	160	437	-.138	.051	.026	-.371
160	318	.162	.120	.803	-.124	160	368	-.103	.028	-.009	-.251	160	438	-.140	.046	-.023	-.391
160	319	-.226	.067	-.025	-.541	160	369	-.094	.032	.012	-.211	160	439	-.153	.060	-.002	-.521
160	320	-.213	.070	-.023	-.569	160	370	-.094	.034	.025	-.210	160	440	-.179	.084	-.018	-.725
160	321	-.130	.061	.059	-.568	160	371	-.101	.030	.012	-.215	160	441	-.194	.096	-.007	-.802
160	322	-.077	.071	.201	-.568	160	372	-.093	.036	.143	-.187	160	442	-.212	.084	-.033	-.856
160	323	-.066	.153	.516	-1.061	160	373	-.105	.030	.005	-.254	160	443	-.210	.087	-.022	-.831
160	324	-.157	.194	.568	-1.127	160	374	-.102	.034	.028	-.278	160	444	-.112	.049	.008	-.428
160	325	.120	.137	.821	-.251	160	375	-.107	.034	.043	-.367	160	445	-.107	.046	.010	-.374
160	326	.111	.130	.848	-.246	160	376	-.094	.036	.050	-.224	160	446	-.109	.038	.019	-.405
160	327	-.236	.096	-.001	-.865	160	377	-.101	.032	.020	-.276	160	447	-.113	.038	.028	-.294
160	328	-.240	.069	-.072	-.593	160	378	-.099	.036	.028	-.288	160	448	-.128	.047	.033	-.418
160	329	-.147	.060	.109	-.535	160	379	-.102	.037	.029	-.296	160	449	-.140	.061	.031	-.693
160	330	-.098	.075	.209	-.588	160	380	-.109	.038	.008	-.285	160	450	-.162	.063	-.004	-.644
160	331	-.096	.122	.286	-.979	160	401	-.164	.076	.028	-.679	160	451	-.163	.065	-.002	-.763
160	332	-.143	.122	.414	-.812	160	402	-.165	.074	.060	-.667	160	452	-.094	.034	.023	-.234
160	333	.023	.101	.588	-.256	160	403	-.171	.066	.056	-.489	160	453	-.092	.034	.026	-.232
160	334	.008	.099	.566	-.279	160	404	-.182	.080	.026	-.597	160	454	-.094	.028	-.006	-.208
160	335	-.227	.096	-.012	-.873	160	405	-.222	.090	-.006	-.607	160	455	-.094	.030	.011	-.241
160	336	.008	.075	.363	-.178	160	406	-.146	.068	.062	-.544	160	456	-.101	.032	.011	-.345
160	337	-.219	.095	.102	-.827	160	407	-.157	.064	.011	-.625	160	457	-.105	.037	.017	-.355
160	338	-.222	.086	-.002	-.712	160	408	-.164	.070	.031	-.551	160	458	-.119	.039	-.018	-.344
160	339	-.144	.059	.094	-.498	160	409	-.168	.069	.023	-.476	160	459	-.120	.044	.005	-.433
160	340	-.109	.054	.154	-.465	160	410	-.167	.069	.033	-.516	160	460	-.089	.031	.001	-.212
160	341	-.111	.089	.246	-.692	160	411	-.181	.059	-.021	-.479	160	461	-.086	.031	.005	-.213
160	342	-.140	.114	.312	-.878	160	412	-.157	.060	.000	-.508	160	462	-.089	.029	.019	-.211
160	343	-.038	.068	.270	-.263	160	413	-.154	.057	.001	-.454	160	463	-.101	.027	.003	-.199
160	344	-.057	.057	.174	-.249	160	414	-.159	.059	.015	-.492	160	464	-.091	.030	.013	-.202
160	345	-.163	.077	.114	-.615	160	415	-.164	.055	.014	-.531	160	465	-.108	.033	.014	-.256
160	346	-.165	.069	.051	-.598	160	416	-.171	.063	.051	-.531	160	466	-.097	.033	-.002	-.260
160	347	-.130	.046	.031	-.434	160	417	-.172	.065	.112	-.597	160	467	-.117	.037	.029	-.342
160	348	-.134	.056	.077	-.448	160	418	-.177	.064	-.002	-.655	160	468	-.100	.033	.015	-.241
160	349	-.109	.061	.141	-.405	160	419	-.166	.053	-.033	-.435	160	469	-.100	.030	.005	-.262
160	350	-.125	.070	.104	-.495	160	420	-.163	.051	-.020	-.425	160	470	-.099	.034	.022	-.244
160	351	-.082	.052	.120	-.251	160	421	-.159	.048	-.009	-.369	160	471	-.100	.034	.028	-.241
160	352	-.093	.044	.225	-.266	160	422	-.166	.053	-.030	-.407	160	472	-.102	.036	.035	-.250
160	353	-.117	.045	.074	-.540	160	423	-.175	.054	-.033	-.504	160	473	-.107	.034	-.004	-.255
160	354	-.069	.047	.355	-.284	160	424	-.184	.067	-.004	-.585	160	474	-.098	.037	.022	-.300
160	355	-.113	.043	.134	-.446	160	425	-.181	.068	-.002	-.577	160	475	-.100	.036	.079	-.335
160	356	-.116	.033	.002	-.254	160	426	-.199	.061	-.036	-.499	160	476	-.095	.035	.031	-.236
160	357	-.110	.037	.032	-.278	160	427	-.193	.065	-.017	-.516	160	477	-.101	.026	-.014	-.226
160	358	-.109	.039	.065	-.270	160	428	-.161	.050	-.004	-.396	160	801	.001	.036	.155	-.106
160	359	-.114	.045	.061	-.296	160	429	-.153	.048	.005	-.371	160	802	-.026	.048	.159	-.159

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
160	803	-.042	.040	.176	-.153	170	125	-.161	.062	-.016	-.530	170	209	.041	.118	.624	-.265
160	804	-.100	.037	.020	-.273	170	126	-.168	.061	-.025	-.466	170	210	.021	.094	.390	-.251
160	805	-.100	.027	-.029	-.247	170	127	-.178	.052	-.044	-.403	170	211	.035	.104	.479	-.307
160	806	-.102	.032	-.001	-.209	170	128	-.180	.059	-.027	-.483	170	212	.188	.169	1.019	-.210
160	807	-.111	.033	-.011	-.258	170	129	-.090	.049	.122	-.282	170	213	.200	.171	1.022	-.303
160	808	-.114	.034	-.010	-.275	170	130	-.191	.063	.007	-.539	170	214	.122	.178	.796	-.400
160	809	-.110	.029	.003	-.242	170	131	-.154	.062	-.012	-.725	170	215	.063	.129	.629	-.358
160	810	-.104	.034	.031	-.278	170	132	-.157	.072	.005	-.935	170	216	.066	.113	.531	-.502
160	901	-.202	.076	.024	-.683	170	133	-.160	.075	.005	-1.042	170	217	-.021	.081	.335	-.363
160	902	-.193	.114	.214	-.723	170	134	-.173	.072	.036	-.785	170	218	.030	.093	.405	-.216
160	903	-.265	.141	.286	-.946	170	135	-.183	.062	.066	-.569	170	219	-.042	.063	.272	-.305
160	904	-.279	.076	-.077	-.592	170	136	-.187	.073	.015	-.880	170	220	.159	.151	.813	-.186
160	905	-.213	.099	.160	-.793	170	137	-.150	.082	.070	-1.212	170	221	.185	.159	.871	-.205
160	906	-.297	.111	-.001	-.796	170	138	-.155	.085	.031	-1.324	170	222	.100	.150	.893	-.607
160	907	-.207	.110	.252	-.860	170	139	-.151	.060	-.017	-.620	170	223	.057	.114	.744	-.307
160	908	-.206	.073	-.009	-.390	170	140	-.157	.065	.023	-.533	170	224	.043	.093	.636	-.208
160	909	-.184	.073	.017	-.663	170	141	-.151	.070	.043	-.831	170	225	-.041	.059	.208	-.243
160	910	-.268	.102	.006	-.808	170	142	-.173	.087	.036	-1.030	170	226	-.017	.072	.323	-.221
160	911	-.293	.104	-.073	-.741	170	143	-.089	.042	.043	-.323	170	227	-.070	.050	.170	-.276
160	912	-.220	.073	.090	-.597	170	144	-.112	.041	.012	-.391	170	228	.085	.112	.619	-.215
160	913	-.268	.091	.049	-.707	170	145	-.151	.077	.010	-.932	170	229	.124	.113	.644	-.221
160	914	-.190	.091	.231	-.609	170	146	-.155	.081	-.004	-.939	170	230	.053	.138	.691	-.445
160	915	-.173	.073	.199	-.488	170	147	-.157	.079	.066	-.928	170	231	.025	.100	.521	-.306
160	916	-.183	.060	.039	-.599	170	148	-.124	.055	.053	-.449	170	232	.018	.081	.420	-.239
160	917	-.188	.071	.066	-.531	170	149	-.122	.046	.032	-.310	170	233	-.055	.052	.190	-.211
160	918	-.197	.074	.093	-.523	170	150	-.121	.059	.043	-.466	170	234	-.031	.064	.300	-.238
170	101	-.201	.083	.049	-.591	170	151	-.134	.062	.005	-.590	170	235	-.079	.046	.131	-.281
170	102	-.153	.066	.026	-.505	170	152	-.137	.066	.014	-.553	170	236	.015	.077	.444	-.337
170	103	-.162	.081	.053	-.628	170	153	-.119	.056	.054	-.567	170	237	.038	.081	.524	-.198
170	104	-.138	.059	.040	-.542	170	154	-.081	.044	.135	-.361	170	238	-.023	.104	.484	-.471
170	105	-.141	.062	.034	-.530	170	155	-.067	.036	.113	-.231	170	239	-.028	.077	.646	-.394
170	106	-.143	.065	.070	-.446	170	156	-.072	.034	.108	-.199	170	240	-.026	.066	.532	-.217
170	107	-.146	.067	.086	-.609	170	157	-.054	.030	.095	-.195	170	241	-.074	.045	.218	-.268
170	108	-.147	.073	.115	-.825	170	158	-.081	.033	.060	-.284	170	242	-.054	.053	.259	-.251
170	109	-.141	.049	.037	-.457	170	159	-.119	.062	.060	-.674	170	243	-.090	.044	.109	-.318
170	110	-.138	.056	.065	-.483	170	160	-.090	.048	.106	-.375	170	244	-.031	.052	.254	-.243
170	111	-.144	.058	.051	-.487	170	161	-.059	.035	.081	-.178	170	245	-.023	.049	.185	-.203
170	112	-.145	.058	.054	-.602	170	162	-.047	.037	.142	-.179	170	246	-.071	.065	.252	-.361
170	113	-.151	.049	.027	-.420	170	163	-.111	.066	.110	-.750	170	247	-.062	.052	.266	-.303
170	114	-.153	.060	.065	-.478	170	164	-.080	.054	.172	-.471	170	248	-.057	.048	.206	-.248
170	115	-.066	.067	.283	-.322	170	165	-.042	.041	.181	-.391	170	249	-.081	.037	.066	-.241
170	116	-.163	.061	.026	-.579	170	166	-.041	.042	.262	-.274	170	250	-.069	.041	.086	-.233
170	117	-.155	.050	-.022	-.474	170	201	-.132	.179	.532	-.764	170	251	-.088	.059	.123	-.357
170	118	-.154	.058	-.007	-.516	170	202	-.018	.224	.821	-.792	170	252	-.048	.039	.110	-.239
170	119	-.159	.060	-.009	-.561	170	203	-.150	.146	.587	-.816	170	253	-.044	.036	.101	-.161
170	120	-.156	.049	-.017	-.447	170	204	-.137	.117	.347	-.659	170	254	-.083	.044	.104	-.374
170	121	-.156	.053	-.005	-.548	170	205	-.172	.083	.180	-.617	170	255	-.073	.037	.119	-.227
170	122	-.161	.058	-.002	-.882	170	206	.130	.170	.859	-.305	170	256	-.067	.035	.069	-.191
170	123	-.155	.051	-.024	-.452	170	207	.064	.148	.797	-.404	170	257	-.078	.034	.088	-.198
170	124	-.156	.059	-.005	-.508	170	208	.007	.095	.514	-.340	170	258	-.073	.034	.091	-.226

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
170	259	-.095	.040	.057	-.316
170	260	-.067	.035	.057	-.224
170	261	-.067	.031	.046	-.196
170	262	-.069	.031	.041	-.176
170	263	-.054	.033	.077	-.174
170	264	-.048	.033	.082	-.167
170	265	-.055	.033	.056	-.208
170	266	-.055	.035	.081	-.256
170	267	-.074	.036	.052	-.254
170	268	-.048	.037	.095	-.207
170	269	-.041	.034	.126	-.191
170	270	-.036	.036	.137	-.198
170	271	-.040	.035	.150	-.183
170	272	-.048	.034	.131	-.251
170	273	-.041	.038	.163	-.168
170	274	-.044	.040	.163	-.164
170	275	-.042	.041	.202	-.149
170	276	-.036	.034	.122	-.140
170	277	-.051	.036	.104	-.226
170	301	-.189	.100	.186	-.654
170	302	-.099	.134	.452	-.703
170	303	-.044	.191	.766	-.942
170	304	-.218	.094	.046	-1.037
170	305	.002	.110	.511	-.339
170	306	-.111	.104	.440	-.512
170	307	-.021	.166	.734	-.831
170	308	.099	.172	.942	-.385
170	309	-.236	.098	.037	-.738
170	310	-.219	.071	-.020	-.631
170	311	-.088	.074	.301	-.403
170	312	-.013	.093	.456	-.616
170	313	.023	.139	.638	-.778
170	314	-.053	.158	.594	-.844
170	315	.166	.156	.849	-.199
170	316	.161	.158	.851	-.237
170	317	-.186	.077	.059	-.549
170	318	.148	.141	.922	-.375
170	319	-.233	.083	-.025	-.874
170	320	-.225	.086	.068	-.724
170	321	-.108	.069	.257	-.425
170	322	-.032	.066	.376	-.335
170	323	-.001	.125	.474	-1.051
170	324	-.076	.195	.794	-.952
170	325	.180	.153	.862	-.180
170	326	.162	.147	.903	-.142
170	327	-.263	.099	.117	-.941
170	328	-.252	.071	-.040	-.651
170	329	-.130	.064	.201	-.413
170	330	-.053	.072	.325	-.430
170	331	-.025	.112	.353	-.927
170	332	-.078	.145	.406	-.785
170	333	.128	.127	.789	-.154
170	334	.115	.127	.799	-.164
170	335	-.242	.098	.016	-.808
170	336	.071	.103	.616	-.238
170	337	-.278	.103	.099	-.996
170	338	-.273	.097	-.028	-.855
170	339	-.137	.064	.077	-.509
170	340	-.069	.053	.151	-.328
170	341	-.044	.091	.226	-.719
170	342	-.071	.140	.363	-.881
170	343	.052	.087	.612	-.189
170	344	.027	.065	.413	-.181
170	345	-.226	.097	.221	-1.045
170	346	-.233	.087	-.042	-.895
170	347	-.119	.051	.056	-.364
170	348	-.072	.048	.132	-.349
170	349	-.047	.056	.224	-.344
170	350	-.052	.079	.289	-.612
170	351	-.010	.053	.269	-.299
170	352	-.020	.043	.198	-.240
170	353	-.167	.071	.070	-.864
170	354	-.047	.052	.189	-.342
170	355	-.156	.071	.147	-.577
170	356	-.175	.055	.009	-.680
170	357	-.098	.040	.045	-.391
170	358	-.060	.040	.101	-.254
170	359	-.043	.045	.164	-.383
170	360	-.047	.045	.122	-.409
170	361	-.074	.043	.211	-.189
170	362	-.039	.044	.218	-.202
170	363	-.082	.035	.084	-.196
170	364	-.101	.038	.039	-.380
170	365	-.076	.036	.144	-.202
170	366	-.063	.037	.137	-.185
170	367	-.057	.039	.159	-.233
170	368	-.060	.036	.124	-.243
170	369	-.056	.034	.127	-.212
170	370	-.048	.035	.125	-.168
170	371	-.088	.031	.048	-.203
170	372	-.041	.035	.129	-.152
170	373	-.064	.030	.038	-.168
170	374	-.064	.035	.070	-.177
170	375	-.060	.038	.058	-.189
170	376	-.045	.036	.133	-.180
170	377	-.064	.027	.017	-.151
170	378	-.060	.033	.048	-.162
170	379	-.051	.035	.079	-.170
170	380	-.045	.042	.122	-.173
170	401	-.166	.102	.057	-.807
170	402	-.190	.098	.090	-.716
170	403	-.200	.082	.031	-.681
170	404	-.222	.103	.049	-.882
170	405	-.260	.104	.008	-.742
170	406	-.166	.086	.057	-.785
170	407	-.174	.074	.016	-.791
170	408	-.190	.089	.051	-.761
170	409	-.196	.090	.066	-.853
170	410	-.198	.088	.069	-.567
170	411	-.216	.080	-.011	-.913
170	412	-.170	.075	.014	-.633
170	413	-.165	.069	.037	-.679
170	414	-.172	.075	.024	-.761
170	415	-.177	.064	-.014	-.501
170	416	-.187	.077	.011	-.549
170	417	-.191	.079	.057	-.647
170	418	-.203	.077	-.017	-.673
170	419	-.202	.069	-.001	-.530
170	420	-.188	.063	-.022	-.516
170	421	-.181	.058	-.009	-.453
170	422	-.185	.060	.000	-.550
170	423	-.183	.060	-.036	-.548
170	424	-.193	.076	.015	-.691
170	425	-.192	.082	.052	-.702
170	426	-.224	.078	-.026	-.733
170	427	-.218	.084	-.014	-.744
170	428	-.191	.070	-.021	-.676
170	429	-.185	.067	-.017	-.574
170	430	-.195	.063	-.024	-.528
170	431	-.215	.079	.003	-.660
170	432	-.231	.095	.040	-.895
170	433	-.234	.094	.012	-.704
170	434	-.247	.083	-.019	-.654
170	435	-.242	.088	.009	-.600
170	436	-.163	.057	-.011	-.506
170	437	-.159	.059	-.010	-.560
170	438	-.179	.063	-.001	-.562
170	439	-.207	.084	-.007	-.716
170	440	-.244	.108	-.007	-1.074
170	441	-.262	.116	-.005	-1.219
170	442	-.275	.100	-.058	-1.815
170	443	-.271	.103	-.044	-1.771
170	444	-.130	.050	.020	-.385
170	445	-.119	.048	.021	-.384
170	446	-.128	.043	.097	-.359
170	447	-.148	.060	.001	-.514
170	448	-.189	.083	-.021	-.885
170	449	-.222	.108	-.017	-1.176
170	450	-.235	.082	-.034	-.884
170	451	-.227	.078	-.007	-.794

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
170	452	-.090	.036	.042	-.288	170	915	-.136	.077	.208	-.489	180	147	-.111	.046	.017	-.407
170	453	-.083	.034	.036	-.213	170	916	-.154	.065	.017	-.519	180	148	-.105	.035	-.003	-.344
170	454	-.088	.028	.026	-.216	170	917	-.178	.082	.061	-.608	180	149	-.102	.034	.022	-.321
170	455	-.092	.032	.026	-.219	170	918	-.196	.084	.147	-.595	180	150	-.100	.044	.048	-.380
170	456	-.107	.037	.015	-.385	180	101	-.173	.085	.056	-.762	180	151	-.101	.045	.040	-.430
170	457	-.125	.048	.029	-.396	180	102	-.164	.077	.026	-.755	180	152	-.104	.047	.031	-.480
170	458	-.185	.068	-.039	-.770	180	103	-.143	.065	.054	-.442	180	153	-.102	.041	.012	-.335
170	459	-.179	.070	-.009	-.875	180	104	-.130	.055	.048	-.420	180	154	-.078	.037	.055	-.277
170	460	-.083	.034	.023	-.237	180	105	-.131	.057	.057	-.391	180	155	-.068	.034	.040	-.218
170	461	-.080	.034	.024	-.237	180	106	-.121	.058	.088	-.466	180	156	-.066	.033	.057	-.194
170	462	-.081	.028	.003	-.202	180	107	-.126	.058	.074	-.495	180	157	-.069	.029	.051	-.168
170	463	-.085	.027	.015	-.174	180	108	-.130	.064	.118	-.714	180	158	-.064	.034	.050	-.247
170	464	-.084	.030	.023	-.186	180	109	-.126	.045	.056	-.350	180	159	-.096	.048	.050	-.418
170	465	-.091	.032	.034	-.197	180	110	-.122	.052	.101	-.378	180	160	-.079	.041	.083	-.388
170	466	-.110	.043	.012	-.356	180	111	-.127	.052	.100	-.398	180	161	-.059	.028	.054	-.183
170	467	-.103	.034	.022	-.258	180	112	-.129	.050	.083	-.416	180	162	-.041	.031	.073	-.156
170	468	-.083	.033	.038	-.188	180	113	-.133	.043	-.008	-.377	180	163	-.089	.045	.076	-.302
170	469	-.087	.029	.027	-.183	180	114	-.133	.053	.015	-.511	180	164	-.072	.042	.085	-.277
170	470	-.088	.032	.039	-.199	180	115	-.110	.052	.172	-.377	180	165	-.048	.030	.118	-.143
170	471	-.091	.031	.022	-.197	180	116	-.150	.058	.043	-.485	180	166	-.040	.032	.106	-.141
170	472	-.093	.032	.024	-.207	180	117	-.126	.038	-.015	-.343	180	201	-.069	.184	.589	-.762
170	473	-.094	.029	.024	-.176	180	118	-.123	.043	-.002	-.372	180	202	-.148	.170	.554	-.783
170	474	-.089	.032	.024	-.194	180	119	-.126	.044	-.006	-.403	180	203	-.142	.123	.267	-1.009
170	475	-.092	.031	.015	-.185	180	120	-.130	.034	-.005	-.269	180	204	-.148	.102	.213	-.803
170	476	-.089	.031	.010	-.188	180	121	-.130	.040	.013	-.292	180	205	-.170	.079	.118	-.578
170	477	-.087	.025	-.005	-.178	180	122	-.137	.043	-.006	-.309	180	206	.019	.149	.826	-.501
170	801	-.041	.033	.143	-.131	180	123	-.127	.037	-.023	-.449	180	207	-.137	.139	.500	-.761
170	802	-.033	.041	.132	-.150	180	124	-.125	.043	-.005	-.506	180	208	-.066	.085	.350	-.393
170	803	-.033	.038	.126	-.163	180	125	-.129	.042	-.013	-.430	180	209	-.036	.089	.442	-.351
170	804	-.081	.035	.022	-.256	180	126	-.135	.040	-.028	-.343	180	210	-.034	.075	.294	-.303
170	805	-.081	.025	.017	-.182	180	127	-.141	.039	-.032	-.328	180	211	-.022	.085	.381	-.366
170	806	-.086	.030	.028	-.211	180	128	-.141	.046	-.007	-.410	180	212	.096	.156	.745	-.350
170	807	-.081	.034	.060	-.227	180	129	-.100	.048	.124	-.295	180	213	.117	.167	.796	-.521
170	808	-.083	.033	.052	-.247	180	130	-.160	.056	-.009	-.539	180	214	-.154	.182	.514	-.955
170	809	-.083	.029	.024	-.187	180	131	-.111	.037	-.013	-.286	180	215	-.069	.104	.442	-.589
170	810	-.085	.032	.038	-.199	180	132	-.110	.042	.003	-.287	180	216	-.040	.082	.399	-.311
170	901	-.157	.080	.108	-.708	180	133	-.114	.040	-.006	-.288	180	217	-.086	.067	.292	-.365
170	902	-.167	.114	.293	-1.022	180	134	-.121	.040	.000	-.295	180	218	-.041	.066	.274	-.259
170	903	-.289	.164	.408	-.968	180	135	-.139	.040	-.013	-.397	180	219	-.072	.050	.140	-.277
170	904	-.219	.080	.012	-.642	180	136	-.141	.046	.005	-.383	180	220	.079	.112	.691	-.518
170	905	-.202	.111	.161	-.707	180	137	-.104	.043	.030	-.586	180	221	.094	.117	.693	-.552
170	906	-.225	.116	.232	-.925	180	138	-.107	.043	.024	-.636	180	222	-.135	.179	.767	-.824
170	907	-.197	.118	.490	-.765	180	139	-.110	.034	-.010	-.367	180	223	-.054	.105	.618	-.457
170	908	-.157	.069	.073	-.712	180	140	-.115	.037	-.005	-.315	180	224	-.040	.084	.450	-.291
170	909	-.145	.069	.081	-.507	180	141	-.128	.047	.019	-.521	180	225	-.081	.058	.262	-.236
170	910	-.212	.103	.135	-.763	180	142	-.129	.046	-.001	-.437	180	226	-.055	.065	.331	-.315
170	911	-.239	.101	.045	-.770	180	143	-.091	.036	.059	-.326	180	227	-.086	.047	.191	-.274
170	912	-.172	.077	.077	-.514	180	144	-.084	.032	.032	-.215	180	228	.044	.093	.533	-.420
170	913	-.227	.100	.014	-.802	180	145	-.105	.047	.028	-.481	180	229	.049	.088	.487	-.348
170	914	-.179	.104	.252	-.726	180	146	-.108	.048	.023	-.480	180	230	-.114	.150	.463	-.722

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
180	231	-.058	.088	.540	-.387	180	304	-.304	.132	.230	-1.017	180	354	-.064	.056	.225	-.279
180	232	-.046	.072	.493	-.272	180	305	-.027	.147	.820	-.423	180	355	-.124	.071	.184	-.537
180	233	-.085	.051	.169	-.296	180	306	-.000	.144	.640	-.479	180	356	-.148	.057	.057	-.626
180	234	-.062	.057	.259	-.229	180	307	.095	.184	.880	-.827	180	357	-.080	.046	.154	-.267
180	235	-.088	.043	.108	-.279	180	308	.101	.175	.902	-.342	180	358	-.048	.045	.230	-.223
180	236	-.007	.068	.318	-.358	180	309	-.383	.160	.270	-1.246	180	359	-.038	.046	.234	-.266
180	237	.004	.068	.393	-.266	180	310	-.379	.119	-.068	-1.254	180	360	-.045	.040	.144	-.317
180	238	-.125	.112	.407	-.714	180	311	-.073	.116	.428	-.731	180	361	-.048	.046	.180	-.363
180	239	-.078	.065	.240	-.362	180	312	.061	.152	.747	-.551	180	362	-.046	.046	.237	-.400
180	240	-.063	.056	.237	-.241	180	313	.120	.175	1.000	-.993	180	363	-.069	.039	.108	-.270
180	241	-.087	.043	.205	-.239	180	314	.131	.169	.824	-.589	180	364	-.086	.038	.039	-.255
180	242	-.068	.048	.290	-.231	180	315	.136	.163	.930	-.721	180	365	-.067	.037	.088	-.221
180	243	-.086	.040	.126	-.252	180	316	.151	.159	1.013	-.585	180	366	-.056	.037	.099	-.218
180	244	-.043	.052	.254	-.322	180	317	-.255	.119	.205	-.839	180	367	-.055	.038	.108	-.206
180	245	-.037	.050	.247	-.430	180	318	.003	.130	.603	-.621	180	368	-.065	.031	.104	-.178
180	246	-.120	.068	.169	-.528	180	319	-.375	.136	.139	-1.058	180	369	-.064	.035	.083	-.203
180	247	-.086	.047	.182	-.296	180	320	-.394	.159	.034	-1.237	180	370	-.058	.036	.148	-.218
180	248	-.073	.043	.215	-.224	180	321	-.096	.111	.527	-.606	180	371	-.071	.033	.062	-.210
180	249	-.088	.035	.071	-.236	180	322	.041	.106	.732	-.282	180	372	-.058	.035	.106	-.181
180	250	-.075	.039	.112	-.251	180	323	.118	.149	.943	-.608	180	373	-.049	.032	.120	-.161
180	251	-.086	.036	.042	-.252	180	324	.100	.179	.851	-1.057	180	374	-.050	.037	.121	-.207
180	252	-.062	.042	.137	-.217	180	325	.123	.123	.672	-.532	180	375	-.050	.037	.121	-.187
180	253	-.064	.044	.103	-.271	180	326	.171	.120	.700	-.381	180	376	-.045	.034	.136	-.169
180	254	-.110	.049	.054	-.335	180	327	-.359	.155	.291	-1.144	180	377	-.054	.027	.048	-.132
180	255	-.088	.040	.052	-.272	180	328	-.389	.130	-.056	-1.068	180	378	-.051	.033	.104	-.153
180	256	-.078	.038	.094	-.267	180	329	-.101	.095	.487	-.475	180	379	-.049	.034	.121	-.255
180	257	-.084	.033	.088	-.291	180	330	.025	.112	.834	-.432	180	380	-.043	.036	.146	-.190
180	258	-.077	.035	.097	-.211	180	331	.078	.130	.810	-.896	180	401	-.187	.098	.054	-1.067
180	259	-.087	.037	.060	-.282	180	332	.062	.116	.655	-.751	180	402	-.188	.091	.115	-.808
180	260	-.069	.037	.055	-.377	180	333	.079	.100	.727	-.388	180	403	-.202	.074	.069	-.553
180	261	-.067	.033	.044	-.251	180	334	.080	.102	.751	-.291	180	404	-.253	.108	.082	-.898
180	262	-.070	.034	.049	-.224	180	335	-.255	.112	.015	-.967	180	405	-.319	.108	-.055	-.918
180	263	-.060	.033	.057	-.169	180	336	-.030	.102	.650	-.409	180	406	-.151	.068	.146	-.563
180	264	-.069	.034	.046	-.231	180	337	-.312	.156	.279	-1.164	180	407	-.176	.068	.033	-.550
180	265	-.070	.028	.039	-.165	180	338	-.347	.141	-.005	-1.297	180	408	-.196	.082	.062	-.724
180	266	-.071	.031	.061	-.185	180	339	-.112	.078	.303	-.465	180	409	-.239	.096	.034	-.978
180	267	-.077	.031	.043	-.209	180	340	-.013	.069	.361	-.257	180	410	-.277	.119	.045	-1.134
180	268	-.071	.034	.091	-.191	180	341	.031	.092	.573	-.594	180	411	-.391	.140	-.083	-1.179
180	269	-.068	.035	.088	-.192	180	342	.035	.108	.596	-.788	180	412	-.162	.067	.062	-.541
180	270	-.064	.035	.117	-.201	180	343	.038	.086	.550	-.337	180	413	-.160	.063	.054	-.565
180	271	-.061	.034	.133	-.182	180	344	.033	.073	.443	-.237	180	414	-.170	.067	.052	-.584
180	272	-.062	.032	.134	-.179	180	345	-.205	.121	.170	-.822	180	415	-.200	.071	.045	-.538
180	273	-.051	.034	.092	-.205	180	346	-.238	.104	.068	-.990	180	416	-.237	.098	.057	-.760
180	274	-.058	.036	.080	-.171	180	347	-.098	.060	.251	-.401	180	417	-.285	.124	.066	-1.261
180	275	-.055	.036	.080	-.189	180	348	-.031	.054	.249	-.275	180	418	-.361	.134	-.026	-1.068
180	276	-.046	.032	.084	-.154	180	349	-.020	.054	.301	-.256	180	419	-.352	.117	-.076	-.953
180	277	-.054	.032	.067	-.184	180	350	-.017	.059	.313	-.381	180	420	-.169	.066	.009	-.629
180	301	-.240	.119	.428	-.759	180	351	-.021	.057	.251	-.287	180	421	-.168	.061	.039	-.463
180	302	-.066	.180	.647	-.730	180	352	-.022	.049	.206	-.240	180	422	-.176	.067	.037	-.473
180	303	-.126	.198	.881	-.748	180	353	-.128	.056	.063	-.508	180	423	-.200	.071	.087	-.587

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
180	424	-.234	.110	.058	-.770	180	474	-.062	.034	.060	-.212	190	119	-.125	.038	.015	-.281
180	425	-.263	.130	.097	-.974	180	475	-.067	.035	.063	-.267	190	120	-.129	.035	-.017	-.299
180	426	-.362	.132	.003	-1.015	180	476	-.062	.035	.076	-.238	190	121	-.132	.044	.012	-.334
180	427	-.351	.139	-.001	-1.071	180	477	-.068	.027	.016	-.171	190	122	-.140	.051	.013	-.361
180	428	-.164	.057	-.009	-.531	180	801	-.056	.029	.060	-.159	190	123	-.122	.036	-.007	-.289
180	429	-.160	.056	-.004	-.572	180	802	-.053	.037	.187	-.185	190	124	-.122	.041	-.003	-.332
180	430	-.178	.062	-.022	-.491	180	803	-.052	.035	.132	-.168	190	125	-.125	.040	-.014	-.339
180	431	-.211	.087	.032	-.717	180	804	-.066	.036	.056	-.222	190	126	-.132	.040	-.006	-.298
180	432	-.255	.115	.046	-1.183	180	805	-.069	.024	.019	-.161	190	127	-.133	.038	-.025	-.284
180	433	-.296	.135	.054	-1.288	180	806	-.075	.028	.050	-.175	190	128	-.134	.046	.042	-.501
180	434	-.370	.122	-.117	-1.034	180	807	-.066	.031	.042	-.175	190	129	-.133	.040	-.012	-.351
180	435	-.360	.127	-.089	-1.056	180	808	-.065	.032	.070	-.172	190	130	-.156	.059	-.015	-.462
180	436	-.139	.047	-.002	-.410	180	809	-.060	.029	.084	-.209	190	131	-.110	.038	.042	-.398
180	437	-.134	.050	.014	-.404	180	810	-.061	.034	.143	-.189	190	132	-.110	.043	.042	-.445
180	438	-.149	.048	.006	-.398	180	901	-.140	.080	.138	-.573	190	133	-.114	.041	.037	-.419
180	439	-.173	.067	.054	-.606	180	902	-.159	.110	.305	-.701	190	134	-.126	.043	.042	-.322
180	440	-.216	.086	.008	-.703	180	903	-.237	.135	.377	-.960	190	135	-.146	.044	-.030	-.351
180	441	-.263	.112	-.003	-1.045	180	904	-.229	.068	-.016	-.571	190	136	-.147	.051	-.018	-.392
180	442	-.342	.126	-.017	-1.084	180	905	-.150	.087	.170	-.572	190	137	-.097	.040	.051	-.349
180	443	-.330	.127	.004	-1.006	180	906	-.193	.105	.177	-.728	190	138	-.102	.040	.030	-.346
180	444	-.111	.040	.054	-.340	180	907	-.244	.176	.569	-.939	190	139	-.104	.035	.010	-.245
180	445	-.100	.041	.061	-.310	180	908	-.139	.060	.053	-.485	190	140	-.112	.039	.020	-.281
180	446	-.107	.035	-.009	-.270	180	909	-.136	.065	.087	-.443	190	141	-.128	.051	.007	-.435
180	447	-.113	.044	.006	-.363	180	910	-.218	.091	.191	-.617	190	142	-.134	.056	.030	-.472
180	448	-.145	.058	.037	-.592	180	911	-.256	.087	.003	-.653	190	143	-.096	.038	.023	-.294
180	449	-.189	.082	.037	-.695	180	912	-.155	.071	.081	-.551	190	144	-.076	.035	.057	-.213
180	450	-.257	.100	-.034	-.907	180	913	-.234	.087	.090	-.626	190	145	-.094	.042	.060	-.291
180	451	-.243	.093	-.034	-.863	180	914	-.203	.117	.284	-.679	190	146	-.097	.042	.035	-.295
180	452	-.082	.034	.049	-.256	180	915	-.119	.072	.242	-.438	190	147	-.101	.042	.018	-.327
180	453	-.075	.033	.049	-.270	180	916	-.152	.057	.034	-.438	190	148	-.099	.034	.022	-.231
180	454	-.079	.030	.028	-.196	180	917	-.196	.084	.050	-.679	190	149	-.089	.035	.035	-.260
180	455	-.079	.034	.047	-.247	180	918	-.235	.094	.119	-.742	190	150	-.089	.044	.075	-.314
180	456	-.090	.036	.054	-.292	190	101	-.213	.086	.007	-.591	190	151	-.090	.046	.039	-.373
180	457	-.107	.048	.066	-.475	190	102	-.173	.080	.010	-.631	190	152	-.095	.049	.030	-.429
180	458	-.150	.056	.013	-.469	190	103	-.138	.052	.032	-.353	190	153	-.095	.040	-.002	-.359
180	459	-.146	.058	.024	-.428	190	104	-.118	.049	.050	-.415	190	154	-.074	.037	.027	-.248
180	460	-.074	.036	.061	-.222	190	105	-.120	.050	.034	-.441	190	155	-.058	.035	.051	-.193
180	461	-.070	.035	.059	-.199	190	106	-.115	.047	.035	-.385	190	156	-.057	.036	.066	-.179
180	462	-.073	.028	.013	-.181	190	107	-.122	.048	.030	-.351	190	157	-.067	.027	.097	-.237
180	463	-.067	.028	.016	-.171	190	108	-.125	.052	.047	-.377	190	158	-.052	.036	.108	-.190
180	464	-.077	.030	.020	-.229	190	109	-.120	.038	.007	-.272	190	159	-.084	.042	.051	-.436
180	465	-.077	.036	.040	-.247	190	110	-.116	.043	.022	-.278	190	160	-.083	.040	.063	-.367
180	466	-.089	.041	.037	-.374	190	111	-.120	.043	.020	-.303	190	161	-.055	.027	.032	-.183
180	467	-.086	.041	.044	-.279	190	112	-.124	.042	.011	-.313	190	162	-.038	.032	.098	-.142
180	468	-.066	.036	.045	-.205	190	113	-.131	.041	.000	-.329	190	163	-.081	.041	.030	-.339
180	469	-.062	.030	.056	-.169	190	114	-.133	.052	.022	-.422	190	164	-.077	.041	.078	-.417
180	470	-.062	.034	.060	-.207	190	115	-.167	.056	.056	-.407	190	165	-.051	.029	.104	-.156
180	471	-.067	.034	.056	-.214	190	116	-.171	.074	.104	-.705	190	166	-.035	.033	.083	-.145
180	472	-.074	.037	.059	-.247	190	117	-.123	.034	-.005	-.252	190	201	-.014	.155	.635	-.559
180	473	-.065	.030	.044	-.225	190	118	-.121	.039	.012	-.273	190	202	-.216	.146	.367	-.717

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
190	203	-.101	.081	.172	-.532	190	253	-.063	.048	.113	-.357	190	326	.191	.146	.846	-.300
190	204	-.131	.066	.118	-.519	190	254	-.118	.052	.064	-.358	190	327	-.370	.225	.435	-1.188
190	205	-.191	.081	.010	-.490	190	255	-.087	.039	.061	-.300	190	328	-.460	.166	-.020	-1.248
190	206	.029	.166	.835	-.477	190	256	-.075	.036	.054	-.221	190	329	-.063	.105	.415	-.500
190	207	-.249	.137	.287	-.835	190	257	-.079	.031	.061	-.200	190	330	.092	.117	.683	-.284
190	208	-.123	.068	.144	-.375	190	258	-.067	.033	.072	-.204	190	331	.160	.130	.890	-.168
190	209	-.036	.082	.377	-.288	190	259	-.074	.034	.034	-.213	190	332	.160	.108	.686	-.112
190	210	-.027	.064	.256	-.239	190	260	-.066	.038	.094	-.375	190	333	.094	.145	.784	-.505
190	211	-.023	.078	.342	-.242	190	261	-.065	.033	.061	-.259	190	334	.114	.138	.768	-.471
190	212	.137	.182	.790	-.523	190	262	-.076	.036	.038	-.215	190	335	-.282	.133	.039	-1.010
190	213	.155	.201	.842	-.437	190	263	-.068	.035	.040	-.206	190	336	-.096	.093	.294	-.475
190	214	-.320	.165	.332	-1.049	190	264	-.068	.032	.052	-.178	190	337	-.255	.190	.485	-1.275
190	215	-.127	.093	.302	-.545	190	265	-.066	.029	.054	-.197	190	338	-.333	.164	.096	-1.236
190	216	-.065	.067	.443	-.295	190	266	-.062	.031	.061	-.199	190	339	-.067	.091	.411	-.429
190	217	-.115	.051	.189	-.311	190	267	-.068	.032	.054	-.184	190	340	.027	.068	.491	-.168
190	218	-.057	.055	.322	-.246	190	268	-.070	.035	.078	-.200	190	341	.065	.081	.576	-.144
190	219	-.077	.043	.200	-.250	190	269	-.068	.033	.057	-.229	190	342	.064	.083	.662	-.205
190	220	.119	.155	.796	-.358	190	270	-.062	.033	.069	-.272	190	343	.014	.104	.466	-.668
190	221	.131	.164	.749	-.418	190	271	-.059	.031	.068	-.189	190	344	.026	.085	.489	-.419
190	222	-.333	.169	.239	-1.135	190	272	-.060	.031	.059	-.183	190	345	-.153	.134	.368	-1.196
190	223	-.136	.093	.211	-.553	190	273	-.053	.033	.067	-.176	190	346	-.209	.115	.171	-1.028
190	224	-.088	.061	.187	-.317	190	274	-.062	.033	.057	-.182	190	347	-.056	.073	.439	-.378
190	225	-.131	.045	.034	-.323	190	275	-.059	.033	.052	-.207	190	348	.011	.071	.346	-.202
190	226	-.072	.049	.160	-.265	190	276	-.055	.030	.059	-.157	190	349	.010	.063	.381	-.169
190	227	-.092	.040	.066	-.252	190	277	-.057	.031	.052	-.163	190	350	.002	.060	.276	-.205
190	228	.053	.127	.517	-.553	190	301	-.298	.123	.268	-1.045	190	351	-.037	.069	.327	-.575
190	229	.054	.120	.571	-.397	190	302	.010	.213	.641	-.710	190	352	-.028	.057	.219	-.382
190	230	-.264	.136	.163	-.849	190	303	-.122	.213	.980	-.791	190	353	-.113	.056	.131	-.488
190	231	-.126	.068	.104	-.411	190	304	-.375	.193	.733	-1.256	190	354	-.083	.058	.171	-.388
190	232	-.090	.048	.116	-.309	190	305	.143	.139	.744	-.353	190	355	-.087	.071	.243	-.671
190	233	-.125	.038	.027	-.276	190	306	.132	.129	.703	-.353	190	356	-.112	.055	.131	-.835
190	234	-.079	.041	.130	-.219	190	307	.239	.159	.861	-.223	190	357	-.057	.051	.274	-.310
190	235	-.094	.035	.068	-.244	190	308	.224	.174	1.034	-.317	190	358	-.035	.052	.382	-.210
190	236	-.017	.093	.510	-.432	190	309	-.490	.207	.308	-1.793	190	359	-.028	.051	.343	-.257
190	237	-.004	.100	.372	-.522	190	310	-.508	.142	-.173	-1.314	190	360	-.038	.038	.139	-.180
190	238	-.235	.116	.084	-.720	190	311	.019	.120	.551	-.478	190	361	-.055	.048	.146	-.287
190	239	-.125	.063	.071	-.445	190	312	.218	.155	.835	-.215	190	362	-.047	.050	.164	-.303
190	240	-.091	.047	.078	-.306	190	313	.303	.171	1.015	-.206	190	363	-.052	.040	.108	-.215
190	241	-.112	.037	.022	-.288	190	314	.318	.154	1.024	-.180	190	364	-.073	.035	.109	-.209
190	242	-.077	.039	.097	-.222	190	315	.206	.202	1.108	-.636	190	365	-.062	.037	.116	-.181
190	243	-.089	.037	.034	-.237	190	316	.283	.194	1.076	-.499	190	366	-.057	.037	.115	-.165
190	244	-.053	.067	.230	-.435	190	317	-.349	.155	.243	-1.054	190	367	-.055	.037	.132	-.182
190	245	-.048	.072	.241	-.443	190	318	-.060	.145	.557	-.567	190	368	-.059	.039	.053	-.173
190	246	-.170	.079	.066	-.616	190	319	-.451	.181	.180	-1.144	190	369	-.060	.036	.056	-.223
190	247	-.107	.050	.075	-.334	190	320	-.503	.174	.053	-1.317	190	370	-.055	.037	.074	-.222
190	248	-.083	.041	.080	-.314	190	321	-.037	.112	.529	-.489	190	371	-.062	.035	.085	-.196
190	249	-.092	.033	.029	-.227	190	322	.164	.110	.710	-.246	190	372	-.066	.037	.129	-.214
190	250	-.070	.035	.104	-.217	190	323	.241	.150	.869	-.185	190	373	-.046	.037	.164	-.189
190	251	-.087	.036	.041	-.220	190	324	.259	.151	.844	-.350	190	374	-.050	.041	.241	-.250
190	252	-.069	.048	.156	-.451	190	325	.151	.168	.804	-.519	190	375	-.053	.041	.217	-.251

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
190	376	-.049	.039	.155	-.202	190	446	-.092	.037	.049	-.242	190	909	-.138	.055	.031	-.410
190	377	-.040	.031	.125	-.145	190	447	-.095	.044	.070	-.285	190	910	-.282	.099	.009	-.759
190	378	-.036	.037	.126	-.147	190	448	-.129	.057	.059	-.425	190	911	-.325	.095	-.053	-.807
190	379	-.040	.036	.138	-.148	190	449	-.190	.090	.031	-.825	190	912	-.142	.055	-.073	-.380
190	380	-.040	.036	.139	-.162	190	450	-.229	.106	.018	-1.578	190	913	-.311	.095	-.018	-.766
190	401	-.190	.111	.066	-.931	190	451	-.214	.099	.033	-1.393	190	914	-.245	.109	.124	-.741
190	402	-.198	.101	.022	-.893	190	452	-.069	.034	.057	-.199	190	915	-.104	.061	.165	-.341
190	403	-.233	.090	.023	-.692	190	453	-.063	.034	.059	-.191	190	916	-.157	.056	.022	-.475
190	404	-.338	.141	-.032	-1.011	190	454	-.065	.033	.071	-.269	190	917	-.240	.102	.066	-.838
190	405	-.419	.136	-.079	-.996	190	455	-.067	.036	.134	-.230	190	918	-.342	.105	.021	-.845
190	406	-.140	.070	.064	-.522	190	456	-.079	.041	.047	-.328	200	101	-.202	.076	.011	-.627
190	407	-.168	.071	.086	-.626	190	457	-.108	.061	.033	-.522	200	102	-.148	.053	-.006	-.498
190	408	-.210	.092	.102	-.776	190	458	-.126	.062	.142	-.611	200	103	-.126	.046	.037	-.398
190	409	-.280	.112	.033	-.803	190	459	-.124	.063	.167	-.719	200	104	-.113	.040	.010	-.264
190	410	-.393	.150	.001	-1.194	190	460	-.063	.038	.083	-.232	200	105	-.114	.040	.015	-.264
190	411	-.508	.177	-.121	-1.486	190	461	-.061	.037	.071	-.249	200	106	-.110	.041	.011	-.257
190	412	-.142	.068	.085	-.620	190	462	-.058	.031	.049	-.147	200	107	-.110	.041	.008	-.258
190	413	-.144	.066	.059	-.540	190	463	-.062	.027	.022	-.240	200	108	-.111	.043	.019	-.273
190	414	-.164	.075	.050	-.573	190	464	-.058	.034	.069	-.192	200	109	-.113	.034	-.006	-.229
190	415	-.229	.083	.011	-.777	190	465	-.070	.032	.041	-.228	200	110	-.110	.038	.011	-.241
190	416	-.313	.127	.097	-.957	190	466	-.066	.041	.078	-.405	200	111	-.110	.038	.008	-.239
190	417	-.411	.157	.121	-1.089	190	467	-.078	.038	.062	-.289	200	112	-.113	.038	.005	-.252
190	418	-.508	.177	-.086	-1.266	190	468	-.068	.035	.035	-.285	200	113	-.116	.034	-.011	-.259
190	419	-.487	.143	-.121	-1.000	190	469	-.066	.027	.054	-.174	200	114	-.115	.042	.011	-.302
190	420	-.152	.066	.062	-.602	190	470	-.064	.031	.071	-.200	200	115	-.182	.050	-.026	-.393
190	421	-.153	.065	.064	-.507	190	471	-.067	.031	.064	-.198	200	116	-.165	.061	.007	-.748
190	422	-.176	.075	.082	-.622	190	472	-.071	.033	.052	-.283	200	117	-.122	.033	-.004	-.246
190	423	-.222	.089	.028	-.769	190	473	-.068	.030	.042	-.211	200	118	-.119	.037	.013	-.264
190	424	-.290	.134	.052	-1.027	190	474	-.063	.033	.046	-.178	200	119	-.120	.037	.004	-.284
190	425	-.372	.157	.089	-1.289	190	475	-.066	.032	.038	-.177	200	120	-.123	.035	-.011	-.288
190	426	-.494	.156	-.106	-1.374	190	476	-.063	.032	.035	-.170	200	121	-.123	.043	.034	-.368
190	427	-.479	.165	-.069	-1.470	190	477	-.066	.027	.037	-.167	200	122	-.127	.049	.042	-.618
190	428	-.145	.059	-.001	-.502	190	801	-.062	.029	.071	-.150	200	123	-.123	.036	.003	-.259
190	429	-.145	.061	.024	-.589	190	802	-.061	.036	.100	-.232	200	124	-.121	.040	.013	-.277
190	430	-.165	.064	-.028	-.692	190	803	-.061	.037	.140	-.206	200	125	-.122	.039	-.004	-.270
190	431	-.204	.094	.005	-.952	190	804	-.052	.035	.080	-.275	200	126	-.125	.039	-.007	-.323
190	432	-.279	.126	.035	-1.175	190	805	-.059	.028	.044	-.147	200	127	-.127	.036	-.011	-.330
190	433	-.386	.164	-.030	-1.546	190	806	-.061	.032	.065	-.180	200	128	-.125	.044	.039	-.393
190	434	-.431	.148	.025	-1.202	190	807	-.064	.035	.114	-.244	200	129	-.155	.045	-.004	-.379
190	435	-.408	.152	.085	-1.170	190	808	-.061	.035	.143	-.254	200	130	-.153	.055	.029	-.508
190	436	-.119	.044	.028	-.411	190	809	-.057	.029	.056	-.164	200	131	-.114	.040	.008	-.343
190	437	-.114	.046	.017	-.410	190	810	-.056	.035	.113	-.202	200	132	-.113	.044	.013	-.378
190	438	-.132	.046	-.011	-.490	190	901	-.137	.067	.161	-.447	200	133	-.115	.041	.033	-.309
190	439	-.147	.065	.008	-.729	190	902	-.172	.080	.117	-.652	200	134	-.120	.040	.000	-.325
190	440	-.206	.095	.030	-1.134	190	903	-.249	.113	.199	-.716	200	135	-.130	.041	-.026	-.301
190	441	-.298	.142	.026	-1.229	190	904	-.284	.073	-.081	-.593	200	136	-.127	.047	.001	-.368
190	442	-.362	.148	-.060	-1.243	190	905	-.129	.065	.054	-.623	200	137	-.099	.051	.047	-.577
190	443	-.339	.148	-.027	-1.133	190	906	-.199	.102	.131	-.671	200	138	-.102	.050	.031	-.648
190	444	-.101	.041	.026	-.304	190	907	-.317	.190	.473	-.989	200	139	-.102	.034	.031	-.298
190	445	-.091	.041	.057	-.298	190	908	-.130	.046	.039	-.328	200	140	-.106	.040	.061	-.292

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
200	141	-.115	.046	.035	-.454	200	225	-.156	.042	-.009	-.312	200	275	-.073	.033	.054	-.190
200	142	-.127	.056	.033	-.614	200	226	-.087	.041	.124	-.223	200	276	-.061	.028	.030	-.157
200	143	-.106	.037	.033	-.280	200	227	-.096	.035	.016	-.232	200	277	-.059	.031	.071	-.175
200	144	-.091	.037	.021	-.273	200	228	-.077	.145	.351	-.728	200	301	-.285	.160	.494	-.850
200	145	-.072	.038	.061	-.229	200	229	-.076	.154	.472	-.730	200	302	-.097	.223	.710	-.773
200	146	-.075	.037	.047	-.226	200	230	-.420	.167	.072	-1.203	200	303	-.127	.229	.861	-.882
200	147	-.082	.038	.038	-.254	200	231	-.213	.088	.071	-.576	200	304	-.282	.248	.831	-1.141
200	148	-.087	.029	.028	-.200	200	232	-.136	.055	.117	-.379	200	305	.205	.141	.707	-.180
200	149	-.082	.037	.028	-.261	200	233	-.147	.040	-.006	-.312	200	306	.228	.130	.743	-.199
200	150	-.077	.045	.049	-.325	200	234	-.095	.038	.110	-.243	200	307	.275	.155	.890	-.153
200	151	-.067	.035	.057	-.217	200	235	-.101	.035	.033	-.225	200	308	.178	.191	.982	-.451
200	152	-.072	.035	.057	-.195	200	236	-.097	.110	.374	-.609	200	309	-.408	.282	.614	-1.476
200	153	-.077	.034	.043	-.241	200	237	-.110	.115	.404	-.570	200	310	-.534	.169	.116	-1.095
200	154	-.064	.034	.041	-.204	200	238	-.351	.132	-.012	-1.121	200	311	.131	.133	.674	-.225
200	155	-.053	.039	.071	-.260	200	239	-.191	.070	.007	-.576	200	312	.334	.170	.911	-.092
200	156	-.050	.042	.078	-.278	200	240	-.127	.047	.049	-.349	200	313	.401	.186	1.038	-.092
200	157	-.067	.028	.026	-.165	200	241	-.130	.035	-.004	-.286	200	314	.351	.151	.931	-.116
200	158	-.043	.035	.117	-.156	200	242	-.094	.037	.035	-.233	200	315	.062	.225	.865	-.925
200	159	-.062	.037	.059	-.231	200	243	-.098	.036	.028	-.237	200	316	.272	.234	1.055	-1.073
200	160	-.065	.039	.081	-.263	200	244	-.109	.086	.159	-.786	200	317	-.354	.134	.257	-.996
200	161	-.046	.031	.070	-.162	200	245	-.120	.087	.156	-.601	200	318	-.170	.124	.418	-.668
200	162	-.029	.039	.114	-.209	200	246	-.279	.097	.008	-.837	200	319	-.360	.217	.289	-1.139
200	163	-.065	.037	.064	-.251	200	247	-.163	.054	-.005	-.423	200	320	-.504	.214	.148	-1.304
200	164	-.063	.038	.069	-.275	200	248	-.111	.039	.037	-.300	200	321	.050	.124	.598	-.325
200	165	-.051	.029	.048	-.187	200	249	-.108	.034	.011	-.271	200	322	.289	.142	.816	-.121
200	166	-.028	.034	.097	-.168	200	250	-.084	.035	.042	-.223	200	323	.311	.174	1.008	-.106
200	201	-.157	.127	.314	-.703	200	251	-.094	.036	.018	-.240	200	324	.311	.174	.970	-.263
200	202	-.304	.104	.164	-.790	200	252	-.102	.066	.105	-.438	200	325	.014	.216	.873	-.763
200	203	-.137	.062	.102	-.411	200	253	-.110	.070	.091	-.497	200	326	.147	.195	1.077	-.505
200	204	-.141	.053	.065	-.386	200	254	-.197	.079	-.022	-.780	200	327	-.306	.253	.433	-1.412
200	205	-.178	.067	-.004	-.472	200	255	-.126	.047	.019	-.347	200	328	-.455	.183	.147	-1.185
200	206	-.105	.134	.450	-.688	200	256	-.090	.038	.028	-.262	200	329	.028	.118	.505	-.344
200	207	-.406	.132	-.055	-1.103	200	257	-.084	.033	.040	-.256	200	330	.189	.135	.775	-.125
200	208	-.194	.056	.002	-.464	200	258	-.079	.034	.042	-.241	200	331	.238	.145	.949	-.090
200	209	-.092	.059	.159	-.325	200	259	-.070	.036	.062	-.246	200	332	.176	.111	.665	-.089
200	210	-.059	.048	.151	-.235	200	260	-.089	.057	.063	-.520	200	333	-.033	.173	.657	-.811
200	211	-.053	.054	.266	-.228	200	261	-.082	.046	.035	-.421	200	334	.056	.170	.656	-.750
200	212	-.014	.171	.769	-.581	200	262	-.108	.040	.018	-.298	200	335	-.277	.114	.094	-.884
200	213	-.035	.194	.708	-.625	200	263	-.092	.036	.018	-.235	200	336	-.183	.103	.206	-.619
200	214	-.506	.178	-.002	-1.412	200	264	-.079	.033	.037	-.211	200	337	-.214	.198	.632	-1.295
200	215	-.224	.087	.042	-.579	200	265	-.069	.031	.035	-.159	200	338	-.344	.176	.319	-1.442
200	216	-.122	.054	.098	-.287	200	266	-.063	.033	.042	-.176	200	339	.012	.110	.493	-.500
200	217	-.142	.044	.011	-.349	200	267	-.063	.034	.057	-.179	200	340	.130	.095	.665	-.072
200	218	-.087	.042	.083	-.227	200	268	-.087	.040	.053	-.288	200	341	.163	.112	.865	-.083
200	219	-.089	.037	.033	-.216	200	269	-.083	.034	.045	-.218	200	342	.118	.103	.725	-.147
200	220	-.030	.174	.680	-.712	200	270	-.076	.034	.067	-.238	200	343	-.068	.139	.567	-.623
200	221	-.038	.187	.694	-.716	200	271	-.070	.032	.062	-.187	200	344	-.005	.106	.474	-.534
200	222	-.499	.177	.064	-1.327	200	272	-.061	.032	.058	-.190	200	345	-.137	.133	.401	-.845
200	223	-.231	.095	.065	-.629	200	273	-.067	.036	.066	-.276	200	346	-.232	.114	.091	-.848
200	224	-.143	.057	.112	-.370	200	274	-.080	.034	.052	-.282	200	347	-.005	.080	.530	-.255

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
200	348	.074	.085	.610	-.167	200	418	-.531	.201	.064	-1.453	200	468	-.062	.035	.056	-.233
200	349	.107	.095	.563	-.177	200	419	-.489	.170	.088	-1.052	200	469	-.054	.030	.077	-.174
200	350	.065	.084	.485	-.192	200	420	-.133	.058	.103	-.482	200	470	-.057	.036	.099	-.214
200	351	-.091	.098	.285	-.602	200	421	-.140	.059	.164	-.509	200	471	-.059	.038	.068	-.252
200	352	-.031	.079	.238	-.463	200	422	-.169	.072	.115	-.619	200	472	-.070	.043	.071	-.314
200	353	-.141	.065	.140	-.488	200	423	-.241	.088	.039	-.817	200	473	-.055	.031	.049	-.207
200	354	-.134	.065	.124	-.415	200	424	-.337	.125	.111	-1.217	200	474	-.052	.034	.091	-.173
200	355	-.081	.097	.453	-.521	200	425	-.499	.170	-.022	-1.367	200	475	-.055	.035	.091	-.208
200	356	-.133	.071	.128	-.482	200	426	-.516	.176	-.055	-1.309	200	476	-.053	.035	.083	-.173
200	357	-.028	.060	.458	-.207	200	427	-.489	.189	.113	-1.377	200	477	-.064	.030	.016	-.239
200	358	.007	.065	.590	-.159	200	428	-.129	.054	.025	-.497	200	801	-.075	.029	.025	-.179
200	359	.014	.066	.521	-.146	200	429	-.131	.057	.054	-.500	200	802	-.080	.034	.039	-.230
200	360	-.008	.049	.306	-.207	200	430	-.164	.055	-.002	-.616	200	803	-.081	.035	.045	-.220
200	361	-.072	.070	.188	-.443	200	431	-.206	.080	.016	-.740	200	804	-.051	.034	.060	-.181
200	362	-.045	.078	.371	-.479	200	432	-.305	.111	.009	-1.210	200	805	-.065	.029	.042	-.170
200	363	-.048	.047	.304	-.257	200	433	-.481	.176	.006	-1.295	200	806	-.076	.039	.060	-.250
200	364	-.062	.041	.250	-.680	200	434	-.469	.171	.078	-1.186	200	807	-.068	.036	.089	-.245
200	365	-.049	.043	.178	-.580	200	435	-.440	.176	.061	-1.129	200	808	-.063	.035	.069	-.203
200	366	-.045	.040	.160	-.458	200	436	-.118	.041	.023	-.356	200	809	-.063	.032	.087	-.167
200	367	-.046	.039	.162	-.195	200	437	-.113	.044	.080	-.421	200	810	-.063	.039	.155	-.208
200	368	-.054	.032	.123	-.175	200	438	-.139	.044	.001	-.509	200	901	-.113	.052	.094	-.335
200	369	-.069	.045	.111	-.416	200	439	-.164	.061	.014	-.720	200	902	-.171	.062	.029	-.478
200	370	-.061	.044	.145	-.247	200	440	-.250	.089	-.015	-1.093	200	903	-.293	.105	.167	-.858
200	371	-.068	.039	.106	-.236	200	441	-.410	.156	-.048	-1.847	200	904	-.280	.063	-.106	-.600
200	372	-.089	.037	.063	-.294	200	442	-.390	.151	.042	-1.157	200	905	-.119	.054	.049	-.367
200	373	-.043	.040	.158	-.181	200	443	-.362	.153	.095	-1.134	200	906	-.168	.091	.114	-.608
200	374	-.054	.049	.160	-.225	200	444	-.105	.045	.033	-.304	200	907	-.378	.167	.284	-1.093
200	375	-.060	.047	.152	-.292	200	445	-.095	.045	.073	-.314	200	908	-.116	.036	.014	-.253
200	376	-.057	.043	.163	-.242	200	446	-.109	.037	.054	-.247	200	909	-.126	.043	-.004	-.302
200	377	-.035	.034	.108	-.136	200	447	-.117	.046	.043	-.301	200	910	-.274	.085	.038	-.659
200	378	-.025	.045	.283	-.159	200	448	-.173	.061	.018	-.428	200	911	-.316	.082	-.083	-.645
200	379	-.033	.045	.275	-.143	200	449	-.288	.109	-.041	-.812	200	912	-.129	.053	.056	-.319
200	380	-.041	.040	.299	-.156	200	450	-.272	.106	.015	-.890	200	913	-.296	.085	-.092	-.664
200	401	-.135	.060	.011	-.707	200	451	-.250	.098	.038	-.732	200	914	-.328	.103	-.016	-.777
200	402	-.158	.065	.041	-.554	200	452	-.071	.039	.071	-.287	200	915	-.076	.062	.228	-.327
200	403	-.216	.071	-.016	-.535	200	453	-.064	.039	.085	-.230	200	916	-.121	.041	.016	-.359
200	404	-.352	.136	-.051	-1.062	200	454	-.065	.034	.056	-.227	200	917	-.195	.070	.010	-.552
200	405	-.429	.145	-.068	-1.213	200	455	-.066	.038	.071	-.239	200	918	-.343	.104	-.021	-.821
200	406	-.105	.059	.096	-.398	200	456	-.093	.044	.090	-.301	210	101	-.175	.059	-.015	-.402
200	407	-.141	.058	.035	-.448	200	457	-.149	.073	.036	-.577	210	102	-.138	.045	-.010	-.326
200	408	-.198	.083	.024	-.611	200	458	-.180	.087	.064	-.720	210	103	-.130	.045	.005	-.339
200	409	-.311	.104	-.025	-.841	200	459	-.169	.087	.115	-.745	210	104	-.111	.042	.035	-.293
200	410	-.527	.176	-.116	-1.430	200	460	-.061	.040	.090	-.278	210	105	-.111	.041	.026	-.276
200	411	-.527	.181	-.096	-1.348	200	461	-.055	.039	.092	-.244	210	106	-.111	.039	.019	-.273
200	412	-.117	.045	.038	-.358	200	462	-.057	.030	.086	-.179	210	107	-.112	.039	.008	-.270
200	413	-.126	.052	.059	-.394	200	463	-.058	.028	.044	-.192	210	108	-.111	.041	.025	-.310
200	414	-.158	.056	.068	-.463	200	464	-.055	.035	.061	-.239	210	109	-.113	.036	.007	-.279
200	415	-.216	.075	-.007	-.761	200	465	-.074	.039	.049	-.257	210	110	-.113	.040	.029	-.296
200	416	-.333	.117	-.019	-1.052	200	466	-.072	.050	.078	-.416	210	111	-.112	.040	.034	-.296
200	417	-.499	.160	-.068	-1.272	200	467	-.082	.048	.061	-.396	210	112	-.112	.040	.051	-.303

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
210	113	-.116	.035	.022	-.257	210	163	-.062	.031	.048	-.168	210	247	-.205	.059	.013	-.479
210	114	-.116	.040	.041	-.263	210	164	-.058	.031	.049	-.165	210	248	-.137	.041	.026	-.313
210	115	-.181	.057	.003	-.412	210	165	-.068	.030	.094	-.223	210	249	-.125	.037	.003	-.260
210	116	-.161	.054	.009	-.405	210	166	-.077	.044	.101	-.256	210	250	-.100	.037	.050	-.232
210	117	-.116	.032	-.012	-.252	210	201	-.280	.100	.020	-.694	210	251	-.109	.039	.019	-.269
210	118	-.116	.036	-.003	-.273	210	202	-.338	.109	-.038	-.862	210	252	-.141	.078	.256	-.453
210	119	-.114	.034	.008	-.227	210	203	-.180	.066	.030	-.498	210	253	-.148	.079	.092	-.590
210	120	-.109	.032	.007	-.218	210	204	-.151	.054	.061	-.437	210	254	-.251	.089	-.043	-.787
210	121	-.109	.038	.031	-.258	210	205	-.174	.060	.030	-.435	210	255	-.154	.051	.001	-.419
210	122	-.109	.039	.027	-.275	210	206	-.251	.130	.416	-.888	210	256	-.109	.040	.045	-.330
210	123	-.118	.034	-.007	-.264	210	207	-.483	.156	-.089	-1.128	210	257	-.094	.033	.013	-.218
210	124	-.118	.038	-.006	-.288	210	208	-.258	.068	-.067	-.540	210	258	-.080	.032	.040	-.199
210	125	-.116	.036	-.014	-.277	210	209	-.154	.062	.069	-.441	210	259	-.080	.035	.037	-.217
210	126	-.116	.037	-.005	-.289	210	210	-.105	.051	.057	-.349	210	260	-.110	.065	.104	-.612
210	127	-.117	.034	-.007	-.286	210	211	-.082	.052	.146	-.298	210	261	-.099	.052	.094	-.551
210	128	-.116	.040	.007	-.323	210	212	-.217	.154	.398	-.823	210	262	-.128	.048	.022	-.386
210	129	-.157	.047	.008	-.360	210	213	-.256	.167	.455	-.982	210	263	-.106	.039	.027	-.261
210	130	-.136	.049	.018	-.361	210	214	-.590	.215	-.137	-1.528	210	264	-.089	.035	.145	-.261
210	131	-.115	.037	-.000	-.330	210	215	-.309	.100	-.040	-.691	210	265	-.081	.032	.050	-.233
210	132	-.115	.041	-.001	-.360	210	216	-.181	.069	.032	-.455	210	266	-.076	.034	.048	-.189
210	133	-.112	.038	-.002	-.327	210	217	-.163	.053	-.000	-.415	210	267	-.074	.035	.047	-.210
210	134	-.113	.037	.014	-.351	210	218	-.116	.040	.057	-.300	210	268	-.109	.043	.088	-.304
210	135	-.113	.035	.022	-.281	210	219	-.109	.039	.038	-.265	210	269	-.096	.032	.038	-.250
210	136	-.111	.040	.034	-.407	210	220	-.221	.162	.359	-.957	210	270	-.089	.032	.038	-.209
210	137	-.104	.046	.034	-.460	210	221	-.238	.169	.382	-1.027	210	271	-.079	.030	.037	-.176
210	138	-.104	.045	.030	-.493	210	222	-.550	.216	-.061	-1.326	210	272	-.076	.033	.045	-.199
210	139	-.101	.035	.009	-.240	210	223	-.294	.103	-.008	-.736	210	273	-.080	.037	.081	-.224
210	140	-.107	.040	.019	-.293	210	224	-.186	.062	.047	-.508	210	274	-.090	.036	.042	-.261
210	141	-.108	.044	.059	-.364	210	225	-.174	.048	-.019	-.386	210	275	-.083	.034	.038	-.285
210	142	-.105	.043	.019	-.346	210	226	-.121	.042	.023	-.282	210	276	-.074	.030	.028	-.178
210	143	-.112	.043	.039	-.305	210	227	-.118	.039	.008	-.295	210	277	-.070	.033	.047	-.217
210	144	-.084	.034	.009	-.218	210	228	-.211	.150	.360	-.885	210	301	-.141	.211	.765	-.908
210	145	-.078	.037	.088	-.338	210	229	-.234	.142	.271	-.799	210	302	-.101	.227	.787	-.720
210	146	-.076	.035	.050	-.234	210	230	-.552	.194	-.093	-1.579	210	303	-.146	.179	.767	-.670
210	147	-.081	.037	.053	-.312	210	231	-.300	.092	.010	-.692	210	304	-.076	.245	.855	-.768
210	148	-.099	.032	.002	-.254	210	232	-.192	.056	-.010	-.430	210	305	.212	.177	.891	-.247
210	149	-.101	.040	.039	-.368	210	233	-.159	.044	.001	-.337	210	306	.222	.160	.819	-.307
210	150	-.101	.045	.044	-.367	210	234	-.116	.039	.045	-.295	210	307	.227	.176	.875	-.325
210	151	-.066	.034	.077	-.182	210	235	-.113	.037	.025	-.259	210	308	.028	.219	.931	-.697
210	152	-.068	.034	.063	-.179	210	236	-.189	.120	.211	-.871	210	309	-.095	.275	.830	-.998
210	153	-.074	.030	.031	-.238	210	237	-.209	.121	.266	-.886	210	310	-.275	.197	.591	-1.008
210	154	-.081	.039	.041	-.392	210	238	-.464	.164	-.076	-1.473	210	311	.189	.147	.777	-.212
210	155	-.091	.053	.103	-.481	210	239	-.259	.079	-.011	-.637	210	312	.309	.184	.970	-.257
210	156	-.092	.054	.125	-.456	210	240	-.167	.050	-.017	-.470	210	313	.325	.196	.981	-.387
210	157	-.072	.028	.024	-.187	210	241	-.143	.041	-.026	-.361	210	314	.225	.166	.784	-.310
210	158	-.055	.033	.093	-.263	210	242	-.109	.038	.023	-.287	210	315	-.194	.177	.732	-.803
210	159	-.059	.031	.043	-.158	210	243	-.108	.038	.023	-.261	210	316	.035	.287	1.055	-.873
210	160	-.057	.031	.053	-.182	210	244	-.167	.093	.092	-.574	210	317	-.219	.156	.435	-.762
210	161	-.063	.030	.036	-.187	210	245	-.174	.095	.198	-.647	210	318	-.266	.105	.224	-.660
210	162	-.073	.046	.160	-.320	210	246	-.359	.119	-.111	-1.183	210	319	-.130	.207	.516	-.973

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
210	320	-.261	.239	.610	-1.285
210	321	.112	.125	.772	-.340
210	322	.259	.153	.909	-.098
210	323	.277	.188	1.019	-.201
210	324	.180	.183	.904	-.319
210	325	-.207	.186	.457	-1.014
210	326	-.034	.211	.794	-.901
210	327	-.134	.204	.612	-1.061
210	328	-.238	.174	.396	-1.086
210	329	.075	.104	.545	-.368
210	330	.173	.139	.814	-.131
210	331	.195	.155	.884	-.185
210	332	.132	.133	.765	-.293
210	333	-.201	.169	.443	-.994
210	334	-.059	.202	.762	-1.013
210	335	-.203	.121	.242	-.668
210	336	-.251	.092	.067	-.660
210	337	-.133	.156	.388	-.987
210	338	-.222	.167	.276	-1.127
210	339	.041	.094	.511	-.264
210	340	.153	.106	.725	-.126
210	341	.168	.135	.878	-.176
210	342	.096	.129	.750	-.257
210	343	-.188	.137	.511	-.845
210	344	-.064	.139	.483	-.578
210	345	-.113	.131	.533	-.817
210	346	-.189	.125	.233	-.891
210	347	.034	.082	.424	-.223
210	348	.106	.100	.609	-.149
210	349	.099	.097	.564	-.188
210	350	.050	.090	.471	-.262
210	351	-.146	.102	.341	-.508
210	352	-.063	.106	.354	-.521
210	353	-.139	.073	.132	-.511
210	354	-.172	.075	.132	-.571
210	355	-.066	.102	.323	-.517
210	356	-.118	.074	.102	-.535
210	357	-.006	.069	.361	-.255
210	358	.033	.080	.423	-.145
210	359	.035	.081	.446	-.174
210	360	-.009	.063	.344	-.190
210	361	-.121	.087	.168	-.525
210	362	-.076	.100	.450	-.575
210	363	-.051	.059	.311	-.347
210	364	-.066	.043	.170	-.288
210	365	-.047	.046	.180	-.210
210	366	-.039	.046	.198	-.211
210	367	-.041	.045	.206	-.212
210	368	-.055	.034	.140	-.216
210	369	-.084	.054	.139	-.427
210	370	-.066	.052	.224	-.367
210	371	-.067	.042	.082	-.295
210	372	-.097	.042	.063	-.327
210	373	-.044	.043	.192	-.206
210	374	-.058	.054	.325	-.371
210	375	-.068	.055	.247	-.406
210	376	-.063	.052	.235	-.236
210	377	-.029	.038	.156	-.156
210	378	-.016	.051	.284	-.152
210	379	-.024	.052	.224	-.190
210	380	-.036	.045	.166	-.165
210	401	-.116	.048	.053	-.348
210	402	-.132	.057	.059	-.446
210	403	-.175	.062	.009	-.493
210	404	-.302	.119	.113	-.864
210	405	-.308	.144	.267	-1.068
210	406	-.069	.054	.309	-.285
210	407	-.094	.048	.116	-.340
210	408	-.135	.068	.130	-.478
210	409	-.246	.095	.028	-.634
210	410	-.453	.204	.105	-1.235
210	411	-.306	.171	.271	-.997
210	412	-.102	.040	.032	-.278
210	413	-.100	.047	.096	-.371
210	414	-.137	.047	.031	-.340
210	415	-.150	.060	.025	-.538
210	416	-.257	.108	.006	-.827
210	417	-.452	.201	.044	-1.392
210	418	-.302	.234	.499	-1.251
210	419	-.268	.174	.269	-1.338
210	420	-.104	.039	.006	-.292
210	421	-.101	.046	.068	-.364
210	422	-.136	.050	-.003	-.457
210	423	-.154	.061	.023	-.424
210	424	-.243	.107	.030	-.728
210	425	-.419	.186	.114	-1.566
210	426	-.288	.202	.524	-1.173
210	427	-.272	.212	.565	-1.250
210	428	-.103	.041	.058	-.428
210	429	-.097	.047	.160	-.407
210	430	-.130	.045	.035	-.476
210	431	-.147	.068	.054	-.595
210	432	-.225	.104	.061	-.738
210	433	-.386	.190	.146	-1.290
210	434	-.308	.187	.238	-1.111
210	435	-.288	.191	.250	-1.181
210	436	-.100	.039	.030	-.273
210	437	-.093	.044	.061	-.285
210	438	-.115	.040	.040	-.323
210	439	-.127	.057	.059	-.451
210	440	-.190	.086	.030	-.665
210	441	-.317	.155	-.017	-1.130
210	442	-.258	.152	.173	-1.109
210	443	-.245	.152	.208	-1.152
210	444	-.090	.038	.053	-.313
210	445	-.083	.041	.125	-.329
210	446	-.099	.034	.049	-.280
210	447	-.108	.046	.094	-.378
210	448	-.155	.064	.039	-.465
210	449	-.252	.115	.043	-.928
210	450	-.228	.126	.085	-1.042
210	451	-.215	.117	.089	-.915
210	452	-.083	.037	.051	-.212
210	453	-.073	.038	.077	-.219
210	454	-.080	.032	.032	-.218
210	455	-.084	.040	.020	-.363
210	456	-.113	.054	.051	-.400
210	457	-.176	.096	.015	-.666
210	458	-.154	.087	.097	-.734
210	459	-.150	.087	.118	-.798
210	460	-.075	.035	.032	-.221
210	461	-.066	.034	.070	-.226
210	462	-.065	.032	.080	-.178
210	463	-.075	.033	.047	-.210
210	464	-.075	.040	.131	-.292
210	465	-.106	.059	.050	-.446
210	466	-.082	.052	.160	-.432
210	467	-.099	.057	.054	-.522
210	468	-.066	.036	.068	-.196
210	469	-.068	.030	.050	-.179
210	470	-.070	.038	.067	-.228
210	471	-.078	.042	.075	-.300
210	472	-.093	.055	.049	-.500
210	473	-.072	.028	.019	-.167
210	474	-.067	.034	.050	-.184
210	475	-.075	.038	.040	-.224
210	476	-.076	.039	.043	-.300
210	477	-.081	.035	.023	-.274
210	801	-.082	.029	.048	-.189
210	802	-.085	.033	.079	-.213
210	803	-.088	.035	.080	-.246
210	804	-.058	.032	.079	-.167
210	805	-.060	.030	.079	-.163
210	806	-.071	.041	.130	-.235
210	807	-.074	.040	.115	-.260
210	808	-.070	.039	.077	-.250
210	809	-.072	.034	.041	-.254
210	810	-.076	.042	.140	-.293
210	901	-.109	.049	.106	-.344
210	902	-.182	.065	.045	-.529

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
210	903	-.318	.114	.061	-.884	220	135	-.123	.038	-.015	-.467	220	219	-.128	.049	.117	-.410
210	904	-.252	.063	-.041	-.514	220	136	-.122	.043	-.002	-.530	220	220	-.323	.172	.252	-1.317
210	905	-.112	.049	.103	-.348	220	137	-.104	.046	.038	-.396	220	221	-.338	.180	.381	-1.377
210	906	-.139	.073	.112	-.465	220	138	-.101	.043	.046	-.370	220	222	-.407	.151	.004	-1.117
210	907	-.343	.131	.099	-.944	220	139	-.108	.036	-.007	-.476	220	223	-.267	.094	.029	-.810
210	908	-.123	.034	.040	-.269	220	140	-.125	.049	-.015	-.794	220	224	-.191	.063	.022	-.548
210	909	-.132	.041	.021	-.325	220	141	-.128	.048	.008	-.499	220	225	-.159	.046	-.013	-.418
210	910	-.242	.082	.091	-.615	220	142	-.131	.055	-.016	-.670	220	226	-.135	.045	.004	-.358
210	911	-.289	.082	-.073	-.615	220	143	-.101	.039	.043	-.290	220	227	-.134	.045	.001	-.393
210	912	-.127	.057	.066	-.378	220	144	-.070	.032	.038	-.216	220	228	-.275	.150	.152	-1.151
210	913	-.266	.076	-.003	-.624	220	145	-.087	.034	.049	-.239	220	229	-.292	.159	.250	-1.151
210	914	-.329	.119	.211	-1.008	220	146	-.088	.034	.026	-.222	220	230	-.389	.152	.014	-1.222
210	915	-.075	.079	.314	-.451	220	147	-.095	.036	.020	-.304	220	231	-.252	.086	.005	-.879
210	916	-.113	.038	.011	-.364	220	148	-.115	.034	-.013	-.246	220	232	-.180	.060	.026	-.794
210	917	-.171	.063	.038	-.639	220	149	-.119	.046	.012	-.414	220	233	-.150	.042	-.020	-.381
210	918	-.310	.119	.098	-.877	220	150	-.124	.053	.017	-.474	220	234	-.127	.041	-.003	-.305
220	101	-.155	.051	-.019	-.390	220	151	-.087	.034	.045	-.206	220	235	-.128	.041	.008	-.362
220	102	-.142	.043	.008	-.360	220	152	-.083	.033	.039	-.209	220	236	-.212	.114	.116	-.905
220	103	-.147	.060	.045	-.461	220	153	-.084	.029	.026	-.192	220	237	-.230	.113	.115	-.926
220	104	-.127	.047	.039	-.356	220	154	-.084	.036	.037	-.283	220	238	-.361	.147	-.041	-1.001
220	105	-.128	.046	.047	-.312	220	155	-.092	.051	.108	-.454	220	239	-.222	.075	-.009	-.558
220	106	-.121	.042	.005	-.322	220	156	-.094	.053	.190	-.361	220	240	-.155	.051	.021	-.358
220	107	-.119	.042	.026	-.300	220	157	-.093	.029	.024	-.220	220	241	-.137	.040	.019	-.290
220	108	-.116	.043	.025	-.299	220	158	-.054	.030	.090	-.156	220	242	-.116	.039	.052	-.250
220	109	-.128	.040	-.007	-.290	220	159	-.075	.031	.038	-.178	220	243	-.119	.041	.039	-.285
220	110	-.125	.044	.012	-.288	220	160	-.074	.032	.030	-.182	220	244	-.175	.090	.144	-.644
220	111	-.125	.042	.015	-.288	220	161	-.070	.032	.079	-.204	220	245	-.178	.094	.098	-.808
220	112	-.122	.042	.013	-.299	220	162	-.075	.053	.203	-.281	220	246	-.283	.134	-.016	-1.041
220	113	-.122	.037	-.017	-.271	220	163	-.085	.039	.036	-.232	220	247	-.178	.068	.005	-.609
220	114	-.121	.042	.000	-.300	220	164	-.073	.030	.066	-.193	220	248	-.128	.046	.033	-.372
220	115	-.156	.057	.017	-.504	220	165	-.075	.031	.100	-.208	220	249	-.117	.039	.004	-.300
220	116	-.145	.049	-.023	-.370	220	166	-.072	.048	.286	-.303	220	250	-.099	.039	.039	-.285
220	117	-.130	.035	.017	-.338	220	201	-.300	.103	-.018	-.744	220	251	-.111	.042	.013	-.327
220	118	-.128	.038	.027	-.339	220	202	-.302	.124	-.003	-1.026	220	252	-.152	.066	.099	-.581
220	119	-.126	.035	.038	-.283	220	203	-.184	.072	.059	-.577	220	253	-.148	.066	.127	-.560
220	120	-.125	.033	-.029	-.328	220	204	-.155	.064	.045	-.642	220	254	-.186	.084	-.016	-.765
220	121	-.125	.040	.010	-.588	220	205	-.155	.056	.019	-.641	220	255	-.139	.048	.001	-.379
220	122	-.123	.040	.029	-.550	220	206	-.347	.188	.097	-1.463	220	256	-.114	.040	.028	-.313
220	123	-.132	.042	.007	-.431	220	207	-.385	.147	-.079	-1.175	220	257	-.101	.034	.002	-.239
220	124	-.130	.044	-.007	-.466	220	208	-.268	.087	.015	-.795	220	258	-.090	.035	.019	-.237
220	125	-.126	.039	-.011	-.293	220	209	-.181	.078	.040	-.787	220	259	-.091	.039	.032	-.265
220	126	-.124	.040	-.016	-.327	220	210	-.143	.062	.041	-.560	220	260	-.124	.052	.040	-.576
220	127	-.127	.036	-.005	-.285	220	211	-.122	.061	.072	-.473	220	261	-.115	.041	.007	-.423
220	128	-.124	.041	.012	-.283	220	212	-.319	.163	.213	-1.077	220	262	-.125	.038	-.010	-.338
220	129	-.146	.045	.007	-.337	220	213	-.349	.175	.287	-1.156	220	263	-.117	.036	.029	-.282
220	130	-.118	.048	.071	-.366	220	214	-.410	.149	-.052	-1.021	220	264	-.104	.034	.002	-.225
220	131	-.127	.048	-.000	-.575	220	215	-.275	.106	.057	-.895	220	265	-.100	.031	-.003	-.248
220	132	-.125	.051	.005	-.708	220	216	-.188	.072	.046	-.639	220	266	-.095	.035	.009	-.245
220	133	-.122	.041	-.007	-.347	220	217	-.157	.059	.052	-.538	220	267	-.097	.036	.015	-.246
220	134	-.124	.041	.009	-.327	220	218	-.133	.047	.046	-.349	220	268	-.112	.034	-.000	-.265

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
220	269	-.107	.031	.014	-.246	220	342	.001	.121	.606	-.451	220	412	-.092	.041	.103	-.241
220	270	-.100	.033	.024	-.257	220	343	-.199	.129	.297	-.870	220	413	-.079	.054	.158	-.276
220	271	-.094	.032	.022	-.282	220	344	-.099	.127	.399	-.701	220	414	-.115	.044	.084	-.303
220	272	-.093	.034	.021	-.251	220	345	-.089	.093	.502	-.590	220	415	-.096	.050	.098	-.296
220	273	-.091	.033	.062	-.205	220	346	-.115	.088	.136	-.641	220	416	-.157	.079	.125	-.532
220	274	-.100	.034	.034	-.210	220	347	-.032	.085	.389	-.298	220	417	-.293	.145	.222	-1.157
220	275	-.098	.035	.052	-.218	220	348	.005	.110	.673	-.236	220	418	-.038	.213	.801	-.826
220	276	-.088	.030	.004	-.215	220	349	.007	.122	.580	-.315	220	419	-.033	.168	.639	-.674
220	277	-.083	.033	.015	-.222	220	350	-.023	.116	.495	-.459	220	420	-.098	.036	.049	-.212
220	301	-.090	.222	1.153	-.740	220	351	-.151	.103	.313	-.600	220	421	-.084	.046	.135	-.247
220	302	-.035	.199	.775	-.701	220	352	-.091	.102	.352	-.677	220	422	-.114	.044	.050	-.280
220	303	-.183	.149	.569	-.847	220	353	-.090	.061	.174	-.410	220	423	-.100	.051	.203	-.339
220	304	.071	.213	.863	-.780	220	354	-.155	.074	.162	-.530	220	424	-.147	.081	.200	-.484
220	305	.136	.172	.940	-.363	220	355	-.087	.069	.222	-.595	220	425	-.268	.145	.428	-.692
220	306	.094	.153	.860	-.354	220	356	-.098	.049	.136	-.379	220	426	-.087	.174	.592	-.853
220	307	.103	.166	.876	-.327	220	357	-.088	.062	.237	-.317	220	427	-.074	.177	.647	-.912
220	308	-.149	.239	.843	-1.170	220	358	-.079	.073	.364	-.279	220	428	-.100	.036	.053	-.290
220	309	.065	.218	.923	-.981	220	359	-.080	.075	.337	-.313	220	429	-.085	.042	.178	-.315
220	310	.010	.196	.650	-.654	220	360	-.086	.060	.286	-.270	220	430	-.104	.039	.033	-.280
220	311	.152	.162	.891	-.443	220	361	-.133	.076	.207	-.588	220	431	-.097	.052	.110	-.349
220	312	.171	.168	.939	-.334	220	362	-.108	.088	.320	-.638	220	432	-.134	.070	.088	-.580
220	313	.132	.172	.880	-.324	220	363	-.094	.040	.099	-.327	220	433	-.214	.120	.201	-1.000
220	314	.015	.142	.668	-.430	220	364	-.097	.031	.050	-.231	220	434	-.108	.121	.401	-.800
220	315	-.327	.184	.635	-1.137	220	365	-.109	.038	.051	-.265	220	435	-.112	.121	.491	-.832
220	316	-.242	.265	.766	-1.278	220	366	-.107	.037	.054	-.255	220	436	-.099	.036	.074	-.257
220	317	-.099	.153	.683	-.960	220	367	-.108	.037	.069	-.258	220	437	-.083	.038	.093	-.262
220	318	-.286	.099	.052	-.859	220	368	-.113	.032	.027	-.253	220	438	-.090	.035	.062	-.256
220	319	.018	.148	.658	-.563	220	369	-.115	.042	.054	-.352	220	439	-.086	.044	.101	-.297
220	320	-.022	.218	.898	-.964	220	370	-.108	.041	.179	-.298	220	440	-.111	.059	.107	-.386
220	321	.098	.135	1.017	-.270	220	371	-.074	.037	.059	-.218	220	441	-.160	.097	.144	-.734
220	322	.121	.114	.621	-.172	220	372	-.112	.039	.036	-.266	220	442	-.138	.099	.152	-.681
220	323	.089	.139	.871	-.258	220	373	-.093	.033	.088	-.234	220	443	-.138	.101	.186	-.729
220	324	-.022	.150	.668	-.497	220	374	-.101	.039	.042	-.265	220	444	-.087	.038	.048	-.238
220	325	-.320	.195	.245	-1.212	220	375	-.106	.039	.059	-.319	220	445	-.072	.039	.077	-.299
220	326	-.232	.239	.811	-1.397	220	376	-.104	.039	.052	-.273	220	446	-.075	.035	.057	-.218
220	327	-.042	.144	.537	-1.044	220	377	-.088	.040	.132	-.212	220	447	-.071	.042	.081	-.280
220	328	-.087	.136	.493	-.805	220	378	-.080	.049	.233	-.226	220	448	-.090	.053	.053	-.435
220	329	.032	.101	.680	-.382	220	379	-.084	.048	.197	-.220	220	449	-.123	.081	.040	-.897
220	330	.072	.118	.864	-.212	220	380	-.085	.044	.142	-.224	220	450	-.116	.075	.157	-.659
220	331	.056	.134	.843	-.256	220	401	-.115	.054	.062	-.433	220	451	-.117	.072	.137	-.649
220	332	-.020	.112	.493	-.386	220	402	-.127	.064	.086	-.498	220	452	-.077	.037	.027	-.269
220	333	-.256	.159	.380	-.954	220	403	-.133	.063	.088	-.571	220	453	-.062	.036	.063	-.237
220	334	-.158	.199	.613	-1.089	220	404	-.219	.115	.191	-.737	220	454	-.059	.032	.083	-.179
220	335	-.124	.085	.297	-.642	220	405	-.124	.154	.458	-.740	220	455	-.060	.035	.105	-.229
220	336	-.237	.081	.023	-.677	220	406	-.055	.061	.217	-.287	220	456	-.074	.038	.057	-.353
220	337	-.091	.116	.540	-.738	220	407	-.071	.051	.133	-.277	220	457	-.089	.050	.050	-.471
220	338	-.128	.119	.332	-.892	220	408	-.087	.065	.164	-.356	220	458	-.094	.054	.076	-.542
220	339	.003	.094	.631	-.247	220	409	-.164	.071	.121	-.501	220	459	-.097	.057	.091	-.605
220	340	.048	.094	.493	-.224	220	410	-.256	.134	.286	-.892	220	460	-.065	.032	.064	-.247
220	341	.055	.120	.620	-.212	220	411	-.088	.151	.405	-.755	220	461	-.056	.031	.054	-.191

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
220	462	-.055	.026	.059	-.139	230	107	-.152	.047	-.026	-.357	230	157	-.127	.032	-.001	-.248
220	463	-.068	.026	.029	-.177	230	108	-.148	.047	.000	-.373	230	158	-.027	.035	.157	-.122
220	464	-.064	.030	.050	-.172	230	109	-.170	.046	-.042	-.406	230	159	-.086	.033	.052	-.197
220	465	-.086	.034	.030	-.251	230	110	-.163	.047	-.022	-.403	230	160	-.087	.034	.067	-.207
220	466	-.089	.035	.059	-.267	230	111	-.162	.044	-.028	-.338	230	161	-.091	.033	.092	-.226
220	467	-.102	.039	.024	-.272	230	112	-.159	.043	-.018	-.329	230	162	-.123	.061	.155	-.469
220	468	-.065	.029	.042	-.184	230	113	-.163	.043	-.039	-.354	230	163	-.109	.035	.017	-.263
220	469	-.063	.028	.047	-.156	230	114	-.159	.049	-.014	-.389	230	164	-.090	.033	.048	-.198
220	470	-.063	.033	.073	-.177	230	115	-.197	.074	-.012	-.724	230	165	-.106	.033	.056	-.298
220	471	-.066	.034	.068	-.181	230	116	-.168	.054	.035	-.384	230	166	-.117	.045	.125	-.323
220	472	-.072	.034	.058	-.251	230	117	-.172	.047	-.051	-.555	230	201	-.441	.158	-.110	-1.221
220	473	-.066	.027	.019	-.173	230	118	-.166	.049	-.039	-.587	230	202	-.389	.173	.041	-1.199
220	474	-.059	.032	.044	-.194	230	119	-.163	.043	-.040	-.343	230	203	-.250	.110	.001	-.931
220	475	-.063	.033	.045	-.196	230	120	-.158	.038	-.051	-.342	230	204	-.219	.104	.027	-.978
220	476	-.063	.032	.053	-.195	230	121	-.152	.043	-.022	-.381	230	205	-.208	.079	.004	-.658
220	477	-.078	.028	.052	-.182	230	122	-.153	.044	-.019	-.381	230	206	-.519	.235	-.035	-1.466
220	801	-.105	.032	.028	-.224	230	123	-.167	.045	-.035	-.363	230	207	-.426	.145	-.113	-1.266
220	802	-.105	.036	.044	-.231	230	124	-.162	.049	-.022	-.386	230	208	-.316	.112	-.067	-.887
220	803	-.107	.037	.045	-.260	230	125	-.158	.044	-.019	-.373	230	209	-.240	.111	.067	-.864
220	804	-.060	.034	.080	-.192	230	126	-.151	.042	-.030	-.368	230	210	-.197	.080	.038	-.754
220	805	-.062	.027	.033	-.156	230	127	-.145	.035	-.032	-.325	230	211	-.174	.075	.041	-.588
220	806	-.068	.033	.052	-.184	230	128	-.141	.040	-.017	-.332	230	212	-.466	.188	.038	-1.362
220	807	-.102	.035	.026	-.216	230	129	-.170	.048	-.033	-.489	230	213	-.494	.197	.086	-1.463
220	808	-.105	.038	.038	-.243	230	130	-.114	.047	.058	-.302	230	214	-.456	.159	-.028	-1.224
220	809	-.108	.033	.067	-.275	230	131	-.167	.057	-.037	-.699	230	215	-.345	.137	-.005	-.991
220	810	-.107	.040	.047	-.322	230	132	-.160	.055	-.029	-.528	230	216	-.243	.100	.021	-.931
220	901	-.132	.054	.066	-.486	230	133	-.155	.046	-.021	-.390	230	217	-.199	.079	.022	-.651
220	902	-.186	.076	.038	-.732	230	134	-.153	.047	-.023	-.414	230	218	-.181	.065	.008	-.562
220	903	-.254	.099	.083	-.838	230	135	-.154	.044	-.030	-.612	230	219	-.179	.070	.001	-.664
220	904	-.222	.062	.061	-.514	230	136	-.148	.049	-.012	-.797	230	220	-.490	.197	-.003	-1.287
220	905	-.120	.051	.090	-.342	230	137	-.147	.062	.071	-.578	230	221	-.506	.201	.003	-1.416
220	906	-.132	.062	.131	-.465	230	138	-.143	.054	.041	-.476	230	222	-.446	.148	-.075	-1.069
220	907	-.243	.105	.189	-.845	230	139	-.159	.048	-.027	-.430	230	223	-.340	.140	.041	-1.036
220	908	-.132	.037	-.006	-.301	230	140	-.165	.059	-.019	-.499	230	224	-.249	.100	.081	-.762
220	909	-.141	.046	.002	-.346	230	141	-.158	.062	-.008	-.686	230	225	-.197	.066	-.006	-.764
220	910	-.215	.080	.115	-.549	230	142	-.161	.056	-.009	-.479	230	226	-.171	.063	.038	-.578
220	911	-.272	.081	-.021	-.700	230	143	-.130	.038	.014	-.325	230	227	-.169	.062	.001	-.550
220	912	-.155	.065	.066	-.540	230	144	-.054	.035	.064	-.200	230	228	-.410	.185	.060	-1.238
220	913	-.234	.071	-.017	-.608	230	145	-.125	.040	.030	-.315	230	229	-.433	.193	.018	-1.416
220	914	-.262	.170	.480	-1.093	230	146	-.128	.042	.019	-.397	230	230	-.407	.158	-.067	-1.328
220	915	-.126	.086	.352	-.581	230	147	-.140	.048	.021	-.407	230	231	-.293	.121	-.003	-1.263
220	916	-.124	.045	.036	-.329	230	148	-.162	.048	-.032	-.433	230	232	-.209	.086	-.023	-.817
220	917	-.163	.075	.092	-.531	230	149	-.187	.063	-.027	-.610	230	233	-.186	.060	-.041	-.560
220	918	-.238	.119	.268	-.836	230	150	-.186	.070	-.009	-.633	230	234	-.161	.059	.023	-.523
230	101	-.212	.072	-.037	-.660	230	151	-.116	.033	.002	-.263	230	235	-.161	.056	-.016	-.484
230	102	-.181	.052	-.046	-.433	230	152	-.110	.033	.037	-.269	230	236	-.316	.151	.119	-1.155
230	103	-.194	.072	-.016	-.561	230	153	-.111	.029	-.008	-.253	230	237	-.335	.150	.067	-1.140
230	104	-.161	.054	-.001	-.443	230	154	-.113	.041	.013	-.296	230	238	-.313	.119	-.015	-.913
230	105	-.161	.051	-.020	-.407	230	155	-.148	.067	.045	-.477	230	239	-.226	.075	-.018	-.786
230	106	-.151	.047	-.005	-.372	230	156	-.166	.065	.053	-.488	230	240	-.169	.057	.017	-.691

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
230	241	-.156	.043	-.006	-.442	230	314	-.067	.096	.547	-.380	230	364	-.130	.029	-.025	-.226
230	242	-.141	.045	.006	-.404	230	315	-.456	.189	.280	-1.347	230	365	-.159	.038	.009	-.320
230	243	-.145	.049	-.011	-.368	230	316	-.430	.239	.545	-1.435	230	366	-.147	.036	.013	-.274
230	244	-.217	.088	.157	-.734	230	317	-.019	.157	.636	-.751	230	367	-.140	.036	.019	-.281
230	245	-.240	.097	.080	-1.224	230	318	-.330	.132	.054	-1.081	230	368	-.143	.032	-.004	-.279
230	246	-.213	.083	.011	-.734	230	319	.143	.141	.698	-.394	230	369	-.140	.040	.024	-.422
230	247	-.174	.057	.018	-.424	230	320	.120	.188	.856	-.720	230	370	-.137	.038	.034	-.314
230	248	-.146	.046	.001	-.367	230	321	.147	.156	.782	-.550	230	371	-.071	.032	.052	-.172
230	249	-.136	.038	.018	-.351	230	322	.152	.115	.856	-.119	230	372	-.126	.033	-.006	-.233
230	250	-.130	.041	.021	-.344	230	323	.064	.116	.684	-.245	230	373	-.110	.027	-.018	-.220
230	251	-.143	.049	.028	-.891	230	324	-.098	.119	.618	-.475	230	374	-.134	.036	-.005	-.296
230	252	-.165	.058	-.016	-.530	230	325	-.476	.201	.200	-1.428	230	375	-.130	.035	.009	-.256
230	253	-.160	.046	.031	-.412	230	326	-.386	.237	.521	-1.361	230	376	-.125	.036	.028	-.255
230	254	-.150	.046	.003	-.422	230	327	.047	.131	.626	-.737	230	377	-.133	.031	.020	-.258
230	255	-.139	.040	.028	-.318	230	328	.038	.113	.703	-.480	230	378	-.116	.036	.063	-.244
230	256	-.129	.038	.010	-.274	230	329	.045	.123	.824	-.459	230	379	-.122	.035	.059	-.233
230	257	-.129	.034	-.019	-.304	230	330	.044	.109	.620	-.398	230	380	-.118	.036	.101	-.257
230	258	-.125	.038	.013	-.324	230	331	-.002	.100	.519	-.309	230	401	-.143	.068	.076	-.545
230	259	-.126	.043	.023	-.325	230	332	-.108	.089	.260	-.463	230	402	-.152	.082	.059	-.592
230	260	-.145	.045	.008	-.618	230	333	-.409	.203	.248	-1.439	230	403	-.115	.068	.136	-.499
230	261	-.138	.037	-.024	-.410	230	334	-.334	.253	.471	-1.533	230	404	-.202	.136	.440	-.654
230	262	-.141	.037	-.013	-.373	230	335	-.047	.104	.420	-.527	230	405	-.004	.162	.551	-.704
230	263	-.136	.037	.026	-.790	230	336	-.248	.104	.052	-1.093	230	406	-.035	.065	.273	-.361
230	264	-.121	.032	-.016	-.248	230	337	-.024	.081	.429	-.379	230	407	-.041	.053	.175	-.232
230	265	-.119	.033	.008	-.235	230	338	-.028	.085	.440	-.426	230	408	-.040	.070	.208	-.309
230	266	-.116	.036	.028	-.254	230	339	-.058	.107	.310	-.671	230	409	-.125	.072	.214	-.354
230	267	-.116	.036	.026	-.257	230	340	-.036	.073	.336	-.372	230	410	-.234	.131	.304	-.816
230	268	-.123	.035	.015	-.357	230	341	-.056	.089	.436	-.332	230	411	.037	.147	.581	-.555
230	269	-.130	.031	-.016	-.245	230	342	-.118	.096	.398	-.433	230	412	-.092	.045	.069	-.336
230	270	-.125	.033	-.007	-.259	230	343	-.287	.148	.250	-1.150	230	413	-.052	.067	.266	-.340
230	271	-.117	.032	.009	-.250	230	344	-.228	.152	.257	-1.021	230	414	-.113	.046	.129	-.340
230	272	-.118	.035	.017	-.248	230	345	-.065	.057	.253	-.444	230	415	-.055	.052	.131	-.271
230	273	-.113	.033	-.013	-.249	230	346	-.060	.057	.279	-.456	230	416	-.097	.085	.231	-.435
230	274	-.119	.033	-.007	-.259	230	347	-.160	.105	.195	-.781	230	417	-.260	.145	.411	-.984
230	275	-.118	.034	-.023	-.259	230	348	-.125	.079	.231	-.512	230	418	.167	.216	.890	-.674
230	276	-.114	.026	-.020	-.198	230	349	-.139	.068	.246	-.483	230	419	.142	.166	.671	-.767
230	277	-.105	.031	.005	-.237	230	350	-.162	.070	.247	-.459	230	420	-.099	.040	.054	-.249
230	301	-.135	.216	.983	-.969	230	351	-.212	.088	.124	-.774	230	421	-.063	.054	.195	-.243
230	302	.028	.187	.658	-.644	230	352	-.195	.085	.198	-.746	230	422	-.115	.047	.049	-.336
230	303	-.283	.149	.358	-.922	230	353	-.039	.051	.214	-.305	230	423	-.062	.051	.182	-.254
230	304	.163	.191	.905	-.446	230	354	-.158	.053	.050	-.407	230	424	-.089	.082	.261	-.440
230	305	.172	.175	.774	-.288	230	355	-.107	.047	.106	-.327	230	425	-.219	.148	.329	-.966
230	306	.060	.139	.569	-.334	230	356	-.091	.037	.080	-.243	230	426	.124	.158	.756	-.633
230	307	.082	.136	.636	-.342	230	357	-.199	.071	.048	-.552	230	427	.106	.178	.889	-.642
230	308	-.348	.246	.573	-1.182	230	358	-.178	.064	.120	-.470	230	428	-.092	.042	.081	-.264
230	309	.221	.198	.947	-.419	230	359	-.156	.051	.140	-.378	230	429	-.063	.054	.201	-.275
230	310	.195	.181	.830	-.609	230	360	-.156	.039	.078	-.401	230	430	-.094	.040	.104	-.256
230	311	.233	.194	1.067	-.349	230	361	-.157	.048	.080	-.476	230	431	-.057	.059	.186	-.311
230	312	.203	.174	1.045	-.209	230	362	-.160	.053	.123	-.524	230	432	-.079	.075	.247	-.516
230	313	.119	.142	.872	-.256	230	363	-.127	.036	.014	-.281	230	433	-.166	.139	.400	-.807

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
230	434	.021	.113	.484	-.519	230	807	-.122	.036	.061	-.260	240	129	-.169	.055	-.019	-.469
230	435	.007	.126	.561	-.493	230	808	-.129	.037	.050	-.284	240	130	-.111	.049	.097	-.317
230	436	-.091	.041	.095	-.274	230	809	-.136	.029	-.020	-.237	240	131	-.168	.058	-.014	-.650
230	437	-.062	.049	.178	-.252	230	810	-.131	.034	.009	-.251	240	132	-.163	.058	-.024	-.722
230	438	-.073	.039	.094	-.239	230	901	-.186	.073	.040	-.489	240	133	-.158	.050	-.022	-.486
230	439	-.048	.052	.243	-.276	230	902	-.258	.115	.075	-.959	240	134	-.158	.052	-.007	-.578
230	440	-.061	.063	.306	-.343	230	903	-.311	.120	.042	-.837	240	135	-.158	.047	-.032	-.384
230	441	-.101	.096	.264	-.557	230	904	-.274	.080	-.039	-.637	240	136	-.154	.051	-.011	-.399
230	442	-.051	.068	.282	-.441	230	905	-.156	.056	.031	-.409	240	137	-.153	.063	.026	-.631
230	443	-.062	.075	.253	-.505	230	906	-.161	.068	.058	-.537	240	138	-.153	.055	.028	-.452
230	444	-.087	.046	.176	-.314	230	907	-.233	.090	.106	-.640	240	139	-.167	.050	-.002	-.446
230	445	-.056	.048	.234	-.242	230	908	-.172	.044	-.029	-.353	240	140	-.179	.065	-.001	-.782
230	446	-.052	.036	.097	-.302	230	909	-.186	.059	-.013	-.468	240	141	-.208	.088	.025	-.902
230	447	-.037	.045	.236	-.244	230	910	-.294	.111	.105	-.783	240	142	-.177	.061	-.010	-.568
230	448	-.042	.049	.157	-.278	230	911	-.354	.111	-.096	-.847	240	143	-.129	.039	.002	-.287
230	449	-.060	.060	.150	-.534	230	912	-.225	.088	.056	-.606	240	144	-.044	.042	.148	-.315
230	450	-.067	.049	.145	-.387	230	913	-.305	.096	-.059	-.775	240	145	-.132	.043	.021	-.367
230	451	-.081	.051	.104	-.368	230	914	-.320	.235	.511	-1.228	240	146	-.133	.045	.043	-.365
230	452	-.072	.045	.104	-.309	230	915	-.204	.107	.186	-.509	240	147	-.149	.051	.017	-.440
230	453	-.044	.044	.164	-.233	230	916	-.161	.052	.004	-.420	240	148	-.240	.089	-.061	-.979
230	454	-.034	.037	.141	-.176	230	917	-.186	.080	.069	-.666	240	149	-.202	.064	-.027	-.739
230	455	-.030	.043	.169	-.187	230	918	-.274	.130	.177	-.973	240	150	-.205	.069	.006	-.757
230	456	-.041	.043	.183	-.212	240	101	-.205	.071	-.022	-.640	240	151	-.113	.035	.010	-.268
230	457	-.064	.044	.180	-.266	240	102	-.267	.078	-.083	-.664	240	152	-.110	.035	.019	-.336
230	458	-.082	.043	.167	-.397	240	103	-.191	.075	.055	-.570	240	153	-.109	.030	.010	-.234
230	459	-.091	.050	.151	-.475	240	104	-.239	.078	.007	-.677	240	154	-.113	.044	.044	-.397
230	460	-.045	.042	.107	-.224	240	105	-.234	.071	-.047	-.652	240	155	-.150	.078	.186	-.563
230	461	-.030	.039	.136	-.154	240	106	-.160	.055	.019	-.417	240	156	-.179	.076	.208	-.602
230	462	-.027	.033	.099	-.149	240	107	-.159	.055	.012	-.421	240	157	-.125	.032	-.022	-.263
230	463	-.039	.032	.068	-.194	240	108	-.157	.055	.014	-.407	240	158	-.028	.033	.109	-.132
230	464	-.051	.035	.092	-.198	240	109	-.173	.051	-.037	-.483	240	159	-.088	.033	.024	-.215
230	465	-.089	.036	.043	-.499	240	110	-.167	.052	-.024	-.470	240	160	-.093	.034	.052	-.216
230	466	-.121	.038	.028	-.249	240	111	-.163	.048	-.032	-.372	240	161	-.093	.032	.018	-.202
230	467	-.116	.040	.049	-.319	240	112	-.162	.046	-.021	-.355	240	162	-.129	.063	.089	-.437
230	468	-.033	.039	.129	-.447	240	113	-.163	.043	-.017	-.337	240	163	-.105	.033	.029	-.213
230	469	-.029	.030	.116	-.165	240	114	-.160	.049	.004	-.354	240	164	-.093	.034	.035	-.208
230	470	-.032	.036	.139	-.513	240	115	-.199	.078	.002	-.689	240	165	-.111	.036	.020	-.347
230	471	-.041	.034	.156	-.201	240	116	-.171	.055	-.005	-.400	240	166	-.124	.046	.107	-.314
230	472	-.060	.034	.124	-.567	240	117	-.180	.057	-.049	-.668	240	201	-.541	.168	-.152	-1.240
230	473	-.046	.033	.109	-.134	240	118	-.175	.057	-.037	-.618	240	202	-.454	.179	-.006	-1.394
230	474	-.023	.041	.164	-.143	240	119	-.167	.052	-.029	-.387	240	203	-.356	.151	.026	-1.237
230	475	-.031	.042	.211	-.155	240	120	-.159	.039	-.046	-.315	240	204	-.347	.171	.023	-1.405
230	476	-.036	.040	.149	-.153	240	121	-.154	.044	-.027	-.321	240	205	-.317	.121	-.055	-1.019
230	477	-.073	.031	.128	-.189	240	122	-.151	.045	-.017	-.324	240	206	-.571	.239	-.141	-1.697
230	801	-.123	.030	-.020	-.218	240	123	-.174	.054	-.014	-.451	240	207	-.433	.148	-.086	-1.274
230	802	-.116	.033	.011	-.223	240	124	-.169	.057	.001	-.505	240	208	-.402	.134	-.058	-1.013
230	803	-.119	.031	.005	-.235	240	125	-.159	.048	-.010	-.370	240	209	-.342	.149	.032	-1.080
230	804	-.032	.036	.170	-.144	240	126	-.154	.046	-.021	-.360	240	210	-.312	.122	-.033	-.947
230	805	-.031	.028	.145	-.123	240	127	-.151	.039	-.034	-.345	240	211	-.284	.116	.019	-.848
230	806	-.056	.032	.120	-.190	240	128	-.147	.044	-.006	-.356	240	212	-.542	.213	-.059	-1.694

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
240	213	-.557	.220	-.070	-1.872	240	263	-.172	.044	-.023	-.443	240	336	-.380	.177	-.007	-1.280
240	214	-.461	.189	-.055	-1.387	240	264	-.150	.039	-.008	-.288	240	337	.056	.090	.484	-.212
240	215	-.406	.160	.001	-1.250	240	265	-.152	.041	-.005	-.306	240	338	.064	.094	.511	-.213
240	216	-.337	.135	.036	-1.044	240	266	-.151	.045	.017	-.342	240	339	-.099	.169	.677	-.790
240	217	-.293	.118	-.018	-.836	240	267	-.148	.045	.046	-.333	240	340	-.075	.094	.319	-.603
240	218	-.276	.098	-.035	-.771	240	268	-.164	.047	-.027	-.721	240	341	-.118	.088	.323	-.701
240	219	-.293	.114	-.014	-.866	240	269	-.169	.045	-.008	-.455	240	342	-.223	.099	.275	-.617
240	220	-.525	.192	-.135	-1.444	240	270	-.157	.044	.019	-.388	240	343	-.446	.209	.080	-1.444
240	221	-.539	.197	-.133	-1.477	240	271	-.139	.046	.158	-.345	240	344	-.439	.191	.230	-1.389
240	222	-.434	.171	.025	-1.133	240	272	-.139	.052	.183	-.393	240	345	-.021	.071	.286	-.292
240	223	-.394	.177	.019	-1.176	240	273	-.141	.041	-.001	-.451	240	346	-.007	.073	.364	-.242
240	224	-.330	.138	.033	-1.002	240	274	-.151	.043	-.007	-.512	240	347	-.286	.171	.252	-1.106
240	225	-.292	.107	-.018	-.887	240	275	-.142	.041	.006	-.303	240	348	-.231	.120	.205	-.810
240	226	-.264	.101	.037	-.983	240	276	-.131	.034	.025	-.254	240	349	-.206	.070	.178	-.546
240	227	-.267	.112	.036	-1.159	240	277	-.125	.041	.085	-.267	240	350	-.246	.078	.039	-.612
240	228	-.522	.209	-.035	-1.659	240	301	-.139	.213	.871	-1.118	240	351	-.325	.140	.054	-1.272
240	229	-.523	.200	-.110	-1.518	240	302	.064	.197	.691	-.924	240	352	-.317	.129	.042	-1.181
240	230	-.437	.205	.040	-1.429	240	303	-.295	.159	.344	-1.193	240	353	.020	.065	.313	-.272
240	231	-.380	.190	.011	-1.359	240	304	.199	.202	.877	-.394	240	354	-.221	.091	.136	-.766
240	232	-.313	.149	.006	-1.173	240	305	.204	.197	.650	-.365	240	355	-.108	.061	.158	-.361
240	233	-.267	.101	.002	-.890	240	306	.012	.134	.489	-.526	240	356	-.090	.052	.161	-.287
240	234	-.240	.089	.060	-.728	240	307	.085	.126	.552	-.337	240	357	-.341	.106	.075	-.782
240	235	-.242	.093	-.018	-.817	240	308	-.488	.205	.323	-1.453	240	358	-.290	.102	.039	-.687
240	236	-.430	.188	-.027	-1.372	240	309	.316	.189	.991	-.439	240	359	-.224	.070	-.035	-.587
240	237	-.474	.200	-.082	-1.377	240	310	.367	.168	.981	-.148	240	360	-.216	.052	-.047	-.526
240	238	-.382	.188	.060	-1.316	240	311	.343	.217	1.074	-.518	240	361	-.224	.079	-.008	-.925
240	239	-.320	.153	.029	-1.171	240	312	.285	.183	.936	-.254	240	362	-.234	.093	.104	-.896
240	240	-.265	.121	.013	-.982	240	313	.148	.146	.764	-.257	240	363	-.162	.045	.038	-.370
240	241	-.237	.087	.032	-.703	240	314	-.119	.098	.366	-.568	240	364	-.162	.035	-.005	-.279
240	242	-.217	.079	-.021	-.611	240	315	-.601	.208	-.094	-1.522	240	365	-.209	.055	-.041	-.488
240	243	-.219	.079	.002	-.692	240	316	-.610	.232	.325	-1.670	240	366	-.200	.051	-.023	-.475
240	244	-.315	.151	-.037	-1.142	240	317	.103	.186	.842	-.587	240	367	-.184	.047	-.042	-.387
240	245	-.331	.145	-.038	-1.248	240	318	-.466	.172	-.017	-1.745	240	368	-.185	.038	-.042	-.353
240	246	-.266	.128	.093	-1.074	240	319	.295	.141	.892	-.099	240	369	-.188	.059	.007	-.513
240	247	-.232	.099	.041	-.907	240	320	.331	.177	1.078	-.271	240	370	-.180	.053	.011	-.545
240	248	-.208	.083	.138	-.769	240	321	.273	.203	1.144	-.644	240	371	-.048	.041	.129	-.172
240	249	-.194	.057	.015	-.525	240	322	.215	.125	.751	-.368	240	372	-.166	.042	.027	-.337
240	250	-.187	.058	.022	-.510	240	323	.087	.122	.684	-.382	240	373	-.118	.035	.015	-.262
240	251	-.191	.063	.023	-.623	240	324	-.141	.104	.366	-.578	240	374	-.195	.052	.004	-.454
240	252	-.221	.087	-.035	-.783	240	325	-.571	.198	-.073	-1.508	240	375	-.179	.049	.006	-.393
240	253	-.218	.074	-.050	-.664	240	326	-.581	.220	.135	-1.520	240	376	-.159	.048	.107	-.351
240	254	-.200	.067	.004	-.652	240	327	.188	.131	.695	-.202	240	377	-.184	.049	.032	-.359
240	255	-.183	.054	.004	-.519	240	328	.203	.129	.949	-.165	240	378	-.140	.054	.147	-.330
240	256	-.168	.045	.001	-.372	240	329	.124	.196	1.006	-.862	240	379	-.162	.052	.138	-.360
240	257	-.166	.046	.010	-.385	240	330	.100	.150	.792	-.475	240	380	-.144	.052	.289	-.349
240	258	-.168	.050	.004	-.377	240	331	.002	.123	.498	-.439	240	401	-.203	.085	.075	-.656
240	259	-.170	.057	.026	-.453	240	332	-.182	.093	.183	-.581	240	402	-.204	.102	.117	-.640
240	260	-.198	.076	-.001	-.843	240	333	-.583	.222	-.074	-1.663	240	403	-.103	.092	.193	-.532
240	261	-.195	.066	-.000	-.604	240	334	-.573	.254	.273	-1.751	240	404	-.099	.212	.572	-.800
240	262	-.183	.055	-.027	-.880	240	335	.077	.134	.604	-.760	240	405	.081	.202	.618	-.916

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
240	406	.002	.086	.358	-.315	240	456	.004	.062	.416	-.226	250	101	-.323	.091	-.105	-.876
240	407	-.004	.066	.237	-.273	240	457	-.037	.066	.415	-.303	250	102	-.289	.070	-.117	-.598
240	408	.019	.087	.396	-.298	240	458	-.063	.059	.217	-.313	250	103	-.296	.093	-.040	-.842
240	409	-.058	.088	.332	-.430	240	459	-.082	.071	.220	-.378	250	104	-.273	.081	-.061	-.645
240	410	-.137	.169	.521	-.725	240	460	-.031	.061	.430	-.406	250	105	-.271	.075	-.023	-.568
240	411	.160	.140	.777	-.340	240	461	.007	.051	.353	-.211	250	106	-.259	.073	-.056	-.580
240	412	-.092	.047	.157	-.350	240	462	.022	.041	.234	-.113	250	107	-.256	.070	-.060	-.575
240	413	-.006	.076	.351	-.329	240	463	.012	.036	.147	-.094	250	108	-.249	.069	-.029	-.578
240	414	-.091	.058	.235	-.289	240	464	-.014	.043	.185	-.149	250	109	-.286	.073	-.112	-.813
240	415	.019	.069	.372	-.226	240	465	-.081	.038	.070	-.220	250	110	-.273	.075	-.090	-.731
240	416	.007	.099	.447	-.431	240	466	-.148	.051	.049	-.364	250	111	-.272	.071	-.072	-.659
240	417	-.129	.189	.524	-.793	240	467	-.133	.050	.052	-.323	250	112	-.266	.069	-.063	-.646
240	418	.343	.191	.936	-.461	240	468	.010	.046	.274	-.219	250	113	-.272	.062	-.097	-.543
240	419	.307	.157	.902	-.266	240	469	.041	.040	.233	-.080	250	114	-.264	.069	-.072	-.565
240	420	-.101	.048	.080	-.292	240	470	.037	.047	.284	-.118	250	115	-.297	.086	-.094	-.871
240	421	-.036	.065	.267	-.272	240	471	.023	.048	.290	-.132	250	116	-.120	.086	.193	-.435
240	422	-.090	.058	.188	-.326	240	472	-.017	.042	.196	-.142	250	117	-.289	.073	-.105	-.659
240	423	.006	.061	.363	-.217	240	473	-.015	.041	.133	-.145	250	118	-.275	.072	-.079	-.557
240	424	.001	.095	.478	-.380	240	474	.057	.053	.293	-.098	250	119	-.272	.073	-.082	-.583
240	425	-.131	.186	.599	-.876	240	475	.050	.055	.318	-.143	250	120	-.260	.056	-.090	-.614
240	426	.310	.151	.848	-.167	240	476	.040	.053	.331	-.126	250	121	-.249	.062	-.033	-.613
240	427	.296	.177	.939	-.205	240	477	-.031	.042	.147	-.154	250	122	-.248	.063	-.032	-.602
240	428	-.091	.050	.115	-.315	240	801	-.156	.037	-.019	-.295	250	123	-.302	.093	-.055	-1.004
240	429	-.028	.064	.226	-.227	240	802	-.153	.040	.009	-.321	250	124	-.287	.091	-.059	-.796
240	430	-.066	.049	.244	-.234	240	803	-.156	.043	.002	-.367	250	125	-.278	.086	-.087	-.832
240	431	.010	.065	.439	-.177	240	804	.024	.049	.212	-.132	250	126	-.267	.082	-.085	-.784
240	432	.004	.082	.539	-.341	240	805	.033	.041	.244	-.116	250	127	-.268	.068	-.055	-.785
240	433	-.075	.161	.667	-.739	240	806	-.022	.045	.205	-.161	250	128	-.261	.075	-.033	-.811
240	434	.176	.123	.843	-.517	240	807	-.171	.042	.020	-.356	250	129	-.289	.083	-.052	-.723
240	435	.161	.142	.914	-.649	240	808	-.165	.044	-.046	-.403	250	130	-.077	.086	.259	-.433
240	436	-.081	.053	.154	-.483	240	809	-.191	.037	-.061	-.343	250	131	-.322	.117	-.077	-1.271
240	437	-.022	.062	.278	-.336	240	810	-.186	.042	-.037	-.391	250	132	-.307	.114	.003	-1.065
240	438	-.042	.046	.175	-.231	240	901	-.265	.093	.053	-.721	250	133	-.299	.115	-.042	-1.194
240	439	.015	.057	.283	-.202	240	902	-.364	.153	.013	-1.129	250	134	-.289	.109	-.027	-1.037
240	440	.010	.068	.201	-.296	240	903	-.390	.133	.112	-.880	250	135	-.276	.080	-.097	-.883
240	441	-.013	.113	.384	-.584	240	904	-.373	.097	-.094	-.771	250	136	-.269	.087	-.051	-.819
240	442	.053	.079	.557	-.175	240	905	-.159	.062	.075	-.469	250	137	-.325	.146	.069	-1.456
240	443	.030	.093	.610	-.220	240	906	-.214	.077	.066	-.560	250	138	-.319	.129	.072	-1.284
240	444	-.076	.056	.173	-.397	240	907	-.234	.100	.053	-.653	250	139	-.348	.128	-.037	-1.067
240	445	-.019	.057	.278	-.239	240	908	-.230	.055	-.056	-.444	250	140	-.344	.139	-.059	-1.193
240	446	-.016	.047	.230	-.199	240	909	-.244	.073	-.030	-.529	250	141	-.288	.104	-.023	-.833
240	447	.024	.057	.303	-.154	240	910	-.395	.122	-.004	-.947	250	142	-.331	.128	-.032	-1.118
240	448	.020	.065	.423	-.267	240	911	-.454	.121	-.139	-.984	250	143	-.251	.084	.051	-.634
240	449	.003	.080	.344	-.541	240	912	-.340	.101	-.006	-.771	250	144	-.023	.058	.243	-.349
240	450	-.004	.061	.303	-.212	240	913	-.409	.116	-.110	-.859	250	145	-.222	.103	.051	-.893
240	451	-.039	.065	.266	-.272	240	914	-.447	.249	.416	-1.281	250	146	-.241	.107	.032	-.893
240	452	-.067	.064	.195	-.459	240	915	-.333	.112	.064	-.791	250	147	-.283	.129	.167	-1.146
240	453	-.009	.059	.252	-.263	240	916	-.232	.065	-.039	-.597	250	148	-.344	.116	-.103	-1.117
240	454	.006	.050	.279	-.180	240	917	-.231	.093	.053	-.922	250	149	-.370	.146	-.027	-1.455
240	455	.023	.058	.389	-.177	240	918	-.376	.152	.052	-1.259	250	150	-.362	.152	-.005	-1.481

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
250	151	-.154	.061	.081	-.541	250	235	-.310	.110	-.056	-.961	250	308	-.375	.120	-.130	-1.184
250	152	-.147	.061	.128	-.520	250	236	-.393	.166	-.043	-1.214	250	309	.400	.207	1.088	-.146
250	153	-.155	.066	.104	-.538	250	237	-.388	.157	-.047	-1.392	250	310	.382	.175	.984	-.029
250	154	-.215	.129	.077	-1.104	250	238	-.350	.171	.099	-1.565	250	311	.245	.288	1.124	-.805
250	155	-.339	.185	.086	-2.065	250	239	-.333	.162	.099	-2.185	250	312	.238	.212	.987	-.718
250	156	-.367	.162	.009	-1.594	250	240	-.312	.134	.044	-1.195	250	313	.139	.157	.741	-.346
250	157	-.181	.072	.006	-.616	250	241	-.286	.102	-.044	-.980	250	314	-.069	.085	.297	-.414
250	158	.029	.050	.223	-.121	250	242	-.263	.085	.027	-.658	250	315	-.364	.122	-.093	-1.119
250	159	-.100	.055	.143	-.343	250	243	-.271	.090	-.014	-.776	250	316	-.376	.135	-.036	-1.350
250	160	-.113	.063	.113	-.491	250	244	-.320	.144	.005	-1.239	250	317	.200	.193	.902	-.584
250	161	-.189	.109	.066	-.914	250	245	-.330	.138	-.021	-1.179	250	318	-.313	.085	-.074	-.689
250	162	-.291	.147	.149	-1.612	250	246	-.298	.143	.094	-1.390	250	319	.307	.145	.825	-.118
250	163	-.131	.058	.155	-.400	250	247	-.282	.122	.010	-1.001	250	320	.294	.165	1.032	-.132
250	164	-.113	.065	.130	-.508	250	248	-.269	.099	.044	-.855	250	321	.118	.303	1.083	-1.092
250	165	-.203	.088	.124	-.841	250	249	-.235	.071	-.006	-.686	250	322	.158	.170	.678	-.798
250	166	-.239	.107	.000	-1.193	250	250	-.227	.075	.048	-.692	250	323	.083	.164	.700	-.931
250	201	-.424	.122	-.127	-.972	250	251	-.269	.088	.036	-.703	250	324	-.096	.108	.287	-.521
250	202	-.373	.150	-.048	-1.117	250	252	-.258	.106	-.012	-1.243	250	325	-.366	.134	-.065	-1.161
250	203	-.317	.108	-.049	-.979	250	253	-.248	.077	-.021	-.824	250	326	-.371	.140	-.039	-1.111
250	204	-.316	.117	-.053	-1.180	250	254	-.232	.078	.027	-.795	250	327	.192	.121	.808	-.171
250	205	-.319	.094	-.084	-.789	250	255	-.225	.068	.020	-.598	250	328	.203	.107	.687	-.115
250	206	-.359	.119	-.120	-1.003	250	256	-.201	.054	.025	-.589	250	329	.007	.265	.688	-1.087
250	207	-.302	.082	-.084	-.804	250	257	-.201	.059	.029	-.550	250	330	.027	.199	.636	-1.036
250	208	-.331	.089	-.105	-.838	250	258	-.201	.064	.048	-.509	250	331	-.027	.135	.500	-.704
250	209	-.326	.118	.022	-.943	250	259	-.207	.072	-.002	-.620	250	332	-.154	.096	.321	-.508
250	210	-.297	.095	-.064	-.962	250	260	-.224	.078	.005	-.822	250	333	-.399	.166	-.041	-1.319
250	211	-.289	.099	-.009	-.988	250	261	-.226	.073	-.044	-.784	250	334	-.416	.183	.137	-1.369
250	212	-.337	.109	-.039	-1.142	250	262	-.230	.075	-.038	-.643	250	335	.131	.123	.706	-.548
250	213	-.347	.114	-.038	-1.309	250	263	-.216	.065	-.021	-.534	250	336	-.341	.138	.017	-1.101
250	214	-.321	.093	.036	-1.008	250	264	-.174	.050	.017	-.506	250	337	.075	.091	.482	-.218
250	215	-.321	.102	.006	-1.055	250	265	-.175	.063	.004	-.678	250	338	.088	.096	.523	-.191
250	216	-.312	.095	-.017	-.929	250	266	-.174	.072	.053	-.694	250	339	-.204	.231	.518	-1.251
250	217	-.307	.097	-.046	-1.074	250	267	-.168	.070	.052	-.682	250	340	-.153	.161	.331	-1.048
250	218	-.301	.086	-.047	-.791	250	268	-.185	.054	-.024	-.560	250	341	-.153	.116	.394	-.906
250	219	-.311	.104	-.053	-.859	250	269	-.201	.062	-.044	-.542	250	342	-.237	.104	.224	-.603
250	220	-.369	.130	-.094	-1.216	250	270	-.174	.050	.151	-.517	250	343	-.393	.169	-.045	-1.232
250	221	-.379	.131	-.099	-1.241	250	271	-.162	.063	.035	-.581	250	344	-.384	.150	-.033	-1.325
250	222	-.332	.119	.024	-.937	250	272	-.170	.078	.061	-.868	250	345	.003	.081	.375	-.333
250	223	-.324	.126	.004	-1.058	250	273	-.174	.051	-.025	-.517	250	346	.025	.087	.582	-.252
250	224	-.311	.106	.010	-.897	250	274	-.181	.061	-.040	-.587	250	347	-.404	.184	.157	-1.489
250	225	-.331	.096	-.102	-.909	250	275	-.159	.052	-.032	-.518	250	348	-.301	.151	.143	-1.301
250	226	-.311	.093	-.009	-.797	250	276	-.154	.044	-.033	-.425	250	349	-.245	.101	.064	-.937
250	227	-.322	.112	-.086	-.900	250	277	-.152	.055	.000	-.527	250	350	-.260	.089	-.020	-.760
250	228	-.399	.160	-.058	-1.287	250	301	-.048	.239	.774	-.897	250	351	-.318	.134	.031	-1.051
250	229	-.399	.156	-.072	-1.121	250	302	.020	.190	.686	-.644	250	352	-.350	.137	.123	-1.104
250	230	-.360	.166	-.001	-1.310	250	303	-.289	.119	.098	-1.045	250	353	.088	.090	.553	-.227
250	231	-.346	.166	.045	-1.186	250	304	.250	.195	.964	-.417	250	354	-.286	.131	.111	-1.357
250	232	-.325	.136	-.014	-1.151	250	305	.187	.213	.921	-.859	250	355	-.085	.086	.355	-.398
250	233	-.329	.104	-.077	-.914	250	306	-.010	.126	.499	-.460	250	356	-.058	.073	.299	-.352
250	234	-.300	.096	-.074	-.888	250	307	.134	.138	.571	-.330	250	357	-.392	.117	-.115	-1.016

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
250	358	-.348	.118	-.015	-.912	250	428	-.100	.064	.278	-.331	250	801	-.170	.050	-.014	-.459
250	359	-.261	.090	-.003	-.860	250	429	-.009	.084	.372	-.270	250	802	-.165	.049	-.012	-.405
250	360	-.248	.066	-.082	-.581	250	430	-.018	.070	.347	-.241	250	803	-.175	.049	-.002	-.394
250	361	-.255	.100	.088	-.901	250	431	.066	.095	.533	-.190	250	804	.035	.052	.318	-.137
250	362	-.269	.115	.130	-1.093	250	432	.079	.113	.710	-.338	250	805	.072	.047	.290	-.048
250	363	-.179	.054	.112	-.472	250	433	.042	.173	.726	-.664	250	806	.013	.053	.327	-.126
250	364	-.183	.043	-.026	-.373	250	434	.192	.107	.702	-.109	250	807	-.200	.052	-.046	-.450
250	365	-.261	.071	-.078	-.634	250	435	.160	.127	.758	-.387	250	808	-.220	.057	-.030	-.499
250	366	-.245	.062	-.055	-.559	250	436	-.091	.065	.180	-.460	250	809	-.236	.046	-.083	-.473
250	367	-.221	.058	-.054	-.525	250	437	-.003	.078	.321	-.359	250	810	-.225	.053	-.051	-.519
250	368	-.221	.049	-.074	-.424	250	438	.004	.067	.373	-.217	250	901	-.283	.084	.033	-.669
250	369	-.217	.069	.034	-.673	250	439	.078	.089	.530	-.195	250	902	-.326	.107	-.008	-.871
250	370	-.208	.065	.177	-.563	250	440	.093	.104	.574	-.281	250	903	-.330	.101	-.012	-.840
250	371	-.031	.042	.148	-.167	250	441	.082	.127	.541	-.495	250	904	-.369	.099	.022	-.834
250	372	-.196	.056	-.010	-.649	250	442	.100	.087	.542	-.146	250	905	-.258	.079	-.000	-.629
250	373	-.138	.041	.053	-.318	250	443	.049	.102	.563	-.305	250	906	-.256	.093	.048	-.680
250	374	-.241	.061	-.041	-.630	250	444	-.090	.073	.196	-.455	250	907	-.202	.118	.166	-.770
250	375	-.225	.060	.039	-.547	250	445	.006	.076	.313	-.268	250	908	-.272	.067	-.066	-.654
250	376	-.194	.056	.104	-.474	250	446	.022	.059	.288	-.170	250	909	-.281	.080	-.006	-.727
250	377	-.223	.057	.043	-.500	250	447	.082	.078	.473	-.162	250	910	-.398	.123	.011	-.895
250	378	-.160	.064	.152	-.480	250	448	.091	.092	.619	-.207	250	911	-.456	.121	-.106	-.909
250	379	-.200	.054	.039	-.492	250	449	.069	.099	.663	-.310	250	912	-.388	.099	-.006	-.819
250	380	-.176	.055	.065	-.535	250	450	.034	.088	.511	-.329	250	913	-.398	.096	-.142	-.771
250	401	-.222	.098	.113	-.852	250	451	-.012	.087	.395	-.377	250	914	-.340	.182	.313	-1.049
250	402	-.209	.120	.297	-.785	250	452	-.072	.077	.230	-.487	250	915	-.359	.107	.025	-.769
250	403	-.127	.130	.268	-.721	250	453	.018	.073	.351	-.277	250	916	-.267	.070	-.045	-.570
250	404	.015	.236	.708	-.840	250	454	.040	.055	.339	-.151	250	917	-.244	.108	.099	-.761
250	405	.061	.251	.841	-.876	250	455	.070	.066	.503	-.177	250	918	-.410	.166	.172	-1.109
250	406	.020	.109	.421	-.310	250	456	.054	.069	.478	-.171	260	101	-.297	.074	-.078	-.720
250	407	.027	.088	.351	-.268	250	457	.006	.078	.520	-.279	260	102	-.295	.071	-.061	-.709
250	408	.064	.117	.485	-.310	250	458	-.019	.090	.491	-.346	260	103	-.281	.081	-.053	-.678
250	409	.012	.119	.504	-.393	250	459	-.043	.100	.398	-.367	260	104	-.282	.077	-.022	-.741
250	410	.028	.216	.688	-.774	250	460	-.042	.079	.402	-.401	260	105	-.280	.073	-.055	-.660
250	411	.237	.159	.787	-.315	250	461	.022	.064	.391	-.221	260	106	-.272	.072	-.072	-.802
250	412	-.083	.062	.135	-.330	250	462	.048	.048	.261	-.160	260	107	-.269	.068	-.065	-.671
250	413	.032	.102	.385	-.324	250	463	.042	.043	.214	-.090	260	108	-.262	.067	-.056	-.610
250	414	-.036	.089	.299	-.289	250	464	.011	.048	.216	-.186	260	109	-.291	.064	-.124	-.674
250	415	.088	.099	.484	-.187	250	465	-.083	.045	.092	-.298	260	110	-.282	.066	-.104	-.596
250	416	.080	.130	.640	-.427	250	466	-.179	.064	.086	-.453	260	111	-.277	.063	-.082	-.566
250	417	.065	.232	.922	-.878	250	467	-.145	.058	.097	-.374	260	112	-.271	.062	-.075	-.528
250	418	.328	.198	1.075	-.457	250	468	.031	.057	.294	-.156	260	113	-.265	.056	-.107	-.562
250	419	.310	.169	1.106	-.204	250	469	.080	.052	.336	-.078	260	114	-.259	.063	-.084	-.623
250	420	-.098	.062	.155	-.357	250	470	.075	.059	.328	-.084	260	115	-.261	.065	-.092	-.678
250	421	-.003	.092	.383	-.317	250	471	.059	.058	.342	-.099	260	116	-.222	.085	.345	-.313
250	422	-.023	.092	.349	-.333	250	472	.005	.050	.283	-.131	260	117	-.290	.069	-.119	-1.034
250	423	.073	.091	.518	-.153	250	473	-.013	.047	.281	-.157	260	118	-.278	.067	-.106	-.851
250	424	.081	.128	.650	-.415	250	474	.089	.063	.467	-.071	260	119	-.269	.062	-.092	-.659
250	425	.034	.218	.782	-.657	250	475	.081	.066	.473	-.099	260	120	-.262	.058	-.104	-.540
250	426	.296	.144	.861	-.092	250	476	.068	.064	.427	-.090	260	121	-.253	.064	-.072	-.543
250	427	.268	.169	.965	-.212	250	477	-.012	.052	.303	-.141	260	122	-.251	.064	-.061	-.549

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
260	123	-.317	.092	-.134	-.983
260	124	-.304	.089	-.108	-.985
260	125	-.291	.079	-.106	-.747
260	126	-.278	.074	-.089	-.715
260	127	-.269	.058	-.104	-.594
260	128	-.263	.064	-.084	-.603
260	129	-.258	.058	-.063	-.532
260	130	-.004	.074	.362	-.243
260	131	-.355	.114	-.117	-1.122
260	132	-.344	.113	-.092	-1.095
260	133	-.330	.099	-.077	-1.095
260	134	-.317	.092	-.049	-1.135
260	135	-.302	.073	-.112	-.720
260	136	-.297	.080	-.109	-.720
260	137	-.359	.148	-.032	-1.371
260	138	-.349	.127	-.030	-1.009
260	139	-.361	.114	-.117	-1.090
260	140	-.355	.118	-.094	-1.144
260	141	-.333	.118	-.027	-1.076
260	142	-.349	.111	-.073	-.928
260	143	-.288	.090	-.075	-.836
260	144	.015	.064	.283	-.260
260	145	-.299	.120	.129	-1.164
260	146	-.307	.121	.399	-1.033
260	147	-.353	.139	.051	-1.457
260	148	-.386	.121	-.113	-1.347
260	149	-.384	.117	-.121	-1.107
260	150	-.377	.124	-.092	-1.050
260	151	-.191	.068	.020	-.521
260	152	-.180	.066	.040	-.556
260	153	-.203	.073	.039	-.662
260	154	-.289	.133	.047	-1.253
260	155	-.410	.166	.025	-1.431
260	156	-.424	.153	-.028	-1.406
260	157	-.239	.093	-.036	-.827
260	158	.051	.056	.390	-.146
260	159	-.128	.061	.147	-.387
260	160	-.149	.072	.091	-.528
260	161	-.253	.110	.034	-1.093
260	162	-.358	.130	.042	-.978
260	163	-.162	.060	.049	-.547
260	164	-.142	.070	.198	-.640
260	165	-.293	.112	.015	-.939
260	166	-.313	.113	-.025	-1.013
260	201	-.393	.104	-.099	-.838
260	202	-.321	.105	-.053	-.790
260	203	-.275	.076	-.037	-.624
260	204	-.276	.080	-.077	-.724
260	205	-.286	.074	-.111	-.687
260	206	-.280	.072	-.089	-.754
260	207	-.276	.064	-.064	-.550
260	208	-.288	.069	-.086	-.689
260	209	-.270	.078	-.058	-.712
260	210	-.276	.069	-.062	-.687
260	211	-.277	.076	-.056	-.790
260	212	-.289	.073	-.078	-.661
260	213	-.296	.075	-.077	-.688
260	214	-.285	.067	-.074	-.655
260	215	-.284	.073	-.073	-.620
260	216	-.282	.070	-.075	-.654
260	217	-.282	.072	-.065	-.719
260	218	-.280	.062	-.114	-.563
260	219	-.283	.071	-.101	-.706
260	220	-.293	.084	-.068	-.819
260	221	-.297	.084	-.077	-.822
260	222	-.290	.076	-.096	-.803
260	223	-.290	.079	-.086	-.749
260	224	-.289	.073	-.088	-.610
260	225	-.289	.064	-.089	-.586
260	226	-.277	.061	-.089	-.633
260	227	-.281	.067	-.097	-.719
260	228	-.305	.100	-.031	-.993
260	229	-.302	.092	-.059	-.979
260	230	-.295	.105	.002	-1.210
260	231	-.294	.099	.012	-1.127
260	232	-.289	.084	-.027	-.957
260	233	-.291	.071	-.096	-.771
260	234	-.278	.066	-.028	-.620
260	235	-.286	.073	-.034	-.826
260	236	-.312	.107	-.060	-1.022
260	237	-.289	.089	-.069	-1.006
260	238	-.282	.097	-.038	-1.098
260	239	-.282	.091	-.051	-.768
260	240	-.270	.077	-.041	-.715
260	241	-.287	.073	-.082	-.724
260	242	-.281	.072	-.058	-.711
260	243	-.297	.081	-.083	-.736
260	244	-.300	.105	-.034	-.857
260	245	-.290	.096	-.079	-1.184
260	246	-.281	.100	-.073	-.989
260	247	-.280	.097	-.073	-1.003
260	248	-.260	.078	-.031	-.905
260	249	-.272	.071	-.079	-.791
260	250	-.280	.082	-.066	-.810
260	251	-.320	.095	.002	-.834
260	252	-.274	.101	-.041	-.972
260	253	-.286	.092	-.094	-1.166
260	254	-.276	.089	-.018	-1.073
260	255	-.270	.082	-.054	-.722
260	256	-.240	.070	-.046	-.726
260	257	-.254	.084	-.030	-.872
260	258	-.255	.085	-.046	-.739
260	259	-.262	.093	-.041	-.739
260	260	-.272	.092	-.089	-1.017
260	261	-.290	.096	-.092	-1.362
260	262	-.280	.078	-.105	-.887
260	263	-.269	.070	-.114	-.811
260	264	-.219	.071	.028	-.660
260	265	-.234	.098	-.042	-.853
260	266	-.234	.114	.033	-1.199
260	267	-.225	.107	.031	-.967
260	268	-.234	.065	-.050	-.645
260	269	-.251	.076	-.047	-.660
260	270	-.208	.065	-.010	-.643
260	271	-.208	.090	.058	-.758
260	272	-.222	.109	.069	-.814
260	273	-.209	.063	-.027	-.652
260	274	-.225	.079	-.004	-.977
260	275	-.198	.069	.032	-.706
260	276	-.189	.063	-.020	-.531
260	277	-.189	.079	.056	-.679
260	301	-.060	.242	.761	-.792
260	302	-.198	.175	.455	-.720
260	303	-.243	.095	.206	-.665
260	304	.154	.199	.864	-.528
260	305	-.092	.251	.749	-1.102
260	306	-.165	.105	.402	-.815
260	307	.043	.133	.492	-.463
260	308	-.319	.089	-.055	-.840
260	309	.357	.235	1.113	-.318
260	310	.355	.189	.942	-.151
260	311	-.229	.292	.767	-1.331
260	312	-.077	.290	.732	-1.337
260	313	-.029	.141	.508	-.821
260	314	-.154	.061	.138	-.524
260	315	-.289	.074	-.097	-.827
260	316	-.297	.082	-.088	-.924
260	317	.316	.196	.970	-.635
260	318	-.300	.062	-.129	-.637
260	319	.262	.154	.898	-.373
260	320	.281	.186	1.117	-.285
260	321	-.331	.311	.833	-1.708
260	322	-.233	.251	.429	-1.395
260	323	-.102	.161	.563	-.962
260	324	-.185	.098	.224	-1.053
260	325	-.302	.088	-.005	-.885
260	326	-.324	.098	-.115	-1.047
260	327	.166	.138	.958	-.230
260	328	.201	.130	.752	-.102
260	329	-.395	.274	.559	-1.306

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
260	330	-.308	.298	.488	-1.526	260	380	-.210	.060	-.018	-.653	260	450	.090	.099	.571	-.265
260	331	-.183	.179	.332	-1.221	260	401	-.283	.116	.156	-1.015	260	451	.049	.098	.487	-.263
260	332	-.215	.084	.182	-.760	260	402	-.286	.136	.292	-.914	260	452	-.073	.077	.308	-.426
260	333	-.321	.105	.003	-1.218	260	403	-.224	.155	.381	-.709	260	453	.041	.076	.398	-.282
260	334	-.334	.121	.168	-1.313	260	404	.090	.282	.895	-.796	260	454	.067	.064	.376	-.174
260	335	.247	.149	.835	-.179	260	405	-.192	.237	.690	-.889	260	455	.111	.077	.469	-.109
260	336	-.312	.091	-.040	-.968	260	406	.085	.125	.517	-.488	260	456	.094	.078	.475	-.126
260	337	.097	.125	.715	-.416	260	407	.056	.093	.410	-.233	260	457	.041	.080	.430	-.261
260	338	.124	.134	.732	-.345	260	408	.101	.126	.544	-.231	260	458	-.002	.083	.498	-.338
260	339	-.500	.209	.271	-1.473	260	409	.102	.142	.652	-.388	260	459	-.013	.091	.449	-.365
260	340	-.385	.188	.155	-1.400	260	410	.192	.181	.899	-.450	260	460	-.048	.073	.337	-.357
260	341	-.250	.145	.146	-1.331	260	411	.254	.159	.886	-.238	260	461	.033	.060	.426	-.256
260	342	-.247	.097	.060	-.852	260	412	-.042	.069	.240	-.288	260	462	.069	.048	.297	-.094
260	343	-.303	.110	-.021	-1.193	260	413	.095	.115	.561	-.262	260	463	.070	.053	.345	-.091
260	344	-.330	.104	-.082	-1.010	260	414	.046	.099	.484	-.275	260	464	.036	.052	.215	-.128
260	345	.017	.106	.562	-.473	260	415	.196	.114	.637	-.130	260	465	-.079	.046	.098	-.239
260	346	.043	.114	.610	-.357	260	416	.223	.154	.821	-.286	260	466	-.207	.073	.072	-.516
260	347	-.505	.165	-.066	-1.278	260	417	.305	.212	.012	-.476	260	467	-.153	.066	.081	-.439
260	348	-.404	.165	-.122	-1.175	260	418	.359	.209	.089	-.361	260	468	.039	.061	.360	-.153
260	349	-.316	.148	-.007	-1.098	260	419	.320	.172	.940	-.157	260	469	.106	.063	.451	-.079
260	350	-.285	.107	-.024	-1.077	260	420	-.058	.063	.188	-.311	260	470	.105	.074	.467	-.086
260	351	-.301	.103	-.014	-.889	260	421	.068	.098	.420	-.309	260	471	.093	.074	.420	-.107
260	352	-.311	.097	-.079	-1.108	260	422	.066	.092	.489	-.291	260	472	.020	.058	.274	-.153
260	353	.147	.098	.667	-.120	260	423	.209	.116	.635	-.140	260	473	-.014	.048	.185	-.195
260	354	-.291	.098	-.036	-.998	260	424	.253	.164	.919	-.343	260	474	.133	.073	.472	-.047
260	355	-.080	.084	.365	-.383	260	425	.291	.197	.941	-.446	260	475	.136	.079	.561	-.086
260	356	-.046	.079	.481	-.309	260	426	.270	.152	.862	-.140	260	476	.120	.078	.570	-.098
260	357	-.466	.153	-.120	-1.328	260	427	.212	.156	.853	-.171	260	477	.017	.056	.352	-.156
260	358	-.426	.156	-.015	-1.166	260	428	-.062	.065	.201	-.326	260	801	-.239	.083	-.035	-.810
260	359	-.330	.127	.026	-1.063	260	429	.055	.092	.461	-.279	260	802	-.212	.065	-.041	-.775
260	360	-.294	.082	-.089	-.748	260	430	.067	.074	.425	-.147	260	803	-.221	.062	-.057	-.596
260	361	-.284	.091	-.070	-.940	260	431	.189	.115	.686	-.121	260	804	.056	.065	.471	-.160
260	362	-.293	.104	-.033	-1.140	260	432	.228	.139	.804	-.154	260	805	.115	.066	.501	-.031
260	363	-.226	.059	.050	-.482	260	433	.241	.158	.892	-.483	260	806	.040	.070	.455	-.125
260	364	-.224	.049	-.003	-.445	260	434	.228	.139	.816	-.142	260	807	-.246	.064	-.044	-.651
260	365	-.336	.091	-.125	-.959	260	435	.164	.138	.806	-.258	260	808	-.280	.072	-.036	-.709
260	366	-.313	.081	-.091	-.777	260	436	-.074	.069	.237	-.354	260	809	-.308	.066	-.111	-.699
260	367	-.283	.073	-.042	-.755	260	437	.049	.088	.423	-.275	260	810	-.296	.075	-.053	-.710
260	368	-.276	.057	-.082	-.593	260	438	.060	.065	.351	-.133	260	901	-.300	.079	-.046	-.723
260	369	-.276	.079	-.105	-.842	260	439	.159	.095	.611	-.136	260	902	-.302	.077	-.067	-.727
260	370	-.266	.075	-.055	-.785	260	440	.189	.111	.678	-.095	260	903	-.294	.094	-.063	-.685
260	371	-.017	.045	.202	-.170	260	441	.181	.122	.737	-.247	260	904	-.359	.096	-.081	-.761
260	372	-.244	.068	-.058	-.626	260	442	.152	.114	.693	-.184	260	905	-.289	.086	-.020	-.718
260	373	-.156	.051	.090	-.423	260	443	.079	.113	.591	-.278	260	906	-.327	.099	-.030	-.734
260	374	-.298	.083	.011	-.792	260	444	-.084	.068	.201	-.345	260	907	-.294	.106	-.071	-.721
260	375	-.275	.079	-.023	-.789	260	445	.032	.072	.306	-.294	260	908	-.317	.075	-.081	-.657
260	376	-.227	.071	.032	-.799	260	446	.055	.066	.464	-.152	260	909	-.303	.079	-.035	-.696
260	377	-.267	.068	-.052	-.539	260	447	.132	.087	.581	-.114	260	910	-.429	.114	-.060	-.932
260	378	-.184	.076	.155	-.485	260	448	.147	.097	.668	-.142	260	911	-.466	.117	-.132	-.982
260	379	-.240	.061	-.064	-.520	260	449	.125	.104	.772	-.115	260	912	-.423	.096	-.033	-.817

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
260	913	-.416	.098	-.158	-.782
260	914	-.305	.129	.147	-.916
260	915	-.384	.102	-.103	-.814
260	916	-.319	.071	-.089	-.628
260	917	-.322	.119	.110	-.767
260	918	-.477	.159	.138	-1.092
270	101	-.300	.073	-.097	-.665
270	102	-.311	.071	-.099	-.712
270	103	-.284	.075	-.080	-.665
270	104	-.303	.077	-.088	-.666
270	105	-.298	.071	-.100	-.682
270	106	-.286	.068	-.097	-.900
270	107	-.281	.064	-.102	-.580
270	108	-.276	.063	-.097	-.531
270	109	-.311	.072	-.129	-.845
270	110	-.300	.073	-.095	-.840
270	111	-.289	.065	-.105	-.655
270	112	-.281	.062	-.083	-.580
270	113	-.277	.053	-.117	-.507
270	114	-.272	.059	-.092	-.525
270	115	-.264	.057	-.090	-.506
270	116	-.054	.099	.490	-.263
270	117	-.338	.086	-.159	-1.099
270	118	-.326	.085	-.117	-1.129
270	119	-.313	.075	-.124	-.996
270	120	-.289	.058	-.122	-.605
270	121	-.279	.063	-.100	-.611
270	122	-.276	.064	-.092	-.622
270	123	-.359	.099	-.154	-1.748
270	124	-.350	.097	-.115	-1.273
270	125	-.334	.084	-.102	-1.117
270	126	-.317	.077	-.076	-.891
270	127	-.313	.065	-.134	-.605
270	128	-.307	.071	-.110	-.631
270	129	-.289	.060	-.097	-.506
270	130	-.050	.084	.362	-.183
270	131	-.388	.113	-.031	-1.114
270	132	-.381	.115	-.022	-1.099
270	133	-.369	.102	-.056	-1.242
270	134	-.357	.093	-.074	-.957
270	135	-.353	.086	-.147	-.944
270	136	-.349	.093	-.110	-.943
270	137	-.393	.151	-.008	-1.295
270	138	-.388	.136	-.024	-1.102
270	139	-.400	.115	-.087	-1.333
270	140	-.400	.124	-.092	-1.404
270	141	-.382	.118	-.107	-1.167
270	142	-.396	.117	-.112	-1.271
270	143	-.343	.103	.021	-.893
270	144	.019	.063	.298	-.218
270	145	-.343	.132	.059	-1.034
270	146	-.348	.136	.062	-1.037
270	147	-.390	.152	.121	-1.393
270	148	-.422	.135	-.125	-1.442
270	149	-.431	.133	-.114	-1.489
270	150	-.426	.141	-.115	-1.371
270	151	-.219	.087	.050	-.788
270	152	-.204	.080	.159	-.697
270	153	-.239	.098	.113	-.808
270	154	-.339	.152	.097	-1.308
270	155	-.448	.186	-.030	-1.559
270	156	-.455	.169	-.055	-1.357
270	157	-.294	.136	-.018	-1.235
270	158	.066	.062	.331	-.112
270	159	-.149	.074	.135	-.498
270	160	-.176	.091	.199	-.630
270	161	-.278	.130	.021	-1.040
270	162	-.386	.156	.061	-1.310
270	163	-.187	.076	.074	-.518
270	164	-.161	.084	.279	-.654
270	165	-.323	.120	-.058	-1.067
270	166	-.338	.119	-.019	-1.298
270	201	-.368	.095	-.117	-.755
270	202	-.276	.073	-.083	-.594
270	203	-.272	.068	-.063	-.564
270	204	-.278	.072	-.069	-.788
270	205	-.281	.067	-.087	-.609
270	206	-.270	.065	-.081	-.536
270	207	-.268	.061	-.112	-.670
270	208	-.272	.059	-.111	-.587
270	209	-.260	.064	-.076	-.516
270	210	-.270	.059	-.050	-.633
270	211	-.270	.066	-.063	-.763
270	212	-.266	.060	-.056	-.549
270	213	-.273	.061	-.069	-.554
270	214	-.268	.056	-.099	-.497
270	215	-.265	.060	-.081	-.490
270	216	-.262	.058	-.092	-.479
270	217	-.266	.059	-.095	-.509
270	218	-.276	.060	-.104	-.836
270	219	-.280	.067	-.070	-.938
270	220	-.283	.072	-.036	-.785
270	221	-.287	.070	-.066	-.785
270	222	-.283	.066	-.114	-.621
270	223	-.283	.068	-.113	-.650
270	224	-.280	.064	-.102	-.658
270	225	-.278	.055	-.122	-.567
270	226	-.269	.056	-.083	-.576
270	227	-.277	.062	-.075	-.651
270	228	-.289	.080	-.042	-.771
270	229	-.301	.077	-.055	-.755
270	230	-.296	.082	-.045	-.842
270	231	-.297	.083	-.085	-.935
270	232	-.294	.074	-.097	-.914
270	233	-.289	.062	-.109	-.572
270	234	-.285	.064	-.025	-.591
270	235	-.297	.070	-.029	-.598
270	236	-.306	.101	-.059	-.831
270	237	-.305	.090	-.060	-.935
270	238	-.300	.097	-.010	-1.044
270	239	-.301	.095	-.100	-1.290
270	240	-.293	.079	-.066	-.812
270	241	-.317	.073	-.062	-.636
270	242	-.321	.079	-.065	-.677
270	243	-.341	.088	-.075	-.729
270	244	-.326	.122	.008	-1.340
270	245	-.323	.105	-.060	-1.044
270	246	-.315	.115	.033	-1.183
270	247	-.311	.108	-.063	-1.319
270	248	-.298	.088	.003	-.678
270	249	-.348	.091	-.065	-.784
270	250	-.355	.102	-.038	-.900
270	251	-.356	.106	-.087	-.909
270	252	-.334	.116	-.007	-1.174
270	253	-.315	.101	-.107	-1.051
270	254	-.309	.107	-.048	-1.037
270	255	-.303	.106	-.002	-.960
270	256	-.276	.089	.050	-.928
270	257	-.332	.113	-.018	-.923
270	258	-.332	.112	-.027	-.817
270	259	-.339	.122	-.027	-.831
270	260	-.347	.125	-.073	-1.185
270	261	-.329	.113	-.117	-1.153
270	262	-.314	.094	-.097	-1.030
270	263	-.303	.091	-.073	-1.027
270	264	-.250	.096	.129	-.909
270	265	-.279	.139	.039	-1.029
270	266	-.280	.148	.036	-.999
270	267	-.266	.143	.068	-.979
270	268	-.260	.082	.010	-.683
270	269	-.287	.106	.002	-1.096
270	270	-.247	.096	.114	-.829
270	271	-.262	.141	.187	-1.186
270	272	-.275	.156	.074	-1.274
270	273	-.238	.080	.034	-.652
270	274	-.263	.105	.025	-1.017
270	275	-.230	.095	.101	-.937
270	276	-.214	.084	.046	-.845
270	277	-.211	.100	.106	-.911
270	301	-.201	.213	.471	-.924

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
270	302	-.380	.132	.174	-.904	270	352	-.342	.100	-.088	-.933	270	422	.151	.100	.588	-.130
270	303	-.287	.083	.011	-.586	270	353	.187	.103	.620	-.065	270	423	.295	.111	.726	.020
270	304	.090	.187	.840	-.571	270	354	-.327	.113	-.044	-1.061	270	424	.349	.149	.959	-.049
270	305	-.381	.254	.436	-1.341	270	355	-.078	.091	.450	-.493	270	425	.375	.165	1.060	-.055
270	306	-.244	.106	.052	-.845	270	356	-.054	.081	.343	-.355	270	426	.345	.144	.814	-.193
270	307	-.046	.114	.298	-.569	270	357	-.508	.158	-.137	-1.259	270	427	.275	.144	.894	-.208
270	308	-.308	.083	-.051	-.816	270	358	-.488	.162	-.039	-1.394	270	428	-.039	.063	.313	-.261
270	309	.319	.196	1.050	-.356	270	359	-.401	.143	-.005	-1.364	270	429	.104	.088	.494	-.149
270	310	.309	.151	.862	-.129	270	360	-.338	.096	-.103	-.871	270	430	.129	.085	.633	-.100
270	311	-.430	.189	.444	-1.232	270	361	-.316	.105	-.060	-.996	270	431	.273	.128	1.028	-.031
270	312	-.324	.278	.477	-1.715	270	362	-.327	.117	.042	-1.104	270	432	.327	.151	1.083	-.037
270	313	-.142	.164	.307	-.895	270	363	-.234	.064	.025	-.528	270	433	.339	.161	.917	-.100
270	314	-.187	.059	.005	-.499	270	364	-.253	.059	-.068	-.538	270	434	.287	.147	.831	-.117
270	315	-.289	.065	-.087	-.542	270	365	-.415	.128	-.147	-1.125	270	435	.218	.146	.876	-.218
270	316	-.295	.071	-.096	-.674	270	366	-.381	.111	-.105	-1.054	270	436	-.069	.064	.220	-.287
270	317	-.438	.176	1.101	-.045	270	367	-.339	.100	-.080	-.909	270	437	.070	.086	.578	-.193
270	318	-.282	.051	-.115	-.531	270	368	-.313	.074	-.100	-.725	270	438	.076	.068	.425	-.125
270	319	.311	.150	.906	-.110	270	369	-.320	.108	-.062	-1.115	270	439	.198	.110	.782	-.051
270	320	.340	.170	.964	-.115	270	370	-.296	.091	.101	-.907	270	440	.244	.132	.876	-.035
270	321	-.531	.193	.597	-1.341	270	371	-.061	.053	.338	-.182	270	441	.243	.140	.805	-.086
270	322	-.485	.229	.231	-1.378	270	372	-.296	.103	-.026	-.841	270	442	.195	.128	.755	-.183
270	323	-.253	.210	.233	-1.465	270	373	-.156	.060	.092	-.454	270	443	.122	.128	.642	-.325
270	324	-.231	.109	.070	-1.225	270	374	-.345	.104	-.064	-1.207	270	444	-.088	.069	.228	-.480
270	325	-.292	.072	-.033	-.685	270	375	-.315	.103	-.028	-1.212	270	445	.049	.076	.387	-.240
270	326	-.296	.073	-.003	-.765	270	376	-.243	.085	.158	-.782	270	446	.070	.063	.379	-.127
270	327	.252	.163	.970	-.261	270	377	-.308	.089	.050	-.870	270	447	.172	.093	.532	-.066
270	328	.264	.145	.901	-.147	270	378	-.199	.094	.374	-.716	270	448	.202	.108	.642	-.125
270	329	-.583	.205	.283	-1.929	270	379	-.283	.083	.082	-.883	270	449	.178	.109	.597	-.374
270	330	-.530	.267	.327	-1.684	270	380	-.242	.077	.026	-.768	270	450	.121	.114	.606	-.239
270	331	-.315	.219	.244	-1.491	270	401	-.310	.140	.390	-.840	270	451	.080	.109	.507	-.268
270	332	-.270	.102	.032	-.854	270	402	-.333	.134	.382	-.825	270	452	-.078	.079	.371	-.404
270	333	-.302	.088	-.015	-1.033	270	403	-.343	.134	.205	-.875	270	453	.046	.078	.475	-.193
270	334	-.310	.097	-.025	-1.225	270	404	-.049	.316	.824	-.953	270	454	.077	.067	.525	-.108
270	335	-.348	.145	.854	.013	270	405	-.319	.227	.797	-.917	270	455	.121	.087	.612	-.081
270	336	-.293	.066	-.129	-.698	270	406	.118	.119	.571	-.259	270	456	.122	.091	.549	-.111
270	337	.134	.129	.774	-.313	270	407	.100	.101	.489	-.230	270	457	.055	.090	.527	-.184
270	338	.155	.136	.824	-.305	270	408	.146	.128	.634	-.268	270	458	-.006	.093	.540	-.413
270	339	-.554	.180	.074	-1.362	270	409	.186	.150	.711	-.349	270	459	-.013	.096	.535	-.390
270	340	-.516	.176	.030	-1.151	270	410	.262	.159	.850	-.371	270	460	-.052	.078	.373	-.397
270	341	-.346	.181	.136	-1.157	270	411	.268	.130	.718	-.079	270	461	.034	.064	.387	-.177
270	342	-.290	.125	.042	-.995	270	412	.015	.075	.363	-.248	270	462	.072	.054	.357	-.117
270	343	-.301	.089	.013	-.900	270	413	.165	.113	.588	-.197	270	463	.087	.061	.350	-.075
270	344	-.343	.098	-.103	-1.263	270	414	.140	.112	.637	-.196	270	464	.038	.060	.325	-.161
270	345	.051	.109	.526	-.298	270	415	.274	.113	.667	-.037	270	465	-.086	.051	.114	-.298
270	346	.076	.118	.613	-.260	270	416	.325	.153	.944	-.141	270	466	-.212	.076	.083	-.544
270	347	-.579	.190	-.050	-1.451	270	417	.403	.181	1.014	-.204	270	467	-.170	.072	.293	-.489
270	348	-.496	.191	.042	-1.443	270	418	.417	.190	1.198	-.198	270	468	.059	.071	.429	-.166
270	349	-.384	.178	-.005	-1.204	270	419	.364	.147	.882	.002	270	469	.141	.074	.484	-.028
270	350	-.325	.134	.016	-.973	270	420	-.014	.063	.228	-.258	270	470	.143	.089	.572	-.072
270	351	-.332	.124	.016	-1.166	270	421	.149	.100	.549	-.190	270	471	.129	.092	.628	-.097

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
270	472	.045	.071	.471	-.146	280	117	-.379	.142	-.026	-1.252	280	201	-.299	.086	-.084	-.766
270	473	-.003	.056	.352	-.150	280	118	-.372	.138	-.027	-1.170	280	202	-.254	.073	-.056	-.636
270	474	.166	.098	.772	-.067	280	119	-.354	.127	-.021	-1.004	280	203	-.260	.073	-.079	-.643
270	475	.169	.104	.725	-.066	280	120	-.340	.106	-.097	-.870	280	204	-.273	.080	-.058	-.760
270	476	.158	.105	.703	-.071	280	121	-.332	.112	-.086	-.906	280	205	-.290	.080	-.052	-.694
270	477	.040	.069	.449	-.150	280	122	-.322	.111	-.053	-.864	280	206	-.266	.082	-.029	-.912
270	801	-.286	.117	-.021	-.870	280	123	-.398	.147	.001	-1.427	280	207	-.264	.068	-.087	-.741
270	802	-.254	.090	-.011	-.880	280	124	-.388	.145	.016	-1.369	280	208	-.263	.056	-.094	-.553
270	803	-.261	.086	-.012	-.986	280	125	-.374	.135	.018	-1.287	280	209	-.257	.073	-.070	-.708
270	804	.092	.071	.499	-.109	280	126	-.370	.133	.010	-1.385	280	210	-.276	.070	-.084	-.680
270	805	.168	.079	.556	-.036	280	127	-.367	.118	-.124	-1.375	280	211	-.278	.081	-.069	-.919
270	806	.083	.090	.501	-.160	280	128	-.362	.126	-.094	-1.344	280	212	-.275	.080	-.030	-.749
270	807	-.283	.081	-.040	-.694	280	129	-.287	.078	-.097	-.940	280	213	-.278	.080	-.016	-.680
270	808	-.328	.093	-.071	-.798	280	130	-.062	.102	.554	-.289	280	214	-.269	.072	-.061	-.687
270	809	-.329	.067	-.161	-.693	280	131	-.376	.144	.049	-1.422	280	215	-.265	.074	-.074	-.756
270	810	-.316	.075	-.117	-.752	280	132	-.373	.141	.070	-1.236	280	216	-.264	.072	-.093	-.788
270	901	-.311	.080	.005	-.763	280	133	-.383	.137	.033	-1.098	280	217	-.270	.074	-.087	-.869
270	902	-.295	.070	-.082	-.629	280	134	-.401	.145	-.050	-1.380	280	218	-.274	.065	-.111	-.643
270	903	-.293	.077	-.053	-.612	280	135	-.415	.142	-.122	-1.442	280	219	-.281	.074	-.091	-.701
270	904	-.348	.075	-.109	-.643	280	136	-.410	.153	-.104	-1.574	280	220	-.294	.101	-.011	-.812
270	905	-.313	.091	-.025	-.701	280	137	-.305	.136	.060	-1.107	280	221	-.294	.096	-.030	-.760
270	906	-.361	.093	-.068	-.999	280	138	-.307	.134	.174	-1.151	280	222	-.288	.077	-.027	-.766
270	907	-.361	.101	-.036	-.804	280	139	-.349	.138	-.056	-1.357	280	223	-.285	.077	-.056	-.846
270	908	-.344	.082	-.079	-.791	280	140	-.422	.162	-.030	-1.638	280	224	-.277	.069	-.108	-.682
270	909	-.313	.074	-.038	-.664	280	141	-.424	.140	-.146	-1.478	280	225	-.267	.061	-.032	-.707
270	910	-.419	.105	-.144	-.983	280	142	-.443	.159	-.090	-1.675	280	226	-.266	.064	-.074	-.648
270	911	-.442	.110	-.155	-.987	280	143	-.281	.109	-.062	-1.084	280	227	-.282	.072	-.084	-.737
270	912	-.418	.090	-.123	-.772	280	144	.039	.079	.501	-.210	280	228	-.301	.104	-.013	-.805
270	913	-.410	.096	-.139	-.795	280	145	-.257	.098	-.048	-.944	280	229	-.303	.091	-.030	-.734
270	914	-.391	.118	-.048	-1.041	280	146	-.249	.119	-.004	-.975	280	230	-.296	.095	-.054	-1.100
270	915	-.389	.097	-.085	-.778	280	147	-.279	.139	.051	-1.067	280	231	-.294	.091	-.071	-.976
270	916	-.352	.070	-.145	-.657	280	148	-.428	.145	-.107	-1.458	280	232	-.282	.069	-.089	-.724
270	917	-.394	.120	.049	-.820	280	149	-.466	.157	-.086	-1.616	280	233	-.291	.070	-.103	-.697
270	918	-.535	.152	.051	-1.161	280	150	-.477	.164	-.155	-1.623	280	234	-.294	.078	-.106	-.746
280	101	-.336	.107	-.014	-.985	280	151	-.204	.062	-.002	-.569	280	235	-.317	.089	-.088	-.853
280	102	-.350	.098	-.085	-.967	280	152	-.190	.055	.068	-.498	280	236	-.318	.121	-.015	-1.006
280	103	-.350	.121	.089	-.943	280	153	-.185	.056	.023	-.875	280	237	-.323	.107	-.042	-.844
280	104	-.341	.113	.020	-1.237	280	154	-.221	.105	.055	-1.218	280	238	-.316	.112	-.014	-.932
280	105	-.331	.104	-.023	-1.118	280	155	-.350	.167	.107	-1.707	280	239	-.312	.103	-.088	-1.015
280	106	-.370	.137	.080	-1.167	280	156	-.393	.147	.140	-1.289	280	240	-.297	.082	-.053	-.949
280	107	-.345	.122	.017	-1.080	280	157	-.263	.096	-.029	-.918	280	241	-.300	.075	-.096	-.744
280	108	-.334	.116	-.005	-1.036	280	158	.039	.057	.424	-.140	280	242	-.305	.083	-.066	-.754
280	109	-.376	.135	-.004	-1.201	280	159	-.152	.054	.065	-.427	280	243	-.324	.095	-.052	-.877
280	110	-.369	.136	.032	-1.185	280	160	-.158	.058	.121	-.542	280	244	-.298	.112	-.027	-.895
280	111	-.350	.123	.055	-1.016	280	161	-.181	.075	.052	-.739	280	245	-.321	.114	-.071	-.918
280	112	-.348	.117	-.072	-1.021	280	162	-.310	.133	.155	-1.100	280	246	-.312	.119	-.081	-1.321
280	113	-.347	.109	-.114	-1.149	280	163	-.204	.059	.023	-.464	280	247	-.307	.112	-.045	-1.217
280	114	-.341	.119	-.091	-1.287	280	164	-.162	.051	.142	-.438	280	248	-.297	.088	-.030	-.795
280	115	-.276	.083	-.036	-.837	280	165	-.240	.082	-.036	-.918	280	249	-.327	.099	.123	-.977
280	116	.165	.156	.846	-.226	280	166	-.277	.095	-.027	-1.631	280	250	-.328	.108	.074	-.994

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
280	251	-.359	.109	-.073	-.952	280	324	-.332	.157	.069	-1.098	280	374	-.365	.114	-.065	-1.135
280	252	-.295	.116	-.032	-1.216	280	325	-.302	.103	.038	-.926	280	375	-.333	.107	-.039	-.888
280	253	-.297	.092	-.027	-.844	280	326	-.316	.101	.004	-.947	280	376	-.271	.090	.039	-.759
280	254	-.291	.104	-.031	-.999	280	327	.187	.168	.826	-.366	280	377	-.334	.093	.051	-.802
280	255	-.283	.101	.124	-1.027	280	328	.216	.135	.660	-.211	280	378	-.223	.100	.251	-.712
280	256	-.271	.085	.010	-.795	280	329	-.581	.222	-.080	-1.585	280	379	-.302	.085	-.044	-.779
280	257	-.296	.102	-.015	-.944	280	330	-.577	.244	.202	-1.631	280	380	-.264	.083	.014	-.782
280	258	-.287	.100	-.021	-.794	280	331	-.426	.217	.164	-1.321	280	401	-.302	.182	.416	-1.041
280	259	-.286	.105	.027	-.831	280	332	-.345	.131	-.056	-1.023	280	402	-.366	.151	.534	-.951
280	260	-.298	.113	-.068	-1.098	280	333	-.320	.119	-.006	-.838	280	403	-.375	.133	.321	-.863
280	261	-.299	.112	-.071	-1.067	280	334	-.330	.121	.043	-1.032	280	404	-.167	.303	.853	-.990
280	262	-.303	.100	.022	-.907	280	335	.356	.154	.870	-.030	280	405	-.298	.249	.950	-1.002
280	263	-.291	.098	-.016	-.864	280	336	-.320	.089	-.135	-.795	280	406	.120	.123	.663	-.263
280	264	-.246	.099	.079	-.982	280	337	.114	.132	.563	-.480	280	407	.139	.112	.592	-.201
280	265	-.266	.120	.042	-.959	280	338	.139	.141	.633	-.494	280	408	.166	.139	.688	-.259
280	266	-.263	.130	-.021	-.982	280	339	-.587	.217	-.065	-1.569	280	409	.218	.159	.797	-.235
280	267	-.253	.126	.008	-.896	280	340	-.557	.184	-.000	-1.321	280	410	.257	.164	.837	-.180
280	268	-.244	.079	-.013	-.732	280	341	-.426	.189	.027	-1.344	280	411	.293	.137	.722	-.152
280	269	-.277	.101	-.044	-.954	280	342	-.353	.152	.043	-1.127	280	412	.057	.096	.475	-.249
280	270	-.239	.088	.021	-.854	280	343	-.326	.115	.031	-.868	280	413	.221	.131	.695	-.189
280	271	-.249	.128	.080	-.974	280	344	-.350	.111	-.054	-1.669	280	414	.221	.138	.720	-.173
280	272	-.259	.148	.176	-1.566	280	345	.029	.128	.687	-.505	280	415	.317	.145	.899	-.045
280	273	-.236	.085	.026	-.782	280	346	.055	.138	.721	-.530	280	416	.360	.177	.980	-.261
280	274	-.250	.108	.105	-.985	280	347	-.568	.214	.012	-1.573	280	417	.361	.181	1.128	-.342
280	275	-.235	.094	.059	-.977	280	348	-.516	.201	-.050	-1.533	280	418	.354	.198	1.159	-.390
280	276	-.233	.086	-.055	-.779	280	349	-.414	.164	.034	-1.200	280	419	.310	.142	.764	-.137
280	277	-.227	.102	.084	-1.071	280	350	-.354	.143	.048	-1.436	280	420	.005	.083	.406	-.256
280	301	-.345	.138	.169	-.925	280	351	-.327	.114	-.023	-.903	280	421	.159	.121	.722	-.167
280	302	-.405	.127	-.089	-.953	280	352	-.354	.114	-.088	-1.111	280	422	.191	.133	.834	-.135
280	303	-.317	.107	.021	-.867	280	353	.160	.127	.804	-.167	280	423	.321	.128	.824	.030
280	304	-.134	.135	.424	-.695	280	354	-.333	.120	-.064	-1.184	280	424	.370	.162	1.018	-.048
280	305	-.446	.189	-.065	-1.445	280	355	-.101	.102	.349	-.408	280	425	.359	.170	1.021	-.135
280	306	-.357	.132	-.037	-.979	280	356	-.061	.091	.315	-.360	280	426	.324	.166	.921	-.264
280	307	-.182	.147	.218	-.778	280	357	-.535	.183	-.112	-1.650	280	427	.275	.160	.878	-.335
280	308	-.306	.090	-.002	-.704	280	358	-.517	.188	.010	-1.517	280	428	-.037	.075	.314	-.368
280	309	.230	.168	.863	-.322	280	359	-.429	.171	.073	-1.347	280	429	.118	.106	.486	-.220
280	310	.288	.145	.763	-.171	280	360	-.349	.113	-.027	-1.003	280	430	.137	.094	.513	-.119
280	311	-.549	.182	.009	-1.516	280	361	-.325	.119	-.013	-1.049	280	431	.276	.141	.871	-.122
280	312	-.537	.220	.219	-1.817	280	362	-.337	.133	-.012	-1.391	280	432	.333	.161	1.069	-.125
280	313	-.336	.192	.141	-1.228	280	363	-.253	.067	-.053	-.576	280	433	.320	.168	1.023	-.161
280	314	-.288	.102	.036	-.788	280	364	-.262	.058	.005	-.512	280	434	.258	.151	.899	-.266
280	315	-.297	.083	.076	-.704	280	365	-.406	.135	-.097	-1.272	280	435	.209	.147	.789	-.246
280	316	-.305	.088	-.002	-.766	280	366	-.381	.118	-.090	-.965	280	436	-.084	.066	.256	-.322
280	317	.413	.175	.998	-.086	280	367	-.342	.102	-.076	-.861	280	437	.054	.085	.534	-.213
280	318	-.291	.064	-.115	-.614	280	368	-.338	.077	-.162	-.798	280	438	.077	.073	.428	-.117
280	319	.236	.141	.797	-.311	280	369	-.329	.112	-.045	-.917	280	439	.194	.117	.739	-.058
280	320	.260	.171	.925	-.245	280	370	-.321	.097	.043	-.856	280	440	.239	.143	.909	-.108
280	321	-.555	.213	.048	-1.438	280	371	-.024	.054	.210	-.232	280	441	.225	.151	.777	-.185
280	322	-.546	.197	-.039	-1.456	280	372	-.300	.108	-.036	-.942	280	442	.207	.154	.729	-.373
280	323	-.400	.200	.127	-1.319	280	373	-.181	.063	.128	-.569	280	443	.128	.148	.741	-.507

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
280	444	-.102	.073	.338	-.431
280	445	.038	.078	.429	-.271
280	446	.061	.063	.376	-.162
280	447	.145	.100	.584	-.150
280	448	.168	.130	.695	-.176
280	449	.139	.142	.660	-.333
280	450	.094	.139	.605	-.408
280	451	.060	.128	.508	-.317
280	452	-.079	.086	.224	-.577
280	453	.038	.077	.414	-.302
280	454	.064	.059	.301	-.137
280	455	.104	.077	.482	-.147
280	456	.085	.088	.503	-.208
280	457	.028	.095	.498	-.244
280	458	-.021	.103	.406	-.415
280	459	-.027	.101	.366	-.411
280	460	-.043	.080	.312	-.366
280	461	.034	.068	.457	-.173
280	462	.060	.052	.426	-.122
280	463	.058	.050	.276	-.113
280	464	.015	.057	.309	-.189
280	465	-.103	.052	.100	-.342
280	466	-.230	.080	.169	-.581
280	467	-.176	.077	.085	-.478
280	468	.038	.061	.309	-.232
280	469	.111	.064	.408	-.065
280	470	.107	.077	.491	-.090
280	471	.093	.080	.498	-.111
280	472	.016	.063	.316	-.188
280	473	-.018	.051	.288	-.144
280	474	.120	.086	.569	-.107
280	475	.114	.094	.568	-.106
280	476	.100	.095	.651	-.128
280	477	.007	.078	.475	-.178
280	801	-.312	.136	-.011	-1.085
280	802	-.269	.098	-.002	-.823
280	803	-.276	.095	.021	-.902
280	804	.073	.079	.616	-.121
280	805	.140	.089	.710	-.073
280	806	.061	.101	.701	-.191
280	807	-.298	.090	-.065	-.813
280	808	-.342	.107	-.100	-.832
280	809	-.364	.087	-.152	-.914
280	810	-.346	.096	-.094	-.996
280	901	-.324	.099	-.022	-1.010
280	902	-.293	.081	-.055	-.735
280	903	-.286	.084	-.030	-.658
280	904	-.346	.073	-.113	-.677
280	905	-.344	.122	.082	-1.051
280	906	-.369	.105	-.027	-.909
280	907	-.372	.106	-.028	-.855
280	908	-.358	.089	-.091	-.814
280	909	-.334	.086	-.110	-.798
280	910	-.407	.108	-.123	-.940
280	911	-.426	.114	-.119	-.942
280	912	-.394	.101	-.096	-.963
280	913	-.389	.108	-.117	-.923
280	914	-.420	.128	-.073	-1.231
280	915	-.375	.109	-.053	-.924
280	916	-.362	.077	-.132	-.730
280	917	-.409	.125	.108	-.876
280	918	-.502	.151	.017	-1.181
290	101	-.334	.106	-.027	-.860
290	102	-.380	.123	-.048	-1.013
290	103	-.357	.120	-.002	-1.140
290	104	-.361	.145	.076	-1.351
290	105	-.361	.133	-.008	-1.137
290	106	-.362	.137	-.001	-1.280
290	107	-.344	.119	-.037	-1.046
290	108	-.328	.109	-.035	-.978
290	109	-.369	.135	-.019	-1.114
290	110	-.358	.136	.002	-.948
290	111	-.346	.124	.057	-.917
290	112	-.340	.116	-.047	-1.242
290	113	-.338	.099	-.108	-.940
290	114	-.329	.109	-.078	-1.036
290	115	-.277	.083	-.027	-.806
290	116	.179	.168	.890	-.221
290	117	-.391	.153	-.077	-1.394
290	118	-.379	.147	.002	-1.118
290	119	-.364	.132	.111	-1.165
290	120	-.337	.104	-.065	-1.140
290	121	-.326	.110	-.024	-1.046
290	122	-.321	.108	-.049	-.982
290	123	-.372	.142	-.009	-1.606
290	124	-.362	.140	.002	-1.293
290	125	-.363	.138	-.039	-1.108
290	126	-.366	.141	-.049	-1.397
290	127	-.374	.128	-.123	-1.369
290	128	-.366	.137	-.088	-1.424
290	129	-.288	.073	-.077	-.747
290	130	.065	.116	.660	-.223
290	131	-.351	.128	-.027	-1.102
290	132	-.353	.135	.027	-1.138
290	133	-.382	.146	-.012	-1.217
290	134	-.415	.163	.007	-1.574
290	135	-.405	.130	-.103	-1.281
290	136	-.399	.140	-.076	-1.388
290	137	-.285	.120	.015	-1.199
290	138	-.283	.118	-.023	-.969
290	139	-.347	.131	-.057	-1.006
290	140	-.415	.161	-.029	-1.617
290	141	-.453	.167	-.108	-1.581
290	142	-.452	.159	-.143	-1.817
290	143	-.281	.090	-.095	-.828
290	144	.054	.083	.525	-.173
290	145	-.238	.071	-.024	-.619
290	146	-.234	.076	-.035	-.623
290	147	-.253	.100	.014	-.857
290	148	-.372	.144	-.006	-1.208
290	149	-.433	.130	-.080	-1.397
290	150	-.445	.137	-.058	-1.615
290	151	-.199	.059	-.049	-.482
290	152	-.183	.053	-.035	-.543
290	153	-.183	.046	-.022	-.511
290	154	-.225	.087	.012	-1.007
290	155	-.370	.146	-.052	-1.338
290	156	-.403	.129	-.088	-1.252
290	157	-.251	.089	-.047	-.774
290	158	.046	.059	.377	-.130
290	159	-.151	.054	.003	-.405
290	160	-.155	.055	.067	-.448
290	161	-.185	.076	.124	-.771
290	162	-.312	.129	.220	-1.097
290	163	-.201	.059	.054	-.487
290	164	-.160	.051	.157	-.410
290	165	-.234	.075	.016	-1.016
290	166	-.270	.084	.025	-.951
290	201	-.290	.089	-.055	-.761
290	202	-.268	.086	-.031	-.701
290	203	-.275	.088	-.008	-.801
290	204	-.291	.095	-.019	-.695
290	205	-.305	.087	-.047	-.669
290	206	-.271	.092	-.026	-.813
290	207	-.251	.067	-.069	-.802
290	208	-.273	.067	-.043	-.637
290	209	-.264	.078	-.048	-.642
290	210	-.277	.076	-.060	-.709
290	211	-.282	.091	.010	-.724
290	212	-.278	.091	-.032	-.648
290	213	-.284	.091	-.041	-.640
290	214	-.269	.078	-.075	-.642
290	215	-.267	.079	-.067	-.706
290	216	-.262	.076	-.062	-.711
290	217	-.271	.082	-.051	-.740
290	218	-.275	.076	-.072	-.634
290	219	-.288	.090	-.034	-.747
290	220	-.287	.107	.038	-.960
290	221	-.292	.105	-.024	-.975
290	222	-.284	.084	-.085	-.704

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
290	223	-.278	.079	-.095	-.716	290	273	-.207	.063	-.030	-.558	290	346	-.038	.145	.625	-.730
290	224	-.262	.066	-.008	-.577	290	274	-.212	.080	.005	-.661	290	347	-.444	.182	-.083	-1.348
290	225	-.264	.057	-.087	-.567	290	275	-.211	.075	.028	-.871	290	348	-.444	.178	-.083	-1.425
290	226	-.269	.068	-.044	-.558	290	276	-.215	.070	-.008	-.565	290	349	-.379	.152	.036	-1.078
290	227	-.288	.082	-.003	-.706	290	277	-.206	.077	.010	-.717	290	350	-.333	.135	-.005	-1.066
290	228	-.301	.113	-.031	-.963	290	301	-.346	.142	.309	-1.015	290	351	-.301	.111	.006	-1.148
290	229	-.304	.102	-.047	-.861	290	302	-.399	.122	-.070	-1.097	290	352	-.333	.120	-.039	-1.401
290	230	-.291	.098	-.072	-.775	290	303	-.319	.103	.017	-.770	290	353	-.111	.127	.782	-.295
290	231	-.280	.086	-.005	-.718	290	304	-.137	.138	.507	-.613	290	354	-.295	.108	-.059	-1.275
290	232	-.270	.071	-.094	-.790	290	305	-.433	.180	.019	-1.341	290	355	-.148	.104	.400	-.594
290	233	-.267	.066	-.052	-.592	290	306	-.407	.128	.013	-1.015	290	356	-.121	.100	.401	-.617
290	234	-.273	.075	-.059	-.640	290	307	-.309	.127	.064	-.892	290	357	-.442	.185	-.106	-1.501
290	235	-.293	.089	-.042	-.682	290	308	-.308	.105	.063	-.803	290	358	-.425	.181	-.064	-1.326
290	236	-.298	.121	-.012	-1.094	290	309	.101	.175	.741	-.505	290	359	-.367	.148	.061	-1.043
290	237	-.308	.110	-.075	-.985	290	310	.186	.152	.744	-.332	290	360	-.329	.104	.028	-.885
290	238	-.299	.110	-.044	-1.406	290	311	-.454	.189	-.068	-1.468	290	361	-.301	.110	-.009	-.918
290	239	-.282	.092	-.049	-.960	290	312	-.459	.196	.024	-1.506	290	362	-.310	.123	-.032	-1.212
290	240	-.272	.071	-.041	-.711	290	313	-.386	.165	.056	-1.191	290	363	-.249	.064	-.054	-.536
290	241	-.292	.081	-.045	-.744	290	314	-.346	.116	.036	-.935	290	364	-.266	.057	-.072	-.567
290	242	-.297	.092	-.031	-.790	290	315	-.300	.102	.044	-.801	290	365	-.386	.140	-.114	-1.223
290	243	-.315	.106	-.035	-.875	290	316	-.309	.109	-.000	-.876	290	366	-.363	.121	-.100	-1.027
290	244	-.299	.125	.033	-1.365	290	317	.398	.201	1.033	-.114	290	367	-.334	.104	-.035	-.919
290	245	-.305	.110	-.035	-1.109	290	318	-.288	.071	-.104	-.735	290	368	-.314	.074	-.129	-.660
290	246	-.296	.111	-.018	-1.080	290	319	.101	.148	.626	-.365	290	369	-.302	.094	-.070	-.862
290	247	-.284	.099	.153	-1.028	290	320	.139	.188	.878	-.582	290	370	-.294	.085	-.044	-.716
290	248	-.285	.091	-.039	-.896	290	321	-.423	.182	-.023	-1.807	290	371	-.043	.054	.205	-.218
290	249	-.280	.084	-.042	-.899	290	322	-.453	.171	-.099	-1.486	290	372	-.262	.100	.011	-.993
290	250	-.278	.091	-.031	-.866	290	323	-.388	.178	.175	-1.303	290	373	-.185	.056	.034	-.443
290	251	-.326	.118	-.038	-1.016	290	324	-.362	.164	.068	-1.187	290	374	-.320	.097	-.113	-.811
290	252	-.261	.092	-.027	-.843	290	325	-.303	.112	-.013	-1.021	290	375	-.306	.093	-.042	-.790
290	253	-.265	.088	-.050	-.933	290	326	-.314	.107	-.025	-.987	290	376	-.263	.079	-.034	-.806
290	254	-.255	.090	-.023	-.955	290	327	.090	.172	.772	-.495	290	377	-.294	.075	-.034	-.702
290	255	-.242	.082	-.032	-.918	290	328	.095	.141	.706	-.487	290	378	-.226	.077	.212	-.601
290	256	-.247	.078	-.007	-.723	290	329	-.462	.192	-.109	-1.409	290	379	-.262	.070	-.077	-.653
290	257	-.270	.086	-.072	-.694	290	330	-.463	.202	-.030	-1.557	290	380	-.243	.070	-.011	-.678
290	258	-.261	.084	-.059	-.619	290	331	-.399	.179	.144	-1.485	290	401	-.250	.228	.813	-1.283
290	259	-.254	.088	-.023	-.713	290	332	-.381	.138	-.004	-1.173	290	402	-.338	.176	.586	-1.041
290	260	-.266	.090	-.036	-.838	290	333	-.325	.118	-.027	-.931	290	403	-.343	.159	.325	-.862
290	261	-.280	.093	-.077	-.878	290	334	-.333	.128	-.022	-1.088	290	404	-.123	.322	.844	-1.035
290	262	-.273	.091	-.064	-.803	290	335	.305	.173	.021	-.114	290	405	-.248	.230	.943	-1.079
290	263	-.257	.090	-.033	-.803	290	336	-.301	.074	-.102	-.973	290	406	.133	.137	.595	-.287
290	264	-.232	.084	.057	-.826	290	337	.035	.149	.647	-.562	290	407	.145	.131	.700	-.239
290	265	-.234	.085	-.042	-.836	290	338	.061	.160	.741	-.587	290	408	.166	.156	.822	-.293
290	266	-.230	.089	-.057	-.752	290	339	-.496	.198	-.095	-1.573	290	409	.197	.167	.915	-.380
290	267	-.217	.087	-.042	-.760	290	340	-.519	.178	-.127	-1.398	290	410	.217	.169	.824	-.304
290	268	-.214	.066	-.024	-.678	290	341	-.444	.180	.100	-1.317	290	411	.248	.153	.739	-.256
290	269	-.230	.079	.065	-.704	290	342	-.390	.167	.107	-1.179	290	412	.064	.111	.439	-.280
290	270	-.238	.086	.048	-.696	290	343	-.341	.130	.061	-1.081	290	413	.201	.145	.701	-.259
290	271	-.236	.101	.112	-1.009	290	344	-.318	.104	-.074	-1.208	290	414	.222	.155	.775	-.175
290	272	-.226	.096	.014	-.917	290	345	-.063	.133	.461	-.778	290	415	.308	.148	.832	-.025

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
290	416	.333	.181	1.033	-.097
290	417	.297	.178	.924	-.178
290	418	.272	.217	.989	-.619
290	419	.270	.152	.817	-.227
290	420	.014	.095	.412	-.340
290	421	.152	.124	.625	-.219
290	422	.195	.137	.756	-.131
290	423	.324	.147	.895	.014
290	424	.345	.181	1.107	-.059
290	425	.288	.178	1.048	-.224
290	426	.173	.182	1.007	-.636
290	427	.204	.171	.891	-.665
290	428	-.034	.091	.475	-.485
290	429	.099	.114	.663	-.217
290	430	.131	.102	.666	-.103
290	431	.224	.145	.891	-.097
290	432	.244	.170	.932	-.164
290	433	.196	.177	.861	-.238
290	434	.140	.175	.970	-.634
290	435	.140	.160	.866	-.568
290	436	-.077	.079	.456	-.428
290	437	.043	.087	.546	-.217
290	438	.080	.072	.489	-.144
290	439	.156	.104	.774	-.114
290	440	.173	.133	.813	-.119
290	441	.135	.152	.828	-.245
290	442	.081	.168	.810	-.417
290	443	.058	.148	.680	-.362
290	444	-.081	.087	.485	-.499
290	445	.036	.082	.590	-.297
290	446	.058	.063	.418	-.135
290	447	.106	.082	.583	-.161
290	448	.104	.104	.699	-.235
290	449	.064	.124	.686	-.285
290	450	.008	.146	.654	-.551
290	451	.013	.119	.596	-.397
290	452	-.057	.092	.347	-.451
290	453	.042	.078	.401	-.259
290	454	.068	.061	.401	-.195
290	455	.082	.068	.509	-.166
290	456	.049	.082	.575	-.171
290	457	-.014	.093	.453	-.257
290	458	-.084	.131	.447	-.950
290	459	-.051	.109	.410	-.690
290	460	-.031	.074	.513	-.418
290	461	.032	.065	.572	-.234
290	462	.058	.053	.369	-.105
290	463	.046	.045	.254	-.136
290	464	-.007	.049	.178	-.233
290	465	-.107	.051	.071	-.325
290	466	-.224	.072	.058	-.719
290	467	-.182	.077	.052	-.558
290	468	.035	.058	.340	-.140
290	469	.092	.057	.492	-.070
290	470	.085	.068	.632	-.092
290	471	.068	.070	.640	-.111
290	472	-.001	.059	.333	-.195
290	473	-.015	.047	.220	-.175
290	474	.111	.068	.459	-.058
290	475	.102	.076	.489	-.090
290	476	.086	.079	.540	-.103
290	477	-.045	.057	.256	-.194
290	801	-.294	.113	-.067	-.900
290	802	-.245	.083	-.053	-.646
290	803	-.250	.084	-.051	-.769
290	804	.055	.062	.407	-.119
290	805	.083	.059	.472	-.050
290	806	-.001	.076	.456	-.173
290	807	-.261	.072	-.015	-.637
290	808	-.284	.084	-.056	-.762
290	809	-.324	.095	-.090	-.764
290	810	-.313	.104	-.053	-.787
290	901	-.322	.113	.100	-.898
290	902	-.293	.089	.040	-.723
290	903	-.292	.097	.014	-.784
290	904	-.332	.080	-.060	-.758
290	905	-.355	.127	.047	-.865
290	906	-.366	.118	.012	-1.023
290	907	-.342	.109	-.003	-.854
290	908	-.370	.100	-.053	-.810
290	909	-.360	.106	-.050	-.851
290	910	-.392	.118	-.083	-.931
290	911	-.405	.124	-.089	-.926
290	912	-.426	.107	-.138	-.926
290	913	-.416	.123	-.117	-.952
290	914	-.420	.136	-.031	-1.095
290	915	-.405	.115	-.128	-.971
290	916	-.378	.086	-.143	-.763
290	917	-.390	.137	.165	-.910
290	918	-.450	.148	-.047	-1.110
300	101	-.319	.101	.007	-.787
300	102	-.392	.133	-.008	-1.099
300	103	-.388	.129	-.021	-.987
300	104	-.340	.147	.193	-1.124
300	105	-.378	.153	.036	-1.205
300	106	-.408	.161	.015	-1.368
300	107	-.398	.148	-.002	-1.324
300	108	-.384	.141	-.062	-1.637
300	109	-.344	.133	.064	-1.139
300	110	-.338	.138	.060	-1.305
300	111	-.358	.140	.102	-1.141
300	112	-.384	.148	.063	-1.116
300	113	-.381	.122	-.096	-1.119
300	114	-.369	.132	-.058	-1.202
300	115	-.265	.084	-.045	-.688
300	116	.238	.158	.869	-.180
300	117	-.386	.163	.047	-1.478
300	118	-.375	.156	.178	-1.047
300	119	-.382	.154	.114	-1.194
300	120	-.387	.125	.012	-1.2[illegible]
300	121	-.375	.135	-.070	-1.4[illegible]
300	122	-.367	.132	-.069	-1.425
300	123	-.366	.153	.061	-1.124
300	124	-.358	.150	.083	-1.932
300	125	-.379	.154	.027	-1.211
300	126	-.401	.159	-.013	-1.415
300	127	-.405	.133	-.121	-1.139
300	128	-.396	.143	-.090	-1.187
300	129	-.295	.092	-.081	-.732
300	130	.131	.147	.779	-.166
300	131	-.358	.152	-.017	-1.453
300	132	-.358	.161	.050	-1.378
300	133	-.401	.175	.044	-1.527
300	134	-.446	.186	-.058	-1.608
300	135	-.429	.142	-.160	-1.515
300	136	-.421	.153	-.093	-1.810
300	137	-.269	.106	-.002	-.785
300	138	-.274	.112	.016	-.925
300	139	-.331	.131	-.020	-1.048
300	140	-.414	.164	-.065	-1.519
300	141	-.482	.188	-.130	-1.853
300	142	-.450	.163	-.151	-1.471
300	143	-.275	.091	-.074	-.911
300	144	.063	.086	.546	-.160
300	145	-.224	.070	-.000	-.570
300	146	-.217	.073	.022	-.580
300	147	-.235	.095	.037	-.788
300	148	-.317	.112	-.025	-.900
300	149	-.418	.144	.029	-1.382
300	150	-.435	.150	.123	-1.584
300	151	-.202	.060	-.033	-.532
300	152	-.188	.051	-.025	-.430
300	153	-.181	.044	-.054	-.489
300	154	-.199	.077	.007	-.678
300	155	-.315	.142	.119	-1.093
300	156	-.361	.132	.164	-.986
300	157	-.254	.091	-.074	-.752
300	158	.032	.052	.256	-.158
300	159	-.152	.054	.015	-.397
300	160	-.154	.052	.060	-.486

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
300	161	-.154	.057	.047	-.423	300	245	-.284	.090	-.044	-.902	300	318	-.267	.058	-.124	-.567
300	162	-.260	.122	.201	-.728	300	246	-.271	.084	.082	-.789	300	319	-.044	.135	.514	-.667
300	163	-.214	.060	-.033	-.503	300	247	-.265	.076	-.011	-.702	300	320	-.025	.163	.667	-.892
300	164	-.160	.047	.041	-.354	300	248	-.269	.077	-.069	-.596	300	321	-.335	.143	-.050	-1.446
300	165	-.211	.066	.037	-.733	300	249	-.271	.081	-.077	-.912	300	322	-.351	.115	-.079	-1.096
300	166	-.248	.080	.248	-.653	300	250	-.264	.086	-.035	-.875	300	323	-.336	.140	-.000	-1.315
300	201	-.279	.083	-.044	-.659	300	251	-.267	.088	-.021	-.870	300	324	-.340	.136	.008	-1.311
300	202	-.270	.087	-.030	-.791	300	252	-.252	.091	-.020	-1.061	300	325	-.298	.097	-.017	-.898
300	203	-.285	.092	.006	-.935	300	253	-.265	.087	-.036	-.654	300	326	-.286	.088	-.045	-.772
300	204	-.294	.100	.029	-.963	300	254	-.253	.082	.051	-.663	300	327	-.082	.158	.497	-.747
300	205	-.303	.091	.002	-.728	300	255	-.248	.087	.016	-1.151	300	328	-.066	.134	.474	-.567
300	206	-.265	.081	-.022	-.600	300	256	-.271	.102	-.032	-1.049	300	329	-.380	.160	-.045	-1.431
300	207	-.252	.071	-.035	-.751	300	257	-.254	.083	-.003	-.654	300	330	-.379	.164	-.021	-1.684
300	208	-.257	.065	-.103	-.631	300	258	-.243	.079	-.062	-.658	300	331	-.353	.145	.294	-1.638
300	209	-.267	.079	-.037	-.648	300	259	-.235	.081	-.046	-.724	300	332	-.329	.111	-.049	-1.258
300	210	-.283	.083	-.069	-.802	300	260	-.239	.075	.010	-.692	300	333	-.288	.097	-.045	-1.061
300	211	-.284	.097	-.007	-.841	300	261	-.247	.074	-.041	-.631	300	334	-.295	.108	-.065	-1.243
300	212	-.293	.094	-.054	-.784	300	262	-.240	.072	-.036	-.639	300	335	.158	.121	.738	-.122
300	213	-.288	.096	-.054	-.906	300	263	-.225	.075	.029	-.593	300	336	-.292	.068	-.129	-.595
300	214	-.265	.078	-.077	-.766	300	264	-.238	.095	.032	-1.300	300	337	-.130	.151	.542	-.671
300	215	-.260	.079	-.077	-.778	300	265	-.251	.087	-.072	-.797	300	338	-.197	.166	.652	-.704
300	216	-.259	.076	-.066	-.727	300	266	-.242	.088	-.004	-.875	300	339	-.413	.171	-.074	-1.353
300	217	-.268	.084	-.052	-.815	300	267	-.232	.088	-.004	-.857	300	340	-.398	.136	-.109	-1.195
300	218	-.282	.082	-.067	-.769	300	268	-.216	.071	-.010	-.623	300	341	-.360	.144	.028	-1.339
300	219	-.293	.096	-.033	-.830	300	269	-.221	.072	.036	-.726	300	342	-.338	.142	.078	-1.580
300	220	-.285	.093	-.046	-.825	300	270	-.251	.102	.004	-.935	300	343	-.297	.106	-.010	-.985
300	221	-.290	.093	-.047	-.845	300	271	-.246	.093	.016	-.779	300	344	-.307	.087	-.102	-1.131
300	222	-.293	.077	-.090	-.715	300	272	-.227	.084	-.025	-.904	300	345	-.141	.129	.502	-.666
300	223	-.270	.071	-.051	-.663	300	273	-.200	.064	.001	-.544	300	346	-.121	.140	.521	-.660
300	224	-.261	.066	-.079	-.541	300	274	-.195	.074	.112	-.668	300	347	-.378	.150	-.086	-1.040
300	225	-.278	.075	-.084	-.682	300	275	-.214	.087	.020	-1.196	300	348	-.393	.158	-.036	-1.251
300	226	-.282	.090	-.017	-.862	300	276	-.197	.056	-.053	-.507	300	349	-.338	.128	-.033	-1.048
300	227	-.305	.109	.024	-.850	300	277	-.189	.061	-.007	-.508	300	350	-.320	.126	.044	-1.057
300	228	-.300	.111	-.050	-1.083	300	301	-.322	.121	.063	-.913	300	351	-.287	.104	-.015	-1.016
300	229	-.303	.101	-.067	-.876	300	302	-.336	.108	-.020	-.819	300	352	-.303	.089	-.089	-1.437
300	230	-.289	.096	-.030	-1.024	300	303	-.296	.102	-.018	-.826	300	353	.049	.086	.643	-.243
300	231	-.276	.080	-.081	-.820	300	304	-.198	.107	.364	-.789	300	354	-.267	.080	-.023	-.912
300	232	-.264	.066	-.054	-.608	300	305	-.322	.114	-.062	-.948	300	355	-.193	.092	.216	-.539
300	233	-.287	.075	-.092	-.618	300	306	-.353	.105	-.054	-.891	300	356	-.189	.085	.183	-.585
300	234	-.290	.091	-.033	-.676	300	307	-.315	.109	.023	-.873	300	357	-.349	.127	-.076	-1.317
300	235	-.311	.111	-.004	-.857	300	308	-.293	.097	.027	-.791	300	358	-.342	.122	-.062	-1.096
300	236	-.305	.118	.005	-1.076	300	309	-.038	.154	.629	-.665	300	359	-.318	.110	.035	-1.268
300	237	-.301	.100	-.059	-.871	300	310	.026	.147	.601	-.483	300	360	-.294	.084	-.032	-.906
300	238	-.299	.097	-.041	-.977	300	311	-.330	.125	-.045	-1.096	300	361	-.264	.080	-.035	-.754
300	239	-.278	.084	-.059	-.789	300	312	-.336	.133	-.009	-1.222	300	362	-.271	.087	-.050	-.977
300	240	-.271	.075	-.077	-.685	300	313	-.320	.123	.004	-1.114	300	363	-.241	.061	-.060	-.549
300	241	-.291	.086	-.097	-.713	300	314	-.334	.108	.083	-.944	300	364	-.256	.058	-.094	-.538
300	242	-.291	.098	-.054	-.815	300	315	-.289	.095	-.030	-1.031	300	365	-.311	.097	-.061	-.914
300	243	-.305	.113	-.044	-.948	300	316	-.295	.101	-.057	-1.069	300	366	-.301	.090	-.077	-.759
300	244	-.290	.118	-.052	-1.066	300	317	.306	.184	1.051	-.226	300	367	-.289	.086	-.053	-.769

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
300	368	-.291	.063	-.106	-.817	300	438	.115	.104	.822	-.139	300	901	-.322	.115	.181	-.846
300	369	-.273	.075	-.056	-.739	300	439	.151	.107	.926	-.123	300	902	-.304	.096	.014	-.750
300	370	-.272	.076	-.077	-.837	300	440	.122	.097	.669	-.211	300	903	-.290	.092	-.024	-.694
300	371	-.054	.047	.143	-.226	300	441	.048	.103	.606	-.371	300	904	-.334	.086	-.015	-.681
300	372	-.250	.082	.005	-.765	300	442	-.069	.147	.656	-.588	300	905	-.349	.126	-.009	-.973
300	373	-.204	.059	.025	-.473	300	443	-.005	.125	.566	-.692	300	906	-.370	.128	.056	-.895
300	374	-.279	.082	-.058	-.766	300	444	-.045	.090	.356	-.412	300	907	-.322	.109	-.008	-.893
300	375	-.269	.077	-.069	-.683	300	445	.058	.092	.514	-.191	300	908	-.391	.107	-.065	-1.067
300	376	-.258	.079	-.041	-.797	300	446	.112	.091	.594	-.151	300	909	-.395	.128	-.047	-1.096
300	377	-.288	.074	-.075	-.776	300	447	.128	.093	.649	-.113	300	910	-.390	.118	-.073	-1.118
300	378	-.247	.080	.042	-.880	300	448	.085	.081	.430	-.219	300	911	-.395	.127	-.069	-1.309
300	379	-.261	.077	-.041	-.990	300	449	.006	.082	.443	-.259	300	912	-.401	.103	-.096	-.918
300	380	-.256	.081	-.011	-.978	300	450	-.129	.129	.360	-.695	300	913	-.388	.120	-.100	-1.031
300	401	-.275	.234	.891	-.904	300	451	-.038	.104	.495	-.402	300	914	-.358	.118	-.055	-1.182
300	402	-.346	.166	.684	-.865	300	452	-.027	.088	.525	-.332	300	915	-.388	.112	-.084	-.878
300	403	-.328	.159	.414	-.833	300	453	.058	.085	.524	-.179	300	916	-.399	.097	-.105	-.861
300	404	-.104	.294	.916	-1.091	300	454	.091	.068	.518	-.124	300	917	-.382	.139	.150	-.983
300	405	-.271	.181	.795	-.940	300	455	.084	.065	.450	-.143	300	918	-.409	.127	-.029	-1.109
300	406	.146	.148	.791	-.314	300	456	.031	.059	.312	-.158	310	101	-.300	.097	.040	-.726
300	407	.151	.140	.785	-.196	300	457	-.050	.068	.356	-.361	310	102	-.348	.137	-.020	-1.012
300	408	.154	.163	.805	-.211	300	458	-.193	.101	.333	-.608	310	103	-.434	.143	.015	-.931
300	409	.166	.170	.850	-.255	300	459	-.084	.109	.374	-.694	310	104	-.252	.150	.122	-1.115
300	410	.173	.169	.869	-.293	300	460	-.008	.077	.414	-.443	310	105	-.322	.177	.152	-1.358
300	411	.223	.172	.861	-.388	300	461	.048	.073	.505	-.198	310	106	-.374	.173	.031	-1.257
300	412	.104	.137	.689	-.304	300	462	.064	.056	.338	-.122	310	107	-.423	.184	.082	-1.428
300	413	.235	.166	1.022	-.195	300	463	.042	.045	.245	-.120	310	108	-.462	.191	-.072	-1.459
300	414	.268	.178	1.094	-.174	300	464	-.009	.044	.134	-.199	310	109	-.281	.128	.004	-1.164
300	415	.337	.171	.903	-.070	300	465	-.101	.044	.044	-.305	310	110	-.285	.141	.096	-1.100
300	416	.319	.191	1.035	-.171	300	466	-.233	.074	.041	-.631	310	111	-.347	.172	.118	-1.223
300	417	.230	.169	.891	-.231	300	467	-.178	.080	.150	-.513	310	112	-.441	.194	.101	-1.487
300	418	.128	.241	1.099	-.872	300	468	.033	.057	.354	-.123	310	113	-.462	.166	-.040	-1.310
300	419	.245	.176	.977	-.238	300	469	.075	.047	.316	-.051	310	114	-.453	.175	-.054	-1.337
300	420	.063	.127	.581	-.400	300	470	.065	.052	.289	-.091	310	115	-.247	.076	-.023	-.687
300	421	.195	.156	.858	-.231	300	471	.042	.059	.242	-.119	310	116	.291	.180	.867	-.222
300	422	.252	.172	1.009	-.122	300	472	-.016	.048	.187	-.193	310	117	-.315	.160	.023	-1.305
300	423	.315	.149	.950	.002	300	473	-.016	.044	.238	-.165	310	118	-.310	.159	.130	-1.220
300	424	.284	.162	.944	-.062	300	474	.076	.052	.427	-.076	310	119	-.345	.176	.080	-1.316
300	425	.176	.144	.751	-.248	300	475	.053	.052	.350	-.096	310	120	-.427	.164	-.025	-1.400
300	426	.016	.184	.676	-.588	300	476	.037	.049	.304	-.127	310	121	-.441	.187	-.021	-1.613
300	427	.147	.185	.868	-.607	300	477	-.061	.046	.191	-.217	310	122	-.434	.184	-.040	-1.461
300	428	.004	.118	.585	-.318	300	801	-.259	.082	-.051	-.641	310	123	-.308	.149	.028	-1.315
300	429	.127	.137	.852	-.207	300	802	-.218	.066	.020	-.532	310	124	-.306	.153	.014	-1.140
300	430	.191	.134	.819	-.085	300	803	-.226	.068	-.041	-.620	310	125	-.346	.177	.116	-1.595
300	431	.237	.150	.891	-.090	300	804	.042	.053	.284	-.112	310	126	-.399	.190	.072	-1.522
300	432	.205	.136	.908	-.100	300	805	.061	.045	.339	-.073	310	127	-.407	.152	-.113	-1.273
300	433	.108	.121	.696	-.205	300	806	-.022	.056	.351	-.184	310	128	-.402	.165	-.081	-1.600
300	434	-.027	.177	.703	-.670	300	807	-.253	.068	-.065	-.650	310	129	-.256	.079	-.080	-.661
300	435	.094	.164	.704	-.607	300	808	-.268	.071	-.055	-.682	310	130	.157	.143	.720	-.152
300	436	-.026	.107	.503	-.383	300	809	-.288	.062	-.128	-.601	310	131	-.292	.136	-.035	-1.142
300	437	.098	.115	.632	-.248	300	810	-.279	.071	-.101	-.683	310	132	-.294	.146	.076	-1.197

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
310	133	-.337	.162	.099	-1.120	310	217	-.243	.075	-.008	-.588	310	267	-.214	.079	-.051	-.759
310	134	-.392	.172	.014	-1.508	310	218	-.251	.075	-.065	-.749	310	268	-.189	.064	-.008	-.592
310	135	-.425	.147	-.120	-1.310	310	219	-.258	.089	-.017	-.832	310	269	-.209	.068	-.000	-.627
310	136	-.423	.159	-.098	-1.421	310	220	-.255	.078	-.014	-.789	310	270	-.239	.095	.014	-.853
310	137	-.256	.116	.084	-1.036	310	221	-.256	.077	-.015	-.701	310	271	-.239	.095	-.031	-.854
310	138	-.257	.123	.040	-1.141	310	222	-.247	.055	-.094	-.508	310	272	-.223	.082	-.001	-.682
310	139	-.283	.123	-.006	-.986	310	223	-.239	.055	-.067	-.515	310	273	-.193	.062	.024	-.675
310	140	-.359	.154	.133	-1.329	310	224	-.242	.059	-.036	-.560	310	274	-.193	.067	.053	-.769
310	141	-.429	.169	-.011	-1.789	310	225	-.253	.071	-.079	-.608	310	275	-.222	.090	-.008	-.921
310	142	-.400	.138	-.119	-1.325	310	226	-.254	.084	-.034	-.728	310	276	-.215	.069	-.037	-.589
310	143	-.242	.084	-.063	-.912	310	227	-.248	.102	-.004	-.786	310	277	-.207	.074	-.017	-.589
310	144	.074	.072	.408	-.176	310	228	-.258	.091	-.034	-.866	310	301	-.304	.113	.058	-.851
310	145	-.209	.066	.016	-.717	310	229	-.263	.077	-.070	-.865	310	302	-.277	.081	-.067	-.621
310	146	-.201	.065	.041	-.661	310	230	-.252	.070	-.075	-.802	310	303	-.257	.084	-.029	-.712
310	147	-.210	.082	.037	-.718	310	231	-.244	.062	-.072	-.611	310	304	-.232	.093	.132	-.659
310	148	-.318	.135	.075	-1.141	310	232	-.246	.063	-.029	-.572	310	305	-.260	.077	-.040	-.648
310	149	-.369	.160	.172	-1.271	310	233	-.274	.077	-.057	-.627	310	306	-.287	.076	-.110	-.668
310	150	-.399	.157	.245	-1.334	310	234	-.274	.091	-.034	-.708	310	307	-.282	.087	-.057	-.734
310	151	-.196	.059	-.018	-.518	310	235	-.288	.110	-.026	-.837	310	308	-.266	.082	-.027	-.659
310	152	-.185	.051	-.056	-.442	310	236	-.278	.107	-.039	-.935	310	309	-.174	.124	.384	-.569
310	153	-.176	.042	-.054	-.393	310	237	-.271	.087	-.045	-.950	310	310	-.058	.137	.444	-.487
310	154	-.185	.068	.038	-.620	310	238	-.262	.080	-.019	-.794	310	311	-.274	.077	-.050	-.702
310	155	-.286	.121	.280	-1.196	310	239	-.255	.073	-.053	-.625	310	312	-.276	.081	-.058	-.761
310	156	-.335	.115	.248	-1.012	310	240	-.258	.074	-.084	-.598	310	313	-.278	.085	-.006	-.744
310	157	-.236	.075	-.084	-.731	310	241	-.264	.078	-.060	-.682	310	314	-.286	.082	-.046	-.788
310	158	.026	.051	.285	-.131	310	242	-.262	.088	-.055	-.731	310	315	-.257	.073	-.025	-.587
310	159	-.147	.049	.032	-.348	310	243	-.269	.102	-.036	-.808	310	316	-.291	.076	-.041	-.654
310	160	-.149	.048	.058	-.362	310	244	-.248	.100	.016	-.968	310	317	-.257	.168	.919	-.375
310	161	-.139	.057	.123	-.546	310	245	-.253	.097	-.037	-.942	310	318	-.251	.054	-.068	-.507
310	162	-.224	.121	.282	-.844	310	246	-.243	.088	-.022	-.880	310	319	-.143	.124	.321	-.627
310	163	-.206	.057	-.047	-.472	310	247	-.243	.081	-.004	-.771	310	320	-.121	.168	.664	-.802
310	164	-.149	.047	.087	-.341	310	248	-.258	.088	-.022	-.789	310	321	-.283	.088	-.067	-.805
310	165	-.179	.064	.174	-.417	310	249	-.262	.084	-.094	-.816	310	322	-.284	.075	-.103	-.940
310	166	-.204	.095	.503	-.511	310	250	-.255	.090	-.052	-.764	310	323	-.289	.094	-.025	-1.027
310	201	-.245	.070	-.037	-.531	310	251	-.268	.095	-.022	-.792	310	324	-.294	.104	.070	-1.153
310	202	-.246	.075	-.017	-.559	310	252	-.224	.084	.004	-.794	310	325	-.263	.073	-.039	-.672
310	203	-.255	.081	.005	-.586	310	253	-.234	.079	-.037	-.756	310	326	-.275	.081	-.060	-.759
310	204	-.258	.086	.009	-.610	310	254	-.223	.073	-.047	-.720	310	327	-.166	.130	.381	-.794
310	205	-.295	.089	-.037	-.717	310	255	-.220	.076	-.086	-.713	310	328	-.152	.122	.294	-.676
310	206	-.238	.074	-.034	-.621	310	256	-.246	.099	-.041	-.921	310	329	-.304	.115	-.065	-1.135
310	207	-.240	.059	-.059	-.557	310	257	-.259	.086	-.062	-.794	310	330	-.302	.116	-.063	-1.141
310	208	-.250	.055	-.080	-.512	310	258	-.246	.082	-.060	-.784	310	331	-.297	.113	-.011	-1.087
310	209	-.244	.072	-.024	-.536	310	259	-.237	.085	-.041	-.937	310	332	-.318	.109	-.088	-1.168
310	210	-.246	.072	-.003	-.635	310	260	-.231	.088	-.034	-.772	310	333	-.280	.095	-.077	-.823
310	211	-.245	.087	.037	-.776	310	261	-.231	.081	-.052	-.689	310	334	-.285	.101	-.077	-1.030
310	212	-.245	.075	-.053	-.620	310	262	-.233	.081	-.024	-.738	310	335	.155	.135	.776	-.193
310	213	-.247	.075	-.051	-.588	310	263	-.220	.078	-.015	-.663	310	336	-.261	.062	-.107	-.600
310	214	-.239	.062	-.074	-.533	310	264	-.236	.094	-.042	-.803	310	337	-.188	.126	.294	-.878
310	215	-.237	.064	-.042	-.563	310	265	-.234	.082	-.074	-.746	310	338	-.169	.139	.382	-.923
310	216	-.238	.066	-.029	-.618	310	266	-.225	.080	-.050	-.771	310	339	-.333	.140	-.067	-1.188

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
310	340	-.326	.107	-.085	-1.046
310	341	-.315	.121	-.060	-1.157
310	342	-.317	.133	.037	-1.690
310	343	-.280	.101	-.048	-1.062
310	344	-.297	.101	-.122	-1.158
310	345	-.185	.107	.271	-.714
310	346	-.166	.116	.294	-.780
310	347	-.334	.149	-.060	-1.491
310	348	-.349	.132	-.055	-1.045
310	349	-.322	.125	.045	-1.229
310	350	-.319	.133	.077	-1.163
310	351	-.282	.104	-.032	-1.031
310	352	-.291	.096	-.103	-1.009
310	353	.037	.074	.421	-.184
310	354	-.249	.081	-.029	-.683
310	355	-.208	.081	.132	-.662
310	356	-.193	.070	.140	-.529
310	357	-.304	.114	-.047	-1.159
310	358	-.297	.112	-.051	-.935
310	359	-.284	.108	-.011	-.966
310	360	-.285	.085	-.019	-.764
310	361	-.252	.082	-.025	-.672
310	362	-.259	.088	-.013	-.833
310	363	-.234	.058	-.067	-.532
310	364	-.242	.053	-.095	-.499
310	365	-.293	.098	-.074	-.898
310	366	-.284	.093	-.044	-.811
310	367	-.275	.085	-.048	-.847
310	368	-.266	.068	-.090	-.732
310	369	-.251	.079	-.060	-.632
310	370	-.251	.081	-.020	-.737
310	371	-.056	.052	.162	-.228
310	372	-.237	.095	.110	-1.004
310	373	-.206	.054	-.025	-.542
310	374	-.252	.076	-.067	-.648
310	375	-.242	.071	-.014	-.617
310	376	-.242	.078	-.011	-.768
310	377	-.265	.068	-.077	-.576
310	378	-.237	.071	-.027	-.556
310	379	-.240	.072	-.049	-.593
310	380	-.240	.080	-.048	-.803
310	401	-.273	.277	1.100	-1.035
310	402	-.366	.186	.830	-1.050
310	403	-.352	.148	.475	-.914
310	404	-.149	.253	.933	-.834
310	405	-.316	.127	.351	-.943
310	406	.173	.157	.899	-.334
310	407	.183	.135	.670	-.182
310	408	.177	.154	.767	-.262
310	409	.175	.154	.839	-.254
310	410	.176	.148	.705	-.269
310	411	.182	.183	.918	-.474
310	412	.164	.143	.701	-.428
310	413	.294	.166	.914	-.364
310	414	.334	.174	.983	-.252
310	415	.350	.162	1.015	-.072
310	416	.305	.172	1.051	-.160
310	417	.186	.147	.709	-.298
310	418	-.012	.235	.758	-.774
310	419	.264	.184	.848	-.352
310	420	.114	.139	.727	-.308
310	421	.263	.164	.946	-.137
310	422	.331	.180	1.026	-.073
310	423	.349	.158	1.018	-.029
310	424	.287	.167	.878	-.157
310	425	.146	.139	.701	-.262
310	426	-.140	.167	.590	-.714
310	427	.109	.199	.900	-.609
310	428	.038	.124	.658	-.306
310	429	.168	.148	.950	-.200
310	430	.212	.143	.738	-.102
310	431	.250	.166	1.010	-.103
310	432	.195	.150	.814	-.130
310	433	.069	.118	.665	-.243
310	434	-.145	.151	.523	-.736
310	435	.038	.174	.780	-.614
310	436	-.025	.097	.456	-.452
310	437	.084	.112	.636	-.315
310	438	.129	.108	.618	-.124
310	439	.166	.133	.795	-.152
310	440	.125	.123	.770	-.167
310	441	.021	.098	.483	-.300
310	442	-.159	.120	.558	-.617
310	443	-.018	.126	.571	-.532
310	444	-.053	.076	.256	-.376
310	445	.044	.081	.437	-.190
310	446	.097	.088	.563	-.139
310	447	.117	.102	.612	-.129
310	448	.075	.091	.536	-.162
310	449	-.012	.076	.382	-.267
310	450	-.152	.108	.316	-.791
310	451	-.034	.100	.366	-.535
310	452	-.041	.078	.446	-.413
310	453	.037	.073	.430	-.262
310	454	.053	.058	.415	-.097
310	455	.053	.066	.507	-.147
310	456	.010	.063	.636	-.184
310	457	-.062	.059	.289	-.295
310	458	-.172	.078	.208	-.484
310	459	-.068	.089	.377	-.405
310	460	-.022	.068	.229	-.284
310	461	.029	.062	.318	-.183
310	462	.043	.049	.276	-.247
310	463	.026	.041	.200	-.149
310	464	-.020	.042	.209	-.167
310	465	-.108	.043	.058	-.280
310	466	-.210	.067	.092	-.554
310	467	-.172	.068	.082	-.491
310	468	.023	.053	.246	-.169
310	469	.059	.047	.281	-.087
310	470	.049	.052	.273	-.109
310	471	.028	.052	.290	-.121
310	472	-.024	.049	.223	-.194
310	473	-.010	.045	.257	-.137
310	474	.067	.062	.391	-.116
310	475	.042	.062	.370	-.168
310	476	.028	.059	.389	-.180
310	477	-.066	.044	.174	-.196
310	801	-.262	.091	-.042	-.894
310	802	-.221	.069	.032	-.670
310	803	-.216	.070	.022	-.700
310	804	.047	.055	.320	-.114
310	805	.070	.053	.432	-.074
310	806	-.014	.069	.412	-.214
310	807	-.250	.077	-.016	-.546
310	808	-.261	.080	-.018	-.594
310	809	-.270	.070	-.111	-.645
310	810	-.265	.080	-.074	-.665
310	901	-.276	.110	.099	-.787
310	902	-.274	.087	-.020	-.657
310	903	-.263	.085	-.007	-.657
310	904	-.319	.079	.020	-.635
310	905	-.327	.117	.154	-.840
310	906	-.339	.114	-.008	-.826
310	907	-.286	.091	.060	-.713
310	908	-.371	.108	-.080	-.911
310	909	-.389	.139	-.024	-1.096
310	910	-.341	.107	-.078	-.892
310	911	-.342	.113	-.067	-.856
310	912	-.371	.094	-.130	-.744
310	913	-.352	.107	-.075	-.850
310	914	-.307	.093	.058	-.792
310	915	-.365	.104	-.078	-.858
310	916	-.420	.104	-.135	-.887
310	917	-.388	.134	.113	-.963
310	918	-.383	.111	-.073	-.964
320	101	-.303	.092	-.004	-.663
320	102	-.230	.099	.111	-.703
320	103	-.470	.157	.233	-1.031
320	104	-.108	.101	.201	-.609

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
320	105	-.147	.141	.192	-.772	320	155	-.186	.124	.409	-.977	320	239	-.241	.063	-.051	-.656
320	106	-.288	.141	.120	-1.264	320	156	-.225	.137	.556	-.918	320	240	-.243	.063	-.082	-.588
320	107	-.323	.222	.169	-1.464	320	157	-.225	.066	-.044	-.560	320	241	-.236	.068	-.056	-.593
320	108	-.508	.208	.138	-1.554	320	158	-.023	.051	.266	-.196	320	242	-.232	.076	-.007	-.722
320	109	-.193	.073	.027	-.841	320	159	-.131	.050	.080	-.369	320	243	-.230	.083	.021	-.721
320	110	-.175	.111	.110	-.994	320	160	-.130	.051	.073	-.331	320	244	-.220	.089	.003	-.697
320	111	-.213	.184	.162	-1.130	320	161	-.109	.055	.112	-.311	320	245	-.225	.080	.002	-.766
320	112	-.384	.280	.317	-1.462	320	162	-.145	.118	.330	-.519	320	246	-.218	.069	.000	-.583
320	113	-.525	.198	.218	-1.329	320	163	-.200	.056	-.038	-.463	320	247	-.225	.068	-.031	-.555
320	114	-.523	.186	.251	-1.418	320	164	-.134	.050	.099	-.297	320	248	-.241	.070	-.058	-.545
320	115	-.225	.055	.008	-.520	320	165	-.145	.064	.240	-.353	320	249	-.232	.072	-.081	-.739
320	116	-.354	.184	1.015	-.162	320	166	-.151	.111	.477	-.491	320	250	-.226	.075	-.062	-.696
320	117	-.244	.127	.011	-1.257	320	201	-.240	.067	-.039	-.673	320	251	-.227	.070	-.052	-.854
320	118	-.239	.152	.174	-1.287	320	202	-.236	.069	-.003	-.567	320	252	-.183	.076	.032	-.879
320	119	-.291	.215	.139	-1.360	320	203	-.238	.069	-.011	-.528	320	253	-.187	.067	.022	-.630
320	120	-.398	.228	.178	-1.199	320	204	-.258	.088	-.029	-.651	320	254	-.183	.061	.005	-.719
320	121	-.500	.234	.395	-1.474	320	205	-.281	.092	-.008	-.678	320	255	-.194	.063	.006	-.483
320	122	-.517	.203	.549	-1.565	320	206	-.212	.061	-.033	-.549	320	256	-.228	.076	-.048	-.608
320	123	-.228	.102	.006	-1.025	320	207	-.220	.052	-.052	-.425	320	257	-.229	.070	-.054	-.701
320	124	-.216	.125	.102	-1.038	320	208	-.225	.047	-.079	-.438	320	258	-.221	.069	-.005	-.626
320	125	-.240	.177	.164	-1.204	320	209	-.208	.057	-.019	-.441	320	259	-.210	.071	.006	-.743
320	126	-.319	.246	.210	-1.762	320	210	-.218	.058	-.034	-.457	320	260	-.177	.061	-.005	-.562
320	127	-.453	.224	.253	-1.584	320	211	-.214	.062	-.002	-.536	320	261	-.184	.058	-.044	-.603
320	128	-.491	.216	.269	-1.698	320	212	-.223	.062	-.065	-.513	320	262	-.183	.063	-.017	-.530
320	129	-.239	.059	-.080	-.587	320	213	-.223	.061	-.070	-.492	320	263	-.178	.060	.026	-.571
320	130	.186	.148	.931	-.157	320	214	-.229	.051	-.089	-.537	320	264	-.206	.069	.032	-.608
320	131	-.223	.084	-.044	-.987	320	215	-.227	.052	-.067	-.539	320	265	-.211	.058	-.069	-.600
320	132	-.211	.101	.048	-.984	320	216	-.223	.052	-.065	-.498	320	266	-.202	.057	-.041	-.554
320	133	-.225	.138	.100	-1.226	320	217	-.221	.056	-.051	-.542	320	267	-.191	.057	-.028	-.530
320	134	-.280	.185	.123	-1.322	320	218	-.222	.050	-.049	-.459	320	268	-.163	.051	-.022	-.407
320	135	-.390	.185	.165	-1.367	320	219	-.222	.055	-.010	-.495	320	269	-.176	.048	-.008	-.562
320	136	-.432	.192	.266	-1.567	320	220	-.236	.061	-.051	-.590	320	270	-.209	.069	.003	-.585
320	137	-.206	.073	-.006	-1.024	320	221	-.234	.059	-.022	-.494	320	271	-.203	.064	-.026	-.540
320	138	-.192	.076	.046	-.812	320	222	-.228	.045	-.097	-.454	320	272	-.186	.056	-.036	-.511
320	139	-.205	.089	.117	-.917	320	223	-.222	.047	-.069	-.410	320	273	-.162	.053	-.005	-.649
320	140	-.262	.137	.161	-1.148	320	224	-.221	.049	-.070	-.431	320	274	-.166	.056	.024	-.620
320	141	-.321	.150	.185	-1.820	320	225	-.230	.048	-.064	-.452	320	275	-.197	.071	-.005	-.558
320	142	-.353	.132	.226	-1.128	320	226	-.227	.057	-.026	-.526	320	276	-.183	.047	-.037	-.413
320	143	-.231	.066	-.051	-.747	320	227	-.230	.068	.034	-.617	320	277	-.174	.051	-.035	-.436
320	144	-.039	.062	.427	-.182	320	228	-.246	.073	-.060	-.639	320	301	-.341	.120	-.019	-.807
320	145	-.191	.051	-.026	-.473	320	229	-.247	.066	-.061	-.713	320	302	-.263	.077	-.049	-.738
320	146	-.181	.049	.013	-.473	320	230	-.242	.059	-.056	-.619	320	303	-.244	.075	-.021	-.678
320	147	-.171	.059	.082	-.626	320	231	-.237	.053	-.093	-.454	320	304	-.298	.107	.023	-.802
320	148	-.204	.091	.114	-.725	320	232	-.233	.054	-.089	-.489	320	305	-.243	.069	-.055	-.657
320	149	-.241	.117	.283	-.904	320	233	-.240	.053	-.089	-.477	320	306	-.252	.066	-.057	-.689
320	150	-.285	.124	.202	-1.019	320	234	-.239	.064	-.028	-.632	320	307	-.247	.075	-.004	-.651
320	151	-.181	.046	-.021	-.367	320	235	-.240	.078	-.033	-.664	320	308	-.234	.065	.008	-.534
320	152	-.171	.043	-.026	-.345	320	236	-.262	.095	-.058	-1.075	320	309	-.248	.128	.213	-.794
320	153	-.159	.037	-.039	-.331	320	237	-.247	.075	-.051	-.789	320	310	-.236	.134	.287	-.763
320	154	-.142	.060	.092	-.429	320	238	-.240	.067	-.044	-.763	320	311	-.258	.068	-.021	-.531

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
320	312	-.258	.070	.005	-.605
320	313	-.259	.072	-.025	-.558
320	314	-.263	.069	-.062	-.788
320	315	-.233	.063	-.011	-.644
320	316	-.239	.065	-.009	-.648
320	317	.180	.155	.770	-.229
320	318	-.233	.041	-.084	-.377
320	319	-.289	.132	.140	-.854
320	320	-.283	.171	.419	-.943
320	321	-.261	.079	-.043	-.603
320	322	-.261	.062	-.089	-.736
320	323	-.262	.078	-.060	-.836
320	324	-.273	.090	-.043	-1.058
320	325	-.245	.063	-.062	-.624
320	326	-.249	.056	-.056	-.474
320	327	-.255	.143	.219	-.886
320	328	-.277	.137	.233	-.896
320	329	-.287	.092	-.039	-.816
320	330	-.285	.093	.005	-.835
320	331	-.286	.094	-.034	-.885
320	332	-.294	.081	-.096	-.928
320	333	-.254	.067	-.076	-.726
320	334	-.261	.070	-.064	-.785
320	335	.094	.120	.542	-.300
320	336	-.244	.048	-.074	-.431
320	337	-.236	.124	.186	-.786
320	338	-.223	.136	.247	-.799
320	339	-.311	.118	-.053	-1.076
320	340	-.310	.097	-.087	-.916
320	341	-.304	.116	-.024	-1.041
320	342	-.314	.133	.204	-1.324
320	343	-.268	.092	-.058	-1.118
320	344	-.270	.073	-.074	-.813
320	345	-.206	.095	.061	-.711
320	346	-.186	.106	.177	-.720
320	347	-.300	.121	-.048	-.958
320	348	-.283	.105	-.027	-1.158
320	349	-.281	.110	.009	-1.051
320	350	-.283	.125	.075	-1.656
320	351	-.240	.085	-.027	-.728
320	352	-.249	.072	-.060	-.788
320	353	-.017	.074	.427	-.309
320	354	-.213	.062	.022	-.498
320	355	-.204	.070	-.006	-.638
320	356	-.189	.061	.130	-.500
320	357	-.260	.104	.004	-.914
320	358	-.255	.105	.046	-.890
320	359	-.246	.105	.004	-1.104
320	360	-.259	.089	.019	-.729
320	361	-.223	.086	-.024	-.716
320	362	-.232	.094	.003	-.969
320	363	-.209	.059	-.048	-.554
320	364	-.210	.047	-.084	-.431
320	365	-.234	.082	-.006	-.791
320	366	-.226	.078	-.033	-.732
320	367	-.220	.072	-.053	-.629
320	368	-.224	.056	-.062	-.559
320	369	-.208	.067	-.009	-.639
320	370	-.210	.068	-.033	-.665
320	371	-.066	.046	.113	-.278
320	372	-.185	.069	.051	-.543
320	373	-.186	.052	-.060	-.498
320	374	-.210	.075	-.024	-.629
320	375	-.205	.071	-.016	-.608
320	376	-.208	.077	-.004	-.729
320	377	-.214	.059	-.050	-.493
320	378	-.201	.061	-.022	-.502
320	379	-.201	.062	-.030	-.519
320	380	-.204	.067	-.020	-.637
320	401	-.207	.292	.923	-.888
320	402	-.338	.183	.513	-.958
320	403	-.338	.145	.341	-.968
320	404	-.184	.199	.643	-1.023
320	405	-.329	.111	.239	-.872
320	406	.213	.158	.848	-.207
320	407	.204	.136	.726	-.192
320	408	.164	.142	.798	-.195
320	409	.141	.137	.801	-.214
320	410	.141	.130	.716	-.231
320	411	-.001	.197	.662	-.629
320	412	.237	.166	.773	-.263
320	413	.345	.185	.940	-.152
320	414	.364	.189	.958	-.132
320	415	.340	.149	.832	-.045
320	416	.245	.153	.821	-.185
320	417	.096	.124	.628	-.274
320	418	-.249	.219	.577	-.916
320	419	.085	.210	.792	-.600
320	420	.165	.156	.748	-.369
320	421	.285	.166	.902	-.221
320	422	.326	.170	1.038	-.096
320	423	.310	.145	.896	-.040
320	424	.207	.149	.839	-.185
320	425	.045	.124	.532	-.306
320	426	-.278	.167	.368	-.884
320	427	-.033	.221	.740	-.848
320	428	.063	.148	.727	-.538
320	429	.165	.144	.779	-.275
320	430	.218	.137	.859	-.094
320	431	.226	.153	.878	-.093
320	432	.152	.148	.698	-.159
320	433	.017	.126	.511	-.311
320	434	-.260	.175	.306	-.921
320	435	-.034	.198	.650	-.838
320	436	-.014	.112	.609	-.339
320	437	.072	.106	.579	-.235
320	438	.093	.082	.532	-.118
320	439	.110	.100	.678	-.145
320	440	.065	.105	.611	-.238
320	441	-.030	.094	.487	-.294
320	442	-.227	.139	.279	-.904
320	443	-.077	.154	.517	-.833
320	444	-.047	.076	.331	-.320
320	445	.020	.071	.417	-.261
320	446	.039	.056	.321	-.145
320	447	.052	.069	.424	-.140
320	448	.017	.074	.410	-.216
320	449	-.052	.073	.391	-.426
320	450	-.179	.114	.220	-.735
320	451	-.058	.110	.432	-.644
320	452	-.029	.069	.249	-.339
320	453	.023	.063	.327	-.233
320	454	.034	.051	.265	-.234
320	455	.032	.055	.274	-.203
320	456	-.013	.053	.326	-.260
320	457	-.075	.054	.212	-.292
320	458	-.171	.073	.218	-.492
320	459	-.087	.086	.324	-.414
320	460	-.012	.063	.271	-.281
320	461	.027	.060	.341	-.231
320	462	.042	.051	.277	-.141
320	463	.027	.043	.266	-.200
320	464	-.023	.043	.167	-.207
320	465	-.094	.044	.069	-.333
320	466	-.188	.061	-.009	-.565
320	467	-.170	.065	.112	-.417
320	468	.019	.050	.237	-.201
320	469	.053	.047	.328	-.081
320	470	.045	.053	.284	-.105
320	471	.023	.050	.279	-.153
320	472	-.019	.052	.266	-.181
320	473	-.008	.039	.192	-.131
320	474	.057	.056	.429	-.093
320	475	.034	.055	.410	-.121
320	476	.019	.050	.377	-.115
320	477	-.073	.037	.140	-.183
320	801	-.242	.069	-.084	-.537
320	802	-.213	.062	-.044	-.482
320	803	-.194	.060	-.009	-.708
320	804	.049	.061	.394	-.178

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
320	805	.057	.048	.369	-.060	330	127	-.290	.225	.323	-1.112	330	211	-.176	.052	-.014	-.421
320	806	-.031	.060	.321	-.191	330	128	-.384	.217	.430	-1.406	330	212	-.194	.058	-.020	-.445
320	807	-.214	.068	-.042	-.624	330	129	-.216	.052	-.072	-.474	330	213	-.195	.056	-.039	-.470
320	808	-.222	.071	-.043	-.587	330	130	.227	.171	.978	-.201	330	214	-.192	.045	-.045	-.381
320	809	-.217	.066	-.060	-.563	330	131	-.181	.045	-.027	-.426	330	215	-.186	.046	-.035	-.408
320	810	-.215	.074	-.046	-.597	330	132	-.162	.054	.024	-.582	330	216	-.184	.046	-.047	-.372
320	901	-.217	.083	.151	-.649	330	133	-.148	.074	.130	-.710	330	217	-.183	.048	-.044	-.374
320	902	-.238	.069	-.008	-.733	330	134	-.173	.125	.226	-1.084	330	218	-.189	.043	-.028	-.388
320	903	-.233	.074	.073	-.600	330	135	-.265	.156	.257	-.974	330	219	-.184	.047	-.012	-.391
320	904	-.311	.075	-.081	-.642	330	136	-.339	.170	.348	-1.090	330	220	-.207	.053	-.040	-.506
320	905	-.323	.098	-.019	-.797	330	137	-.180	.055	-.008	-.481	330	221	-.206	.050	-.068	-.544
320	906	-.329	.103	.050	-.779	330	138	-.161	.049	-.006	-.495	330	222	-.205	.041	-.083	-.395
320	907	-.257	.080	.017	-.637	330	139	-.144	.044	.041	-.383	330	223	-.195	.041	-.065	-.335
320	908	-.363	.094	-.067	-.789	330	140	-.172	.073	.088	-.759	330	224	-.195	.041	-.072	-.355
320	909	-.324	.125	-.009	-.859	330	141	-.236	.110	.105	-.912	330	225	-.199	.043	-.055	-.356
320	910	-.337	.097	-.008	-.738	330	142	-.276	.107	.318	-.853	330	226	-.191	.047	-.030	-.401
320	911	-.326	.099	.012	-.759	330	143	-.205	.070	-.042	-.980	330	227	-.192	.049	-.016	-.579
320	912	-.379	.095	-.086	-.742	330	144	.051	.065	.405	-.218	330	228	-.231	.075	-.034	-.705
320	913	-.336	.095	-.086	-.678	330	145	-.177	.048	-.032	-.451	330	229	-.212	.058	-.053	-.542
320	914	-.302	.095	.071	-.748	330	146	-.161	.043	-.008	-.345	330	230	-.203	.054	-.050	-.472
320	915	-.368	.103	-.084	-.724	330	147	-.148	.043	.047	-.329	330	231	-.201	.051	-.055	-.416
320	916	-.454	.113	-.143	-.953	330	148	-.133	.050	.085	-.511	330	232	-.198	.049	-.063	-.367
320	917	-.374	.139	.243	-.864	330	149	-.178	.086	.162	-.645	330	233	-.204	.050	-.070	-.472
320	918	-.358	.102	-.042	-.768	330	150	-.218	.099	.196	-.713	330	234	-.195	.053	-.050	-.556
330	101	-.315	.121	-.047	-.831	330	151	-.158	.045	-.020	-.385	330	235	-.193	.055	-.047	-.584
330	102	-.163	.072	.102	-.623	330	152	-.149	.043	.023	-.336	330	236	-.240	.094	-.003	-1.045
330	103	-.315	.207	.463	-.994	330	153	-.134	.037	-.004	-.298	330	237	-.223	.073	.014	-.599
330	104	-.026	.077	.258	-.428	330	154	-.116	.058	.165	-.343	330	238	-.210	.066	-.022	-.556
330	105	-.025	.102	.312	-.608	330	155	-.119	.114	.320	-.528	330	239	-.212	.062	-.028	-.521
330	106	-.224	.091	.094	-.810	330	156	-.137	.125	.397	-.606	330	240	-.213	.059	-.053	-.458
330	107	-.138	.158	.232	-.851	330	157	-.190	.056	-.067	-.471	330	241	-.198	.051	-.063	-.443
330	108	-.383	.204	.383	-1.311	330	158	-.016	.056	.301	-.209	330	242	-.190	.057	-.027	-.701
330	109	-.131	.042	.006	-.569	330	159	-.113	.042	.037	-.301	330	243	-.187	.060	-.018	-.821
330	110	-.096	.060	.135	-.677	330	160	-.112	.045	.083	-.290	330	244	-.182	.079	.004	-.695
330	111	-.069	.099	.246	-.811	330	161	-.087	.053	.127	-.361	330	245	-.187	.071	-.033	-.574
330	112	-.121	.213	.329	-1.337	330	162	-.104	.114	.350	-.533	330	246	-.185	.068	-.012	-.635
330	113	-.322	.237	.290	-1.112	330	163	-.177	.059	-.030	-.518	330	247	-.199	.064	-.050	-.577
330	114	-.375	.203	.432	-1.195	330	164	-.114	.049	.071	-.281	330	248	-.216	.067	-.068	-.659
330	115	-.200	.050	-.047	-.380	330	165	-.105	.055	.184	-.303	330	249	-.214	.066	-.058	-.567
330	116	.397	.187	1.084	-.131	330	166	-.104	.097	.473	-.381	330	250	-.203	.069	-.040	-.767
330	117	-.164	.047	.011	-.564	330	201	-.210	.062	-.015	-.510	330	251	-.200	.073	.015	-.711
330	118	-.135	.065	.091	-.682	330	202	-.202	.065	.057	-.571	330	252	-.138	.052	.014	-.439
330	119	-.111	.116	.153	-.954	330	203	-.203	.062	.002	-.445	330	253	-.138	.050	.007	-.378
330	120	-.157	.187	.222	-.929	330	204	-.240	.104	.021	-.813	330	254	-.137	.047	.006	-.350
330	121	-.313	.264	.409	-1.306	330	205	-.289	.111	-.040	-.793	330	255	-.158	.058	.016	-.438
330	122	-.371	.226	.485	-1.401	330	206	-.188	.059	-.009	-.421	330	256	-.202	.070	-.024	-.568
330	123	-.169	.045	-.022	-.622	330	207	-.194	.048	-.043	-.451	330	257	-.190	.055	-.060	-.470
330	124	-.147	.057	.060	-.561	330	208	-.195	.045	-.033	-.419	330	258	-.180	.055	-.055	-.523
330	125	-.131	.092	.113	-.794	330	209	-.184	.054	-.005	-.425	330	259	-.174	.059	-.040	-.764
330	126	-.168	.189	.260	-1.238	330	210	-.186	.053	-.030	-.435	330	260	-.126	.040	-.005	-.346

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
330	261	-.129	.041	-.011	-.371	330	334	-.248	.071	-.077	-.631	330	404	-.275	.143	.337	-.856
330	262	-.133	.042	.035	-.337	330	335	-.000	.097	.447	-.327	330	405	-.325	.114	.309	-.844
330	263	-.137	.051	.047	-.544	330	336	-.226	.046	-.086	-.423	330	406	.241	.150	.795	-.229
330	264	-.175	.061	.028	-.461	330	337	-.292	.142	.125	-.927	330	407	.223	.132	.740	-.200
330	265	-.182	.052	-.043	-.455	330	338	-.275	.155	.207	-.939	330	408	.163	.129	.709	-.207
330	266	-.174	.054	-.037	-.548	330	339	-.300	.136	.088	-1.202	330	409	.131	.121	.636	-.226
330	267	-.166	.052	-.030	-.513	330	340	-.314	.111	-.032	-1.146	330	410	.135	.121	.593	-.213
330	268	-.132	.041	.031	-.338	330	341	-.307	.135	-.005	-1.304	330	411	-.189	.160	.524	-.747
330	269	-.143	.045	-.018	-.398	330	342	-.315	.154	.016	-1.269	330	412	.314	.168	1.021	-.150
330	270	-.179	.061	-.022	-.505	330	343	-.252	.092	-.022	-.723	330	413	.370	.175	1.115	-.121
330	271	-.177	.051	-.020	-.396	330	344	-.268	.078	-.106	-.709	330	414	.346	.174	1.048	-.112
330	272	-.161	.049	-.022	-.434	330	345	-.243	.115	.055	-.996	330	415	.289	.130	.737	-.043
330	273	-.131	.040	.005	-.362	330	346	-.223	.124	.197	-1.068	330	416	.164	.126	.786	-.150
330	274	-.138	.043	.039	-.376	330	347	-.284	.136	.013	-1.059	330	417	.013	.095	.438	-.266
330	275	-.168	.063	.026	-.501	330	348	-.266	.123	.024	-1.105	330	418	-.375	.161	.350	-.888
330	276	-.163	.043	-.055	-.381	330	349	-.247	.120	.060	-1.331	330	419	-.098	.196	.691	-.674
330	277	-.153	.046	-.033	-.362	330	350	-.249	.131	.156	-1.106	330	420	.242	.178	.888	-.302
330	301	-.358	.114	-.037	-.775	330	351	-.198	.076	.018	-.609	330	421	.324	.184	.941	-.123
330	302	-.256	.083	-.012	-.660	330	352	-.218	.075	-.064	-.841	330	422	.331	.179	.971	-.124
330	303	-.244	.082	.063	-.556	330	353	-.047	.061	.327	-.302	330	423	.268	.128	.784	-.055
330	304	-.370	.125	-.077	-.868	330	354	-.183	.059	-.008	-.469	330	424	.132	.120	.777	-.216
330	305	-.240	.077	.064	-.643	330	355	-.195	.073	.077	-.660	330	425	-.032	.092	.478	-.286
330	306	-.246	.073	-.052	-.699	330	356	-.200	.065	.088	-.536	330	426	-.394	.147	.211	-.882
330	307	-.241	.083	.028	-.654	330	357	-.201	.086	-.005	-.749	330	427	-.202	.216	.624	-.886
330	308	-.226	.070	-.001	-.572	330	358	-.194	.086	.006	-.813	330	428	.150	.178	.929	-.527
330	309	-.369	.130	.093	-.871	330	359	-.188	.080	.032	-.670	330	429	.209	.171	.889	-.194
330	310	-.363	.126	.115	-.871	330	360	-.191	.072	-.042	-.787	330	430	.207	.130	.683	-.168
330	311	-.243	.073	-.020	-.572	330	361	-.155	.061	.040	-.492	330	431	.174	.122	.754	-.125
330	312	-.238	.075	.018	-.595	330	362	-.162	.067	.004	-.801	330	432	.067	.100	.514	-.209
330	313	-.239	.076	-.015	-.601	330	363	-.170	.053	-.027	-.489	330	433	-.067	.087	.335	-.363
330	314	-.246	.071	-.059	-.733	330	364	-.184	.047	-.052	-.386	330	434	-.364	.159	.280	-1.102
330	315	-.214	.056	-.017	-.449	330	365	-.166	.055	-.027	-.542	330	435	-.191	.212	.671	-.869
330	316	-.217	.059	-.025	-.474	330	366	-.160	.052	-.008	-.443	330	436	.033	.132	.683	-.326
330	317	.069	.123	.607	-.327	330	367	-.163	.053	.004	-.465	330	437	.085	.124	.720	-.267
330	318	-.210	.043	-.064	-.416	330	368	-.168	.046	-.057	-.627	330	438	.095	.090	.512	-.212
330	319	-.405	.132	.032	-.883	330	369	-.154	.047	-.032	-.422	330	439	.079	.081	.544	-.202
330	320	-.372	.163	.192	-.949	330	370	-.157	.051	-.037	-.572	330	440	.007	.069	.452	-.221
330	321	-.249	.082	.098	-.693	330	371	-.066	.042	.094	-.271	330	441	-.092	.076	.303	-.379
330	322	-.250	.068	-.042	-.721	330	372	-.134	.055	.124	-.477	330	442	-.295	.139	.224	-.799
330	323	-.255	.081	.004	-.768	330	373	-.149	.041	-.048	-.364	330	443	-.155	.162	.559	-.781
330	324	-.264	.100	.061	-1.536	330	374	-.151	.048	-.020	-.373	330	444	-.013	.086	.376	-.505
330	325	-.229	.059	-.036	-.613	330	375	-.152	.050	-.028	-.421	330	445	.036	.081	.401	-.384
330	326	-.231	.059	-.062	-.722	330	376	-.155	.055	-.021	-.493	330	446	.044	.060	.375	-.180
330	327	-.357	.154	.050	-.937	330	377	-.145	.045	-.038	-.540	330	447	.035	.060	.372	-.190
330	328	-.338	.142	.189	-.927	330	378	-.145	.052	-.022	-.590	330	448	-.014	.059	.426	-.286
330	329	-.275	.094	.016	-.777	330	379	-.147	.056	-.019	-.669	330	449	-.082	.064	.368	-.426
330	330	-.270	.098	.018	-.755	330	380	-.148	.057	.008	-.638	330	450	-.209	.110	.236	-.728
330	331	-.274	.103	-.022	-1.052	330	401	-.161	.310	.967	-.983	330	451	-.096	.109	.282	-.662
330	332	-.296	.098	-.044	-1.321	330	402	-.337	.196	.544	-1.005	330	452	-.018	.063	.273	-.257
330	333	-.244	.067	-.072	-.584	330	403	-.337	.130	.285	-.855	330	453	.023	.061	.366	-.220

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
330	454	.045	.054	.321	-.141	330	917	-.369	.134	.074	-.866	340	149	-.174	.072	.087	-.631
330	455	.035	.055	.304	-.185	330	918	-.364	.109	-.043	-.805	340	150	-.194	.086	.171	-.606
330	456	-.017	.046	.199	-.214	340	101	-.225	.093	.004	-.772	340	151	-.128	.040	.007	-.301
330	457	-.079	.047	.106	-.295	340	102	-.136	.074	.140	-.535	340	152	-.122	.040	.042	-.296
330	458	-.176	.076	.128	-.608	340	103	-.043	.220	.662	-.782	340	153	-.119	.035	-.013	-.249
330	459	-.107	.084	.292	-.489	340	104	.041	.080	.379	-.223	340	154	-.103	.052	.102	-.371
330	460	-.012	.059	.290	-.278	340	105	.060	.096	.485	-.318	340	155	-.105	.098	.483	-.531
330	461	.023	.058	.319	-.166	340	106	-.165	.080	.222	-.629	340	156	-.114	.113	.645	-.654
330	462	.040	.050	.402	-.121	340	107	-.015	.092	.343	-.544	340	157	-.148	.040	-.048	-.444
330	463	.038	.050	.247	-.113	340	108	-.127	.205	.554	-1.156	340	158	-.001	.053	.309	-.284
330	464	-.018	.041	.220	-.147	340	109	-.083	.042	.177	-.346	340	159	-.099	.038	.068	-.259
330	465	-.072	.041	.057	-.257	340	110	-.036	.069	.345	-.391	340	160	-.097	.042	.074	-.299
330	466	-.166	.056	.024	-.515	340	111	.010	.079	.473	-.463	340	161	-.085	.050	.152	-.316
330	467	-.154	.058	.096	-.476	340	112	.049	.117	.581	-.827	340	162	-.093	.092	.365	-.478
330	468	.016	.050	.214	-.150	340	113	-.024	.209	.535	-.797	340	163	-.130	.043	.011	-.340
330	469	.051	.049	.274	-.084	340	114	-.129	.228	.702	-.938	340	164	-.097	.042	.093	-.263
330	470	.045	.057	.279	-.121	340	115	-.166	.048	-.035	-.342	340	165	-.094	.049	.132	-.274
330	471	.024	.053	.257	-.150	340	116	.397	.182	1.011	-.073	340	166	-.078	.093	.493	-.368
330	472	-.008	.053	.234	-.176	340	117	-.116	.036	.032	-.251	340	201	-.182	.058	.000	-.449
330	473	-.003	.041	.223	-.130	340	118	-.077	.047	.140	-.253	340	202	-.176	.062	.021	-.469
330	474	.057	.058	.397	-.091	340	119	-.032	.066	.233	-.426	340	203	-.168	.060	.040	-.448
330	475	.038	.058	.337	-.126	340	120	-.006	.101	.309	-.566	340	204	-.172	.085	.062	-.838
330	476	.024	.052	.339	-.143	340	121	-.078	.212	.511	-.869	340	205	-.232	.101	-.007	-.707
330	477	-.062	.032	.055	-.220	340	122	-.168	.207	.667	-.966	340	206	-.168	.062	.026	-.508
330	801	-.195	.049	-.060	-.509	340	123	-.131	.038	.027	-.434	340	207	-.164	.045	.004	-.400
330	802	-.176	.055	-.020	-.530	340	124	-.101	.045	.112	-.343	340	208	-.166	.048	-.002	-.498
330	803	-.150	.048	.004	-.532	340	125	-.075	.059	.178	-.507	340	209	-.156	.056	.060	-.408
330	804	.057	.058	.321	-.089	340	126	-.057	.102	.295	-.649	340	210	-.150	.045	.008	-.318
330	805	.051	.045	.247	-.081	340	127	-.109	.163	.545	-.734	340	211	-.142	.046	.008	-.305
330	806	-.043	.041	.132	-.189	340	128	-.199	.193	.792	-.884	340	212	-.162	.048	-.012	-.386
330	807	-.153	.050	-.000	-.377	340	129	-.175	.047	-.028	-.389	340	213	-.162	.048	.007	-.391
330	808	-.150	.049	.013	-.366	340	130	.205	.166	.948	-.169	340	214	-.164	.047	-.020	-.386
330	809	-.149	.042	-.043	-.323	340	131	-.145	.045	-.003	-.459	340	215	-.155	.050	-.002	-.400
330	810	-.151	.049	-.015	-.358	340	132	-.121	.048	.120	-.412	340	216	-.152	.050	-.007	-.364
330	901	-.187	.072	.071	-.516	340	133	-.106	.056	.144	-.382	340	217	-.149	.051	-.009	-.333
330	902	-.220	.068	.013	-.573	340	134	-.103	.082	.271	-.688	340	218	-.150	.045	-.012	-.359
330	903	-.209	.071	.041	-.491	340	135	-.159	.128	.367	-.727	340	219	-.147	.048	-.005	-.364
330	904	-.289	.079	.040	-.584	340	136	-.230	.161	.534	-1.014	340	220	-.177	.058	-.002	-.492
330	905	-.272	.087	-.005	-.617	340	137	-.162	.055	-.011	-.438	340	221	-.174	.055	-.000	-.500
330	906	-.322	.101	.039	-.724	340	138	-.137	.047	.009	-.383	340	222	-.184	.046	-.038	-.599
330	907	-.242	.085	.105	-.598	340	139	-.127	.043	.054	-.334	340	223	-.176	.044	-.038	-.421
330	908	-.384	.110	-.062	-.866	340	140	-.139	.065	.097	-.534	340	224	-.170	.043	-.031	-.403
330	909	-.230	.091	.071	-.753	340	141	-.186	.101	.267	-.698	340	225	-.160	.038	-.040	-.301
330	910	-.349	.105	-.058	-.857	340	142	-.242	.113	.255	-.809	340	226	-.154	.041	-.023	-.308
330	911	-.311	.099	.005	-.714	340	143	-.208	.091	-.030	-1.053	340	227	-.152	.042	-.024	-.307
330	912	-.382	.099	-.115	-.803	340	144	.068	.067	.470	-.113	340	228	-.199	.070	-.032	-.597
330	913	-.319	.097	-.020	-.928	340	145	-.147	.047	-.021	-.427	340	229	-.203	.065	-.028	-.527
330	914	-.292	.097	.014	-.786	340	146	-.136	.042	.031	-.364	340	230	-.192	.059	-.015	-.516
330	915	-.361	.109	-.091	-.840	340	147	-.128	.044	.028	-.325	340	231	-.182	.053	-.014	-.440
330	916	-.437	.114	-.076	-1.151	340	148	-.129	.053	.047	-.460	340	232	-.174	.050	-.010	-.447

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
340	233	-.175	.048	-.055	-.491	340	306	-.207	.067	-.034	-.612	340	356	-.183	.056	.023	-.526
340	234	-.168	.051	-.041	-.508	340	307	-.205	.074	.045	-.603	340	357	-.151	.074	.020	-.988
340	235	-.163	.051	-.009	-.494	340	308	-.190	.061	.030	-.494	340	358	-.141	.069	.015	-1.122
340	236	-.219	.088	.021	-.700	340	309	-.336	.105	-.082	-.832	340	359	-.141	.062	.015	-.615
340	237	-.202	.070	-.040	-.554	340	310	-.335	.092	-.006	-.736	340	360	-.146	.056	-.004	-.521
340	238	-.197	.064	-.031	-.521	340	311	-.207	.078	.075	-.643	340	361	-.122	.044	.027	-.317
340	239	-.200	.063	-.049	-.514	340	312	-.201	.079	.080	-.652	340	362	-.125	.045	.020	-.378
340	240	-.199	.061	-.053	-.466	340	313	-.203	.074	.057	-.606	340	363	-.151	.049	.010	-.450
340	241	-.194	.060	-.048	-.622	340	314	-.217	.067	-.036	-.582	340	364	-.164	.043	-.031	-.404
340	242	-.185	.062	-.038	-.577	340	315	-.190	.055	-.030	-.420	340	365	-.133	.046	.020	-.447
340	243	-.178	.063	-.014	-.837	340	316	-.192	.057	-.026	-.470	340	366	-.126	.043	.025	-.405
340	244	-.156	.073	-.005	-.780	340	317	-.019	.091	.385	-.301	340	367	-.128	.043	.024	-.410
340	245	-.151	.066	.010	-.664	340	318	-.178	.042	-.053	-.362	340	368	-.139	.039	-.043	-.481
340	246	-.159	.064	.028	-.549	340	319	-.349	.098	-.108	-.800	340	369	-.128	.038	-.015	-.334
340	247	-.178	.069	.018	-.741	340	320	-.365	.136	.145	-1.000	340	370	-.129	.040	-.011	-.350
340	248	-.200	.075	.012	-.633	340	321	-.229	.093	.147	-.769	340	371	-.052	.039	.097	-.226
340	249	-.224	.088	-.030	-.760	340	322	-.215	.070	-.026	-.605	340	372	-.104	.044	.179	-.289
340	250	-.217	.094	-.005	-.829	340	323	-.223	.083	.029	-.731	340	373	-.119	.036	.006	-.260
340	251	-.199	.083	-.019	-.762	340	324	-.235	.102	.003	-.815	340	374	-.115	.041	.034	-.285
340	252	-.108	.043	.043	-.309	340	325	-.192	.056	-.035	-.618	340	375	-.117	.042	.040	-.299
340	253	-.111	.040	.005	-.471	340	326	-.209	.061	-.058	-.483	340	376	-.120	.044	.060	-.300
340	254	-.114	.043	.028	-.421	340	327	-.334	.119	-.033	-.864	340	377	-.117	.035	-.016	-.338
340	255	-.126	.047	.052	-.438	340	328	-.345	.102	-.021	-.832	340	378	-.116	.042	.010	-.379
340	256	-.152	.057	-.017	-.488	340	329	-.275	.109	.047	-1.040	340	379	-.117	.043	.011	-.425
340	257	-.182	.069	-.040	-.587	340	330	-.272	.113	.058	-.873	340	380	-.118	.045	.037	-.421
340	258	-.174	.071	-.036	-.652	340	331	-.274	.114	.055	-.797	340	401	.011	.299	1.012	-1.090
340	259	-.170	.076	-.029	-.864	340	332	-.279	.102	-.034	-1.144	340	402	-.271	.173	.509	-.893
340	260	-.105	.038	.007	-.297	340	333	-.214	.065	-.025	-.573	340	403	-.278	.125	.305	-.842
340	261	-.111	.033	-.020	-.268	340	334	-.220	.069	-.023	-.606	340	404	-.247	.122	.211	-.763
340	262	-.108	.042	.016	-.323	340	335	-.057	.070	.328	-.337	340	405	-.282	.105	.177	-.818
340	263	-.111	.047	.060	-.380	340	336	-.205	.049	-.076	-.397	340	406	.261	.153	.818	-.185
340	264	-.130	.048	.029	-.481	340	337	-.321	.133	-.000	-.927	340	407	.207	.123	.689	-.201
340	265	-.144	.040	-.025	-.308	340	338	-.312	.142	.099	-.976	340	408	.146	.118	.628	-.220
340	266	-.137	.041	-.026	-.333	340	339	-.309	.152	.095	-1.424	340	409	.109	.108	.555	-.259
340	267	-.132	.040	-.019	-.302	340	340	-.285	.114	-.019	-1.040	340	410	.137	.119	.599	-.241
340	268	-.107	.035	.004	-.341	340	341	-.281	.139	.022	-1.106	340	411	-.283	.107	.270	-.708
340	269	-.118	.035	.015	-.308	340	342	-.287	.165	.130	-1.881	340	412	.365	.182	1.023	-.137
340	270	-.132	.053	.077	-.462	340	343	-.214	.088	-.011	-.823	340	413	.374	.180	1.034	-.117
340	271	-.138	.050	.030	-.450	340	344	-.223	.080	-.068	-.696	340	414	.301	.161	.943	-.241
340	272	-.132	.046	-.003	-.406	340	345	-.231	.105	-.008	-.940	340	415	.238	.113	.744	-.045
340	273	-.108	.033	.022	-.217	340	346	-.218	.107	.090	-.906	340	416	.090	.101	.638	-.194
340	274	-.115	.034	.025	-.233	340	347	-.226	.136	.029	-1.424	340	417	-.027	.073	.316	-.300
340	275	-.126	.043	.014	-.373	340	348	-.225	.137	.029	-1.330	340	418	-.348	.116	.113	-.874
340	276	-.124	.036	-.018	-.284	340	349	-.206	.119	.005	-1.166	340	419	-.251	.125	.315	-.578
340	277	-.118	.040	-.001	-.313	340	350	-.206	.130	.044	-1.002	340	420	.293	.184	1.013	-.154
340	301	-.306	.094	-.056	-.758	340	351	-.161	.077	.012	-.691	340	421	.324	.182	1.022	-.192
340	302	-.223	.074	.017	-.639	340	352	-.167	.057	-.024	-.602	340	422	.281	.163	.851	-.133
340	303	-.220	.081	.053	-.698	340	353	-.059	.049	.135	-.327	340	423	.220	.112	.620	-.055
340	304	-.339	.101	-.092	-.755	340	354	-.153	.049	-.021	-.431	340	424	.061	.093	.475	-.189
340	305	-.206	.075	.054	-.551	340	355	-.184	.070	.005	-.526	340	425	-.069	.072	.202	-.343

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
340	426	-.358	.111	.063	-.817	340	476	.030	.054	.340	-.128	350	121	.010	.145	.459	-.799
340	427	-.280	.148	.563	-.770	340	477	-.046	.031	.097	-.146	350	122	-.074	.178	.542	-1.071
340	428	.184	.174	.998	-.339	340	801	-.164	.045	-.038	-.367	350	123	-.098	.045	.105	-.319
340	429	.213	.169	1.023	-.314	340	802	-.145	.049	-.008	-.342	350	124	-.069	.051	.203	-.283
340	430	.174	.125	.756	-.161	340	803	-.121	.043	.028	-.354	350	125	-.042	.058	.337	-.428
340	431	.132	.110	.623	-.197	340	804	.059	.069	.381	-.156	350	126	-.017	.077	.462	-.609
340	432	.017	.078	.410	-.252	340	805	.066	.051	.374	-.114	350	127	-.027	.130	.524	-.743
340	433	-.092	.064	.233	-.364	340	806	-.024	.042	.203	-.159	350	128	-.110	.188	.682	-.914
340	434	-.338	.111	.184	-.802	340	807	-.124	.045	.021	-.335	350	129	-.142	.051	.000	-.525
340	435	-.243	.155	.520	-.811	340	808	-.120	.044	.018	-.286	350	130	-.205	.164	.904	-.129
340	436	.040	.119	.639	-.302	340	809	-.123	.038	-.011	-.316	350	131	-.107	.039	.017	-.277
340	437	.079	.112	.660	-.289	340	810	-.124	.045	.010	-.352	350	132	-.085	.045	.096	-.243
340	438	.088	.098	.583	-.181	340	901	-.138	.067	.105	-.415	350	133	-.065	.053	.152	-.260
340	439	.067	.090	.465	-.144	340	902	-.172	.061	.006	-.463	350	134	-.054	.071	.259	-.505
340	440	-.016	.065	.295	-.228	340	903	-.190	.074	.055	-.544	350	135	-.081	.098	.277	-.643
340	441	-.107	.062	.181	-.383	340	904	-.214	.072	.111	-.493	350	136	-.130	.134	.371	-.831
340	442	-.299	.124	.068	-.980	340	905	-.217	.076	.021	-.573	350	137	-.121	.047	.041	-.409
340	443	-.186	.149	.276	-.921	340	906	-.261	.083	-.033	-.584	350	138	-.101	.043	.064	-.312
340	444	.004	.081	.728	-.247	340	907	-.203	.077	.019	-.572	350	139	-.093	.044	.071	-.241
340	445	.049	.081	.691	-.187	340	908	-.347	.106	-.069	-.832	350	140	-.097	.063	.161	-.390
340	446	.058	.060	.305	-.161	340	909	-.149	.078	.125	-.544	350	141	-.131	.095	.347	-.605
340	447	.042	.059	.356	-.194	340	910	-.309	.099	.097	-.766	350	142	-.180	.120	.364	-.919
340	448	-.017	.049	.213	-.237	340	911	-.258	.089	.129	-.676	350	143	-.168	.076	.012	-.731
340	449	-.083	.050	.084	-.312	340	912	-.343	.083	-.112	-.697	350	144	.072	.070	.629	-.167
340	450	-.213	.097	.142	-.814	340	913	-.279	.082	-.027	-.652	350	145	-.117	.048	.091	-.325
340	451	-.111	.095	.306	-.499	340	914	-.248	.085	.081	-.607	350	146	-.105	.043	.116	-.298
340	452	-.029	.061	.251	-.264	340	915	-.333	.094	-.080	-.682	350	147	-.104	.046	.048	-.338
340	453	.017	.065	.332	-.232	340	916	-.380	.125	.277	-.973	350	148	-.128	.058	.076	-.438
340	454	.052	.060	.342	-.132	340	917	-.305	.119	.152	-.886	350	149	-.145	.058	.044	-.432
340	455	.051	.064	.336	-.154	340	918	-.295	.093	-.050	-.757	350	150	-.151	.066	.083	-.511
340	456	-.007	.046	.174	-.170	350	101	-.212	.101	.210	-.841	350	151	-.096	.036	.027	-.265
340	457	-.069	.042	.127	-.272	350	102	-.092	.095	.345	-.472	350	152	-.093	.037	.029	-.251
340	458	-.174	.062	.034	-.689	350	103	.083	.209	.785	-.958	350	153	-.093	.035	.007	-.299
340	459	-.114	.071	.153	-.438	350	104	.061	.106	.516	-.407	350	154	-.095	.049	.066	-.340
340	460	-.026	.053	.184	-.216	350	105	.081	.122	.587	-.396	350	155	-.100	.072	.215	-.484
340	461	.007	.053	.257	-.201	350	106	-.097	.123	.466	-.694	350	156	-.102	.077	.285	-.411
340	462	.035	.056	.270	-.151	350	107	.031	.126	.783	-.621	350	157	-.101	.032	.000	-.221
340	463	.041	.051	.284	-.105	350	108	.031	.214	.914	-.936	350	158	-.010	.049	.226	-.182
340	464	-.001	.049	.184	-.177	350	109	-.053	.052	.259	-.324	350	159	-.080	.034	.032	-.240
340	465	-.056	.037	.078	-.195	350	110	-.007	.074	.451	-.350	350	160	-.081	.038	.062	-.251
340	466	-.162	.060	.044	-.487	350	111	.038	.092	.624	-.332	350	161	-.082	.046	.078	-.312
340	467	-.132	.057	.151	-.409	350	112	.080	.112	.732	-.818	350	162	-.090	.075	.269	-.370
340	468	.004	.047	.205	-.130	350	113	.096	.144	.634	-.961	350	163	-.092	.036	.027	-.334
340	469	.038	.052	.337	-.107	350	114	.023	.212	.940	-.884	350	164	-.081	.038	.083	-.256
340	470	.044	.062	.452	-.176	350	115	-.131	.055	.094	-.486	350	165	-.090	.043	.149	-.307
340	471	.031	.058	.408	-.189	350	116	.317	.182	1.184	-.157	350	166	-.085	.071	.299	-.383
340	472	.004	.056	.338	-.192	350	117	-.087	.046	.156	-.412	350	201	-.145	.059	.055	-.413
340	473	-.012	.041	.174	-.148	350	118	-.048	.057	.346	-.300	350	202	-.152	.068	.051	-.472
340	474	.047	.061	.403	-.110	350	119	.007	.068	.472	-.409	350	203	-.143	.067	.055	-.475
340	475	.045	.062	.420	-.110	350	120	.024	.067	.308	-.407	350	204	-.147	.079	.075	-.566

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
350	205	-.208	.090	.018	-.667	350	255	-.108	.050	.106	-.422	350	328	-.287	.085	-.053	-.847
350	206	-.130	.058	.089	-.406	350	256	-.131	.062	.018	-.431	350	329	-.233	.107	.104	-.887
350	207	-.132	.050	.033	-.527	350	257	-.143	.067	.004	-.564	350	330	-.229	.110	.060	-1.111
350	208	-.135	.050	.030	-.395	350	258	-.143	.076	.003	-.601	350	331	-.234	.111	.031	-1.234
350	209	-.127	.060	.063	-.410	350	259	-.142	.084	.016	-.686	350	332	-.243	.104	-.043	-1.072
350	210	-.126	.055	.028	-.470	350	260	-.076	.052	.063	-.683	350	333	-.178	.068	-.021	-.545
350	211	-.119	.056	.048	-.363	350	261	-.075	.039	.040	-.322	350	334	-.183	.072	-.024	-.556
350	212	-.131	.054	.040	-.390	350	262	-.092	.037	.044	-.314	350	335	-.067	.061	.192	-.328
350	213	-.131	.055	.044	-.402	350	263	-.094	.038	.030	-.335	350	336	-.165	.044	-.024	-.371
350	214	-.134	.051	.001	-.440	350	264	-.090	.043	.046	-.315	350	337	-.267	.107	-.026	-.887
350	215	-.132	.054	.026	-.469	350	265	-.101	.039	.008	-.320	350	338	-.260	.112	.002	-.859
350	216	-.128	.052	.031	-.434	350	266	-.099	.040	.011	-.325	350	339	-.260	.150	.083	-1.442
350	217	-.126	.053	.037	-.355	350	267	-.093	.040	.014	-.315	350	340	-.261	.121	.026	-1.308
350	218	-.127	.047	.006	-.379	350	268	-.070	.034	.039	-.212	350	341	-.254	.134	.047	-.980
350	219	-.125	.051	.023	-.394	350	269	-.081	.035	.035	-.307	350	342	-.258	.149	.053	-1.152
350	220	-.148	.056	.019	-.402	350	270	-.094	.047	.066	-.328	350	343	-.182	.078	-.004	-.544
350	221	-.145	.053	.015	-.412	350	271	-.095	.047	.048	-.347	350	344	-.187	.069	-.026	-.576
350	222	-.147	.049	.023	-.364	350	272	-.088	.043	.051	-.303	350	345	-.201	.084	.014	-.781
350	223	-.143	.050	.016	-.348	350	273	-.086	.035	.030	-.252	350	346	-.189	.084	.034	-.787
350	224	-.138	.051	.016	-.373	350	274	-.092	.035	.022	-.291	350	347	-.180	.109	.048	-1.210
350	225	-.136	.051	.006	-.445	350	275	-.096	.036	.025	-.265	350	348	-.170	.103	.130	-1.008
350	226	-.133	.054	.038	-.490	350	276	-.097	.032	.000	-.291	350	349	-.163	.095	.049	-1.119
350	227	-.129	.056	.043	-.618	350	277	-.097	.038	.017	-.298	350	350	-.161	.107	.060	-1.287
350	228	-.166	.072	.072	-.490	350	301	-.233	.082	.029	-.679	350	351	-.124	.055	.033	-.461
350	229	-.157	.058	.003	-.480	350	302	-.169	.065	.044	-.520	350	352	-.133	.050	.001	-.388
350	230	-.155	.055	-.002	-.396	350	303	-.175	.074	.058	-.501	350	353	-.051	.047	.147	-.323
350	231	-.149	.051	.004	-.371	350	304	-.237	.082	.003	-.611	350	354	-.128	.048	.010	-.363
350	232	-.143	.051	.001	-.386	350	305	-.152	.069	.066	-.435	350	355	-.153	.066	.038	-.841
350	233	-.138	.051	-.004	-.635	350	306	-.165	.062	.016	-.671	350	356	-.152	.053	-.011	-.420
350	234	-.135	.055	.026	-.583	350	307	-.165	.068	.021	-.545	350	357	-.109	.059	.079	-.495
350	235	-.129	.055	.028	-.603	350	308	-.153	.063	.029	-.527	350	358	-.104	.057	.077	-.476
350	236	-.161	.078	.023	-.637	350	309	-.246	.088	.003	-.666	350	359	-.106	.056	.097	-.596
350	237	-.160	.071	-.009	-.527	350	310	-.258	.074	-.041	-.752	350	360	-.114	.050	.006	-.643
350	238	-.168	.067	-.007	-.575	350	311	-.174	.073	.077	-.623	350	361	-.094	.042	.036	-.308
350	239	-.170	.068	.026	-.562	350	312	-.170	.070	.055	-.599	350	362	-.096	.043	.034	-.308
350	240	-.168	.068	-.001	-.585	350	313	-.174	.066	.029	-.482	350	363	-.117	.049	.029	-.414
350	241	-.164	.065	-.024	-.642	350	314	-.188	.062	-.004	-.562	350	364	-.137	.047	-.016	-.363
350	242	-.157	.066	-.005	-.550	350	315	-.160	.056	.009	-.449	350	365	-.103	.051	.039	-.381
350	243	-.151	.066	.019	-.596	350	316	-.165	.058	.012	-.474	350	366	-.098	.050	.034	-.387
350	244	-.129	.071	.077	-.609	350	317	-.049	.071	.270	-.302	350	367	-.099	.054	.036	-.461
350	245	-.123	.058	.006	-.559	350	318	-.145	.041	-.014	-.279	350	368	-.108	.041	.031	-.348
350	246	-.137	.059	.026	-.459	350	319	-.280	.082	-.081	-.643	350	369	-.094	.040	.052	-.248
350	247	-.154	.069	.011	-.686	350	320	-.278	.101	-.010	-.751	350	370	-.095	.041	.074	-.248
350	248	-.173	.077	.001	-.526	350	321	-.195	.087	.071	-.728	350	371	-.037	.040	.116	-.164
350	249	-.172	.077	-.012	-.876	350	322	-.190	.068	-.019	-.533	350	372	-.082	.043	.081	-.286
350	250	-.165	.077	.008	-.846	350	323	-.202	.083	.024	-.799	350	373	-.090	.034	.049	-.200
350	251	-.161	.071	.012	-.587	350	324	-.210	.095	.046	-.907	350	374	-.088	.039	.066	-.236
350	252	-.081	.047	.051	-.410	350	325	-.167	.057	.033	-.496	350	375	-.088	.039	.042	-.232
350	253	-.089	.043	.033	-.349	350	326	-.170	.054	-.016	-.391	350	376	-.089	.041	.070	-.270
350	254	-.097	.044	.018	-.389	350	327	-.293	.102	-.036	-.857	350	377	-.085	.033	.016	-.212

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
350	378	-.085	.040	.037	-.239	350	434	-.280	.094	.028	-.840	350	470	.053	.068	.370	-.120
350	379	-.086	.040	.032	-.246	350	435	-.233	.113	.192	-.701	350	471	.042	.062	.338	-.121
350	380	-.088	.041	.031	-.270	350	436	.063	.120	.870	-.318	350	472	.018	.056	.308	-.136
350	401	.130	.292	1.072	-.721	350	437	.083	.112	.761	-.275	350	473	-.019	.040	.178	-.149
350	402	-.175	.187	.554	-.858	350	438	.065	.087	.559	-.236	350	474	.051	.069	.447	-.113
350	403	-.188	.122	.321	-.651	350	439	.048	.076	.468	-.216	350	475	.049	.065	.402	-.166
350	404	-.181	.110	.172	-.853	350	440	-.024	.058	.243	-.281	350	476	.039	.054	.299	-.143
350	405	-.211	.096	.277	-.653	350	441	-.097	.057	.132	-.337	350	477	-.028	.034	.089	-.176
350	406	.218	.171	.965	-.413	350	442	-.253	.098	.090	-.860	350	801	-.125	.035	-.015	-.342
350	407	.148	.119	.554	-.224	350	443	-.162	.123	.235	-.706	350	802	-.114	.042	.025	-.278
350	408	.112	.116	.496	-.270	350	444	.012	.078	.494	-.257	350	803	-.091	.036	.053	-.279
350	409	.076	.103	.450	-.245	350	445	.046	.076	.454	-.253	350	804	.057	.063	.375	-.118
350	410	.100	.118	.589	-.310	350	446	.059	.064	.346	-.214	350	805	.068	.046	.268	-.063
350	411	-.241	.083	.182	-.586	350	447	.044	.060	.306	-.196	350	806	-.013	.040	.120	-.156
350	412	.338	.194	.986	-.341	350	448	-.014	.049	.277	-.218	350	807	-.095	.045	.032	-.454
350	413	.323	.187	.970	-.371	350	449	-.074	.049	.168	-.322	350	808	-.093	.043	.040	-.389
350	414	.242	.157	.787	-.330	350	450	-.207	.086	.080	-.895	350	809	-.091	.036	.025	-.253
350	415	.177	.113	.681	-.191	350	451	-.114	.091	.215	-.759	350	810	-.094	.043	.035	-.275
350	416	.043	.085	.425	-.295	350	452	-.025	.058	.273	-.225	350	901	-.120	.084	.325	-.560
350	417	-.033	.068	.236	-.354	350	453	.022	.069	.413	-.194	350	902	-.156	.074	.070	-.570
350	418	-.264	.097	-.018	-.734	350	454	.047	.062	.408	-.137	350	903	-.150	.069	.082	-.439
350	419	-.241	.081	.047	-.673	350	455	.047	.061	.377	-.211	350	904	-.116	.099	.446	-.503
350	420	.264	.168	.953	-.303	350	456	-.008	.043	.265	-.218	350	905	-.186	.081	.056	-.568
350	421	.278	.168	.945	-.398	350	457	-.059	.039	.194	-.199	350	906	-.217	.083	.049	-.560
350	422	.226	.148	.794	-.344	350	458	-.159	.058	.005	-.502	350	907	-.177	.078	.121	-.687
350	423	.162	.109	.542	-.146	350	459	-.118	.067	.164	-.440	350	908	-.322	.108	.006	-.874
350	424	.019	.079	.299	-.254	350	460	-.031	.052	.241	-.184	350	909	-.096	.100	.307	-.515
350	425	-.070	.065	.158	-.332	350	461	.003	.057	.342	-.161	350	910	-.271	.103	.022	-.775
350	426	-.272	.084	-.025	-.634	350	462	.039	.065	.363	-.137	350	911	-.219	.093	.126	-.656
350	427	-.252	.099	.177	-.665	350	463	.053	.062	.315	-.159	350	912	-.286	.089	.030	-.714
350	428	.180	.157	.928	-.318	350	464	.011	.048	.304	-.172	350	913	-.225	.086	.067	-.665
350	429	.194	.149	.892	-.163	350	465	-.042	.040	.122	-.212	350	914	-.197	.078	.100	-.518
350	430	.174	.123	.731	-.301	350	466	-.139	.059	.097	-.482	350	915	-.292	.095	.010	-.723
350	431	.125	.107	.641	-.171	350	467	-.119	.059	.211	-.453	350	916	-.264	.171	.487	-.895
350	432	.001	.074	.307	-.284	350	468	.003	.052	.292	-.181	350	917	-.221	.123	.252	-.724
350	433	-.090	.064	.139	-.322	350	469	.045	.060	.384	-.112	350	918	-.225	.086	.130	-.551

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
62	125	.285	.132	.829	-.013
62	133	.236	.135	.943	-.109
62	155	-.176	.060	.034	-.497
62	239	-.135	.066	.134	-.440
62	342	-.321	.084	-.086	-.763
62	359	-.455	.225	-.042	-1.816
64	125	.265	.129	.834	-.004
64	133	.222	.132	.825	-.083
64	155	-.189	.062	.044	-.439
64	239	-.131	.065	.125	-.274
64	342	-.328	.078	-.100	-.663
64	359	-.462	.225	-.060	-1.424
66	125	.260	.133	.757	-.035
66	133	.214	.140	.740	-.124
66	155	-.193	.063	.024	-.498
66	239	-.124	.067	.232	-.390
66	342	-.337	.087	-.118	-.874
66	359	-.450	.232	-.037	-2.140
68	125	.261	.134	.866	-.079
68	133	.213	.138	.746	-.080
68	155	-.204	.065	.022	-.490
68	239	-.119	.068	.266	-.365
68	342	-.334	.076	-.141	-.723
68	359	-.423	.219	-.004	-1.798
70	125	.213	.120	.637	-.093
70	133	.172	.124	.683	-.154
70	155	-.201	.061	.081	-.486
70	239	-.105	.070	.188	-.378
70	342	-.324	.074	-.095	-.716
70	359	-.371	.194	-.060	-1.664
72	125	.188	.122	.635	-.098
72	133	.149	.127	.696	-.176
72	155	-.202	.062	.027	-.498
72	239	-.093	.069	.189	-.330
72	342	-.342	.077	-.120	-.788
72	359	-.403	.208	-.024	-1.868
74	125	.207	.124	.614	-.214
74	133	.163	.130	.611	-.268
74	155	-.219	.067	.007	-.515
74	239	-.095	.076	.365	-.314
74	342	-.347	.093	-.126	-.784
74	359	-.368	.165	-.054	-1.565
76	125	.177	.128	.687	-.423
76	133	.136	.130	.712	-.428
76	155	-.217	.065	.015	-.490
76	239	-.079	.075	.285	-.296
76	342	-.346	.071	-.125	-.852
76	359	-.360	.157	-.059	-1.406
78	125	.150	.119	.564	-.417
78	133	.111	.126	.571	-.708
78	155	-.217	.067	.065	-.498
78	239	-.061	.075	.363	-.289
78	342	-.338	.072	-.139	-.803
78	359	-.339	.127	-.046	-1.412
108	125	-.414	.238	.136	-1.507
108	133	-.368	.270	.166	-1.468
108	155	-.243	.067	.000	-.581
108	239	.150	.119	.710	-.181
108	342	-.320	.058	-.180	-.710
108	359	-.323	.078	-.097	-.982
110	125	-.411	.214	.110	-1.308
110	133	-.362	.249	.182	-1.481
110	155	-.231	.064	.051	-.528
110	239	.158	.123	.673	-.164
110	342	-.322	.065	-.127	-.684
110	359	-.331	.091	-.118	-.992
112	125	-.451	.210	.102	-1.687
112	133	-.414	.244	.151	-2.003
112	155	-.236	.062	.006	-.574
112	239	.176	.120	.734	-.158
112	342	-.319	.063	-.120	-.906
112	359	-.330	.088	-.083	-.905
114	125	-.498	.209	.036	-1.532
114	133	-.455	.255	.123	-1.825
114	155	-.243	.066	.063	-.611
114	239	.202	.125	.771	-.123
114	342	-.314	.064	-.103	-.626
114	359	-.330	.101	-.129	-1.087
116	125	-.517	.183	.002	-1.413
116	133	-.496	.228	.124	-1.958
116	155	-.247	.065	-.025	-.556
116	239	.226	.127	.820	-.140
116	342	-.313	.068	-.163	-.686
116	359	-.331	.093	-.141	-1.012
118	125	-.494	.172	.037	-1.362
118	133	-.477	.210	.071	-1.664
118	155	-.247	.068	-.018	-.638
118	239	.224	.130	.765	-.124
118	342	-.316	.064	-.155	-.794
118	359	-.332	.093	-.137	-.983
120	125	-.510	.168	-.072	-1.331
120	133	-.494	.212	.070	-1.824
120	155	-.250	.067	-.007	-.701
120	239	.219	.129	.958	-.080
120	342	-.318	.077	-.112	-.993
120	359	-.340	.102	-.111	-1.024
122	125	-.513	.165	-.095	-1.304
122	133	-.526	.208	-.032	-1.560
122	155	-.260	.072	-.028	-.685
122	239	.249	.139	.864	-.063
122	342	-.323	.080	-.115	-.944
122	359	-.347	.109	-.078	-1.105
124	125	-.478	.152	-.131	-1.453
124	133	-.493	.185	-.048	-1.454
124	155	-.254	.069	-.055	-.638
124	239	.252	.123	.765	-.032
124	342	-.344	.085	-.136	-.947
124	359	-.381	.123	-.133	-1.234
126	125	-.419	.157	.013	-1.496
126	133	-.499	.201	.049	-1.549
126	155	-.242	.066	.014	-.694
126	239	.240	.130	.882	-.057
126	342	-.327	.090	-.142	-.978
126	359	-.347	.105	-.134	-1.097
128	125	-.451	.146	-.079	-1.261
128	133	-.483	.190	-.054	-1.796
128	155	-.247	.072	-.000	-.592
128	239	.258	.139	.838	-.045
128	342	-.329	.095	-.118	-1.040
128	359	-.349	.121	-.104	-1.255
130	125	-.422	.135	-.139	-1.480
130	133	-.449	.178	.246	-1.786
130	155	-.235	.074	-.043	-.627
130	239	.259	.139	.938	-.074
130	342	-.333	.105	-.101	-1.081
130	359	-.348	.125	-.107	-1.140
132	125	-.401	.128	-.072	-1.494
132	133	-.430	.166	-.052	-1.529
132	155	-.240	.078	-.021	-.649
132	239	.277	.135	.859	-.132
132	342	-.331	.098	-.126	-.973
132	359	-.351	.121	-.104	-1.290
134	125	-.368	.122	-.053	-1.222
134	133	-.397	.157	-.003	-1.725
134	155	-.228	.076	-.025	-.673
134	239	.268	.131	1.010	-.051
134	342	-.315	.099	-.095	-1.362
134	359	-.337	.115	-.102	-.956
136	125	-.357	.119	-.099	-1.511
136	133	-.386	.148	-.056	-1.401
136	155	-.223	.075	-.024	-.641
136	239	.263	.135	.821	-.078
136	342	-.337	.108	-.099	-1.014
136	359	-.351	.126	-.093	-1.042
138	125	-.337	.106	-.050	-.960
138	133	-.375	.137	-.075	-1.348
138	155	-.206	.068	.012	-.895
138	239	.237	.129	.894	-.066
138	342	-.363	.133	.171	-1.333
138	359	-.384	.115	-.065	-1.138

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
242	125	-.215	.055	-.046	-.544	250	125	-.269	.069	-.057	-.758	258	125	-.297	.070	-.123	-.765
242	133	-.221	.078	-.030	-.901	250	133	-.289	.099	-.059	-.987	258	133	-.329	.104	-.100	-.953
242	155	-.289	.126	.040	-1.080	250	155	-.372	.165	.027	-1.176	258	155	-.406	.177	.051	-2.015
242	239	-.298	.153	.023	-1.204	250	239	-.316	.155	.080	-1.844	258	239	-.307	.124	.023	-1.279
242	342	-.203	.082	.054	-.549	250	342	-.214	.084	.106	-.586	258	342	-.229	.072	.113	-.584
242	359	-.214	.070	-.012	-.554	250	359	-.254	.086	.001	-.729	258	359	-.268	.100	.004	-.710
244	125	-.235	.064	-.045	-.682	252	125	-.273	.067	-.094	-.704	260	125	-.291	.069	-.134	-.631
244	133	-.245	.090	-.026	-.907	252	133	-.297	.100	-.033	-.949	260	133	-.328	.106	-.025	-.971
244	155	-.309	.138	.062	-1.051	252	155	-.381	.164	.003	-1.624	260	155	-.386	.163	.046	-1.708
244	239	-.309	.161	.135	-1.228	252	239	-.304	.141	.082	-1.038	260	239	-.294	.111	.008	-.972
244	342	-.198	.080	.093	-.563	252	342	-.222	.079	.048	-.603	260	342	-.227	.074	.004	-.772
244	359	-.227	.075	-.033	-.575	252	359	-.263	.094	.014	-.807	260	359	-.265	.102	.029	-.976
246	125	-.252	.071	-.083	-.915	254	125	-.269	.064	-.122	-.613	262	125	-.308	.078	-.120	-.806
246	133	-.264	.101	-.037	-1.034	254	133	-.293	.094	-.048	-.966	262	133	-.344	.112	-.087	-1.165
246	155	-.343	.170	.011	-1.476	254	155	-.389	.166	-.039	-1.500	262	155	-.374	.171	-.013	-1.919
246	239	-.312	.162	.062	-1.538	254	239	-.292	.130	.071	-1.133	262	239	-.293	.100	.049	-1.093
246	342	-.197	.075	.068	-.594	254	342	-.221	.078	.017	-.689	262	342	-.236	.075	-.005	-.882
246	359	-.229	.076	-.027	-.631	254	359	-.267	.092	.016	-.781	262	359	-.273	.108	.005	-.909
248	125	-.266	.069	-.094	-.742	256	125	-.279	.071	-.106	-.972	264	125	-.319	.073	-.129	-.712
248	133	-.286	.106	-.062	-1.009	256	133	-.304	.106	.028	-1.275	264	133	-.360	.108	-.081	-1.169
248	155	-.362	.158	-.033	-1.413	256	155	-.400	.177	-.030	-1.533	264	155	-.362	.163	-.011	-1.714
248	239	-.324	.159	.100	-1.306	256	239	-.294	.124	.016	-1.393	264	239	-.301	.100	-.069	-1.165
248	342	-.223	.087	.083	-.665	256	342	-.224	.077	.039	-.744	264	342	-.245	.080	-.030	-.852
248	359	-.257	.083	-.034	-.794	256	359	-.262	.097	.048	-.735	264	359	-.278	.106	-.005	-.816